

GROUP



DELTA

**FOUNDATION REPORT
PALO COMADO CANYON ROAD OC (WIDEN)**

Agoura Hills, California
Bridge No. 53-1678
07-LA-101-PM-33.5/33.9

Submitted to

CALTRANS

Prepared for

PARSONS

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Project No. LA-1143
September 18, 2014
(Revised June 26, 2017)
(Updated September 1, 2017)



GROUP DELTA

September 18, 2014 (revised June 26, 2017, updated September 1, 2017)

PARSONS
2201 Dupont Drive
Irvine, CA 92612

GDC Project No. LA-1143

Attention: Jon Hermstad, PE

Subject: Foundation Report
PALO COMADO CANYON ROAD OC (WIDEN)
Agoura Hills, California
Bridge No. 53-1678
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Dear Jon:

Group Delta is pleased to submit this Foundation Report for the subject project. This report has been updated to address Caltrans' review comments and revised structural loads and pile-cut-off elevations (including piles below pilasters) for Abutments 1L and 1R. The general and foundation plans, Log of Test Borings (LOTBs), pile data tables and Appendix D (Analysis and Calculations) have been updated. Caltrans' recent review comments and our responses are included in Appendix E.

We appreciate the opportunity to assist you on this important project. Should you have any questions, please call us at (949) 450-2100.

Very truly yours,
GROUP DELTA CONSULTANTS, INC.

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**FOUNDATION REPORT
PALO COMADO CANYON ROAD OC (WIDEN)
AGOURA HILLS, CALIFORNIA
BRIDGE NO. 53-1678
07-LA-101-PM-33.5/33.9**

1.0 INTRODUCTION

1.1 Scope of Work

This report provides foundation recommendations for design and construction of the subject bridge widening project, and was prepared in accordance with the provisions of American Association of State Highway and Transportation Officials (AASHTO) Load and Resistance Factor Design (LRFD) Bridge Design Specifications (6th Edition) with California Amendments (2014), and Caltrans “Foundation Report Preparation for Bridge Foundations,” December 2009.

1.2 Project Description

Caltrans and the City of Agoura Hills (City) propose to improve the existing 4-span Palo Comado Canyon Road interchange at US 101 (PM 33.0/34.4) in Los Angeles County (See Figure 1). The proposed improvements will include widening of Palo Comado Canyon Road Overcrossing (OC) on both sides (from one lane to two lanes in each direction with median turn lane), sidewalks and minor modification of the ramps in order to improve traffic circulation, safety, and bicycle/pedestrian access. Type 1 standard retaining walls will be constructed along both sides of the south abutment approach. Two pairs of architectural pilasters are proposed on both sides of Abutments 1 and 5. Two pilasters on the south side (Abutment 1) will be supported on Abutment 1 footing. Other two pilasters on the north side (just north of Abutment 5) will be supported on individual footings. A topographic plan of the project site including Exploration Locations is shown in Figures 2A and 2B, the bridge General Plan and Foundation Plan are shown in Figures 3A through 3C, and retaining wall plans are shown in Figures 4A through 4C.

Improvements will include new pavements on Palo Comado Canyon Road and the US-101 northbound on- and off-ramps. Pavement recommendations are presented in a separate Pavement Design Report.

The project delivery will be conventional design-bid-build.

1.3 Exceptions to Policy

No exceptions to policy are proposed.

2.0 FIELD INVESTIGATION AND LABORATORY TESTING PROGRAM

2.1 Field Investigation Program

2.1.1 Previous Investigations

For original construction a subsurface investigation was conducted in 1961 and included one rotary boring and two penetration borings. The as-built Log of Test Borings (LOTB) is included in Appendix C. No laboratory data are available from the original investigation. The as-built LOTB also includes construction logs of selected production cast-in-drilled-hole piles.

2.1.2 Current Investigation

Group Delta investigated subsurface conditions at the project site in 2013 by performing six hollow-stem auger borings (A-13-001 through 006) and one hand auger boring (HA-13-007). Field investigations, logging, classification, and presentation of subsurface data were performed in general accordance with Caltrans Soil and Rock Logging, Classification, and Presentation Manual (2010). The boring locations are shown in Figures 2A and 2B. Details of the investigation and boring records are provided in Appendix A. Log of Test Borings (LOTB) sheets are provided in the attached Plates 1 through 11.

2.2 Laboratory Testing Program

Soil samples collected from Group Delta's investigation were packaged in the field and transported to the laboratory for further examination and testing. Tests were performed on selected samples as an aid in classifying the earth materials and to evaluate their physical and chemical properties and engineering characteristics. Laboratory testing for this investigation included:

- Soil and Rock Classification: USCS (ASTM D 2487) and Visual Manual (ASTM D 2488), (ISRM) (1981) standards and the Bureau of Reclamation (2001) standards;
- Moisture content (ASTM D 2216) and Dry Unit Weight (ASTM D 2937);
- Atterberg Limits (ASTM D 4318);
- Percent Passing No. 200 Sieve (ASTM D 1140);
- Direct Shear (ASTM D 3080);
- One-Dimensional Consolidation (ASTM D 2435);
- Expansion Index (D 4829);
- Soil Corrosivity-pH, Sulfate, Chloride, and Minimum Resistivity (CTM 643, 422, and 417);
- Resistance R-Value (CTM 301).

3.0 SITE GEOLOGY AND SUBSURFACE CONDITIONS

3.1 Geology

Based on the "Preliminary Geologic Map of the Los Angeles 30'x60' Quadrangle," (Yerkes and Campbell, 2005) the natural site geology at the bridge site consists of relatively young shallow alluvial deposits originating from Palo Comado and Chesebro Canyons, overlying soft sedimentary bedrock of the Calabasas Formation (Tcb). The site is shown on the geologic map in Figure 5, which shows Tcb exposed at the surface to the northeast and southwest of the bridge. Regionally Calabasas Formation undivided (early late Miocene and late middle Miocene) is generally interbedded clayey to silty sandstone and silty shale, containing local beds of sedimentary breccia (probable Conejo Volcanics) clasts. The formational materials encountered at the site consisted of high plasticity claystone. Approach fills have been placed at the abutments over the alluvial and bedrock materials.

3.2 Site Conditions

The freeway profile is relatively level where it passes under the overcrossing with US-101 centerline elevations of about El. 913 feet. There is a freeway cross-slope with elevations of the shoulders about El. 910 feet on the south side to El. 916 feet on the north side. Abutment approaches have maximum elevations of about El. 935 to 936 feet. Slopes on the sides of the freeway are generally 2h:1v or flatter, except at the abutments where the maximum inclinations are 1.5h:1v without slope paving below the abutments. Abutment slopes have a maximum height of about 26 feet. The topography to the east is rolling hills, with relatively level alluvial valley topography to the west of the overcrossing. Site topography is shown in Figures 2A and 2B.

3.3 Subsurface Soil Conditions

The original LOTB and data from the current investigation were used to characterize subsurface conditions at the site. To illustrate interpreted subsurface layering at the site, a geotechnical cross-section was developed by plotting the current borings (after datum adjustment) on the as-built LOTB profile as shown in Figure 6. The cross-section shows that the soils below original ground (OG) at the site included a layer of alluvial soil overlying the formational soft bedrock. The alluvial soil is generally a relatively thin veneer up to about 5 feet thick, except in the vicinity of Bent 3 where the alluvial soils are on the order of 15 to 20 feet thick indicating presence of a former channel. About 20 to 25 feet of fill was placed at each of the abutment approaches.

Fill soils, alluvial soils, and bedrock materials are mainly cohesive fine grained materials that are similar in grain size and plasticity characteristics; therefore, it appears that the fill and alluvial soils are derived from the formational soils. When classified as soils all materials are Fat Clay, Fat Clay with Sand, and Sandy Fat Clay (CH) with tested 55 to 79 percent passing No. 200 sieve.

The materials have Liquid Limit (LL) ranging from 53 to 68 and Plasticity Index (PI) ranging from 30 to 44. These soils are generally moderately to highly expansive with a single Expansion Index (EI) test result of EI=89 (borderline medium to high). R-values are low with measured R-Values of 6 and 17. The cohesive fill soils are mostly very stiff but range from stiff to hard with undrained shear strengths (S_u) based on pocket penetrometer ranging from 1.0 to 4.0 ksf. Cohesive alluvial soils are mostly very stiff but range from stiff to hard with $S_u = 1.5$ to 4.5 ksf. Pocket penetrometer readings in the bedrock materials generally showed it classifies as a hard cohesive soil with $S_u > 4.5$ ksf, with occasional readings in more weathered zones of $S_u = 2.5$ to 4.0 ksf, which classifies as very stiff to hard soil.

Table 1 presents the soil parameters selected for geotechnical design based on evaluation of the field and laboratory data and test results.

3.4 Groundwater

As shown in Figure 6, groundwater was not encountered in borings during the original subsurface investigation. One of the logged production CIDH piles from original construction reported groundwater near the pile tip at about El. 889 feet (approximately 21 feet below grade) at Bent 2. During our investigation groundwater was found near El. 887 feet (approximately 23 feet below grade) in Boring A-13-003 also near Bent 2. At Bent 4 boring A-13-005 encountered groundwater near El. 871.5 feet (approximately 46 feet below grade). None of other borings or any previous borings or pile logs encountered any groundwater. Based on its sporadic and localized occurrence, the groundwater is interpreted to be localized perched water or seepage; therefore, the permanent groundwater table is not anticipated above the pile tip elevations, although zones of perched groundwater should be expected locally below El. 889 feet.

3.5 Geologic Hazards

There is no evidence of landslides, embankment failures, subsidence, or soil collapse potential at the site. The site soils and formational materials are comprised of high plasticity clay (CH), and these soils are considered expansive, meaning they can swell and shrink in response to changes in moisture.

4.0 SCOUR EVALUATION

The site is not in or adjacent to an active channel so scour is not a design concern.

5.0 CORROSION EVALUATION

Caltrans Corrosion Guidelines (version 2.1, January 2015) define a corrosive area as “an area where the soil contains more than 500 ppm of chlorides, more than 2,000 ppm of sulfates or has a pH of less than 5.5.” Representative samples of the site soils were tested to evaluate the corrosion potential. The tests include pH, electrical resistivity, and soluble chloride and sulfate concentrations. Results of the corrosivity tests are summarized in the following Table and included in Appendix B:

Boring No.	Depth (ft)	USCS Soil Type	Minimum Resistivity CTM 643 (ohm-cm)	pH CTM 643	Soluble Sulfate Content CTM 417 (ppm)	Soluble Chloride Content CTM 422 (ppm)
A-13-003	25-26.5	Fat Clay (CH)	-	7.29	13,250	5
A-13-006	0-5	Fat Clay (CH)	423	7.09	10,500	24

Based on the test results site materials classify as corrosive due to high sulfates in accordance with Caltrans criteria. Any imported soils should be evaluated for corrosion characteristics if they will be in contact with buried or at-grade structures and appropriate mitigative measures should be included. Concrete mix design and minimum concrete cover should be based on California Amendments to AASHTO LRFD Bridge Design Specifications – Sixth Edition (Sections 5.12.3 through 5.12.5) and Section 90-1.02H of the 2015 Standard Specifications.

6.0 SEISMIC RECOMMENDATIONS

6.1 Faulting and Seismicity

The site is located at latitude 34.1433 north, longitude -118.7379 west, and is in a seismically active area and a number of active faults are present in the area surrounding the site. The closest major faults are shown on the Caltrans ARS online fault map in Figure 7 along with their site to rupture distances (R_{rup}) and other fault parameters.

6.2 ARS Curve

The Acceleration Response Spectrum (ARS) curve was developed following the latest Caltrans Seismic Design Criteria (SDC) and Caltrans ARS Online 2012 methodology, which uses the upper bound envelope of probabilistic (975-year return period) and mean deterministic spectra for seismic design. Site subsurface conditions were included in the analysis based on the average shear wave velocity in the upper 30 meters [V_{s30}]. Since the site is underlain at shallow depth by shale bedrock (soil type C) and shallow alluvium and fill (soil type D), we assumed borderline soil type D/C with $V_{s30} = 360$ m/s for this site for selection of ARS curves in the preliminary foundation report. The V_{s30} of 360 m/s is also consistent with available correlations based on undrained shear strength estimated from our investigation. Near fault factors were applied to both the deterministic and probabilistic spectra. No basin factor was applied since the site is not in a deep sedimentary basin. Note that for this site the probabilistic spectrum governs the design envelope across all periods. Peak Ground Acceleration (PGA) is 0.57 g and peak spectral acceleration is 1.31 g at 0.2 second period. Based on probabilistic deaggregation analysis the earthquake magnitude and distance associated with the probabilistic ARS curve is 7.0 and 13.4 km, respectively. The deterministic, probabilistic, and recommended envelope spectra are included in Figure 8. Since liquefaction potential at the site is negligible (see following section) no adjustment to the site response is required for liquefaction. Seismic calculations are presented in Appendix D.

6.3 Liquefaction Evaluation

Three simultaneous conditions are required for liquefaction to occur: (1) cohesionless soils of loose to medium density; (2) saturated conditions; and (3) rapid, large strain, cyclic loading, normally provided by earthquake motions. Since the soils and bedrock at the site are highly plastic cohesive soils, and there is no permanent shallow groundwater table at the site, liquefaction is not an issue for design. Since there is no liquefaction seismic slope stability and lateral spreading are not a significant design concern.

7.0 AS-BUILT FOUNDATION DATA

As-built plans are presented in Appendix C, and a summary of each existing foundation support is presented in Table 2. Note that the datum shift between as-built and current plans has the following adjustment:

$$\text{Elevation (new datum)} = \text{Elevation (old datum)} + 2.34 \text{ feet}$$

A brief summary of the existing bridge and foundations from the as-built data is presented below:

- The bridge structure is a four-span bridge with pre-stressed pre-cast “I” girders built in 1963. One I-girder was replaced on span 3 in 2006;
- All foundations are supported on 45-ton (90 kip) design capacity Cast In Drilled Hole (CIDH) piles (pile diameter = 16 inches);
- The bottom of footing elevation at both abutments is El. 924.5 feet. Average tip elevation at the abutments is El. +886.5 feet. The average pile penetration length at the abutments is 38 feet;
- Based on the Foundation Plan the bottom of footing elevation at Bent 2 is El. 900 feet. Average tip elevation at Bent 2 is about El. 884 to 887 feet. The average pile penetration length is about 13 to 16 feet;
- Bottom of footing elevation at Bent 3 is 903 feet. The average tip elevation at Bent 3 is El. 881 feet. The average pile penetration length is 22 feet;
- Bottom of footing elevation at Bent 4 is 907 feet. The average tip elevation at Bent 4 is at El. 884 to 887 feet. The average pile penetration length is 20 to 23 feet;

Except at Bent 3, all existing piles at the Bents are founded in Formational Soil (Bedrock).

8.0 FOUNDATION RECOMMENDATIONS

8.1 Bridge Foundations and Pilasters

8.1.1 Foundation Type

Due to potentially compressible near surface fill and alluvial soils, and to match the existing foundation type for similar seismic behavior, deep foundations are recommended for support of the widening structure. Due to the cohesive nature of the soils and bedrock, conditions are considered favorable for open-hole drilling. CIDH piles cause less noise and vibration compared to driven piles. In addition, CIDH piles were successfully used for the existing structure. For these reasons, Cast-in-Drilled-Hole (CIDH) piles are the recommended foundation type. Abutment piles are expected to tip above the groundwater at the site and have relatively low demands; therefore, 16-inch diameter standard CIDH piles are recommended for abutments and pilasters. Since subsurface data suggests perched groundwater may be encountered above the tip elevations for bents, and Caltrans requires a minimum 24-inch diameter CIDH if groundwater is present, 24-inch diameter standard CIDH piles are recommended for the bent supports. The General Plan and Foundation Plan are presented in Figures 3A through 3C. General foundation design information is presented in the Foundation Design Data Sheet in Table 3.

8.1.2 Axial Capacity

Axial shaft resistance in general can be developed in side resistance on the edge of the shaft and base resistance at the pile tip. Determination of shaft nominal axial capacity is based on AASHTO LRFD BDS 6th Edition with California Amendments Section 10.8.3.5. Due to difficulty in cleaning and inspecting the shaft bottom and potential for encountering perched water and need for wet construction, end bearing has not been included in the design. Site soils and bedrock are considered cohesive soils for design purposes, and shaft friction or side resistance is computed using the "alpha method," in which a multiplier (α) is applied to undrained shear strength to estimate the nominal skin friction. Recommended minimum center-to-center spacing between piles is 2.5 times the pile diameter. Since the pile caps are in contact with the ground and the soils are stiff to hard, no axial group efficiency reduction is required, and block failure does not control in accordance with AASHTO LRFD Sections 10.8.3.6.2, 10.5.5.2.4, and 10.7.3.9. In accordance with AASHTO C10.8.3.5.1b the upper 5 feet of skin friction and the lower one shaft diameter was neglected in the design. Skin friction in tension was taken as 0.7 times the skin friction in compression.

Foundation loads provided by the Structural Engineer are presented in Table 4, Design Recommendations are summarized in Table 5, and the Pile Data Table is presented in Table 6. Axial capacity calculations are presented in Appendix D.

8.1.3 Lateral Capacity

Lateral capacity of foundations includes the lateral capacity of the piles plus available passive resistance on the embedded pile caps.

8.1.3.1 Lateral Pile Capacity

Lateral capacity of the piles was computed using the computer program LPILE (Ensoft, 2013) using the p-y curve method. Free-head (pinned) boundary condition was assumed at the top of the piles. Non-linear p-y curves were generated by LPILE assuming soil modeled as stiff clay without free water considering the undrained shear strength of the material. Group effects were incorporated into the analysis using the p-multiplier approach based on pile center to center spacing following California Amendments Section 10.7.2.4. Ground slope was modeled in the longitudinal direction at abutments. Cracked moment of inertia equal to 50% of the gross moment of inertia was used to model pile bending stiffness. A summary of lateral pile capacity analyses is presented in Table 7, and supporting calculations are provided in Appendix D.

8.1.3.2 Passive Resistance of Bent Caps

For the bent caps lateral passive resistance was estimated based on the undrained shear strength of the soils adjacent to the pile caps. Ultimate passive resistance depends on the amount of lateral displacement. Ultimate passive resistance may be taken as a uniform lateral pressure of 6 ksf, which is mobilized at a displacement equal to 2% of the thickness of the pile cap. At smaller displacements the passive resistance may be determined in accordance with Figure 9. For the diaphragm abutments passive resistance should be neglected due to unpaved adjacent slopes.

8.1.4 Settlement

Total settlement of pile foundation groups is estimated to be less than 1-inch.

8.1.5 Ultimate Lateral Capacity of Abutment Walls

The ultimate lateral capacity of an abutment wall is a function of the height of the abutment wall that is acted on by passive soil pressure. For abutment walls backfilled with structural backfill in accordance with the 2015 Standard Specifications, the Caltrans Seismic Design Criteria (SDC) Version 1.7, Section 7.8, dated April 2013 recommends a passive pressure of 5 ksf for a wall height of 5.5 feet based on full scale abutment testing conducted at UCLA. For wall heights other than 5.5 feet, the passive pressure may be determined by multiplying the 5-ksf value by the ratio $(H/5.5)$, where H is wall height in feet in accordance with Caltrans SDC. For higher walls, the maximum value of the passive resistance should be limited to 7.3 ksf corresponding to a wall height of 8 feet. Initial stiffness may be taken as 50 kips/inch/ft.

8.1.6 Lateral Earth Pressures on Abutment Walls

The recommendations in Section 8.2.2 may be used for static and seismic lateral earth pressures on the diaphragm abutment walls.

8.2 Retaining Walls

8.2.1 Wall Type

Caltrans Standard Type 1 retaining walls (2015 Standard Plan B3-1A) with level backfill and traffic surcharge are proposed along both sides of the south abutment (Abutment 1) approach for the purpose of widening Palo Comado Canyon Road. Since the PGA at the site is less than 0.6g, the standard designs are applicable. The plans presented in Figures 4A through 4C show that the wall design heights generally range from 6 to 16 feet with the maximum height of 20 feet for a wall length of approximately 8 feet. Based on these considerations and engineering analyses, the proposed Type 1 walls may be supported on spread footings.

8.2.2 Lateral Earth Pressures

Lateral earth pressures recommended below assume all wall backfill complies with the requirements of Caltrans Standard Specifications (2015) Section 19-3.02C (minimum Sand Equivalent of 20 and gradation requirements). Recommended lateral earth pressure parameters are as follows:

- Total unit weight = 120 pcf
- Soil Friction Angle = 34 degrees
- Movement required to reach active state: 0.2% of wall height (1/4 inch per 10-foot of height)
- Coefficient of Static Active Earth Pressure: $K_a = 0.28$
- Static Active Earth Pressure as Equivalent Fluid: 34 pcf (use minimum 36 pcf per Caltrans practice)
- Pseudo-static horizontal acceleration coefficient, $K_h = 1/3$ PGA = 0.19
- Coefficient of Total Static plus Seismic Active Earth Pressure: $K_{ae} = 0.40$
- Total Static plus Seismic Active Earth Pressure as Equivalent Fluid: 48 pcf
- Restrained walls:
 - Coefficient of Static At-Rest Earth Pressure: $K_0 = 0.44$
 - At-rest equivalent fluid pressure (Static): 53 pcf
 - Coefficient of Static plus Seismic At-Rest Earth Pressure: $K_{0e} = 0.63$
 - At-rest equivalent fluid pressure (Seismic): 76 pcf

The above pressures assume that walls are equipped with a drainage system (Standard Plan BO-3 or approved equal) to prevent buildup of hydrostatic pressures in the backfill.

8.2.3 Lateral Resistance

Lateral resistance to sliding may be provided by friction along the base of the foundation and passive resistance on the footing. A sliding friction coefficient of 0.53 may be used for Type 1 walls with a key. Passive resistance to sliding may be taken as an equivalent fluid pressure of 400 pcf; the upper 1-foot of soil should be neglected in computing passive resistance. The leading edge of the footing should have a minimum horizontal setback of 4 feet from the adjacent slope face.

8.2.4 Bearing Capacity

Bearing capacity was evaluated at the service, strength, and extreme event limit states. Resistance factors of 0.55 and 0.8 were applied for the strength and extreme event cases, respectively, in accordance with Table 11.5.7-1 and Section 11.5.8 of AASHTO and California Amendments. Bearing capacity analysis was performed assuming the footings are founded in embankment fill with a maximum 2H:1V (Horizontal:Vertical) slope using Brinch-Hansen's formula and drained strength parameters provided in Table 1. The analysis indicates that for the equivalent base widths and applied bearing stresses listed in the Standard Plans the site soils have adequate bearing capacity for support of the proposed walls up to the maximum proposed design height of 20 feet. The footings have factor of safety of greater than 3.0 for service limit state and Capacity to Demand (C/D) ratios of greater than 1 for strength and extreme limit states. Supporting calculations are provided in Appendix D.

8.2.5 Settlement

Wall settlement based on footing bearing pressures in the Standard Plans is estimated at less than 1 inch, with a differential settlement of 1 inch over 50 feet. Supporting calculations are provided in Appendix D.

8.2.6 Global Stability

Global stability analysis was performed for the most critical sections of the proposed retaining walls, and the analysis indicates the factor of safety exceeds the required minimum of 1.5 for static case and 1.0 for pseudo-static case. Supporting calculations are provided in Appendix D.

8.2.7 Subgrade Preparation

Retaining wall footing subgrade should be excavated and observed by Group Delta during construction. No known unsuitable materials are present. If unsuitable soil is encountered during construction it should be remediated in accordance with the Caltrans Standard Specifications and Standard Special Provisions (SSP). If subgrade is found to be suitable, the surface should be scarified, brought to near optimum moisture content, and compacted to the specified density (95% relative compaction in accordance with the Standard Specifications) prior to placing concrete or steel. Once the subgrade has been approved it should be protected.

Any subgrade disturbed by rainfall or other source of moisture or by construction activities should be removed and replaced with suitable material.

8.3 Approach Fill Earthwork

Additional fills are proposed to widen the abutment approaches. All grading should comply with Caltrans Standard Specifications. To avoid downdrag on abutment piles the approach fills should be placed to at least the finished grade and allowed to settle and stabilize prior to abutment pile foundation construction. Due to presence of stiff to hard overconsolidated soils and bedrock and lack of groundwater table, the settlement is expected to be primarily elastic and occur quickly after completing fill placement. A settlement waiting period of 30 days is recommended. The settlement period should follow Section 19-6.03D of the 2015 Standard Specifications and SSP's. No additional surcharge is required above the finished grade.

Expansive soils should not be placed within 150 feet of bridge abutments. All new fills in this zone should have Expansion Index (EI) of less than 50.

9.0 NOTES TO DESIGNERS

1. Approach fills should be placed and allowed to settle prior to construction of abutment piles. A 30-day waiting period is recommended (see Section 8.3).
2. No permanent groundwater is anticipated at the abutment locations, and therefore inspection tubes and gamma-gamma logging may not be required during abutment pile installation.
3. Perched groundwater was encountered at Bent 2 and Bent 4; therefore, groundwater may be encountered above the pile tip elevations at the bents. The designers should include provisions for inspection tubes in the bent piles in accordance with Bridge Memo to Designers 3-1. In the event that piles require installation in the wet, gamma-gamma integrity testing will be required. If piles are constructed in the dry, no integrity testing will be required.

10.0 CONSTRUCTION CONSIDERATIONS

- The contractor should verify that adequate lateral and overhead clearance is available for operation of drilled pile construction equipment.
- CIDH piles will be drilled in primarily cohesive stiff to hard clay soils and claystone bedrock without a permanent groundwater table, so caving potential is generally considered to be low and open-hole construction is likely to be feasible.
- Perched groundwater has been observed above the pile tip elevation at Bent 2, and may be found elsewhere. The volume of water that may enter the drilled holes, and the ability to dewater the holes effectively, is uncertain. The contractor should be prepared to construct the piles in the wet (slurry method) in the event that field groundwater conditions are such that the piles cannot be constructed in a dry or dewatered hole in accordance with the Standard Specifications.
- Borings were drilled to below the tip elevations without refusal using an 8-inch diameter hollow stem auger. The contractor should select appropriate drilling equipment for the size and depth of piles and the site soil/bedrock conditions. Localized drilling difficulty may be encountered if zones of cemented soils or bedrock are encountered.
- CIDH pile construction and cleaning of the bottom should be performed in accordance with the Standard Specifications.

11.0 LIMITATIONS

The conclusions and recommendations contained in this report are professional opinions, intended for the use of Parsons and their design consultants. This report has been prepared solely for the design of the improvements described herein, and may not contain sufficient information for other uses. The recommendations should not be extrapolated to areas not covered by this report, or used for other facilities without the review and approval of Group Delta.

This report presents recommendations pertaining to the subject site based on the assumptions that the subsurface conditions do not deviate appreciably from those disclosed by our explorations. In view of past grading and the general geology of the area, the possibility of different geologic conditions cannot be discounted. It is the responsibility of the owner to bring any deviations or unexpected conditions observed during construction to the attention of the Geotechnical Engineer. In this way, any required supplemental recommendations can be made with a minimum of delay.

This study was performed in accordance with generally accepted geotechnical engineering principles and practice. The professional engineering work and judgments presented in this report meet the standard of care of our profession at this time. No warranty, express or implied, is made.

The recommendations for this project are to a high degree dependent upon proper quality control of grading and foundation construction. Consequently, the recommendations are made contingent on the opportunity of Group Delta to observe the grading and improvement operations. If parties other than Group Delta are engaged to provide such services, they must be notified that they will be required to assume responsibility for the geotechnical phase of the project by concurring with the recommendations or provide alternate recommendations as deemed appropriate.

12.0 REFERENCES

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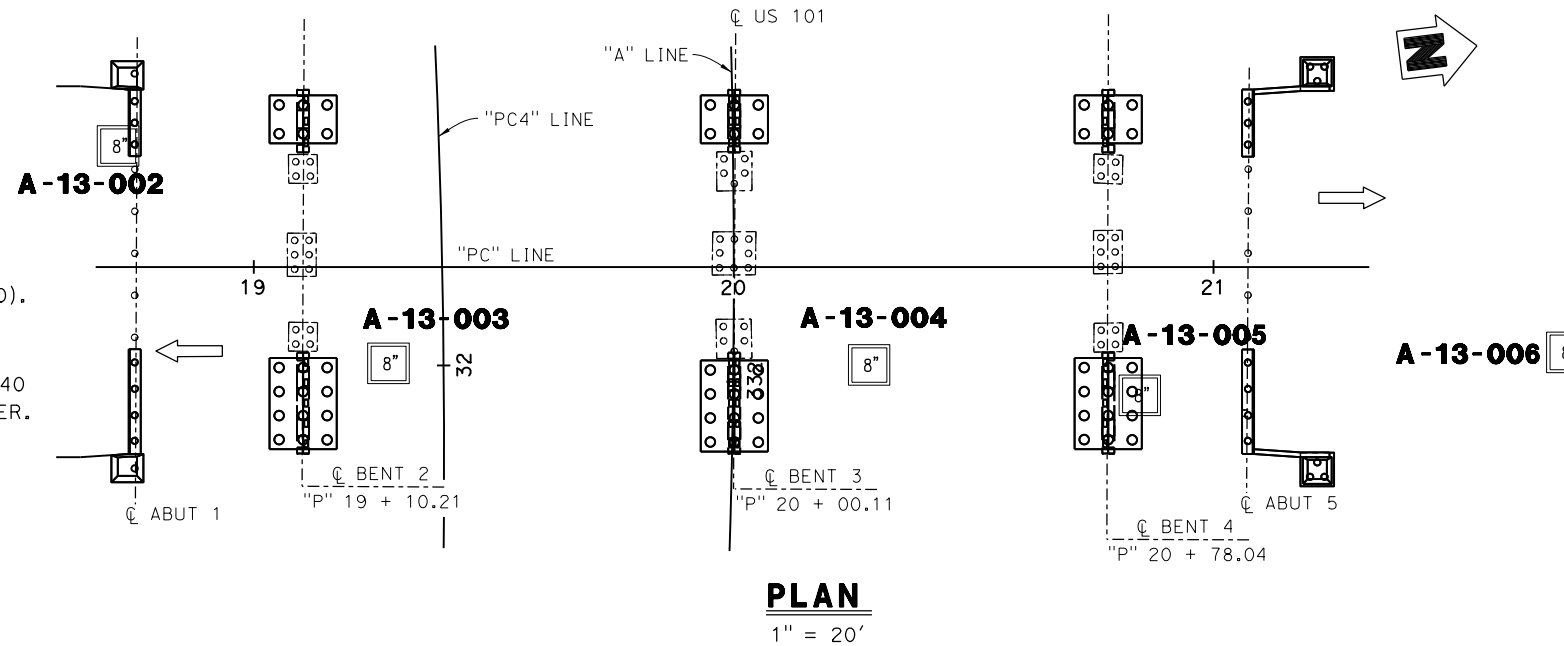
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 NORTHING: 1874980.99, EASTING: 6337736.49, ELEVATION: 903.05
 THE VERTICAL CONTROL DATUM IS BASED ON THE NORTH AMERICAN VERTICAL DATUM 1988 (NAVD88) NATIONAL GEODETIC SERVICES (NGS) BENCHMARK, NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD88).

- NOTES:**
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DIST	COUNTY	ROUTE	POST MILES TOTAL PROJECT	SHEET No	TOTAL SHEETS
07	LA	101	33.5/33.9		

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 DATE: 08-17-17

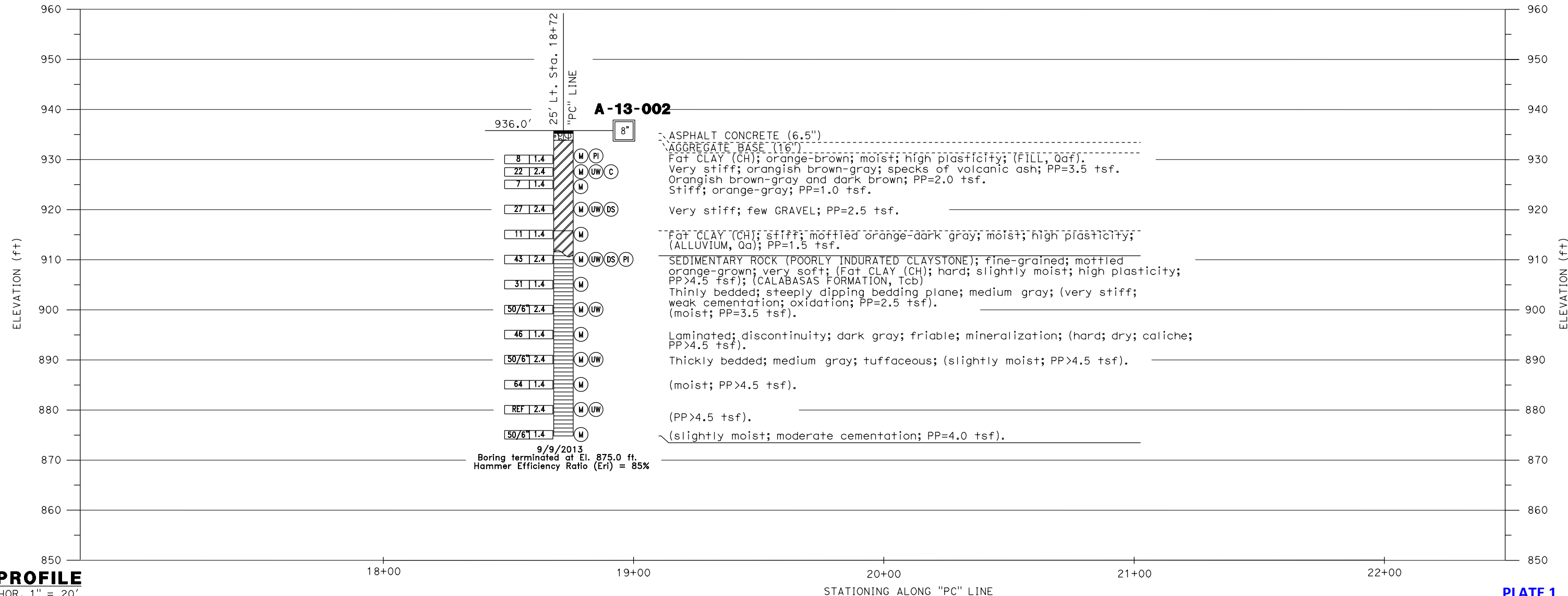
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 EXP. GEOTECHNICAL
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PARSONS
 2201 DUPONT DRIVE, SUITE 200
 IRVINE, CA 92612



PROFILE

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 VER. 1" = 10'

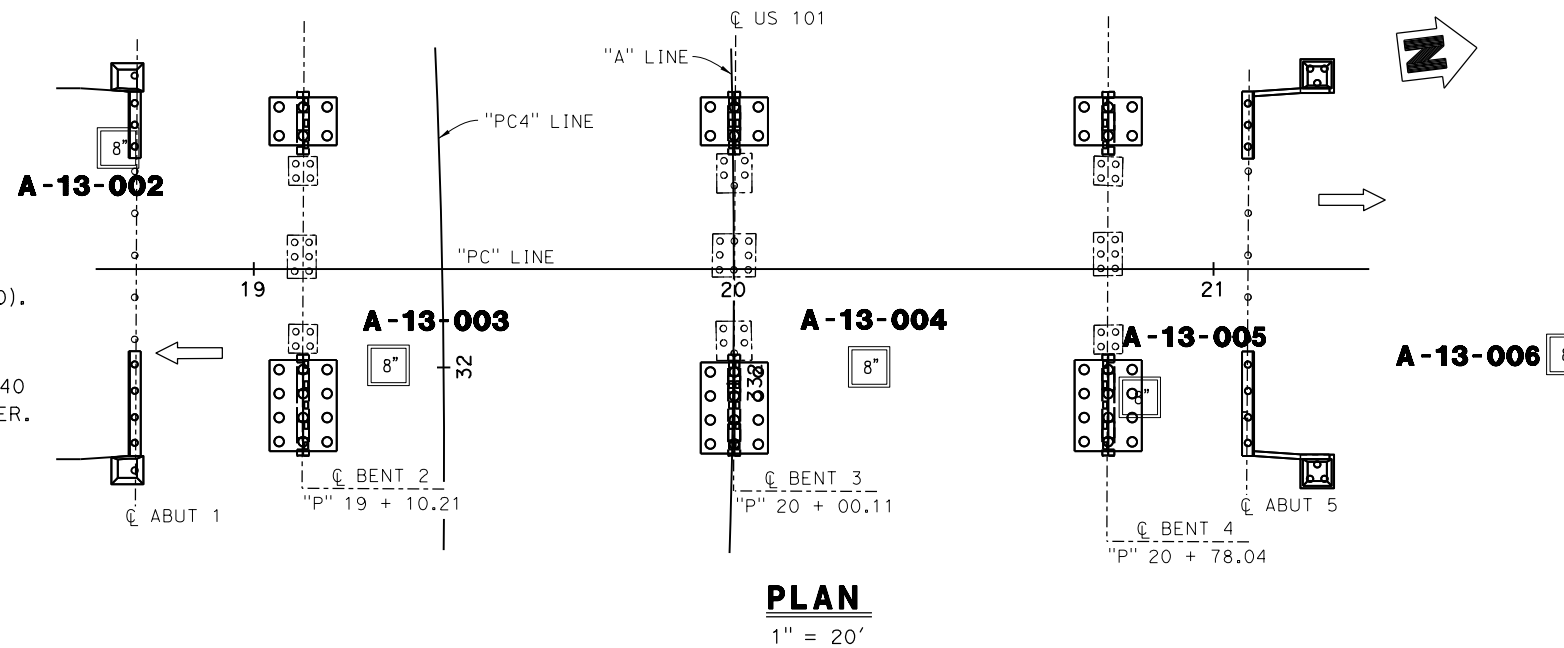
PLATE 1

DESIGN OVERSIGHT	DRAWN BY S. AROUS/B. ANDERSON	S. STONE / T. LATIMER	PREPARED FOR THE STATE OF CALIFORNIA DEPARTMENT OF TRANSPORTATION	JON HERMSTAD PROJECT ENGINEER	BRIDGE NO. 53-1678	PALO COMADO CANYON RD. OC (WIDEN) LOG OF TEST BORINGS 1 of 3
SIGN OFF DATE	CHECKED BY M. DINICOLA/S. SATHIS	FIELD INVESTIGATION BY: DATE: AS SHOWN	CU:1821 EA:070001841	POST MILES 33.69	REVISION DATES	
GS GEOTECHNICAL LOG OF TEST BORINGS SHEET (ENGLISH) (REV. 7/16/10)			ORIGINAL SCALE IN INCHES FOR REDUCED PLANS	0 1 2 3	DISREGARD PRINTS BEARING EARLIER REVISION DATES	SHEET 30 OF 32

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DIST	COUNTY	ROUTE	POST MILES TOTAL PROJECT	SHEET No	TOTAL SHEETS
07	LA	101	33.5/33.9		

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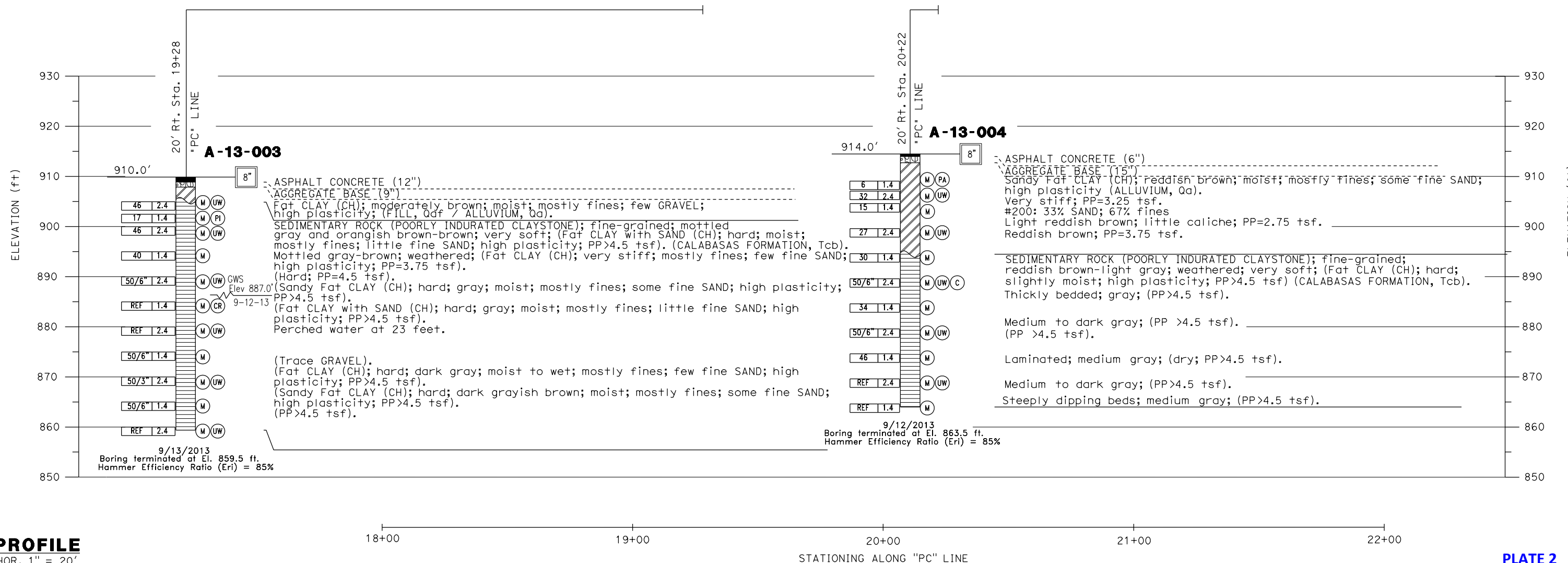
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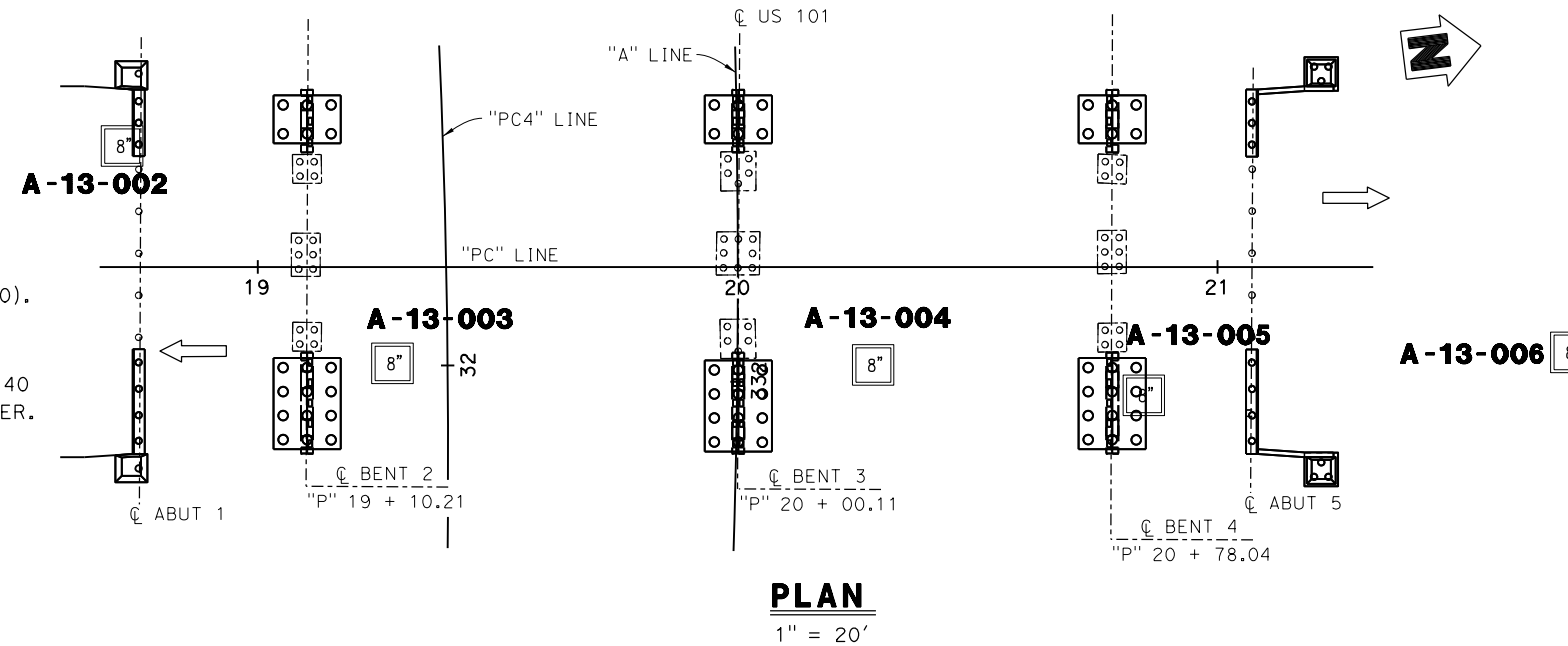
PLATE 2

DESIGN OVERSIGHT	DRAWN BY S.AROUS/B.ANDERSON	S. STONE / T. LATIMER	PREPARED FOR THE STATE OF CALIFORNIA DEPARTMENT OF TRANSPORTATION	JON HERMSTAD PROJECT ENGINEER	BRIDGE NO. 53-1678	PALO COMADO CANYON RD. OC (WIDEN) LOG OF TEST BORINGS 2 of 3
SIGN OFF DATE	CHECKED BY M. DINICOLA/S.SATHIS	FIELD INVESTIGATION BY: DATE: AS SHOWN	CU:1821 EA:070001841	POST MILES 33.69	REVISION DATES	
GS GEOTECHNICAL LOG OF TEST BORINGS SHEET (ENGLISH) (REV. 7/16/10)			ORIGINAL SCALE IN INCHES FOR REDUCED PLANS	0 1 2 3	DISREGARD PRINTS BEARING EARLIER REVISION DATES	SHEET 31 OF 32

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07	LA	101	33.5/33.9		

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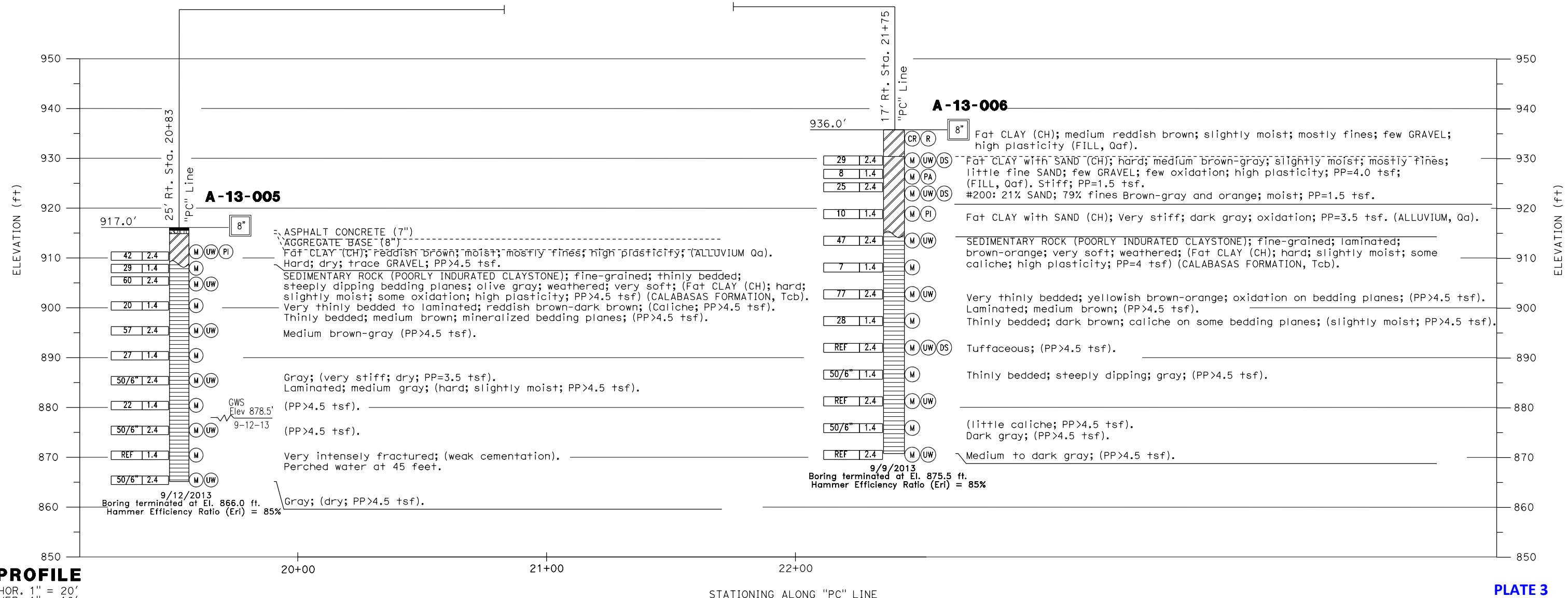
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PROFILE
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PLATE 3

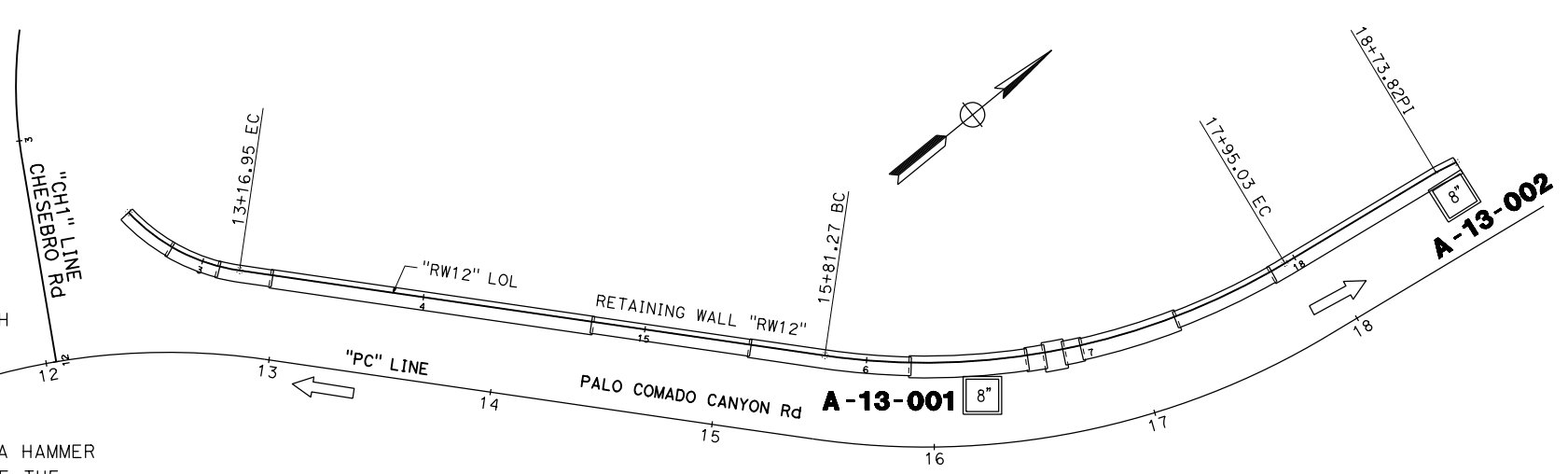
DESIGN OVERSIGHT	DRAWN BY S.AROUS/B.ANDERSON	S. STONE / T. LATIMER	PREPARED FOR THE STATE OF CALIFORNIA DEPARTMENT OF TRANSPORTATION	JON HERMSTAD PROJECT ENGINEER	BRIDGE NO. 53-1678	PALO COMADO CANYON RD. OC (WIDEN) LOG OF TEST BORINGS 3 of 3
SIGN OFF DATE	CHECKED BY M. DINICOLA/S.SATHIS	DATE: AS SHOWN	CU:1821 EA:070001841	POST MILES 33.69	REVISION DATES	
GS GEOTECHNICAL LOG OF TEST BORINGS SHEET (ENGLISH) (REV. 7/16/10)			ORIGINAL SCALE IN INCHES FOR REDUCED PLANS	DISREGARD PRINTS BEARING EARLIER REVISION DATES	SHEET 32 OF 32	

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Caltrans
 CONSULTANT FUNCTIONAL SUPERVISOR: SHAH GHANBARI
 CALCULATED/DESIGNED BY: [Blank]
 CHECKED BY: [Blank]
 CURT SCHEVING
 KONRAD FERNANDES
 REVISED BY: B. ANDERSON
 DATE REVISED: 08/21/17

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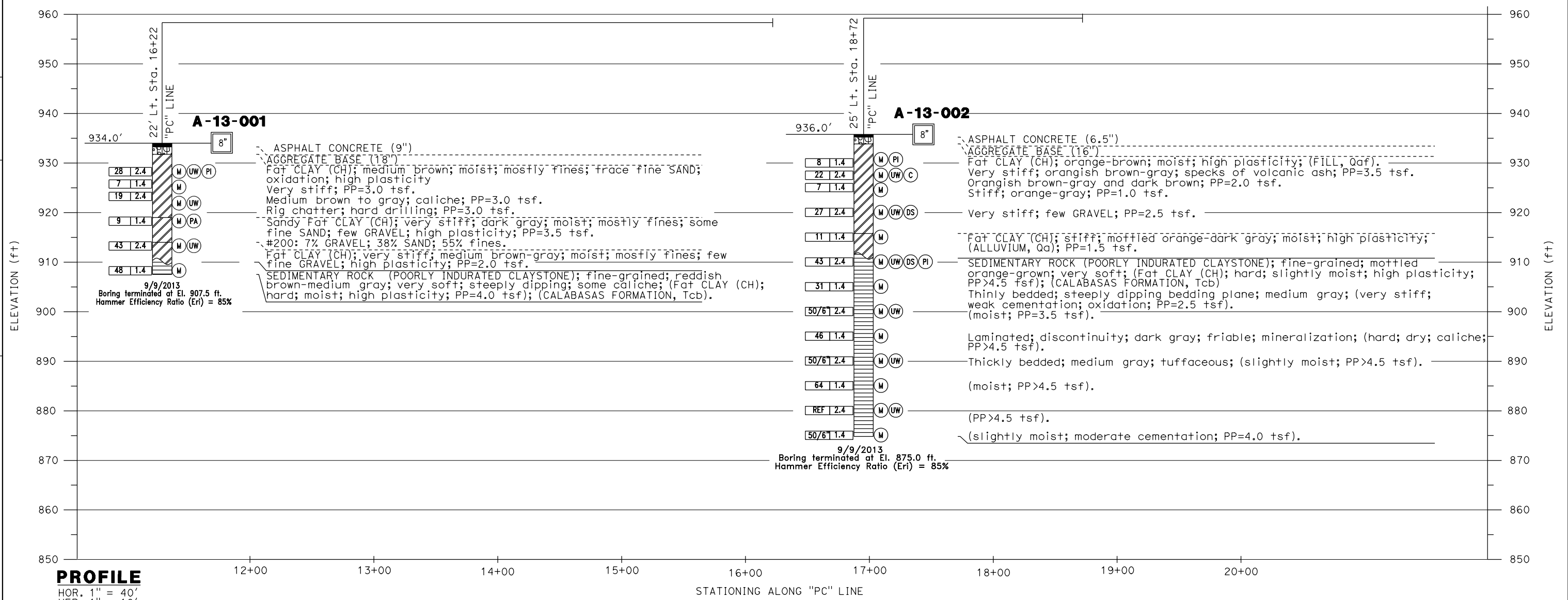
PLAN
 1" = 40'

Dist	COUNTY	ROUTE	POST MILES TOTAL PROJECT	SHEET No.	TOTAL SHEETS
07	LA	101	33.5/33.9		

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 SEPTEMBER 2017

GROUP DELTA, INC. 32 MAUCHLY SUITE B IRVINE, CA 92618	CITY OF AGOURA HILLS 30001 LADYFACE COURT AGOURA HILLS, CA 91301
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PROFILE
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 VER. 1" = 10'

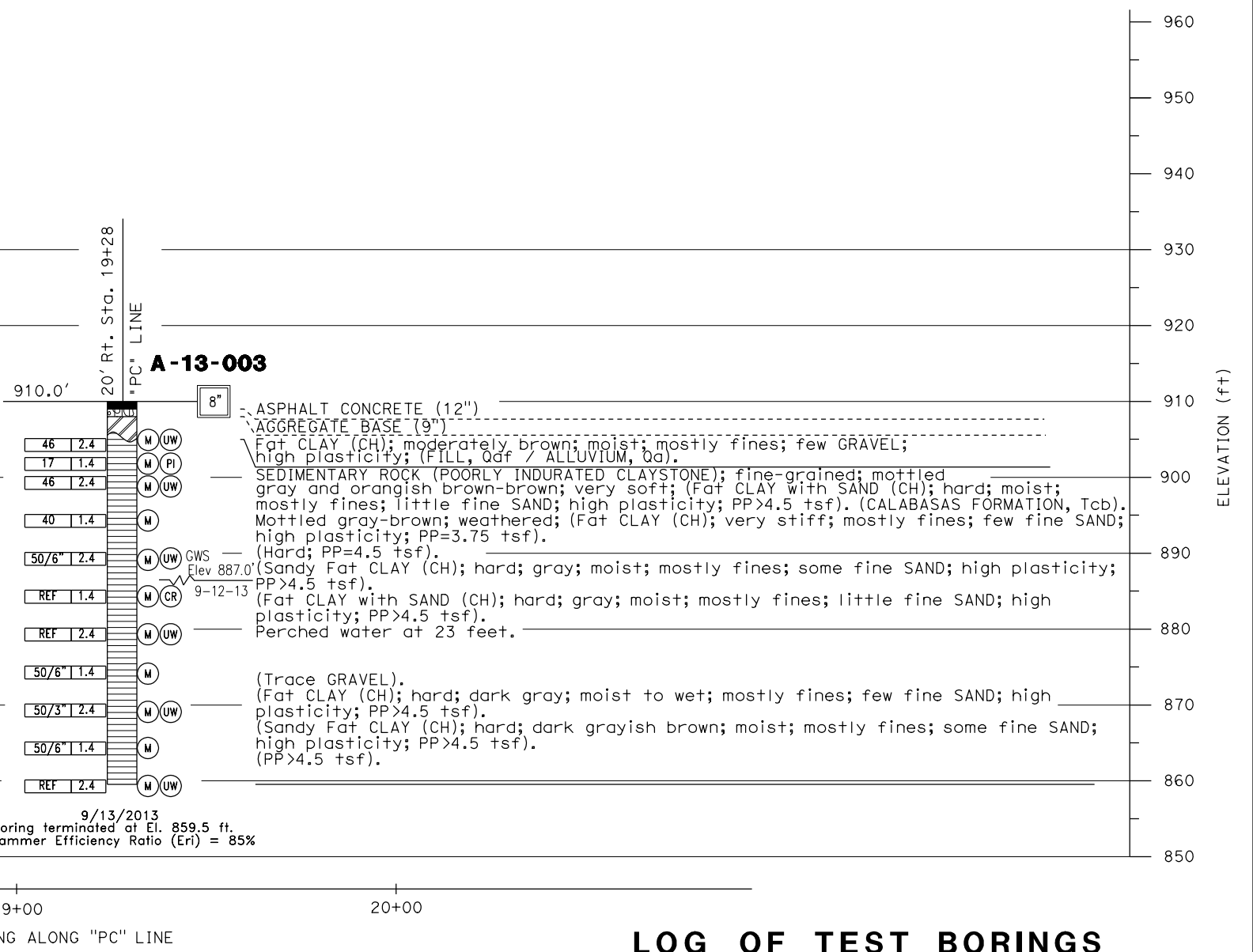
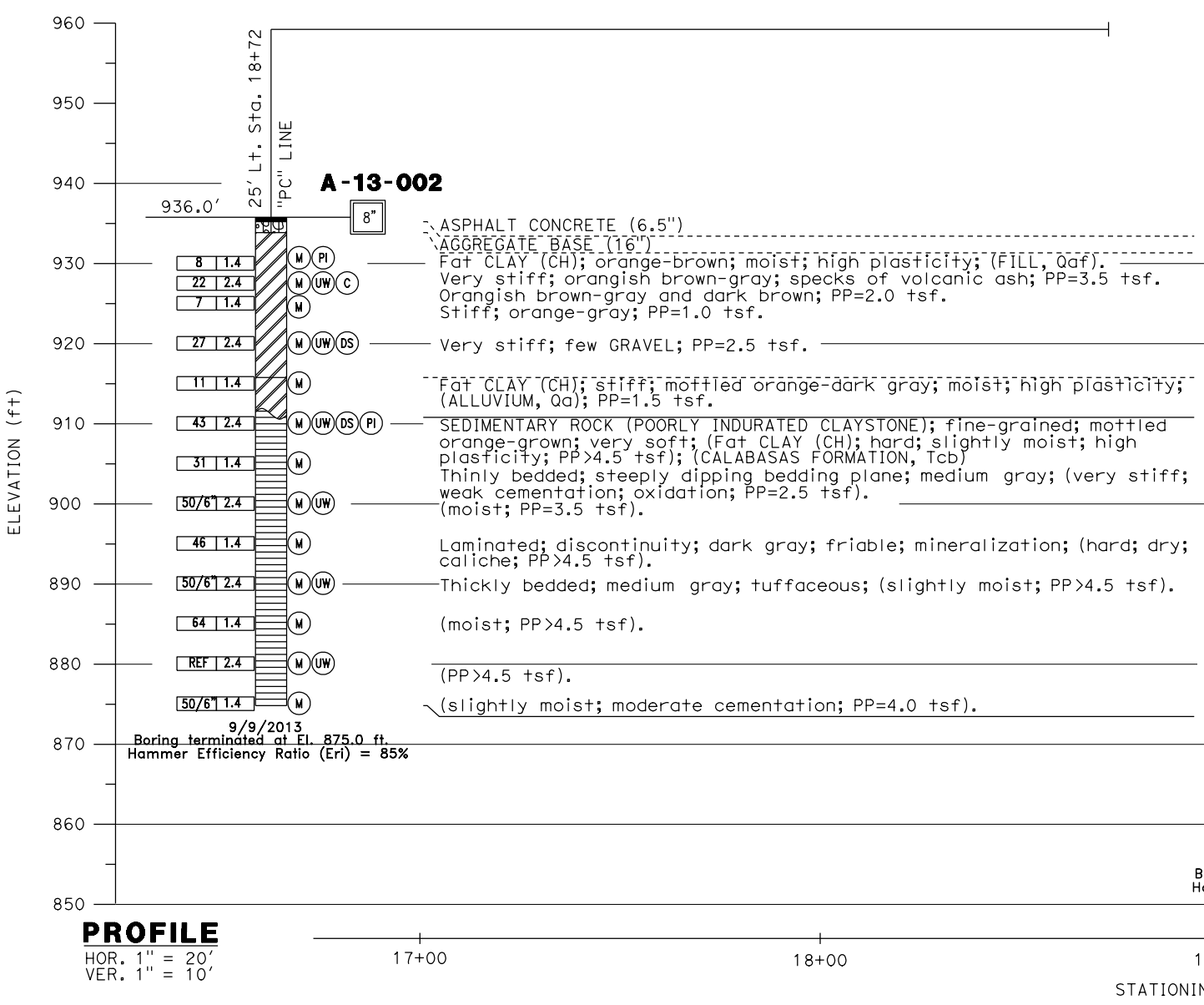
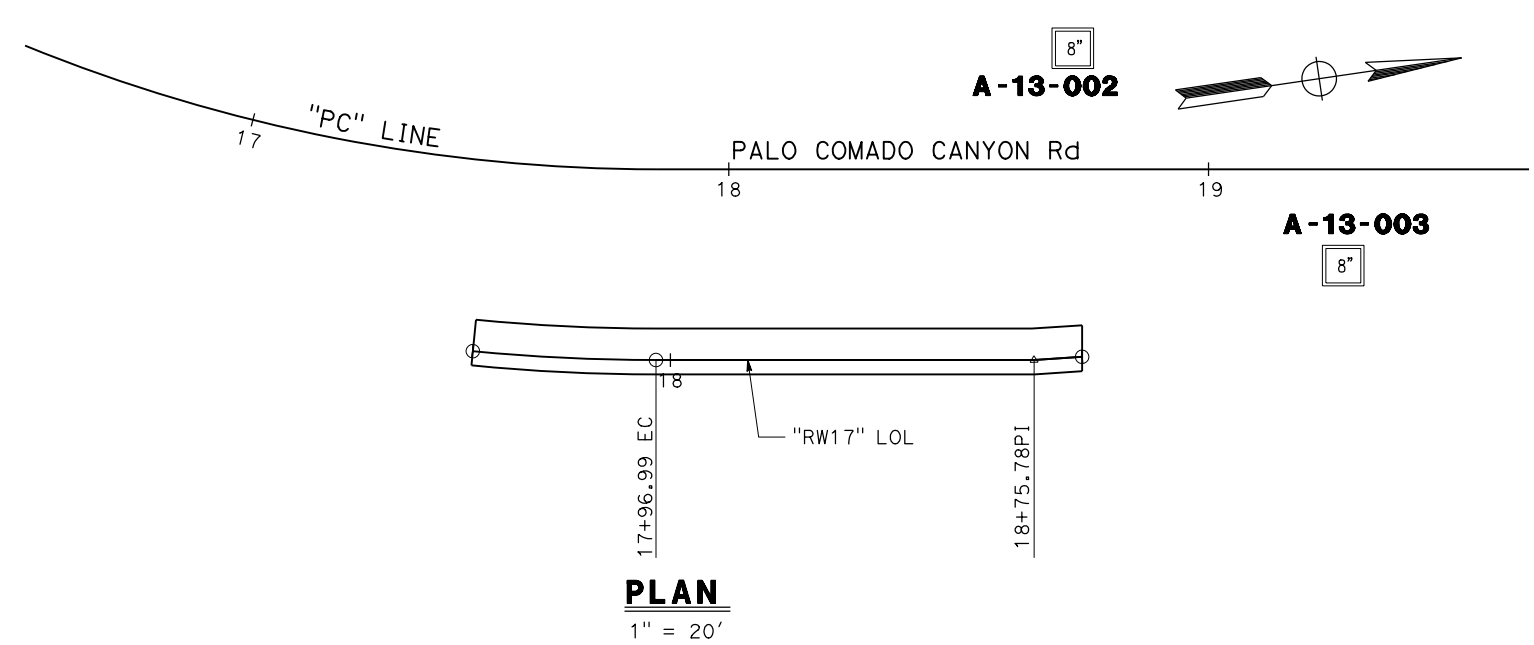
LOG OF TEST BORINGS
 RETAINING WALL No. 12 **PLATE 4**
R1-3

LAST REVISION: 00-00-00 DATE PLOTTED => 24-AUG-2017 TIME PLOTTED => 11:22

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 CONSULTANT FUNCTIONAL SUPERVISOR: SHAH GHANBARI
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 REVISOR: B. ANDERSON
 DATE REVISED: 08/21/17

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Dist	COUNTY	ROUTE	POST MILES TOTAL PROJECT	SHEET No.	TOTAL SHEETS
07	LA	101	33.5/33.9		

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PROFILE
 HOR. 1" = 20'
 VER. 1" = 10'

LOG OF TEST BORINGS
 RETAINING WALL No. 17
PLATE 5
R2-2

**TABLE 1
SOIL PROFILES**

(1) Boring No. (surface elevation)	(2) Location / Feature	(3) Bottom of Layer		(5) USCS Soil Classification	(6) Geologic Unit	(7) Total Unit Weight (pcf)	(8) Undrained Shear Strength (ksf)	(9) Drained Strength Parameters	
		(3) Depth (feet)	(4) Elevation (feet)					(9) Cohesion, c' (psf)	(10) Friction Angle, ϕ' (degrees)
A-13-001 (El. 934')	Abutment 1 Approach Retaining Walls	15	919	CH	Fill, Qaf	120	3.00	300	26
		20	914				3.50		
		24	910	CH	Alluvium, Qal	120	2.00	300	26
		below 24	below 910	CH	Bedrock, Tcb	125	4.00	400	26
A-13-002 (El. 936')	Abutment 1 and Abutment 1 Approach Retaining Walls	7.5	928.5	CH	Fill, Qaf	120	3.50	300	26
		15	921				1.50		
		20	916				2.50		
		25	911	CH	Alluvium, Qal	120	1.50	300	26
		30	906	CH	Bedrock, Tcb	125	4.50	400	26
		35	901				2.50		
		40	896				3.50		
below 40	below 896	4.50							
A-13-003 (El. 910')	Bent 2 and Abutment 1 Approach Retaining Walls	5	905	CH	Fill, Qaf	120	1.50	300	26
		7.5	902.5	CH	Bedrock, Tcb	125	4.50	400	26
		10	900				3.75		
		below 10	below 900				4.50		
A-13-004 (El. 914')	Bent 3	7.5	906.5	CH	Alluvium, Qal	120	3.25	300	26
		15	899				2.75		
		20	894				3.75		
		below 20	below 894	CH	Bedrock, Tcb	125	4.50	400	26
A-13-005 (El. 917')	Bent 4	7.5	909.5	CH	Alluvium, Qal	120	4.50	300	26
		below 7.5	below 909.5	CH	Bedrock, Tcb	125	4.50	400	26
A-13-006 (El. 936')	Abutment 5, Pilaster	7.5	928.5	CH	Fill, Qaf	120	4.00	300	26
		15	921				1.50		
		20	916	CH	Alluvium, Qal	120	3.50	300	26
		25	911	CH	Bedrock, Tcb	125	4.00	400	26
		below 25	below 911				4.50		

Column Notes:

- (1) Exploration number and ground elevation
- (2) Support and/or design feature location
- (3) Depth of bottom of layer below ground surface
- (4) Elevation of bottom of layer
- (5) Soil classification in accordance with the Unified Soil Classification System (USCS) per ASTM D 2487 and 2488
- (6) Interpreted Geologic Unit: Fill, Alluvium, or Bedrock
- (7) Total unit weight used for design
- (8) Undrained Shear Strength used for design, estimated by Pocket Penetrometer
- (9) & (10) Drained shear strength parameters for design based on direct shear test results and plasticity correlations



TABLE 2: SUMMARY OF AS-BUILT FOUNDATION CHARACTERISTICS
Palo Comado OC a.k.a Chesebro Road OC, Bridge No. 53-1678
07-LA-101 PM 33.69

Support Location	Foundation Type	Number of Piles	Capacity			Average Bottom of Pile Cap Elevation	Average Pile Tip Elevation	Average Length of Pile
			Design Compression	Ultimate Compressive	Ultimate Uplift			
			Kips	Kips	Kips			
Abut. 1	Cast In Drilled Hole (CIDH)	5	90	180	90	924.5	886	38.5
Bent 2*	Cast In Drilled Hole (CIDH)	14	90	180	90	900	884 - 887	13 - 16
Bent 3	Cast In Drilled Hole (CIDH)	24	90	180	90	903	881	22.0
Bent 4*	Cast In Drilled Hole (CIDH)	14	90	180	90	907	884 - 887	20 - 23
Abut. 5	Cast In Drilled Hole (CIDH)	5	90	180	90	924.1	887	37.5

Reference: 1962 As-Built Log of Test Borings (LOTB) as-built sheet

Notes:

*Pile data recorded on 1962 As-Built LOTB for Bent 2 and Bent 4 are reversed relative to the As-Built Foundation Plan. For purposes of this report it was assumed that the footing elevation in the Foundation Plan is correct, and that the tip elevations may have been transposed between Bent 2 and Bent 4. Therefore, a range of tip elevations is reported..

1. All piles are vertical (no batter piles).
2. Specified tip elevations are El. +888.0 feet for Abut 1, Abut 5, and Bent 4. Specified tip elevations are El. +882.0 and El. +885.0 feet for Bent 2 and Bent 3, respectively.
3. CIDH pile diameter = 16.0 inches.
4. Recommended axial pile load capacity values for seismic design assuming the piles are in good condition and the connection can transmit the uplift loads. The recommended values are limited to twice the reported design values.



Foundation Design Data Sheet							
Support No.	Pile Type	Finished Grade Elevation (ft)	Cut-off Elevation (ft)	Pile Cap Size (ft)		Permissible Settlement under Service Load (in)*	Number of Piles per Support
				B	L		
Abut 1L	16" CIDH	928	926.36 ^(a)	2.5	20	1"	4
			924.36 ^(b)				
Abut 1R	16" CIDH	928	927.08 ^(a)	2.5	28	1"	5
			925.08 ^(b)				
Bent 2L	24" CIDH	910	901.34	14	10	1"	6
Bent 2R	24" CIDH	910	901.34	14	19	1"	12
Bent 3L	24" CIDH	914	904.59	14	10	1"	6
Bent 3R	24" CIDH	914	904.59	14	19	1"	12
Bent 4L	24" CIDH	917	908.34	14	10	1"	6
Bent 4R	24" CIDH	917	908.34	14	19	1"	12
Abut 5L	16" CIDH	930	926.65	2.5	14	1"	3
Abut 5R	16" CIDH	930	926.69	2.5	22	1"	4
Abut 5 Pilaster	16" CIDH	935.5	930.75	7	7	1"	3

NOTES:

(a). Cut-off elevation for all piles except the pile below the pilaster.

(b). Cut-off elevation for the pile below the pilaster.

* Based on CALTRANS' current practice, the total permissible settlement is one inch for multi-span structures with continuous spans or multi-column bents, one inch for single span structures with diaphragm abutments, and two inches for single span structures with seat abutments. Different permissible settlement under service loads may be allowed if a structural analysis verifies that required level of serviceability is met.



**TABLE 3
FOUNDATION DESIGN
DATA SHEET**

Foundation Factored Design Loads										
Support No.	Service-I Limit State (kips)		Strength/Construction Limit State (Controlling Group, kips)				Extreme Event Limit State (Controlling Group, kips)			
	Total Load Per Support*	Permanent Loads Per Support *	Compression		Tension		Compression		Tension	
			Per Support*	Max. Per Pile	Per Support*	Max. Per Pile	Per Support*	Max. Per Pile	Per Support*	Max. Per Pile
Abut 1L	350	250	450	140	0	0	N/A	N/A	N/A	N/A
Abut 1R	500	300	650	160	0	0	N/A	N/A	N/A	N/A
Bent 2L	660	550	910	260	0	20	550	300	0	140
Bent 2R	600	450	850	180	0	0	1000	320	150	180
Bent 3L	800	650	1100	280	0	20	650	320	0	120
Bent 3R	750	550	1050	200	0	0	1100	340	100	180
Bent 4L	600	460	810	220	0	0	470	300	0	140
Bent 4R	550	400	750	150	0	0	950	320	200	200
Abut 5L	200	150	300	140	0	0	N/A	N/A	N/A	N/A
Abut 5R	350	200	500	150	0	0	N/A	N/A	N/A	N/A
Abut 5 Pilaster	100	100	100	60	0	0	100	150	0	70

* For Bent 2R, Bent 3R, and Bent 4R loads are **per column**.



**TABLE 4
FOUNDATION FACTORED
DESIGN LOADS**

Foundation Design Recommendations												
Support Location	Pile Type	Cut-off Elevation (ft)	Service-I Limit State Load per Support (kips)		Total Permissible Support Settlement (inches)	Required Factored Nominal Resistance Per Pile (kips)				Design Tip Elevations (ft)	Specified Tip Elevation (ft)	Required Nominal Driving Resistance (kips)
			Total	Permanent		Strength/Construction		Extreme Event				
						Comp. ($\phi = 0.7$)	Tension ($\phi = 0.7$)	Comp. ($\phi = 1.0$)	Tension ($\phi = 1.0$)			
Abut 1L	16" CIDH	926.36 ^(a)	350	250	1"	140	0	N/A	N/A	889.11 (a-I)	889.11	N/A
		924.36 ^(b)								916.11 (c)		
Abut 1R	16" CIDH	927.08 ^(a)	500	300	1"	160	0	N/A	N/A	885.83 (a-I)	885.83	N/A
		925.08 ^(b)								916.83 (c)		
Bent 2L	24" CIDH	901.34	660	550	1"	260	20	300	140	867.09 (a-I) 891.09 (b-I) 872.09 (a-II) 879.09 (b-II) 891.09 (c) 880.09 (d)	867.09	N/A
Bent 2R	24" CIDH	901.34	600	450	1"	180	0	320	180	875.09 (a-I) 870.09 (a-II) 875.09 (b-II) 891.09 (c) 880.09 (d)	870.09	N/A
Bent 3L	24" CIDH	904.59	800	650	1"	280	20	320	120	867.34 (a-I) 893.34 (b-I) 873.34 (a-II) 884.34 (b-II) 894.34 (c) 883.34 (d)	867.34	N/A
Bent 3R	24" CIDH	904.59	750	550	1"	200	0	340	180	875.34 (a-I) 871.34 (a-II) 877.34 (b-II) 894.34 (c) 883.34 (d)	871.34	N/A
Bent 4L	24" CIDH	908.34	600	460	1"	220	0	300	140	878.09 (a-I) 879.09 (a-II) 886.09 (b-II) 898.09 (c) 887.09 (d)	878.09	N/A
Bent 4R	24" CIDH	908.34	550	400	1"	150	0	320	200	885.09 (a-I) 877.09 (a-II) 880.09 (b-II) 898.09 (c) 887.09 (d)	877.09	N/A
Abut 5L	16" CIDH	926.65	200	150	1"	140	0	N/A	N/A	894.40 (a-I) 916.40 (c) 908.40 (d)	894.40	N/A
Abut 5R	16" CIDH	926.69	350	200	1"	150	0	N/A	N/A	893.44 (a-I) 916.44 (c) 908.44 (d)	893.44	N/A
Abut 5 Pilaster	16" CIDH	930.75	100	100	1"	60	0	150	70	911.50 (a-I) 904.50 (a-II) 909.50 (b-II) 920.50 (c) 918.50 (d)	904.50	N/A

Notes:
(a). Cut-off elevation for all piles except the pile below the pilaster.
(b). Cut-off elevation for the pile below the pilaster.
1) Design tip elevations are controlled by: (a-I) Compression (Strength Limit), (b-I) Tension (Strength Limit), (a-II) Compression (Extreme Event), (b-II) Tension (Extreme Event), (c) Settlement, (d) Lateral Load.
2) The CIDH specified tip elevation shall not be raised.



TABLE 5
FOUNDATION DESIGN
RECOMMENDATIONS

Pile Data Table						
Location	Pile Type	Cut-Off Elevation (feet)	Nominal Resistance (kips)		Design Tip Elevations (ft)	Specified Tip Elevation (ft)
			Compression	Tension		
Abut 1L	16" CIDH	926.36 ^(a)	200	N/A	889.11 (a)	889.11
		924.36 ^(b)			916.11 (c)	
Abut 1R	16" CIDH	927.08 ^(a)	230	N/A	885.83 (a)	885.83
		925.08 ^(b)			916.83 (c)	
Bent 2L	24" CIDH	901.34	380	140	867.09 (a) 879.09 (b) 891.09 (c) 880.09 (d)	867.09
Bent 2R	24" CIDH	901.34	320	180	870.09 (a) 875.09 (b) 891.09 (c) 880.09 (d)	870.09
Bent 3L	24" CIDH	904.59	400	120	867.34 (a) 884.34 (b) 894.34 (c) 883.34 (d)	867.34
Bent 3R	24" CIDH	904.59	340	180	871.34 (a) 877.34 (b) 894.34 (c) 883.34 (d)	871.34
Bent 4L	24" CIDH	908.34	320	140	878.09 (a) 886.09 (b) 898.09 (c) 887.09 (d)	878.09
Bent 4R	24" CIDH	908.34	320	200	877.09 (a) 880.09 (b) 898.09 (c) 887.09 (d)	877.09
Abut 5L	16" CIDH	926.65	200	N/A	894.40 (a) 916.40 (c) 908.40 (d)	894.40
Abut 5R	16" CIDH	926.69	220	N/A	893.44 (a) 916.44 (c) 908.44 (d)	893.44
Abut 5 Pilaster	16" CIDH	930.75	150	70	904.50 (a) 909.50 (b) 920.50 (c) 918.50 (d)	904.50

Notes:

(a). Cut-off elevation for all piles except the pile below the pilaster.

(b). Cut-off elevation for the pile below the pilaster.

1) Design tip elevations for Bents and Abutments are controlled by: (a) Compression, (b) Tension, (c) Settlement, (d) Lateral Load.

2) The CIDH Specified Tip Elevation shall not be raised.

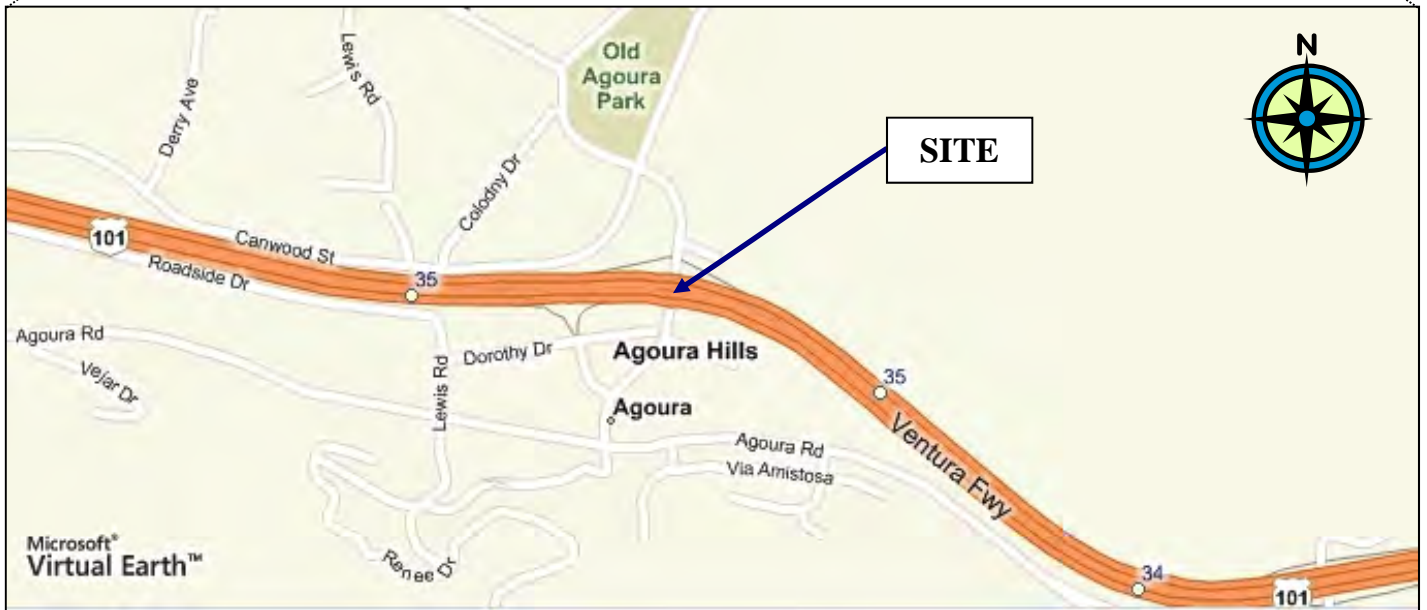


Location	Pile Type	Head Condition	Load Direction	Spacing	Average P-mult	Leading P-mult	Ground Slope	Avg P-mult			Max P-Mult	
								Top Deflection	Top Shear (kips)	Critical Length (ft)	Max Moment (kips-ft)	Depth to Max Moment (ft)
Abut 1R	CIDH 16"	Free	Longitudinal	4D	1	1	1.5:1	0.25	13	15	32	4.5
								0.5	18		50	5
								1	24		79	5.5
			Transverse	4D	0.65	0.88	LEVEL	0.25	14	15	39	4
								0.5	19		61	4.5
								1	26		98	5
Abut 1L	CIDH 16"	Free	Longitudinal	3.375D	0.93	0.93	1.5:1	0.25	13	15	32	4.5
								0.5	18		51	5
								1	25		80	5.5
			Transverse	3.375D	0.58	0.8	LEVEL	0.25	13	15	33	4
								0.5	18		53	4.5
								1	24		84	5
Bent 2R	CIDH 24"	Free	Longitudinal	2.5D	0.48	0.675	LEVEL	0.25	42	17.5	129	5.0
								0.5	57		202	5.5
								1	79		318	6.5
			Transverse	2.5D	0.44	0.675	LEVEL	0.25	39	17.5	129	5.0
								0.5	54		202	5.5
								1	74		318	6.5
Bent 2L	CIDH 24"	Free	Longitudinal	2.5D	0.48	0.675	LEVEL	0.25	42	17.5	129	5.0
								0.5	57		202	5.5
								1	79		318	6.5
			Transverse	3D	0.65	0.75	LEVEL	0.25	52	17.5	136	5.0
								0.5	71		213	5.5
								1	98		334	6.5
Bent 3R	CIDH 24"	Free	Longitudinal	2.5D	0.48	0.675	LEVEL	0.25	31	17.5	109	5.0
								0.5	43		172	5.5
								1	60		274	6.5
			Transverse	2.5D	0.44	0.675	LEVEL	0.25	29	17.5	109	5.0
								0.5	40		172	5.5
								1	56		274	6.5
Bent 3L	CIDH 24"	Free	Longitudinal	2.5D	0.48	0.675	LEVEL	0.25	31	17.5	109	5.0
								0.5	43		172	5.5
								1	59		274	6.5
			Transverse	3D	0.65	0.75	LEVEL	0.25	39	17.5	114	5.0
								0.5	53		181	5.5
								1	74		287	6.5
Bent 4R	CIDH 24"	Free	Longitudinal	2.5D	0.48	0.675	LEVEL	0.25	44	17.5	131	5.0
								0.5	60		205	5.5
								1	82		322	6.5
			Transverse	2.5D	0.44	0.675	LEVEL	0.25	41	17.5	131	5.0
								0.5	56		205	5.5
								1	77		322	6.5
Bent 4L	CIDH 24"	Free	Longitudinal	2.5D	0.48	0.675	LEVEL	0.25	44	17.5	131	5.0
								0.5	60		205	5.5
								1	82		322	6.5
			Transverse	3D	0.65	0.75	LEVEL	0.25	59	17.5	138	5.0
								0.5	75		216	5.5
								1	102		338	6.5
Abut 5R	CIDH 16"	Free	Longitudinal	4D	1	1	1.5:1	0.25	13	15	29	5
								0.5	17		46	5.5
								1	24		75	6
			Transverse	4D	0.67	0.88	LEVEL	0.25	14	15	35	4.5
								0.5	20		56	5
								1	27		90	5.5
Abut 5L	CIDH 16"	Free	Longitudinal	3.375D	0.93	0.93	1.5:1	0.25	12	15	28	5
								0.5	16		45	5.5
								1	23		73	6
			Transverse	3.375D	0.62	0.8	LEVEL	0.25	13	15	34	4.5
								0.5	19		54	5
								1	26		86	5.5
Abut 5 Pilaster	CIDH 16"	Free	Longitudinal	2.25D	1	1	LEVEL	0.25	35	8	45	3
								0.5	46		68	3.5
								1	60		104	4.5
			Transverse	2.25D	0.52	0.64	LEVEL	0.25	14	10	35	4.5
								0.5	19		54	5
								1	26		83	5.5



TABLE 7
SUMMARY OF
LATERAL PILE CAPACITY

Figures



The base maps are from Microsoft's Virtual Earth


	<p>GDC Project No. LA-1143</p>
	<p>Palo Comado Canyon Road OC (Widen) Agoura Hills, California</p> <p>VICINITY MAP</p>

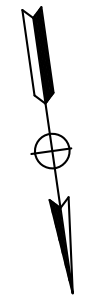
Figure 1

DIST	COUNTY	ROUTE	POST MILES TOTAL PROJECT	SHEET No.	TOTAL SHEETS
07	LA	101	33.5/33.9		

100% SUBMITTAL
NOT FOR CONSTRUCTION
SEPTEMBER 2017

PARSONS
525 B STREET, STE 1600
SAN DIEGO, CA 92101

CITY OF AGOURA HILLS
30001 LADYFACE COURT
AGOURA HILLS, CA 91301



NOTE:
FOR ACCURATE RIGHT OF WAY DATA, CONTACT
RIGHT OF WAY ENGINEERING AT THE DISTRICT OFFICE.

ABBREVIATIONS:
C CUT
F FILL

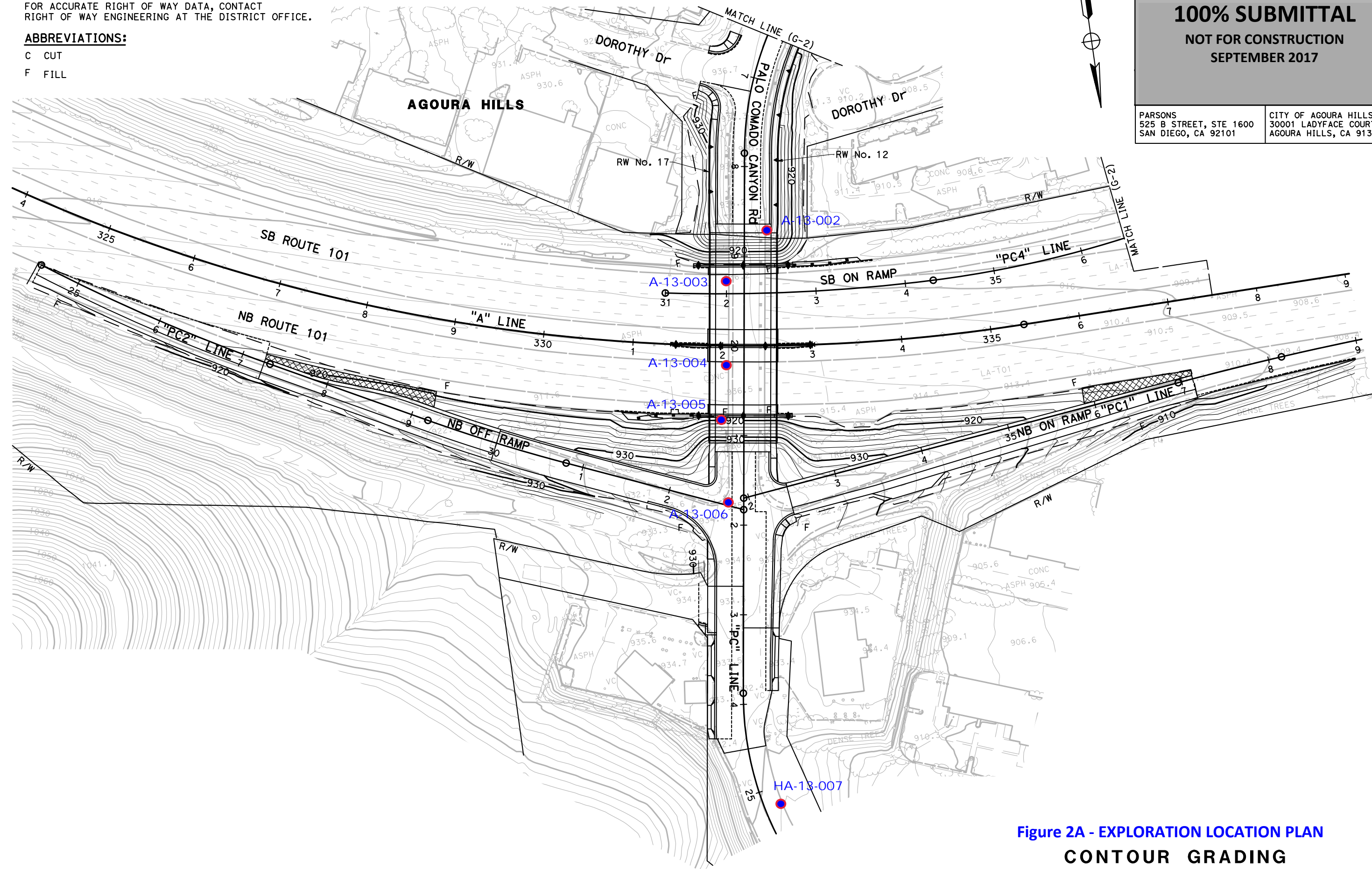


Figure 2A - EXPLORATION LOCATION PLAN
CONTOUR GRADING
SCALE: 1" = 50'

APPROVED FOR CONTOUR GRADING WORK ONLY

G-1

STATE OF CALIFORNIA - DEPARTMENT OF TRANSPORTATION	CONSULTANT FUNCTIONAL SUPERVISOR	CALCULATED-DESIGNED BY	REVISOR
Caltrans	MARK FIRGER	CHECKED BY	DATE REVISED
		KEVIN CASTRO	
		TOMO TAKAHASHI	

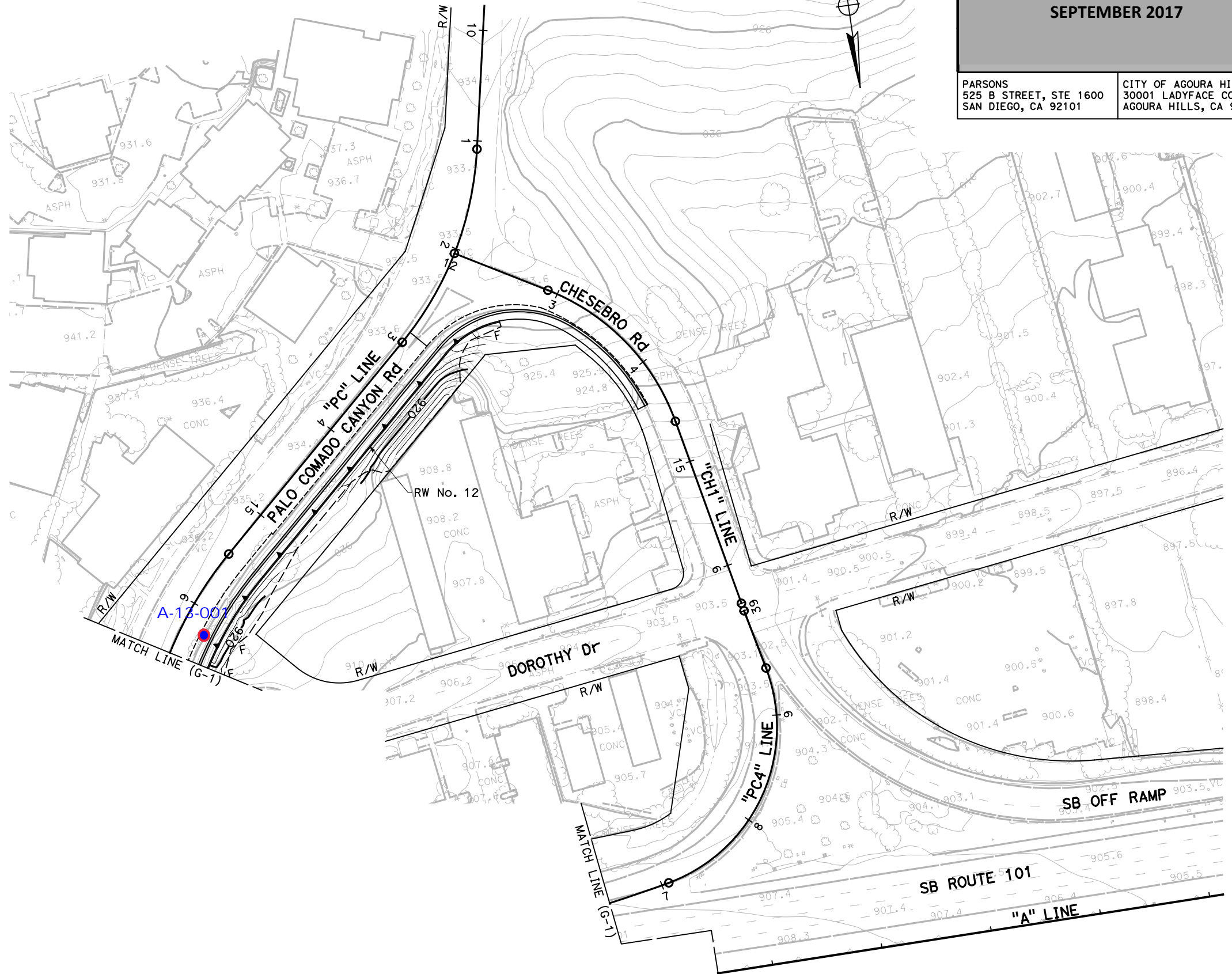
Dist	COUNTY	ROUTE	POST MILES TOTAL PROJECT	SHEET No.	TOTAL SHEETS
07	LA	101	33.5/33.9		

100% SUBMITTAL
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SEPTEMBER 2017

PARSONS
525 B STREET, STE 1600
SAN DIEGO, CA 92101

CITY OF AGOURA HILLS
30001 LADYFACE COURT
AGOURA HILLS, CA 91301

NOTE:
FOR ACCURATE RIGHT OF WAY DATA, CONTACT
RIGHT OF WAY ENGINEERING AT THE DISTRICT OFFICE.



STATE OF CALIFORNIA - DEPARTMENT OF TRANSPORTATION	CONSULTANT FUNCTIONAL SUPERVISOR	CALCULATED/DESIGNED BY	REVISOR
Caltrans	MARK FIRGER	CHECKED BY	DATE REVISOR
		KEVIN CASTRO	
		TOMO TAKAHASHI	

Figure 2B - EXPLORATION LOCATION PLAN

CONTOUR GRADING
SCALE: 1" = 50'

APPROVED FOR CONTOUR GRADING WORK ONLY

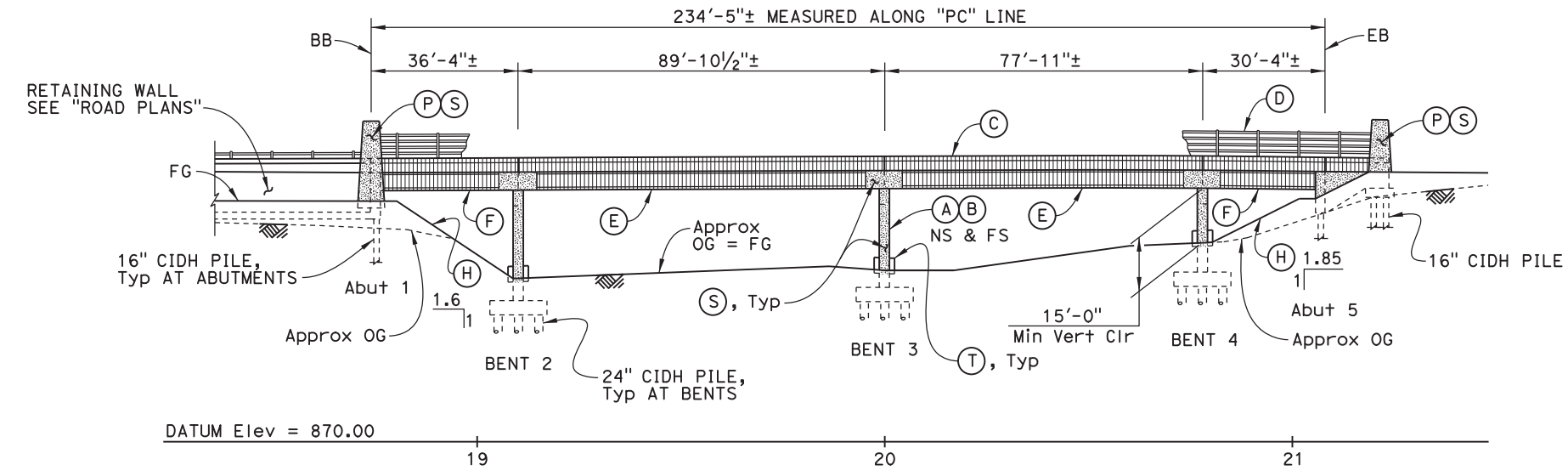
G-2

DIST	COUNTY	ROUTE	POST MILES TOTAL PROJECT	SHEET No	TOTAL SHEETS
07	LA	101	33.5/33.9		

REGISTERED CIVIL ENGINEER DATE _____
 PLANS APPROVAL DATE _____
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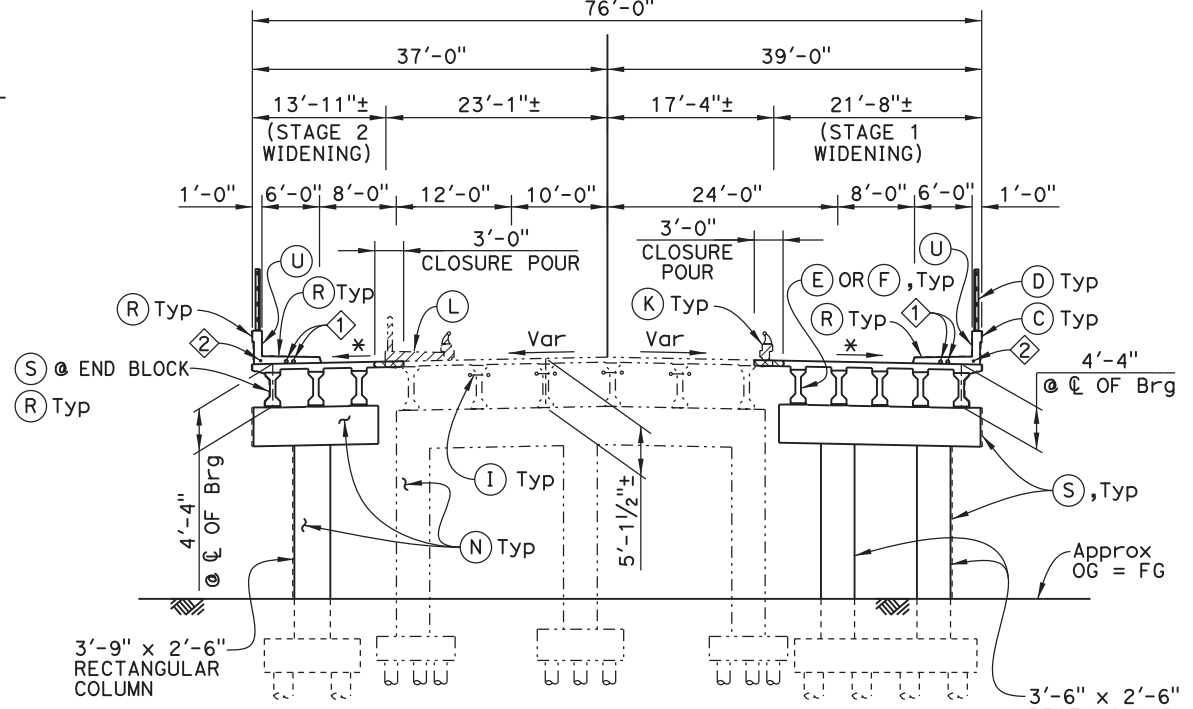
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 AGOURA HILLS, CA 91301
 PARSONS
 2201 DUPONT DRIVE, SUITE 200
 IRVINE, CA 92612



CURVE DATA ①	CURVE DATA ②
R = 1999.95'	R = 1920.11'
Δ = 40°19'10"	Δ = 08°56'23"
T = 734.24'	T = 150.10'
L = 1407.38'	L = 299.59'

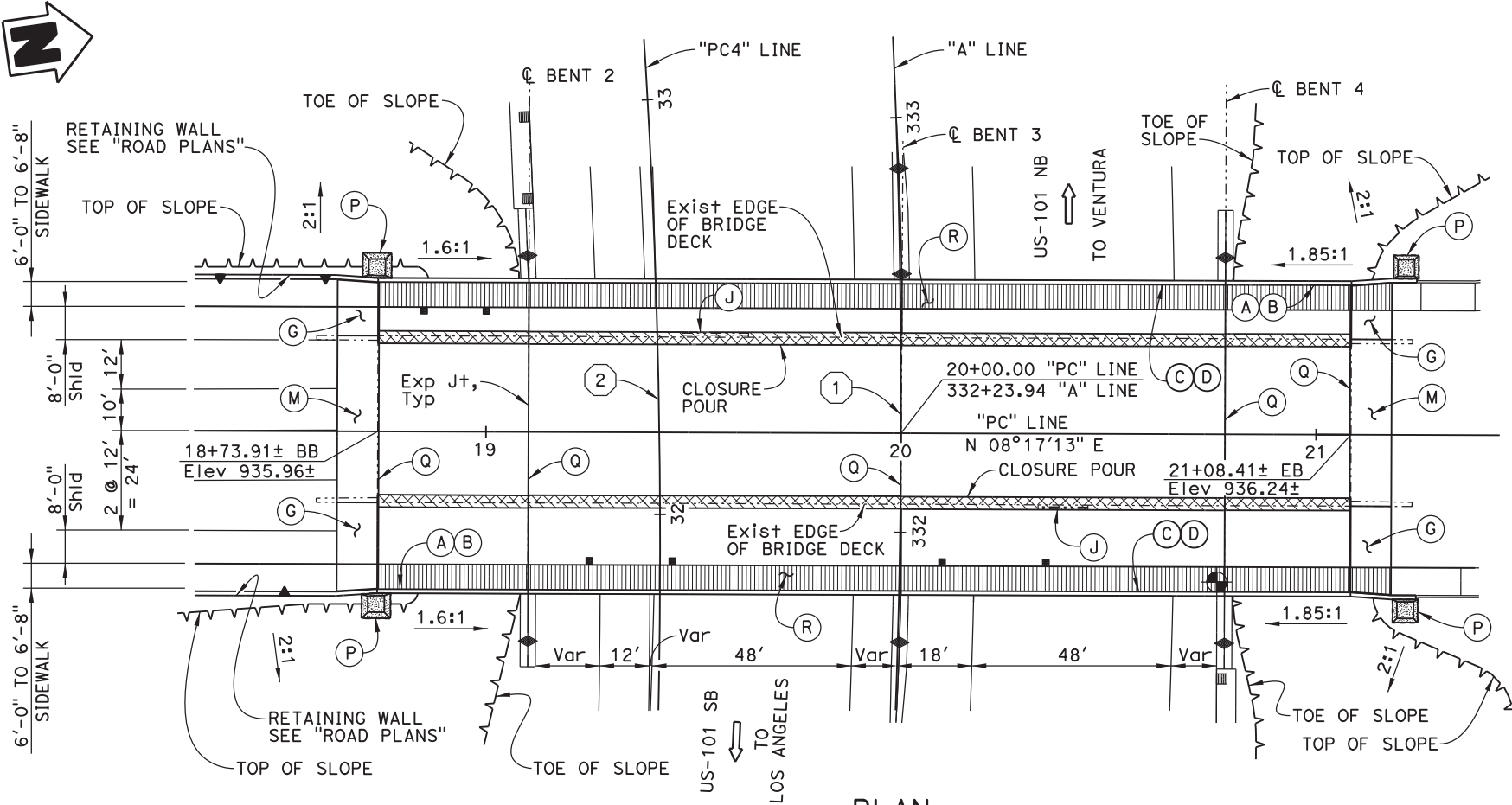
ELEVATION
 1" = 20'

- UTILITIES:**
- ① 2 - 4"Ø Future Utility Openings, See "ELECTRICAL PLANS"
 - ② 1/2"Ø Electrical Conduit for Lighting, See "ELECTRICAL PLANS"



TYPICAL SECTION
 1" = 10'

- NOTES:**
- (A) Paint "Br No. 53-1678"
 - (B) Paint "PALO COMADO CANYON ROAD OC"
 - (C) Concrete Barrier (Type 732SW Mod)
 - (D) Chain Link Railing (Type 7 Mod)
 - (E) 3'-6" PC/PS Conc Girder (Spans 2 & 3)
 - (F) CIP Reinforced Concrete T-Girder (Spans 1 & 4)
 - (G) Structure Approach Slab Type EQ(10)
 - (H) Slope Paving
 - (I) Exist Cable Restrainer
 - (J) Remove Existing Bridge Mounted Sign
 - (K) Remove Existing Barrier
 - (L) Remove Existing Barrier, Sidewalk and Pipe Railing and Refinish Bridge Deck
 - (M) Structure Approach Slab Type R(10D)
 - (N) Stained Concrete
 - (P) Pilaster
 - (Q) Clean Expansion Joint and Place New Joint Seal
- LEGEND:**
- Indicates Existing Structure
 - ▨ Indicates Bridge Removal (Portion)
 - ▨ Indicates Closure Pour
 - ⊙ Indicates Point of Minimum Vertical Clearance
 - * Match Existing Grade & Cross Slope
 - ◆◆ Concrete Barrier (Type 60R), See "ROADWAY PLANS"
 - Indicates MGS, see "ROADWAY PLANS"
 - Indicates Deck Drain (Type D-1)



PLAN
 1" = 20'

Figure 3A

NOTE:
 The contractor shall verify all controlling field dimensions before ordering or fabricating any material.

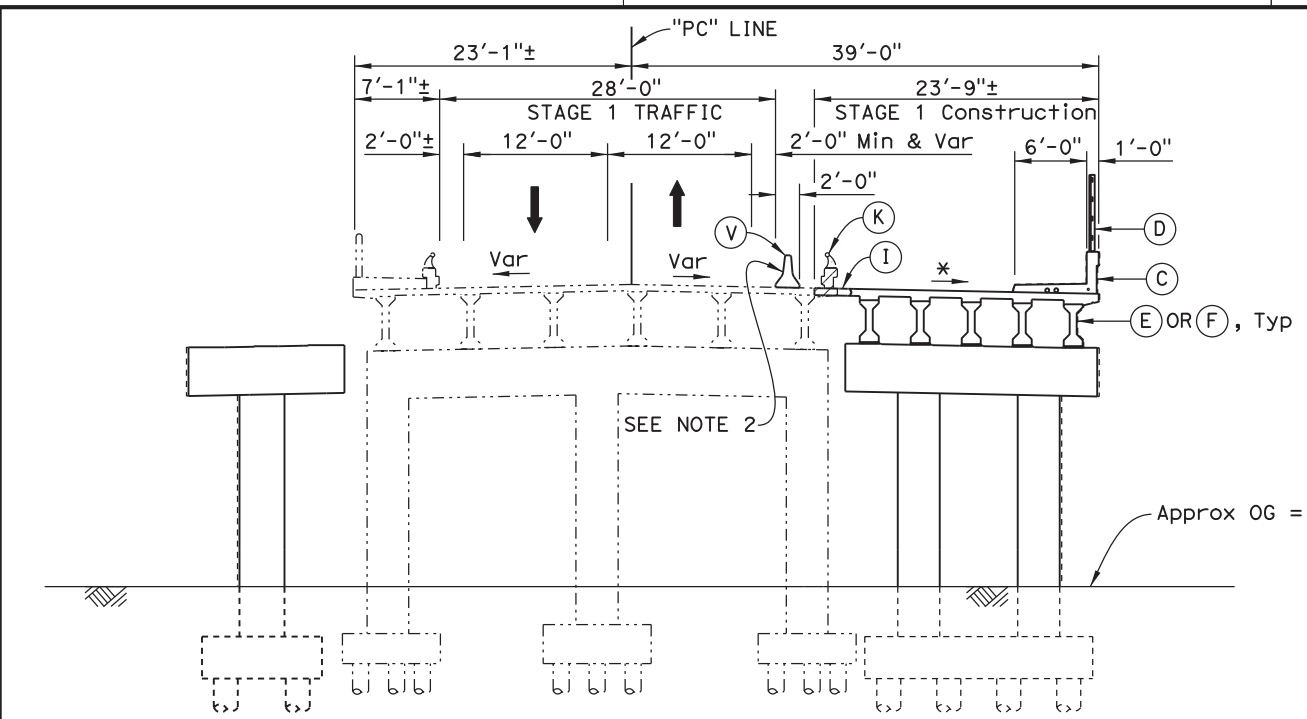
DESIGN OVERSIGHT	DESIGN BY: D. LaFranchi	CHECKED: E. Jeong/G. Douglass	LOAD & RESISTANCE FACTOR DESIGN	LIVE LOADING: HL93 W/"LOW-BOY"; PERMIT DESIGN VEHICLE	PREPARED FOR THE STATE OF CALIFORNIA DEPARTMENT OF TRANSPORTATION	BRIDGE NO. 53-1678	PALO COMADO CANYON RD OC (WIDEN)
SIGN OFF DATE	DETAILS BY: F. Hakemi	CHECKED: E. Jeong	LAYOUT BY: D. LaFranchi	CHECKED: E. Jeong	PROJECT ENGINEER: Jon Hermstad	POST MILES 33.69	
QUANTITIES	BY: D. LaFranchi	CHECKED: E. Jeong	SPECIFICATIONS BY: J. Hermstad	PLANS AND SPECS COMPARED: J. Hermstad	UNIT: 1821	PROJECT NUMBER & PHASE: 0700001841	CONTRACT NO.: 07-257200

DIST	COUNTY	ROUTE	POST MILES TOTAL PROJECT	SHEET No	TOTAL SHEETS
07	LA	101	33.5/33.9		

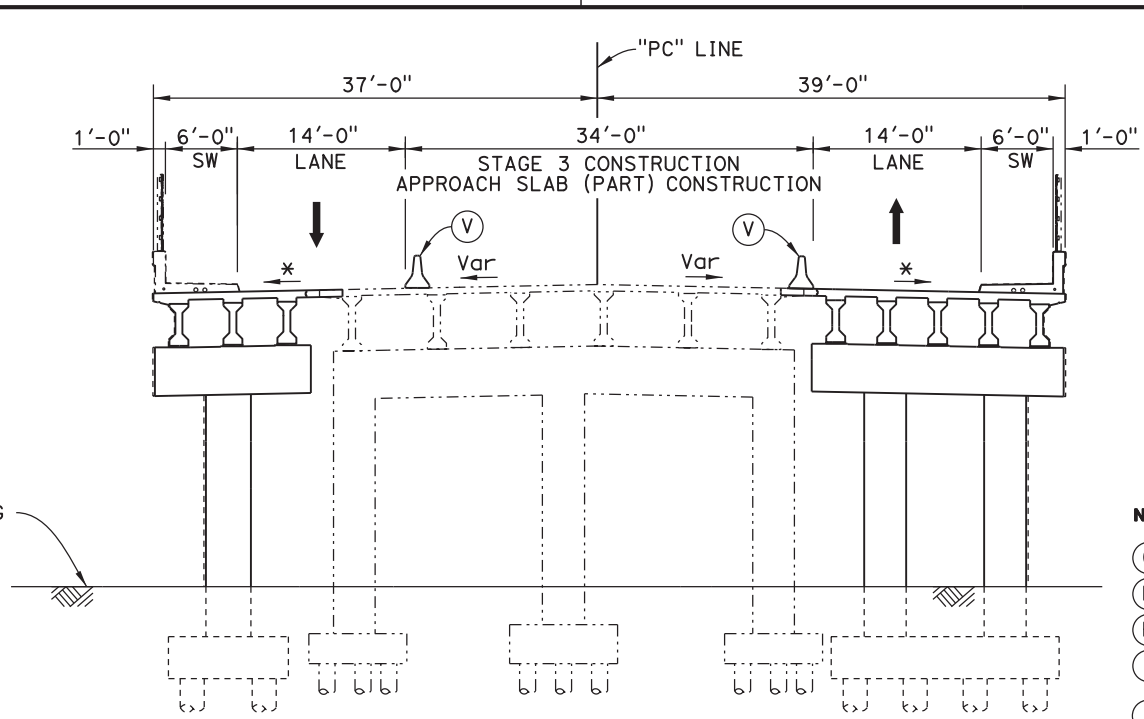
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 PLANS APPROVAL DATE _____
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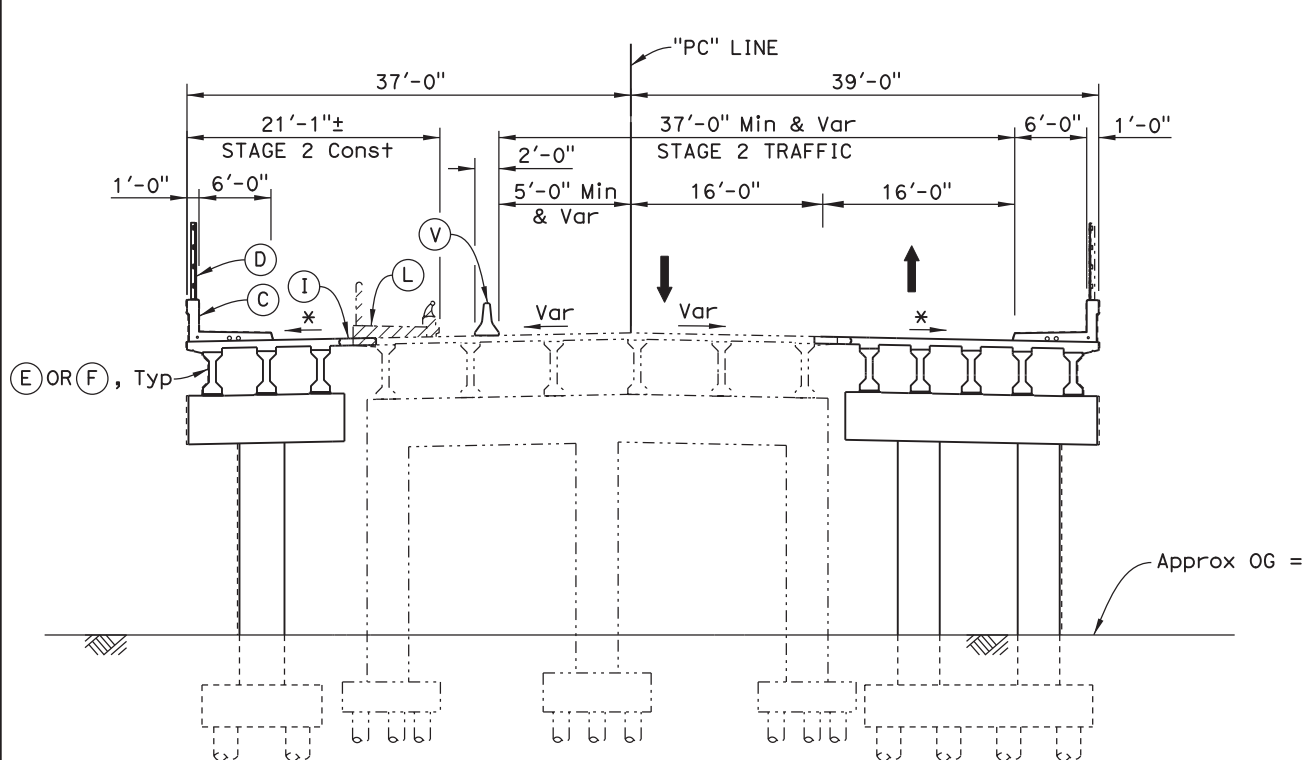
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 IRVINE, CA 92612



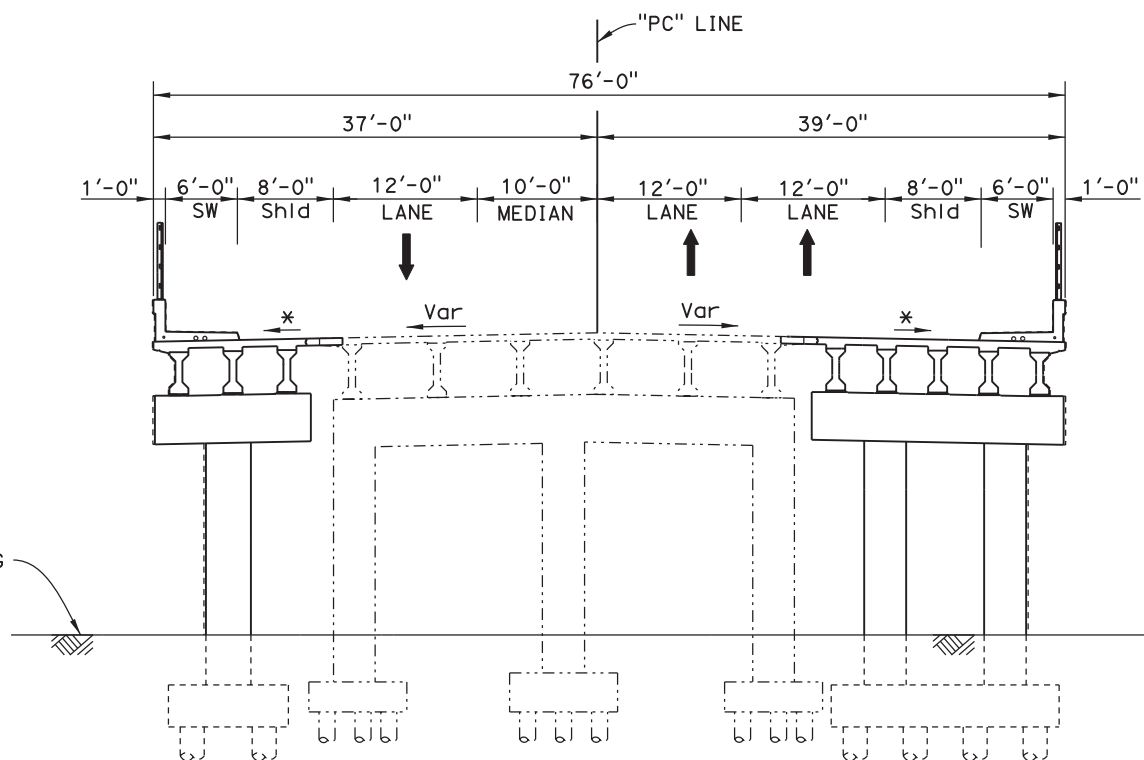
* Match Existing Slope
STAGE 1 CONSTRUCTION
 1/8" = 1'-0"



* Match Existing Slope
STAGE 3 CONSTRUCTION
 1/8" = 1'-0"



* Match Existing Slope
STAGE 2 CONSTRUCTION
 1/8" = 1'-0"



* Match Existing Slope
FINAL STAGE CONSTRUCTION
 1/8" = 1'-0"

NOTES:

- (C) Concrete Barrier (Type 732SW Mod)
- (D) Chain Link Railing (Type 7 Mod)
- (E) 3'-6" PC/PS Conc Girder (Spans 2 & 3)
- (F) CIP Reinforced Concrete T-Girder (Spans 1 & 4)
- (I) Closure Pour
- (K) Remove Existing Barrier
- (L) Remove Existing Barrier, Sidewalk and Pipe Railing and Refinish Bridge Deck
- (V) Temporary Railing (Type K) See "ROADWAY PLANS"

NOTES:

1. For overall project Stage Construction Details and Stage Construction Numbering, see "ROADWAY PLANS".
2. Where distance between K-rail and exposed edge of deck is less than 2'-0", attach K-rail to deck per Standard Plan T3A.

LEGEND:

- Indicates Existing Structure
- ➔ Indicates Traffic Lane
- ▨ Indicates Bridge Removal (Portion)

NOTE:
 The contractor shall verify all controlling field dimensions before ordering or fabricating any material.

DESIGN OVERSIGHT	DESIGN BY: D. LaFranchi	CHECKED: E. Ieong/G. Douglass	PREPARED FOR THE STATE OF CALIFORNIA DEPARTMENT OF TRANSPORTATION Jon Hermsstad PROJECT ENGINEER	BRIDGE NO. 53-1678	PALO COMADO CANYON RD OC (WIDEN) STAGE CONSTRUCTION
SIGN OFF DATE	DETAILS BY: F. Hakemi	CHECKED: E. Ieong		POST MILES 33.69	
DESIGN DETAIL SHEET (ENGLISH) (REV. 03/14/12)	QUANTITIES BY: D. LaFranchi	CHECKED: E. Ieong		UNIT: 1821	
ORIGINAL SCALE IN INCHES FOR REDUCED PLANS			PROJECT NUMBER & PHASE: 0700001841	CONTRACT NO.: 07-257200	DISREGARD PRINTS BEARING EARLIER REVISION DATES
			FILE => 53-1628-a-ap02.dan	REVISION DATES	SHEET 2 OF 32

100% INTERMEDIATE PS&E - SEPTEMBER 2017 (NOT FOR CONSTRUCTION)

Figure 3B

DIST	COUNTY	ROUTE	POST MILES TOTAL PROJECT	SHEET No	TOTAL SHEETS
07	LA	101	33.5/33.9		

PILE DATA TABLE					
LOCATION	PILE TYPE	NOMINAL RESISTANCE (KIPS)		DESIGN TIP ELEVATIONS (FT)	SPECIFIED TIP ELEVATIONS (FT)
		COMPRESSION	TENSION		
ABUTMENT 1L	16" CIDH	200	N/A	889.1 (a); 916.1 (c); 908.1 (d)	889.1
ABUTMENT 1R	16" CIDH	230	N/A	885.8 (a); 916.8 (c); 908.8 (d)	885.8
BENT 2L	24" CIDH	380	140	867.1 (a); 879.1 (b); 891.1 (c); 880.1 (d)	867.1
BENT 2R	24" CIDH	320	180	870.1 (a); 875.1 (b); 891.1 (c); 880.1 (d)	870.1
BENT 3L	24" CIDH	400	120	867.3 (a); 884.3 (b); 894.3 (c); 883.3 (d)	867.3
BENT 3R	24" CIDH	340	180	871.3 (a); 877.3 (b); 894.3 (c); 883.3 (d)	871.3
BENT 4L	24" CIDH	320	140	878.1 (a); 886.1 (b); 898.1 (c); 887.1 (d)	878.1
BENT 4R	24" CIDH	320	200	877.1 (a); 880.1 (b); 898.1 (c); 887.1 (d)	877.1
ABUTMENT 5L	16" CIDH	200	N/A	894.4 (a); 916.4 (c); 908.4 (d)	894.4
ABUTMENT 5R	16" CIDH	220	N/A	893.4 (a); 916.4 (c); 908.4 (d)	893.4
ABUTMENT 5 PILASTER	16" CIDH	150	70	904.5 (a); 909.5 (b); 920.5 (c); 918.5 (d)	904.5

BENCHMARK		
BENCHMARK	Elev (ft)	DESCRIPTION
AA3356	904.20	FD. NGS BENCHMARK PID "AA3356", DES. "101 007", CALIFORNIA DOT BRASS DISK, AT BRIDGE ABUTMENT OVER CHESEBRO CREEK.

REGISTERED CIVIL ENGINEER DATE _____

JON HERMSTAD
No. 66045
Exp. 06/30/18
CIVIL
STATE OF CALIFORNIA

PLANS APPROVAL DATE _____

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30001 LADYFACE COURT
AGOURA HILLS, CA 91301

PARSONS
2201 DUPONT DRIVE, SUITE 200
IRVINE, CA 92612

- NOTES:
- Design tip elevations for Bents and Abutments are controlled by: (a) Compression, (b) Tension, (c) Settlement, (d) Lateral Load.
 - The CIDH Specified Tip Elevation shall not be raised.

LEGEND:

- XXX.XX Indicates Bottom of Exist Footing Elevation
- XXX.XX Indicates Bottom of Footing Elevation
- Indicates Exist Structure
- Indicates Exist Conc Pile
- Indicates New 16" CIDH Conc Pile at Abutments
- Indicates New 24" CIDH Conc Pile at Bents

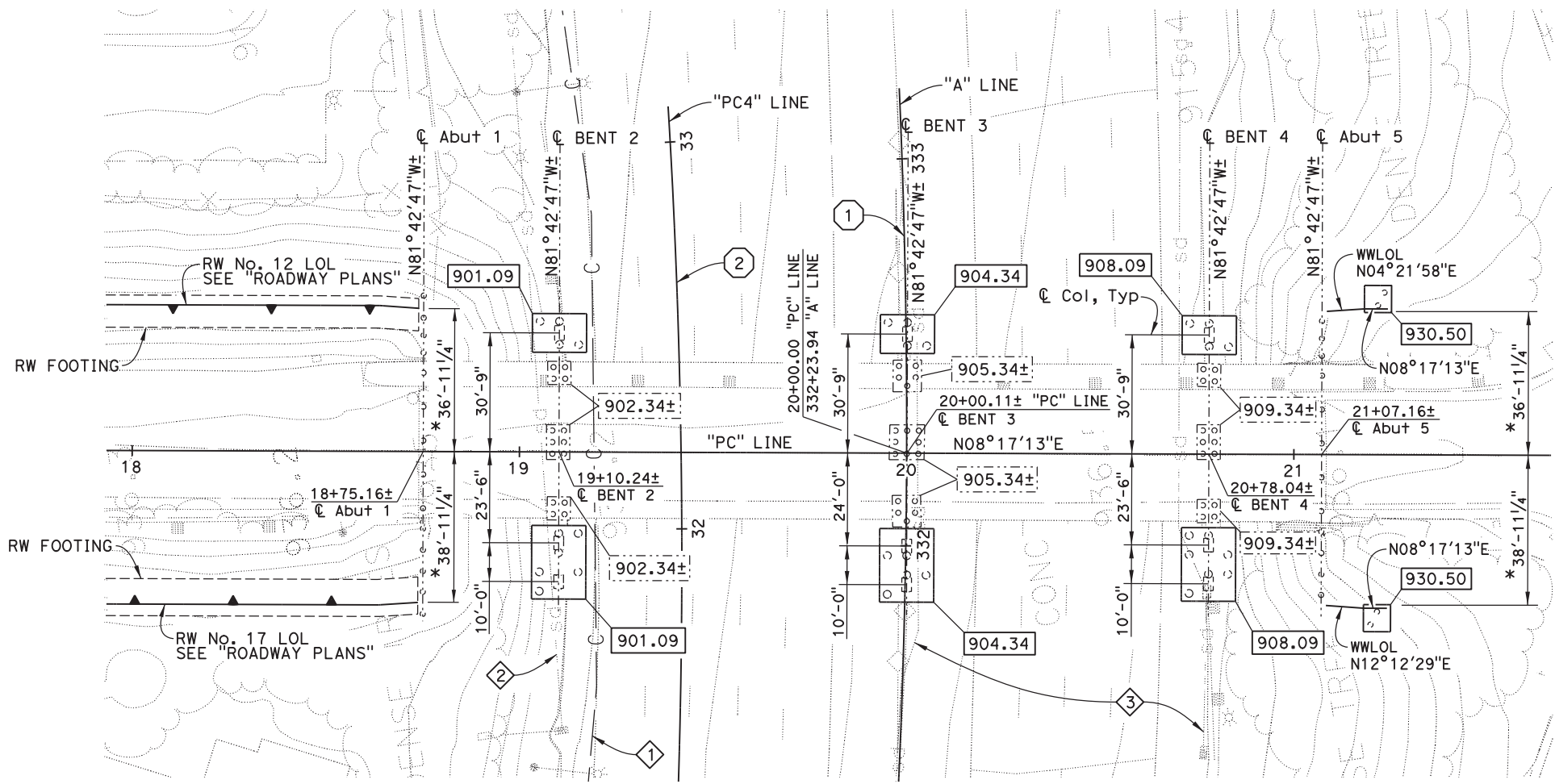
NOTES:

- All piles not shown.
- Existing structure foundation locations are approximate.
- Contours shown represent existing ground.
- The types and locations of all utilities are provided for information only. The Contractor shall verify all existing utilities and notify utility agencies prior to any removal, relocation or new construction. See "ROADWAY PLANS" for Utility Details not shown.

UTILITIES:

- ① Exist Caltrans 4" Fiber Optic Cable to be relocated, see "ROADWAY PLANS"
- ② Exist 24" Storm Drain to be relocated, see "ROADWAY PLANS"
- ③ Exist 18" Storm Drain to be relocated, see "ROADWAY PLANS"

CURVE DATA ①	CURVE DATA ②
R = 1999.95'	R = 1920.11'
Δ = 40°19'10"	Δ = 08°56'23"
T = 734.24'	T = 150.10'
L = 1407.38'	L = 299.59'



PLAN
1" = 20'

* MEASURED TO THE INTERSECTION OF WWLOR OR RW LOL WITH C Abut

NOTE:
The contractor shall verify all controlling field dimensions before ordering or fabricating any material.

GEO-TECHNICAL PROFESSIONAL APPROVAL DATE

100% INTERMEDIATE PS&E - SEPTEMBER 2017 (NOT FOR CONSTRUCTION) TIME PLOTTED => 10:34

DESIGN OVERSIGHT	SCALE: X	VERT. DATUM X	HORZ. DATUM X	DESIGN BY D. LaFranchi	CHECKED E. Ieong/G. Douglass	BRIDGE NO. 53-1678	PALO COMADO CANYON RD OC (WIDEN)	
SIGN OFF DATE	PHOTOGRAMMETRY AS OF: X	ALIGNMENT TIES X	QUANTITIES BY D. LaFranchi	DETAILS BY F. Hakemi	CHECKED E. Ieong	PROJECT MILES 33.69		FOUNDATION PLAN
FOUNDATION PLAN SHEET (ENGLISH) (REV. 03/14/12)	FIELD CHECKED BY X	CHECKED BY X	ORIGINAL SCALE IN INCHES FOR REDUCED PLANS	PROJECT NUMBER & PHASE: 0700001841	CHECKED E. Ieong	CONTRACT NO.: 07-257200		
				UNIT: 1821		DISREGARD PRINTS BEARING EARLIER REVISION DATES		
				FILE => 53-1628-e-fdp101.dgn		REVISION DATES: 09/24/14, 09/27/14, 06/26/17, 09/01/17		
						SHEET 4 OF 32		

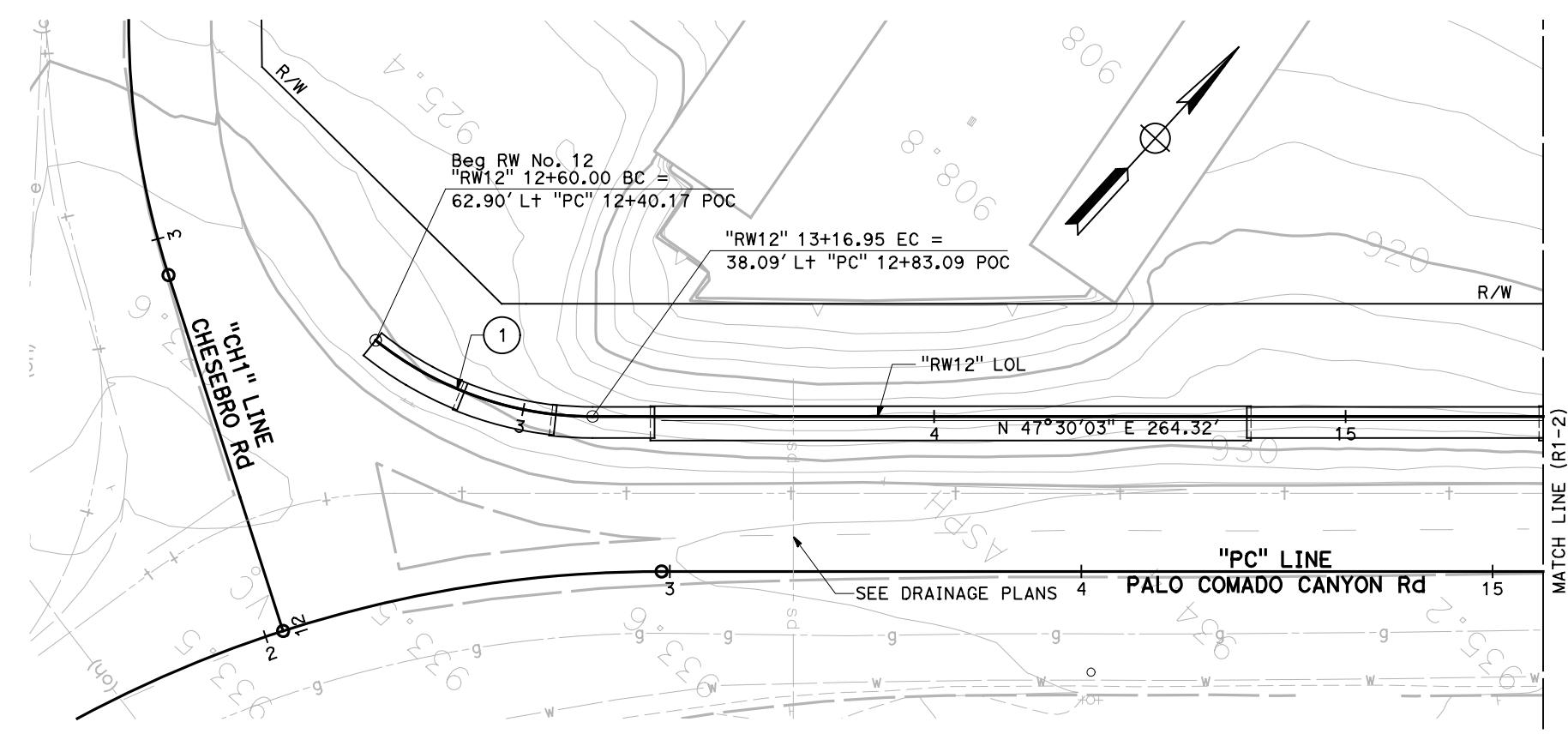
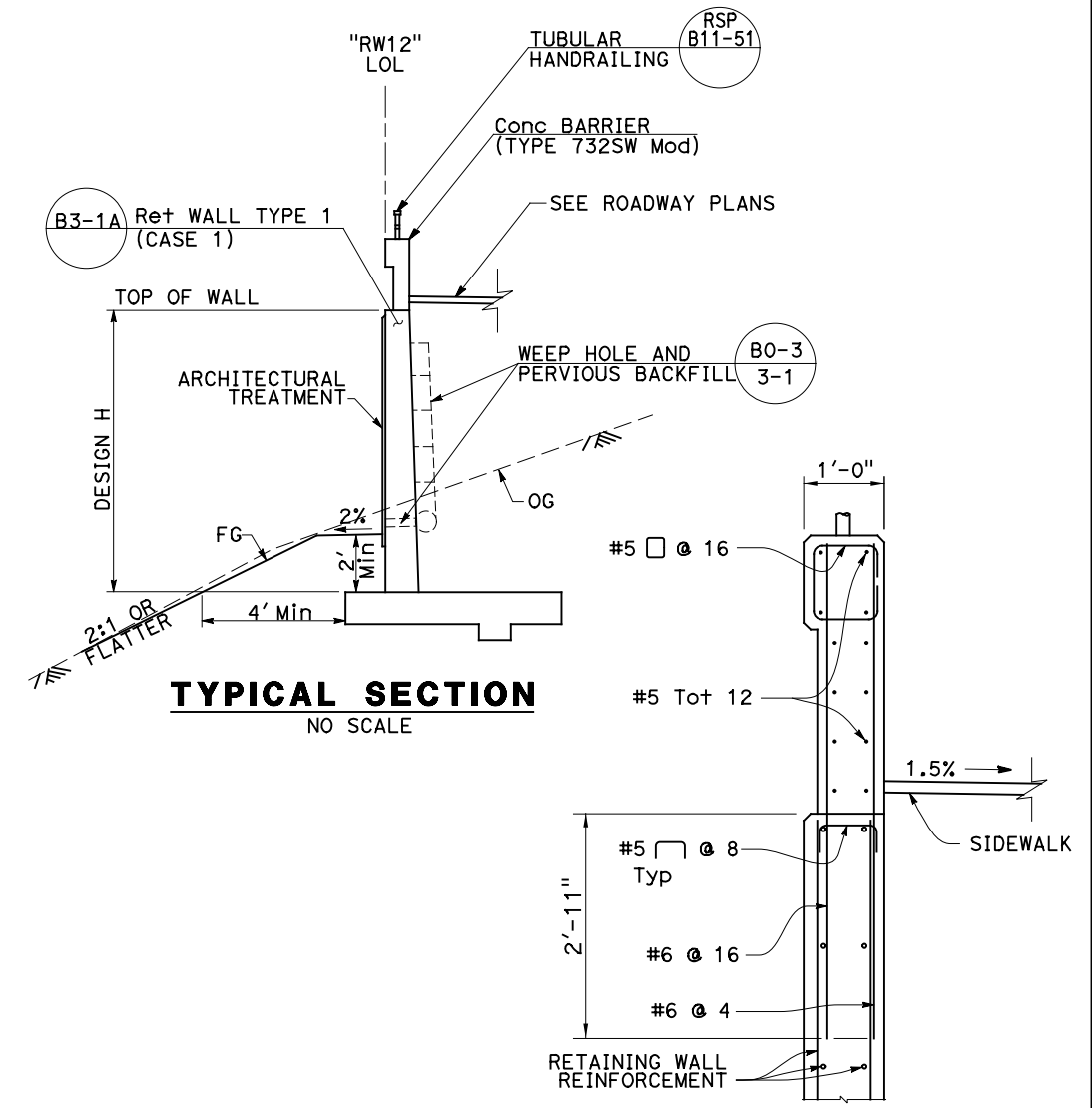
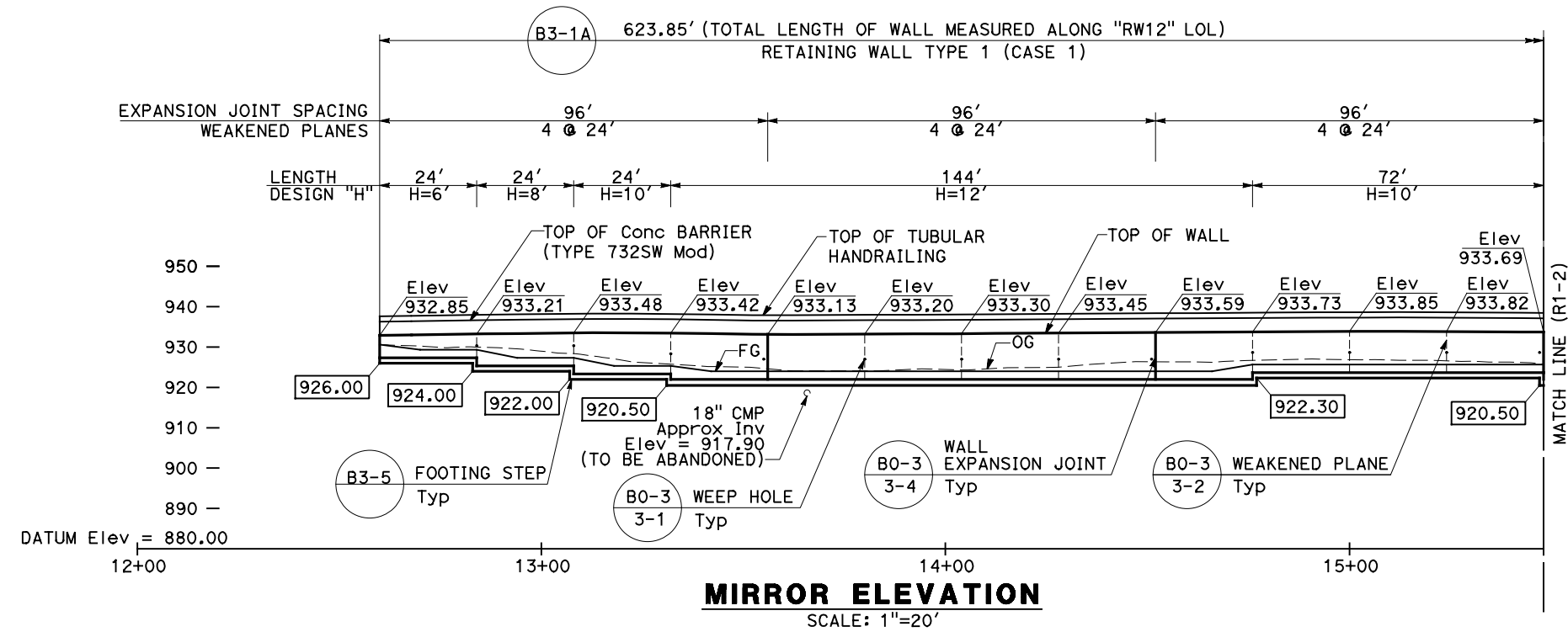
DIST	COUNTY	ROUTE	POST MILES TOTAL PROJECT	SHEET No.	TOTAL SHEETS
07	LA	101	33.5/33.9		

100% SUBMITTAL
NOT FOR CONSTRUCTION
SEPTEMBER 2017

PARSONS 2201 DUPONT DR, STE 200 IRVINE, CA 92612	CITY OF AGOURA HILLS 30001 LADYFACE COURT AGOURA HILLS, CA 91301
--	--

NOTES:

- FOR ACCURATE RIGHT OF WAY DATA, CONTACT RIGHT OF WAY ENGINEERING AT THE DISTRICT OFFICE.
- CONTRACTOR SHALL VERIFY LOCATIONS AND DEPTHS OF ALL UTILITIES PRIOR TO CONSTRUCTION OF THE WALL.



CURVE DATA				
No.	R	Δ	T	L
①	84.33'	38°41'38"	29.61'	56.95'

732SW Mod
NO SCALE

NOTE: FOR DIMENSIONS AND Reinf NOT SHOWN SEE REVISED Std PLAN B11-59

Figure 4A
RETAINING WALL PLAN
RETAINING WALL No. 12
 SCALE AS SHOWN

R1-1

STATE OF CALIFORNIA - DEPARTMENT OF TRANSPORTATION
 CONSULTANT: FUNCTIONAL SUPERVISOR: MARK FIRGER
 DESIGNED BY: KEVIN CASTRO
 CHECKED BY: TOMO TAKAHASHI
 REVISIONS: REVISED BY: DATE

LAST REVISION: DATE PLOTTED => 6/16/2017
 00-00-00 TIME PLOTTED => 4:57:35 PM

DIST	COUNTY	ROUTE	POST MILES TOTAL PROJECT	SHEET No.	TOTAL SHEETS
07	LA	101	33.5/33.9		

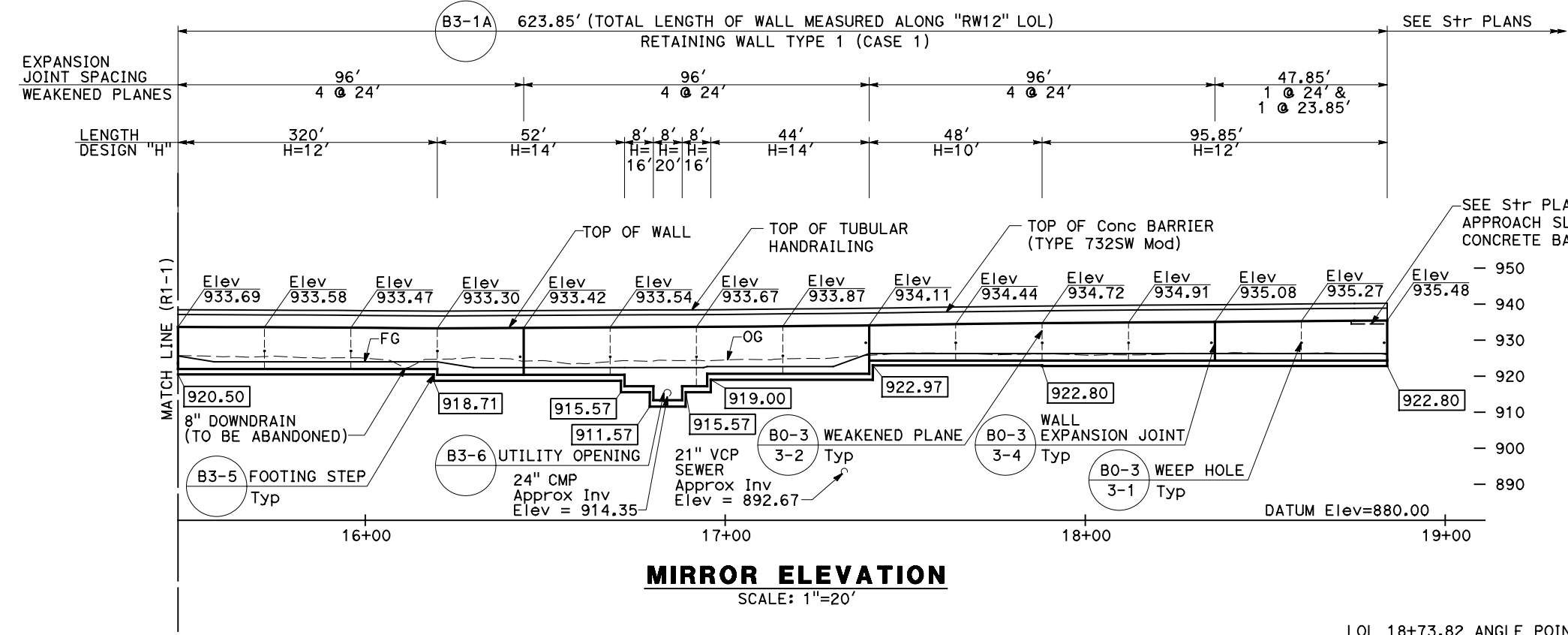
100% SUBMITTAL
NOT FOR CONSTRUCTION
SEPTEMBER 2017

PARSONS
 2201 DUPONT DR, STE 200
 IRVINE, CA 92612

CITY OF AGOURA HILLS
 30001 LADYFACE COURT
 AGOURA HILLS, CA 91301

NOTES:

- FOR ACCURATE RIGHT OF WAY DATA, CONTACT RIGHT OF WAY ENGINEERING AT THE DISTRICT OFFICE.
- CONTRACTOR SHALL VERIFY LOCATIONS AND DEPTHS OF ALL UTILITIES PRIOR TO CONSTRUCTION OF THE WALL.



SUMMARY OF QUANTITIES

ITEM	UNIT	QUANTITY
STRUCTURE EXCAVATION (RETAINING WALL)	CY	856
STRUCTURE BACKFILL (RETAINING WALL)	CY	1,713
PERVIOUS BACKFILL MATERIAL (RETAINING WALL)	CY	138
STRUCTURAL CONCRETE (RETAINING WALL)	CY	644
ARCHITECTURAL TREATMENT	SQFT	6,352
BAR REINFORCING STEEL (RETAINING WALL)	LB	84,396
CONCRETE BARRIER (TYPE 732SW Mod)	LF	624
TUBULAR HANDRAILING	LF	624

CURVE DATA

No.	R	Δ	T	L
(2)	312.33'	39°12'50"	111.26'	213.76'

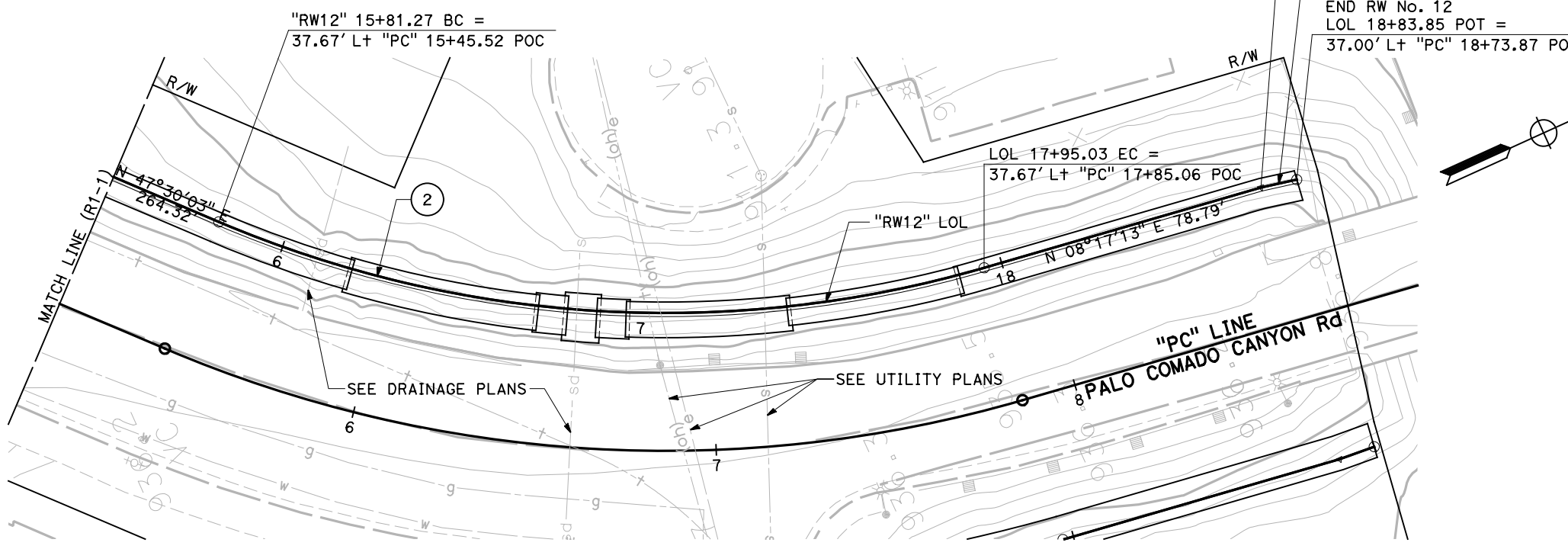


Figure 4B
RETAINING WALL PLAN
RETAINING WALL No. 12
 SCALE AS SHOWN

THIS PLAN ACCURATE FOR RETAINING WALL WORK ONLY.

STATE OF CALIFORNIA - DEPARTMENT OF TRANSPORTATION

REVISOR: KEVIN CASTRO, TOMO TAKAHASHI, MARK FIRGER

DATE: 7/2/2010

LAST REVISION DATE PLOTTED => 6/16/2017
 00-00-00 TIME PLOTTED => 4:57:39 PM

DIST	COUNTY	ROUTE	POST MILES TOTAL PROJECT	SHEET No.	TOTAL SHEETS
07	LA	101	33.5/33.9		

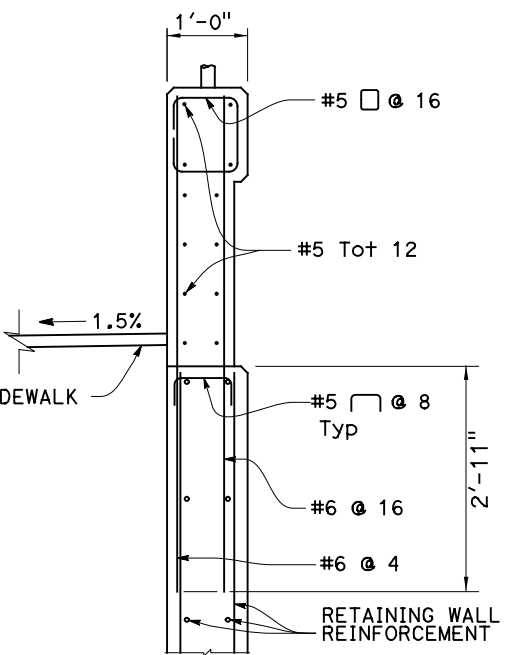
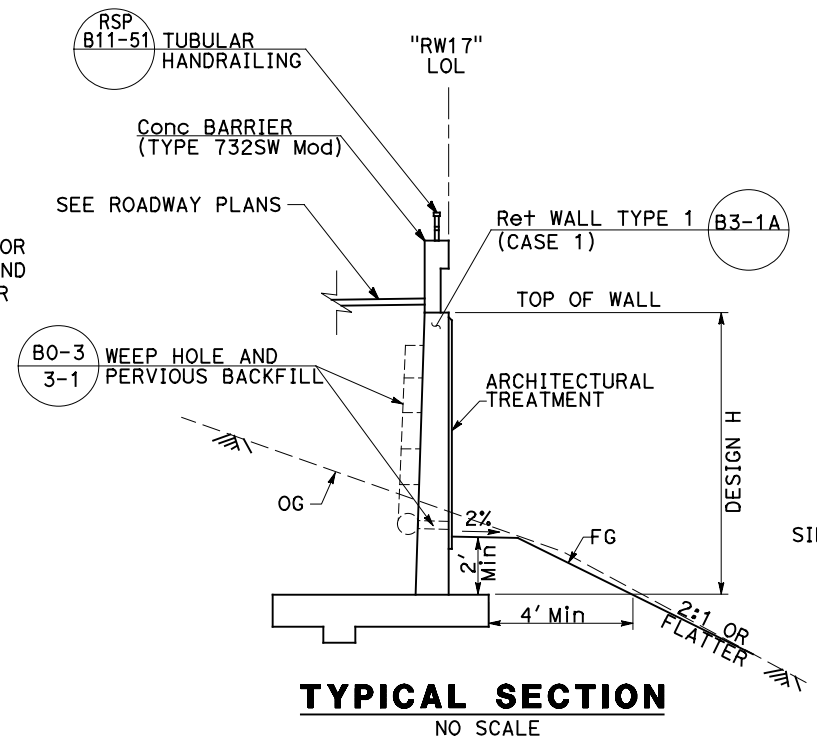
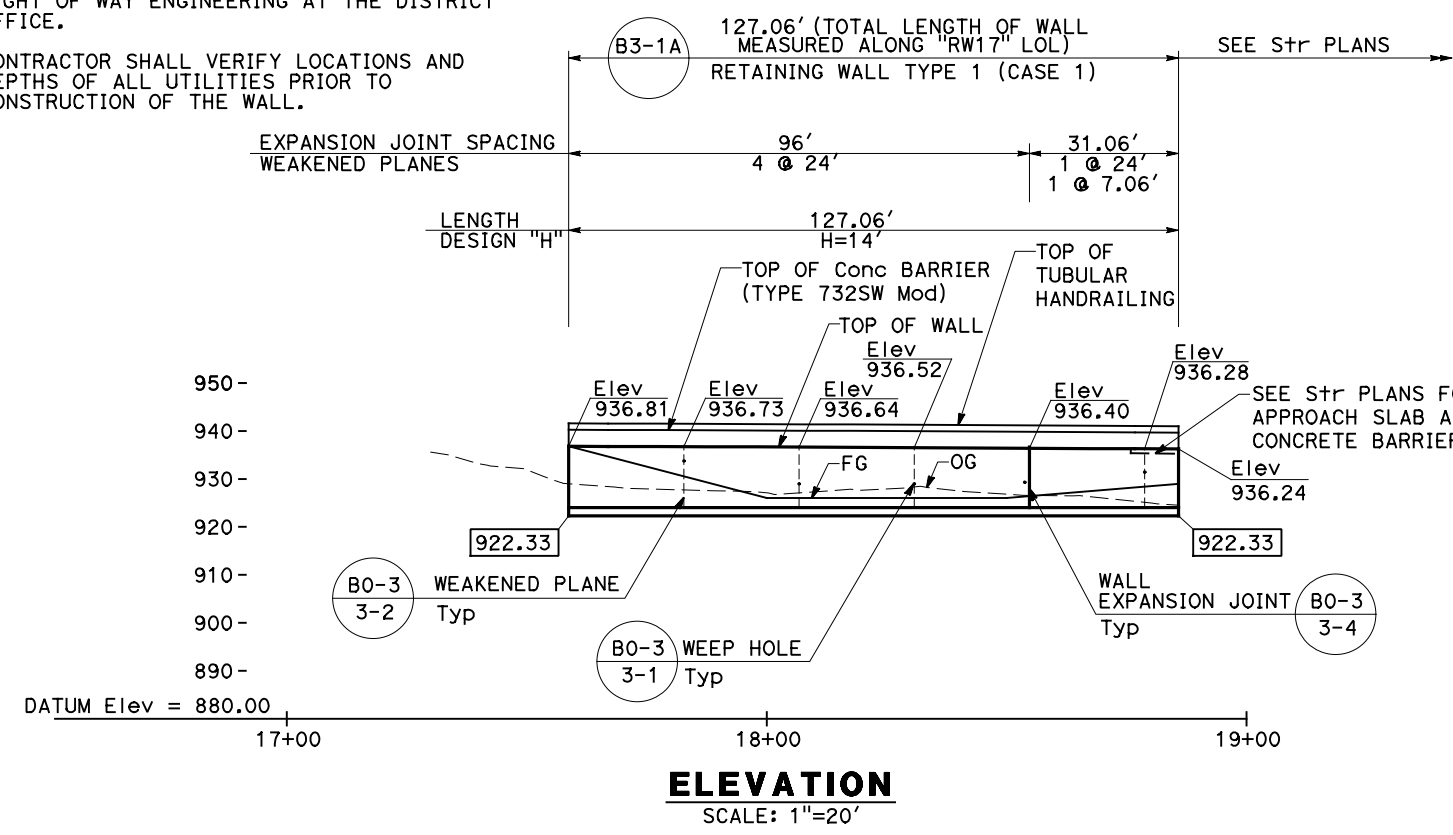
100% SUBMITTAL
NOT FOR CONSTRUCTION
SEPTEMBER 2017

PARSONS
2201 DUPONT DR, STE 200
IRVINE, CA 92612

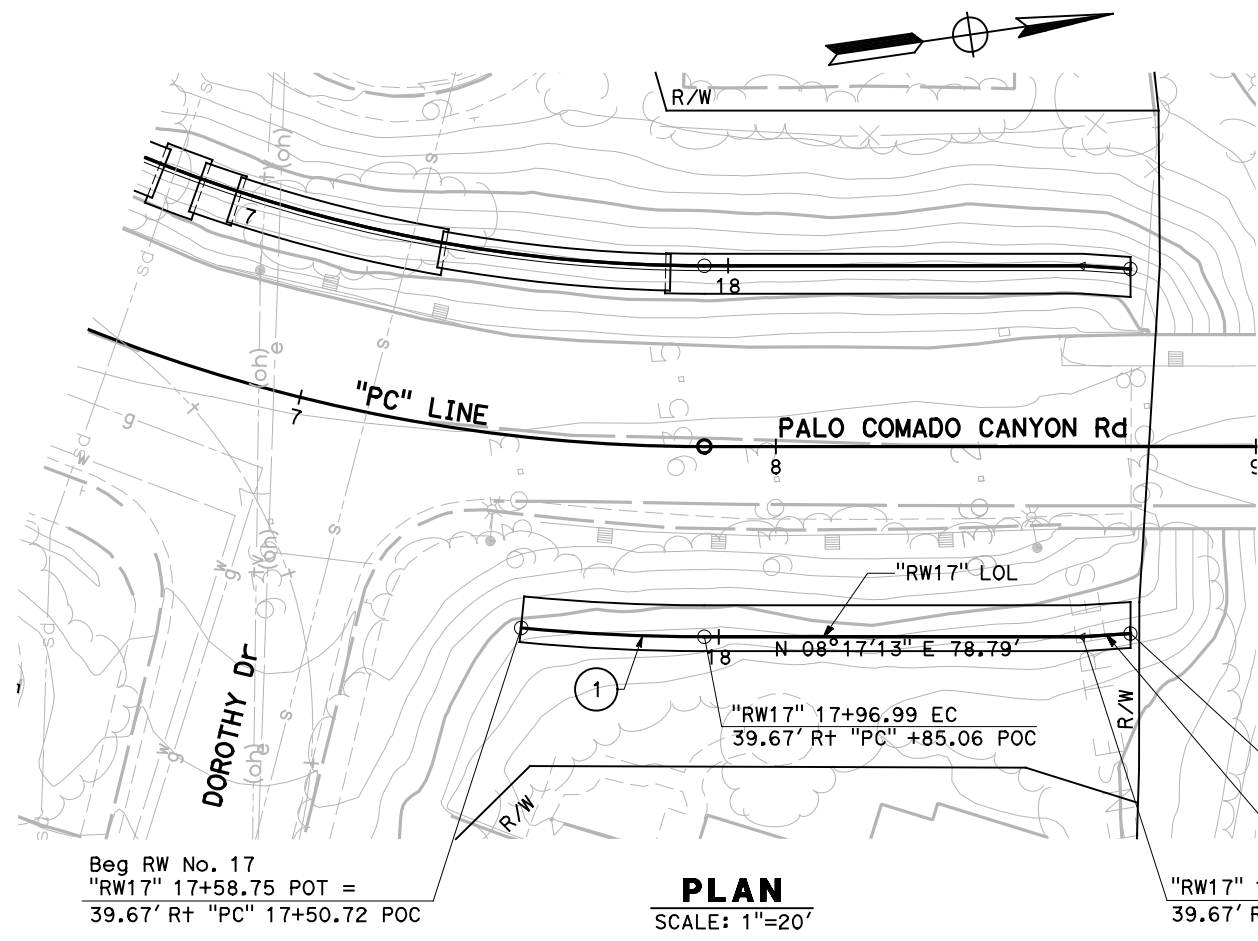
CITY OF AGOURA HILLS
30001 LADYFACE COURT
AGOURA HILLS, CA 91301

NOTES:

- FOR ACCURATE RIGHT OF WAY DATA, CONTACT RIGHT OF WAY ENGINEERING AT THE DISTRICT OFFICE.
- CONTRACTOR SHALL VERIFY LOCATIONS AND DEPTHS OF ALL UTILITIES PRIOR TO CONSTRUCTION OF THE WALL.



732SW Mod NOTE: FOR DIMENSIONS AND Reinf NOT SHOWN SEE REVISED Std PLAN B11-59
NO SCALE



No.	R	Δ	T	L
①	389.67'	05°37'22"	19.14'	38.24'

SUMMARY OF QUANTITIES

ITEM	UNIT	QUANTITY
STRUCTURE EXCAVATION (RETAINING WALL)	CY	215
STRUCTURE BACKFILL (RETAINING WALL)	CY	430
PERVIOUS BACKFILL MATERIAL (RETAINING WALL)	CY	34
STRUCTURAL CONCRETE (RETAINING WALL)	CY	157
ARCHITECTURAL TREATMENT	SQFT	1,597
BAR REINFORCING STEEL (RETAINING WALL)	LB	22,568
CONCRETE BARRIER (TYPE 732SW Mod)	LF	128
TUBULAR HANDRAILING	LF	128

Figure 4C
RETAINING WALL PLAN
RETAINING WALL No. 17
SCALE AS SHOWN

R2-1

STATE OF CALIFORNIA - DEPARTMENT OF TRANSPORTATION
Caltrans
CONSULTANT: FUNCTIONAL SUPERVISOR: MARK FIRGER
DESIGNED BY: KEVIN CASTRO
CHECKED BY: TOMO TAKAHASHI
REVISOR: KEVIN CASTRO
DATE: KEVIN CASTRO

USERNAME => P005248C
DGN FILE => 070000184qb001.dgn

RELATIVE BORDER SCALE IS IN INCHES

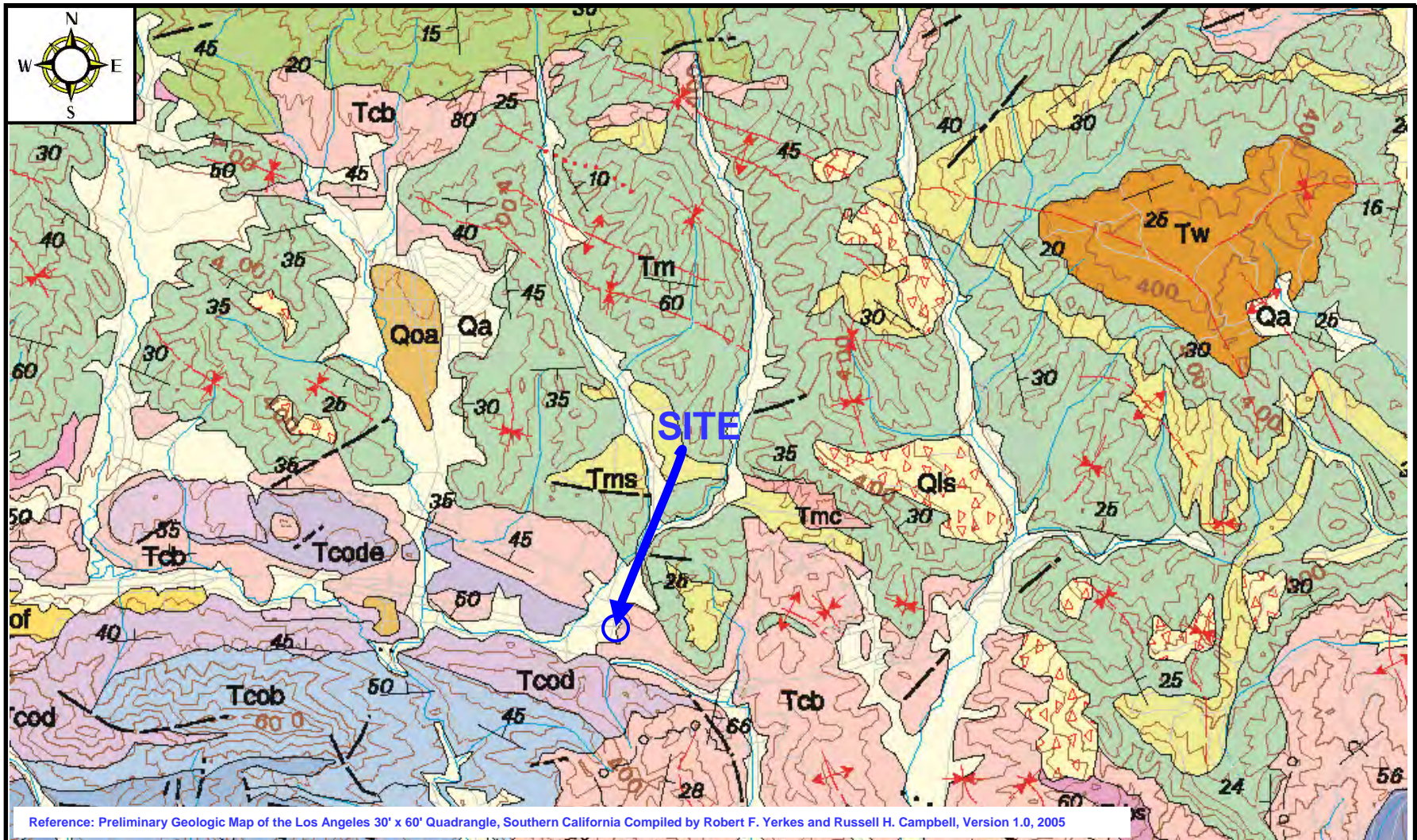
UNIT 1821

PROJECT NUMBER & PHASE

0700001841

THIS PLAN ACCURATE FOR RETAINING WALL WORK ONLY.

LAST REVISION: DATE PLOTTED => 6/16/2017
TIME PLOTTED => 4:57:44 PM



LEGEND

- Qa = Young (Holocene) Alluvium
- Qls = Landslide Debris (Holocene)
- Tm = Modelo Formation, undivided (late Miocene)
- Tms = Modelo Formation, sandstone (late Miocene)
- Tmc = Mint Canyon Formation, undivided (late and middle Miocene)
- Tcb = Calabasas Formation, undivided (early late Miocene and late middle Miocene)
- Tco, Tcob, Tcod = Conejo Volcanics, undivided (middle middle Miocene), basaltic lower zone, dacite-bearing upper zone
- Tw = Towsley Formation, undivided (early Pliocene and late Miocene)



GDC Project No. LA-1143

Palo Comado Canyon Rd OC (Widen)
Agoura Hills, CA

GEOLOGIC MAP

Figure 5

FED. ROAD DIST. NO.	STATE	PROJ. NO.	FISCAL YEAR	SHEET NO.	TOTAL SHEETS
7	CAL.			7	15

BENCH MARK #335-2LAC-5B
 Fd L. ET in middle West edge of D.I. on S. Ver. of Sta 335+02.91
 POT 100' ± E. Chesebro Rd. pointed "TR 197"
 ELEV. 907.95

5 = NO. OF PILES IN FOOTING OF ABUTMENT NO. 1
 ACTUAL LENGTH OF PILES:
 AV. 38.0 MAX. 38.0 MIN. 38.0
 PILE TIP ELEVATION:
 AV. 886.4 MAX. 886.5 MIN. 886.1
 SPECIFIED TIP ELEV. 888.0

14 = NO. OF PILES IN FOOTING OF BENT NO. 2
 ACTUAL LENGTH OF PILES:
 AV. 16.1 MAX. 17.0 MIN. 15.5
 PILE TIP ELEVATION:
 AV. 883.9 MAX. 884.5 MIN. 883.0
 SPECIFIED TIP ELEV. 885.0

14 = NO. OF PILES IN FOOTING OF BENT NO. 4
 ACTUAL LENGTH OF PILES:
 AV. 20.0 MAX. 20.0 MIN. 20.0
 PILE TIP ELEVATION:
 AV. 887.0 MAX. 887.0 MIN. 887.0
 SPECIFIED TIP ELEVATION 888.0

5 = NO. OF PILES IN FOOTING OF ABUTMENT NO. 5
 ACTUAL LENGTH OF PILES:
 AV. 37.9 MAX. 38.1 MIN. 37.6
 PILE TIP ELEVATION:
 AV. 886.6 MAX. 887.1 MIN. 886.4
 SPECIFIED TIP ELEV. 888.0

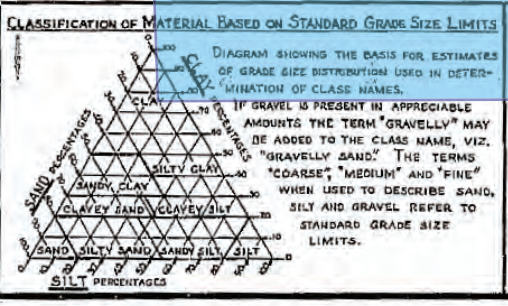
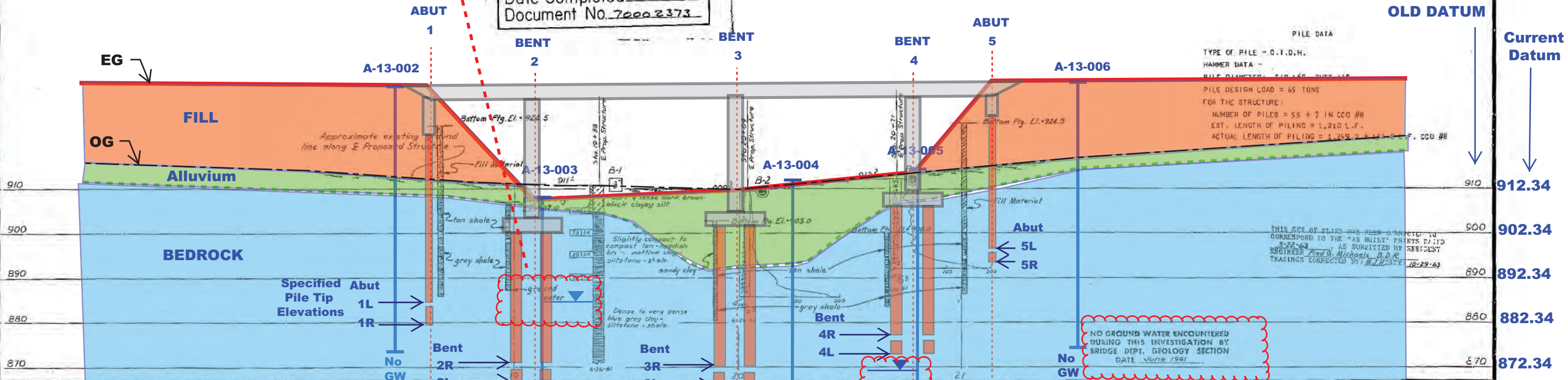
24 = NO. OF PILES IN FOOTING OF BENT NO. 3 (INCLUDING COO #8)
 ACTUAL LENGTH OF PILES:
 AV. 22.0 MAX. 22.0 MIN. 22.0
 PILE TIP ELEVATION:
 AV. 881.0 MAX. 881.0 MIN. 881.0
 SPECIFIED TIP ELEVATION 882.0

Perched groundwater found at Bent 2 on a production pile during original construction and in Group Delta borings A-13-003 and A-13-005, no water reported anywhere else.

AS BUILT PLANS
 Contract No. 63-7V13C58
 Date Completed _____
 Document No. 70002373

ELEVATIONS BASED ON OLD DATUM

Current Datum



LEGEND OF EARTH MATERIALS

GRAVEL	SILTY CLAY OR CLAYEY SILT
SAND	PEAT AND/OR ORGANIC MATTER
SILT	FILL MATERIAL
CLAY	IGNEOUS ROCK
SANDY CLAY OR CLAYEY SAND	SEDIMENTARY ROCK
SANDY SILT OR SILTY SAND	METAMORPHIC ROCK

LEGEND OF BORING OPERATIONS

PENETROMETER	2 1/4" CONE PENETROMETER
SAMPLER BORING (DRY)	ROTARY BORING (WET)
AUGER BORING (DRY)	JET BORING
CORE BORING	TEST PIT

NOTES

The contractor's attention is directed to Section 2, Article (c) of the Standard Specifications and to the Special Provisions accompanying this set of plans.

Classification of earth material as shown on this sheet is based upon field inspection and is not to be construed to imply mechanical analysis.

STATE OF CALIFORNIA
 DEPARTMENT OF PUBLIC WORKS
 DIVISION OF HIGHWAYS

CHESEBRO RD. OVERCROSSING

LOG OF TEST BORINGS

SCALE: Horiz: 1"=40' Vert: 1"=70' BRIDGE 53-1678 FILE DRAWING C-531678-15

Figure 6 - GEOTECHNICAL CROSS SECTION



FAULT NAME	Fault Type	FAULT RUPTURE DISTANCE to SITE, Rrup (km)	MAGNITUDE Mw	PBA (g)
Anacapa-Dume alt1 (FID No. 348)	Reverse	13.0	7.2	0.432
Santa Monica Fault (FID No. 341)	Strike-Slip	14.2	7.0	0.257
Malibu Coast alt 2 (FID No. 346)	Strike-Slip	11.8	6.6	0.267
Oak Ridge Onshore (FID No. 291)	Reverse	25.5	7.4	0.234
Chatsworth fault (FID No. 308)	Reverse	10.3	6.4	0.253
Simi-Santa Rosa fault zone Simi-Santa Rosa Section (FID No. 300)	Strike-Slip	15.7	6.8	0.205
Simi-Santa Rosa fault zone Camarillo-Santa Rosa section (FID No. 314)	Strike-Slip	17.7	6.8	0.182
Sierra Madre fault zone Santa Susana section (FID No. 298)	Reverse	22.6	6.8	0.155
San Cayetano (FID No. 276)	Reverse	30.3	7.2	0.142
Newport Inglewood fault zone N. Los Angeles Basin section (FID No. 342)	Strike-Slip	31.2	7.2	0.131

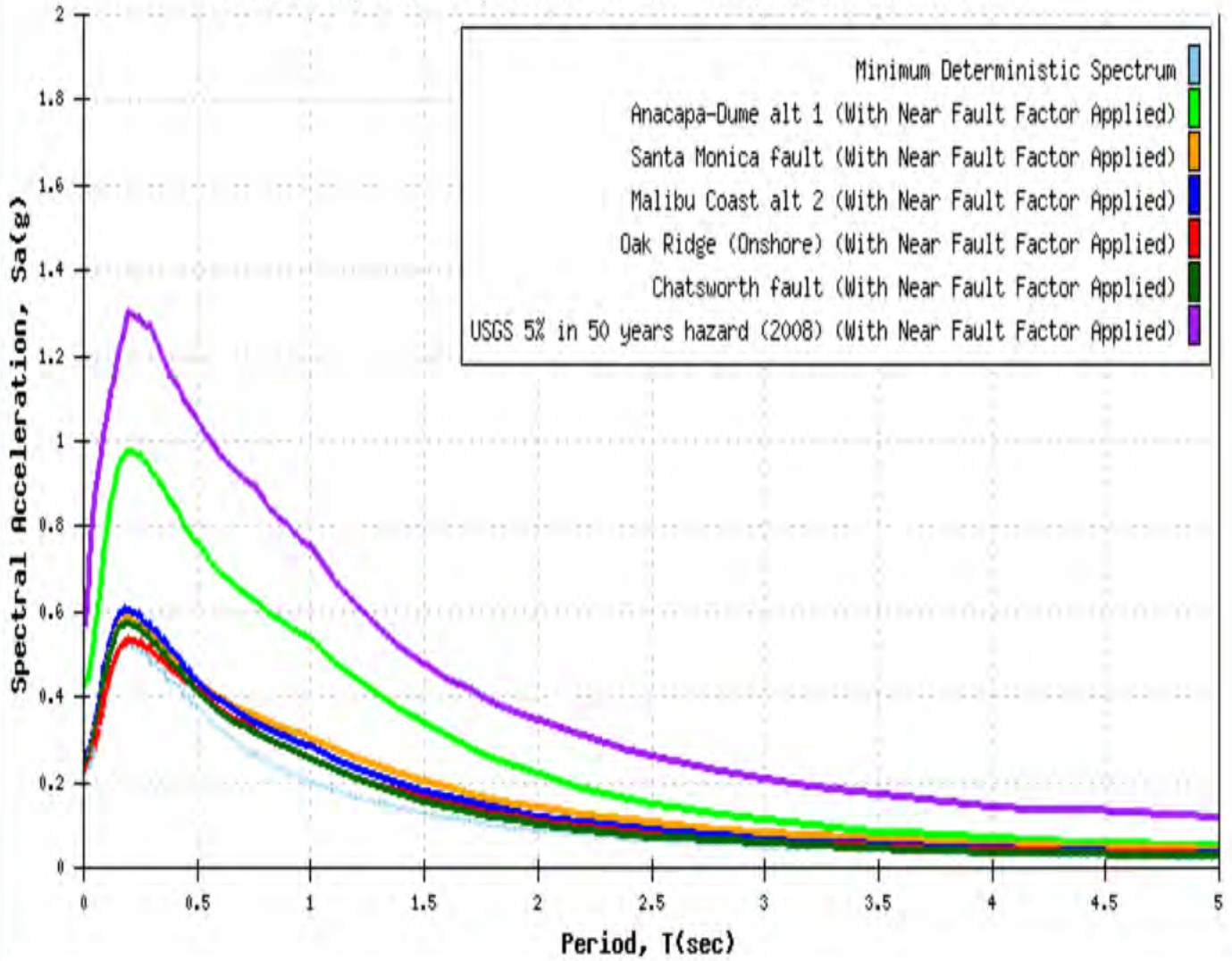
Reference: Caltrans ARS Online



GDC Project No. LA-1143
 Palo Comado Canyon Road OC (Widen)
 Agoura Hills, California
CALTRANS FAULT MAP

Figure 7

Location: LAT=34.143300 LONG=-118.7379 Vs30=360m/s



Period	SA
0.01	0.567
0.05	0.872
0.1	1.049
0.15	1.192
0.2	1.305
0.25	1.282
0.3	1.263
0.4	1.137
0.5	1.048
0.6	0.972
0.7	0.917
0.85	0.828
1	0.752
1.2	0.614
1.5	0.479
2	0.348
3	0.209
4	0.147
5	0.121

Reference: Caltrans ARS Online

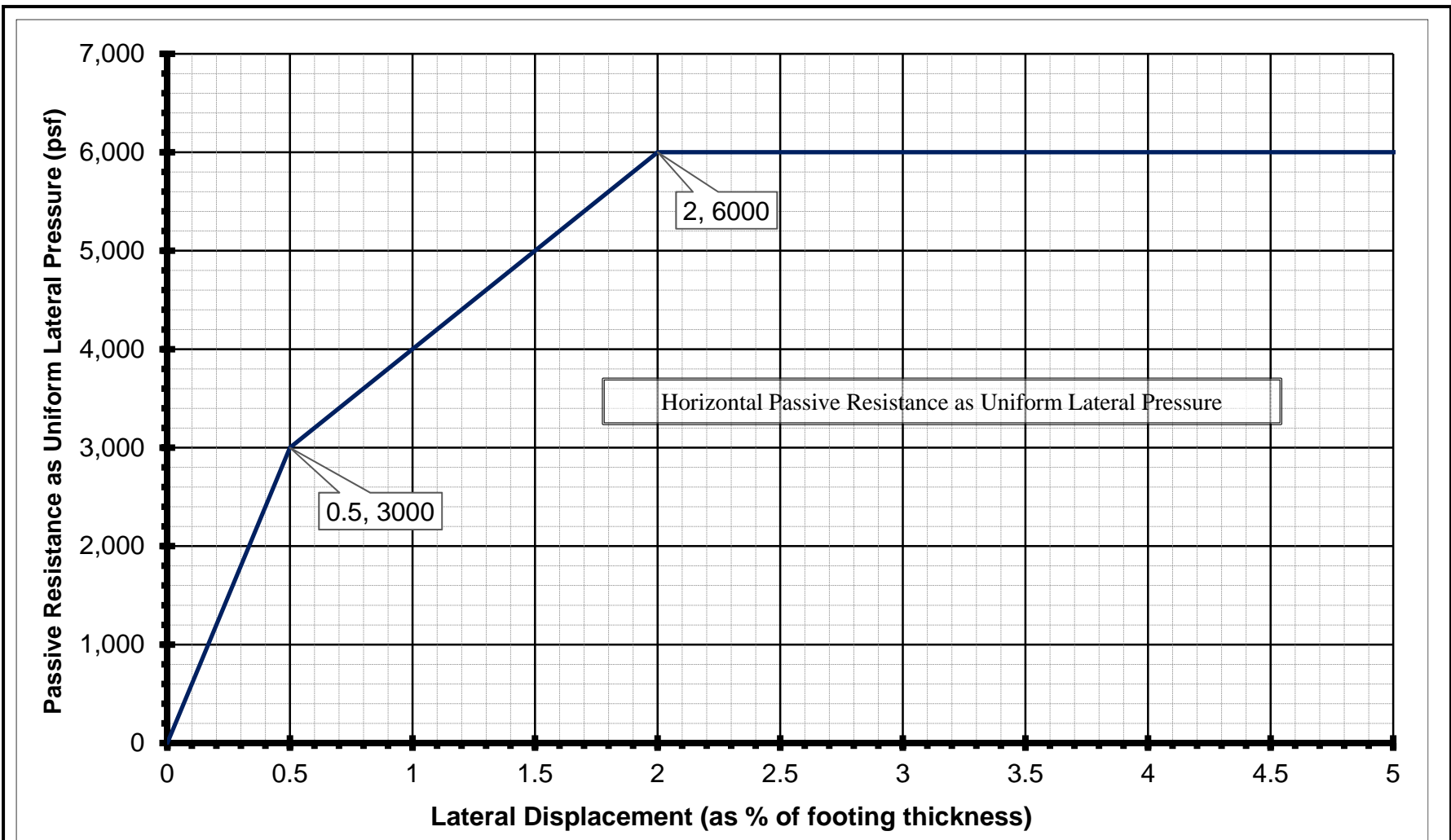


GDC Project No. LA-1143

Palo Comado Canyon Road OC (Widen)
Agoura Hills, California

RECOMMENDED ARS CURVE

Figure 8



GDC Project No. LA-1143

Palo Comado Canyon Rd OC (Widen)
Agoura Hills, CA

PASSIVE RESISTANCE OF PILE CAP

Figure 9

Appendix A Field Investigation

APPENDIX A FIELD INVESTIGATION

A.1 Introduction

The subsurface conditions at the PALO COMADO CANYON RD. (WIDEN) project site were investigated by performing six hollow stem auger borings and one hand auger boring on September 9, 12, and 13, 2013. The locations of the explorations are presented in the exploration plan of the main report. A summary of field explorations is presented in Table A-1.

Prior to beginning the exploration program, access permission and drilling permits were obtained as necessary. Subsurface utility maps were reviewed prior to selecting locations for subsurface investigations. Underground Service Alert (USA) was notified and each exploration location was cleared for underground utilities. Approved traffic control plans were implemented where necessary during field activities. The exploration methods are described in the following sections.

A.2 Soil Drilling and Sampling

Drilling, Logging, and Soil / Rock Classification

Borings were performed by GDC's drilling subcontractors Choice Drilling Inc. under the continuous technical supervision of a GDC field engineer geologist, who visually inspected the soil samples, measured groundwater levels, maintained detailed records of the borings, and visually / manually classified the soils in accordance with the ASTM D 2488 and the Unified Soil Classification System (USCS). Logging and classification was performed in general accordance with Caltrans "Soil and Rock Logging, Classification, and Presentation Manual (2010 Edition)". A Boring Record Legend and Key for Soil Classification are presented in Figures A-1a through A-1f. The boring records are presented in Figures A-2a through A-8a.

Sampling

Bulk samples of soil cuttings were collected at selected depths and drive samples were collected from the borings typically at 2.5 feet for the first ten feet of exploration, and at a typical interval of 5 feet from depth of ten feet to the end of the borehole. The sampling was performed using Standard Penetration Test (SPT) samplers in accordance with ASTM D 1586 and Ring-Lined "California" Split Barrel samplers in accordance with ASTM D 3550.

Bulk samples were collected from the hand auger boring and hollow-stem auger cuttings and placed in plastic bags.

SPT drive samples were obtained using a 2-inch outside diameter and 1.375-inch inside diameter split-spoon sampler without lining. The soil recovered from the SPT sampling was sealed in plastic bags to preserve the natural moisture content.

California drive samples were collected with a 3-inch outside diameter 2.5-inch inside diameter split barrel sampler with a 2.42-inch inside diameter cutting shoe. The sampler barrel is lined with 18-inches of metal rings for sample collection and has an additional length of waste barrel. Stainless steel or brass liner rings for sample collection are 1-inch high, 2.42-inch inside diameter, and 2.5-inch outside diameter. California samples were removed from the sampler, retained in the metal rings and placed in sealed plastic canisters to prevent loss of moisture.

At each sampling interval, the drive samplers were fitted onto sampling rod, lowered to the bottom of the boring, and driven 18 inches or to refusal (50 blows per 6 inches) with a 140-lb hammer free-falling a height of 30-inches using an automatic hammer. Compared to the SPT, the California sampler provides less disturbed samples.

Penetration Resistance

SPT blow counts adjusted to 60% hammer efficiency (N_{60}) are routinely used as an index of the relative density of coarse grained soils, and are sometimes used (but less reliable) to estimate consistency of cohesive soils. For samples collected using non-SPT samplers, different hammer weight and drop height, and/or efficiency different than 60%, correction factors can be applied to estimate the equivalent SPT N_{60} value following the approach of Burmister (1948) as follows:

$$N_{60}^* = N_R * C_E * C_H * C_S$$

where

N_{60}^* = equivalent SPT N_{60}

N_R = Raw Field Blowcount (blows per foot)

C_E = Hammer Efficiency Correction = $E_r / 60\%$

C_H = Hammer Energy Correction = $(W * H) / (140 \text{ lb} * 30 \text{ in})$

C_S = Sampler Size Correction = $[(2.0 \text{ in})^2 - (1.375 \text{ in})^2] / [D_o^2 - D_i^2]$

E_r = hammer efficiency, %

W = actual drive hammer weight, lbs

H = actual drive hammer drop, inch

D_o , D_i = actual sampler outside and inside diameter, respectively, inches

Burmister’s correction assumes that penetration resistance (blowcount) is inversely proportional to the hammer energy. For a hammer other than a 140# hammer with 30” drop the hammer energy correction is equal to the ratio of the theoretical hammer energy (weight times drop) to the theoretical SPT hammer energy, or $C_H = (W * H) / (140 \text{ lb} * 30 \text{ in})$.

Burmister’s correction assumes that penetration resistance (blowcount) is proportional to the annular end area of the drive sampler. For California drive samplers with $D_o=3$ inch and $D_i=2.42$ inch the sampler size correction factor is the ratio of the annular area of an SPT split spoon to that of the California Sampler, or $C_S = [2.0^2 - 1.375^2] / [3^2 - 2.42^2] = 0.67$.

To normalize the field SPT and California blowcounts to a hammer with 60% efficiency, an energy correction factor equal to Hammer Efficiency (%) / 60% was applied to the field blowcounts. Hammer efficiency was determined by Pile Driving Analyzer (PDA) measurement. Hammer efficiency measurements are presented in Figures A-9a through A-9e.

The correction factors applied to obtain N^*_{60} are summarized in the following table:

Hammer Type	Hammer Weight and Drop	C_H	Hammer Efficiency (%)	C_E	Cal Sampler Dimensions	C_S	Combined Correction Factor SPT Samples	Combined Correction Factor CAL Samples
CME Auto	140# 30”	1	85	1.42	$D_o=3.0$ ” $D_i=2.42$ ”	0.67	1.42	0.95

Corrected N^*_{60} are generally used, with due engineering judgment, only for qualitative assessment of in place density or consistency, and are not used for other more critical analyses such as liquefaction.

Relative Density and Consistency

Equivalent SPT N_{60} values were used as the basis for classifying relative density of granular/cohesionless soils. The correlations for consistency and relative density are shown in the Boring Record Legend, Figures A-1a through A-1d. Drive sample field blow counts, SPT

N^*_{60} values, pocket penetrometer readings, and corresponding density/consistency classifications are presented on the boring records.

Relative Density and Consistency

Equivalent SPT N_{60} values were used as the basis for classifying relative density of granular/cohesionless soils. Wherever possible consistency classification of cohesive soils was based on undrained shear strength estimated in the field with a pocket penetrometer and/or Torvane or by testing in the laboratory. The correlations for consistency and relative density are shown in the Boring Record Legend, Figures A-1a through A-1d. Drive sample field blow counts, SPT N^*_{60} values, and corresponding density/consistency classifications are presented on the boring records.

Borehole Abandonment

At the completion of the drilling groundwater was measured (where possible) and the borings were abandoned by backfilling the borehole with drill cuttings. The surface was patched with cold mix asphalt concrete or quickset concrete, as necessary.

Sample Handling and Transport

Geotechnical samples were sealed to prevent moisture loss, packed in appropriate protective containers, and transported to the geotechnical laboratory for further examination and geotechnical testing.

Laboratory Testing

The soils were further examined and tested in the laboratory and classified in accordance with the Unified Soil Classification System following ASTM D 2487 and D 2488 (see Figures A-1e and A-1f). Field classifications presented on the records were modified where necessary on the basis of the laboratory test results. Descriptions of the laboratory tests performed and a summary of the results are presented in Appendix B.

Hand Auger Boring

Choice Drilling Inc. performed one hand-auger Boring A-13-007 at depth of 5 feet. The test data is presented in Figure A-8

A.3 List of Attached Tables and Figures

The following tables and figures are attached and complete this appendix:

List of Tables

Table A-1 Summary of Field Explorations

List of Figures

Figures A-1a through A-1d Boring Record Legend
 Figures A-1e and A-1f Key for Soil Classification
 Figures A-2a through A-8 Boring Records
 Figures A-9a through A-9e Hammer Efficiency Calibrations

**TABLE A-1
 SUMMARY OF FIELD EXPLORATIONS**

Exploration No.	Approximate Exploration Location		Date	Exploration			Groundwater		Figure No.
	Station	Offset (ft)		Type	Surface Elevation (ft)	Total Depth (ft)	Depth (ft)	Elevation (ft)	
A-13-001	16 + 22	22L	9/09/13	HSA	934	26.5	NE	NE	A-2 (a-b)
A-13-002	18 + 72	25L	9/09/13	HSA	936	61	NE	NE	A-3 (a-c)
A-13-003	19 + 28	20R	9/12/13 – 9/13/13	HSA	910	50.4	23	887	A-4 (a-c)
A-13-004	20 + 22	20R	9/12/13	HSA	914	50.5	NE	NE	A-5 (a-c)
A-13-005	20 + 83	25R	9/12/13	HSA	917	51	45.5	871.5	A-6 (a-c)
A-13-006	21 + 75	17R	9/09/13	HSA	936	60.5	NE	NE	A-7 (a-c)
HA-13-007	25 + 43	14L	9/09/13	Hand Auger	928	5.0	NE	NE	A-8

- Notes:**
- 1) Boring locations are illustrated on the Exploration Location Plan in the main report.
 - 2) Stations referenced to centerline of Palo Comado Road, perpendicular offset Right or Left of center line looking up station.
 - 3) Elevations estimated to nearest 0.5 ft using tape measure and topographic map.

Other notes and abbreviations as needed

HSA = Hollow-Stem Auger MR = Mud Rotary NE = Not Encountered L = Left R = Right



SOIL IDENTIFICATION AND DESCRIPTION SEQUENCE

Sequence	Identification Components	Refer to Section		Required	Optional
		Field	Lab		
1	Group Name	2.5.2	3.2.2	●	
2	Group Symbol	2.5.2	3.2.2	●	
	Description Components				
3	Consistency of Cohesive Soil	2.5.3	3.2.3	●	
4	Apparent Density of Cohesionless Soil	2.5.4		●	
5	Color	2.5.5		●	
6	Moisture	2.5.6		●	
7	Percent or Proportion of Soil	2.5.7	3.2.4	●	○
	Particle Size	2.5.8	2.5.8	●	○
	Particle Angularity	2.5.9			○
	Particle Shape	2.5.10			○
8	Plasticity (for fine-grained soil)	2.5.11	3.2.5		○
9	Dry Strength (for fine-grained soil)	2.5.12			○
10	Dilatency (for fine-grained soil)	2.5.13			○
11	Toughness (for fine-grained soil)	2.5.14			○
12	Structure	2.5.15			○
13	Cementation	2.5.16		●	
14	Percent of Cobbles and Boulders	2.5.17		●	
	Description of Cobbles and Boulders	2.5.18		●	
15	Consistency Field Test Result	2.5.3		●	
16	Additional Comments	2.5.19			○

Describe the soil using descriptive terms in the order shown

Minimum Required Sequence:

USCS Group Name (Group Symbol); Consistency or Density; Color; Moisture; Percent or Proportion of Soil; Particle Size; Plasticity (optional).

○ = optional for non-Caltrans projects

Where applicable:

Cementation; % cobbles & boulders;
Description of cobbles & boulders;
Consistency field test result

REFERENCE: Caltrans Soil and Rock Logging, Classification, and Presentation Manual (2010).



HOLE IDENTIFICATION

Holes are identified using the following convention:

H – YY – NNN

Where:

H: Hole Type Code

YY: 2-digit year

NNN: 3-digit number (001-999)

Hole Type Code and Description

Hole Type Code	Description
A	Auger boring (hollow or solid stem, bucket)
R	Rotary drilled boring (conventional)
RC	Rotary core (self-cased wire-line, continuously-sampled)
RW	Rotary core (self-cased wire-line, not continuously sampled)
P	Rotary percussion boring (Air)
HD	Hand driven (1-inch soil tube)
HA	Hand auger
D	Driven (dynamic cone penetrometer)
CPT	Cone Penetration Test
O	Other (note on LOTB)

Description Sequence Examples:

SANDY lean CLAY (CL); very stiff; yellowish brown; moist; mostly fines; some SAND, from fine to medium; few gravels; medium plasticity; PP=2.75.

Well-graded SAND with SILT and GRAVEL and COBBLES (SW-SM); dense; brown; moist; mostly SAND, from fine to coarse; some fine GRAVEL; few fines; weak cementation; 10% GRANITE COBBLES; 3 to 6 inches; hard; subrounded.

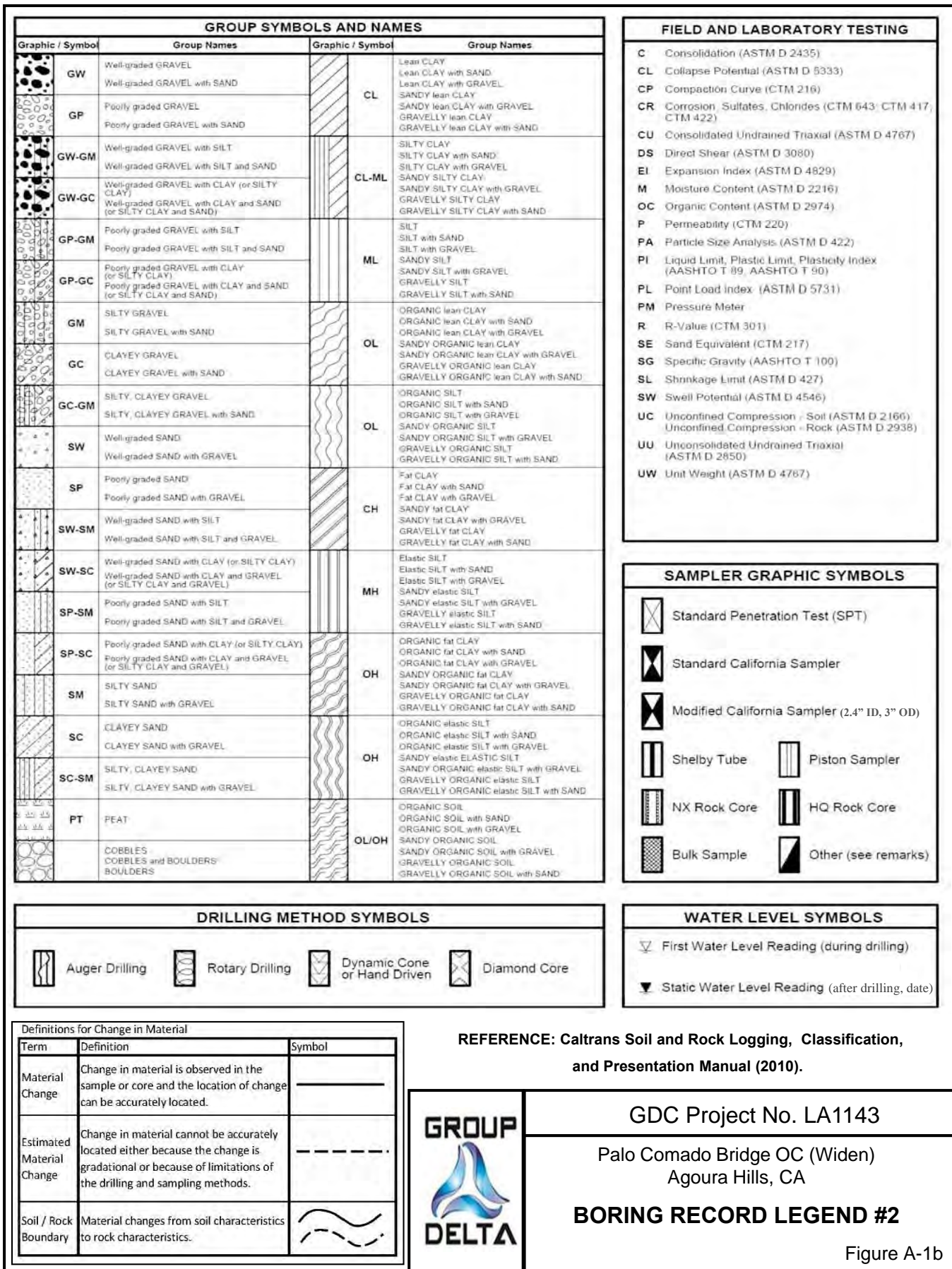
Clayey SAND (SC); medium dense, light brown; wet; mostly fine sand; little fines; low plasticity.

GDC Project No. LA1143

Palo Comado Bridge OC (Widen)
Agoura Hills, CA

BORING RECORD LEGEND #1

Figure A-1a



CONSISTENCY OF COHESIVE SOILS

Description	Shear Strength (tsf)	Pocket Penetrometer, PP Measurement (tsf)	Torvane, TV, Measurement (tsf)	Vane Shear, VS, Measurement (tsf)
Very Soft	Less than 0.12	Less than 0.25	Less than 0.12	Less than 0.12
Soft	0.12 - 0.25	0.25 - 0.5	0.12 - 0.25	0.12 - 0.25
Medium Stiff	0.25 - 0.5	0.5 - 1	0.25 - 0.5	0.25 - 0.5
Stiff	0.5 - 1	1 - 2	0.5 - 1	0.5 - 1
Very Stiff	1 - 2	2 - 4	1 - 2	1 - 2
Hard	Greater than 2	Greater than 4	Greater than 2	Greater than 2

APPARENT DENSITY OF COHESIONLESS SOILS

Description	SPT N_{60} (blows / 12 inches)
Very Loose	0 - 5
Loose	5 - 10
Medium Dense	10 - 30
Dense	30 - 50
Very Dense	Greater than 50

MOISTURE

Description	Criteria
Dry	No discernable moisture
Moist	Moisture present, but no free water
Wet	Visible free water

PERCENT OR PROPORTION OF SOILS

Description	Criteria
Trace	Particles are present but estimated to be less than 5%
Few	5 - 10%
Little	15 - 25%
Some	30 - 45%
Mostly	50 - 100%

PARTICLE SIZE

Description	Size (in)	
Boulder	Greater than 12	
Cobble	3 - 12	
Gravel	Coarse	3/4 - 3
	Fine	1/5 - 3/4
Sand	Coarse	1/16 - 1/5
	Medium	1/64 - 1/16
	Fine	1/300 - 1/64
Silt and Clay	Less than 1/300	

CEMENTATION

Description	Criteria
Weak	Crumbles or breaks with handling or little finger pressure.
Moderate	Crumbles or breaks with considerable finger pressure.
Strong	Will not crumble or break with finger pressure.

Plasticity

Description	Criteria
Nonplastic	A 1/8-in. thread cannot be rolled at any water content.
Low	The thread can barely be rolled and the lump cannot be formed when drier than the plastic limit.
Medium	The thread is easy to roll and not much time is required to reach the plastic limit. The thread cannot be rerolled after reaching the plastic limit. The lump crumbles when drier than the plastic limit.
High	It takes considerable time rolling and kneading to reach the plastic limit. The thread can be rerolled several times after reaching the plastic limit. The lump can be formed without crumbling when drier than the plastic limit.

REFERENCE: Caltrans Soil and Rock Logging, Classification, and Presentation Manual (2010), with the exception of consistency of cohesive soils vs. N_{60} .



GDC Project No. LA1143

Palo Comado Bridge OC (Widen)
Agoura Hills, CA

BORING RECORD LEGEND #3

Figure A-1c

LEGEND OF ROCK MATERIALS		BEDDING SPACING	
	IGNEOUS ROCK	Description	Thickness/Spacing
	SEDIMENTARY ROCK	Massive	Greater than 10 ft
	METAMORPHIC ROCK	Very Thickly Bedded	3 ft - 10 ft
		Thickly Bedded	1 ft - 3 ft
		Moderately Bedded	4 in - 1 ft
		Thinly Bedded	1 in - 4 in
		Very Thinly Bedded	1/4 in - 1 in
		Laminated	Less than 1/4 in

WEATHERING DESCRIPTORS FOR INTACT ROCK						
Description	Diagnostic Features					
	Chemical Weathering-Discoloration-Oxidation		Mechanical Weathering and Grain Boundary Conditions	Texture and Leaching		General Characteristics
	Body of Rock	Fracture Surfaces		Texture	Leaching	
Fresh	No discoloration, not oxidized	No discoloration or oxidation	No separation, intact (tight)	No change	No leaching	Hammer rings when crystalline rocks are struck.
Slightly Weathered	Discoloration or oxidation is limited to surface of, or short distance from, fractures; some feldspar crystals are dull	Minor to complete discoloration or oxidation of most surfaces	No visible separation, intact (tight)	Preserved	Minor leaching of some soluble minerals	Hammer rings when crystalline rocks are struck. Body of rock not weakened.
Moderately Weathered	Discoloration or oxidation extends from fractures usually throughout; Fe-Mg minerals are "rusty"; feldspar crystals are "cloudy"	All fracture surfaces are discolored or oxidized	Partial separation of boundaries visible	Generally preserved	Soluble minerals may be mostly leached	Hammer does not ring when rock is struck. Body of rock is slightly weakened.
Intensely Weathered	Discoloration or oxidation throughout; all feldspars and Fe-Mg minerals are altered to clay to some extent; or chemical alteration produces in situ disaggregation, grain boundary conditions	All fracture surfaces are discolored or oxidized; surfaces friable	Partial separation, rock is friable; in semi-arid conditions, granitics are disaggregated	Texture altered by chemical disintegration (hydration, argillation)	Leaching of soluble minerals may be complete	Dull sound when struck with hammer; usually can be broken with moderate to heavy manual pressure or by light hammer blow without reference to planes of weakness such as incipient or hairline fractures or veinlets. Rock is significantly weakened.
Decomposed	Discolored or oxidized throughout, but resistant minerals such as quartz may be unaltered; all feldspars and Fe-Mg minerals are completely altered to clay		Complete separation of grain boundaries (disaggregated)	Resembles a soil; partial or complete remnant rock structure may be preserved; leaching of soluble minerals usually complete		Can be granulated by hand. Resistant minerals such as quartz may be present as "stringers" or "dikes".

PERCENT CORE RECOVERY (REC)
$\frac{\sum \text{Length of the recovered core pieces (in.)}}{\text{Total length of core run (in.)}} \times 100$

ROCK QUALITY DESIGNATION (RQD)
$\frac{\sum \text{Length of intact core pieces} \geq 4 \text{ in.}}{\text{Total length of core run (in.)}} \times 100$
RQD* indicates soundness criteria not met.

ROCK HARDNESS	
Description	Criteria
Extremely Hard	Cannot be scratched with a pocketknife or sharp pick. Can only be chipped with repeated heavy hammer blows
Very Hard	Cannot be scratched with a pocketknife or sharp pick. Breaks with repeated heavy hammer blows.
Hard	Can be scratched with a pocketknife or sharp pick with difficulty (heavy pressure). Breaks with heavy hammer blows.
Moderately Hard	Can be scratched with a pocketknife or sharp pick with light or moderate pressure. Breaks with moderate hammer blows
Moderately Soft	Can be grooved 1/16 in. deep with a pocketknife or sharp pick with moderate or heavy pressure. Breaks with light hammer blow or heavy manual pressure.
Soft	Can be grooved or gouged easily with a pocketknife or sharp pick with light pressure, can be scratched with fingernail. Breaks with light to moderate manual pressure.
Very Soft	Can be readily indented, grooved or gouged with fingernail, or carved with a pocketknife. Breaks with light manual pressure.

FRACTURE DENSITY	
Description	Observed Fracture Density
Unfractured	No fractures
Very Slightly Fractured	Core lengths greater than 3 ft.
Slightly Fractured	Core lengths mostly from 1 to 3 ft.
Moderately Fractured	Core lengths mostly 4 in. to 1 ft.
Intensely Fractured	Core lengths mostly from 1 to 4 in.
Very Intensely Fractured	Mostly chips and fragments.

REFERENCE Caltrans Soil and Rock Logging, Classification, and Presentation Manual (2010).



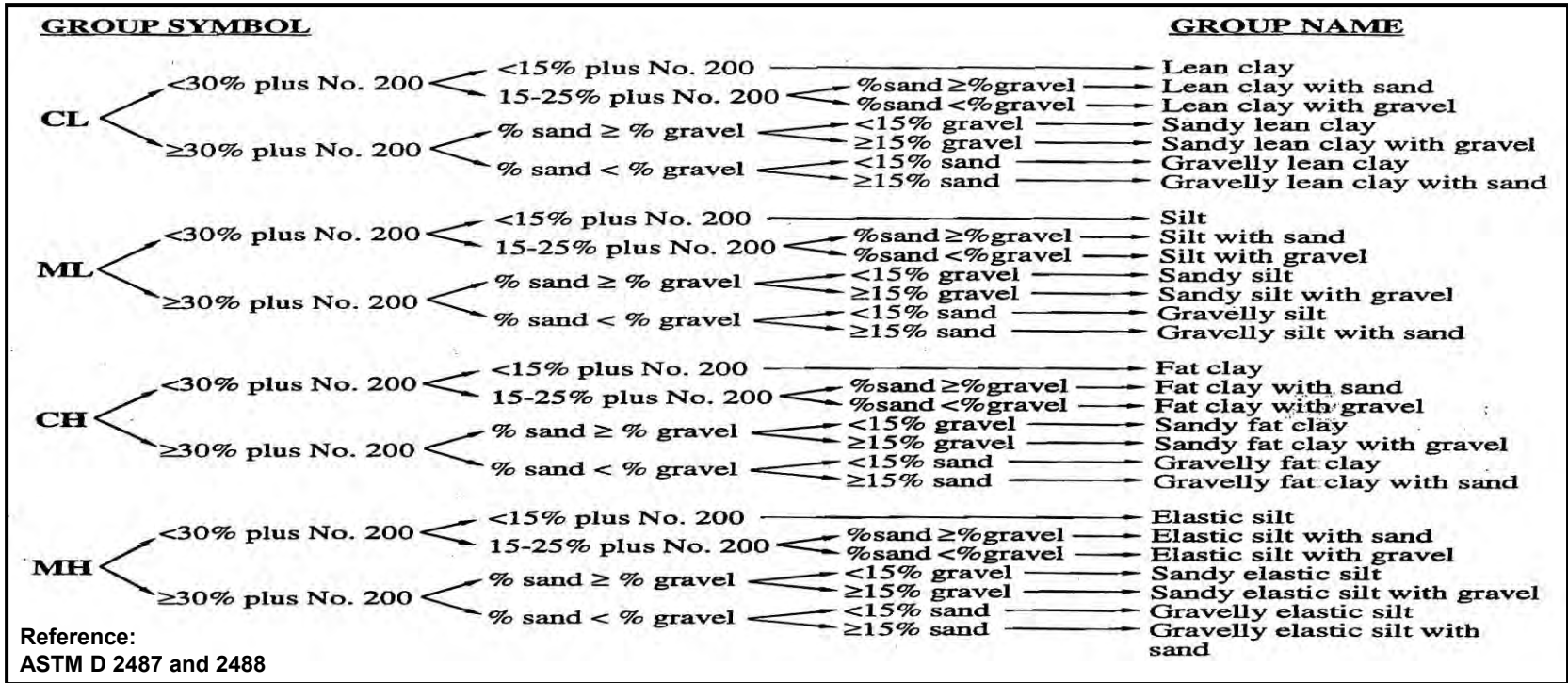
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Palo Comado Bridge OC (Widen)
Agoura Hills, CA

BORING RECORD LEGEND #3

Figure A-1d

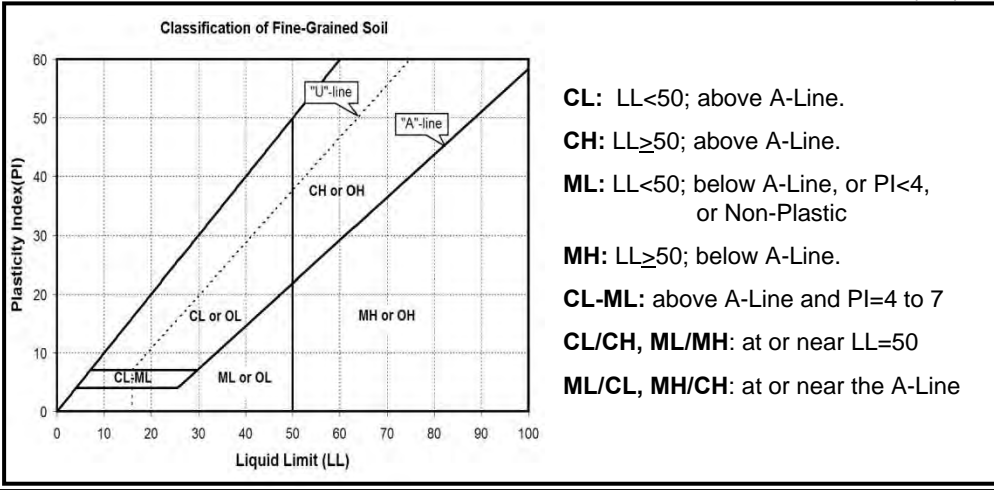
CLASSIFICATION OF INORGANIC FINE GRAINED SOILS (Soils with $\geq 50\%$ finer than No. 200 Sieve)




Laboratory Classification of Clay and Silt

REFERENCE: Caltrans Soil and Rock Logging, Classification, and Presentation Manual (2010).

Field Identification of Clays and Silts



Group Symbol	Dry Strength	Dilatancy	Toughness	Plasticity
ML	None to low	Slow to rapid	Low or thread cannot be formed	Low to nonplastic
CL	Medium to high	None to slow	Medium	Medium
MH	Low to medium	None to slow	Low to medium	Low to medium
CH	High to very high	None	High	High



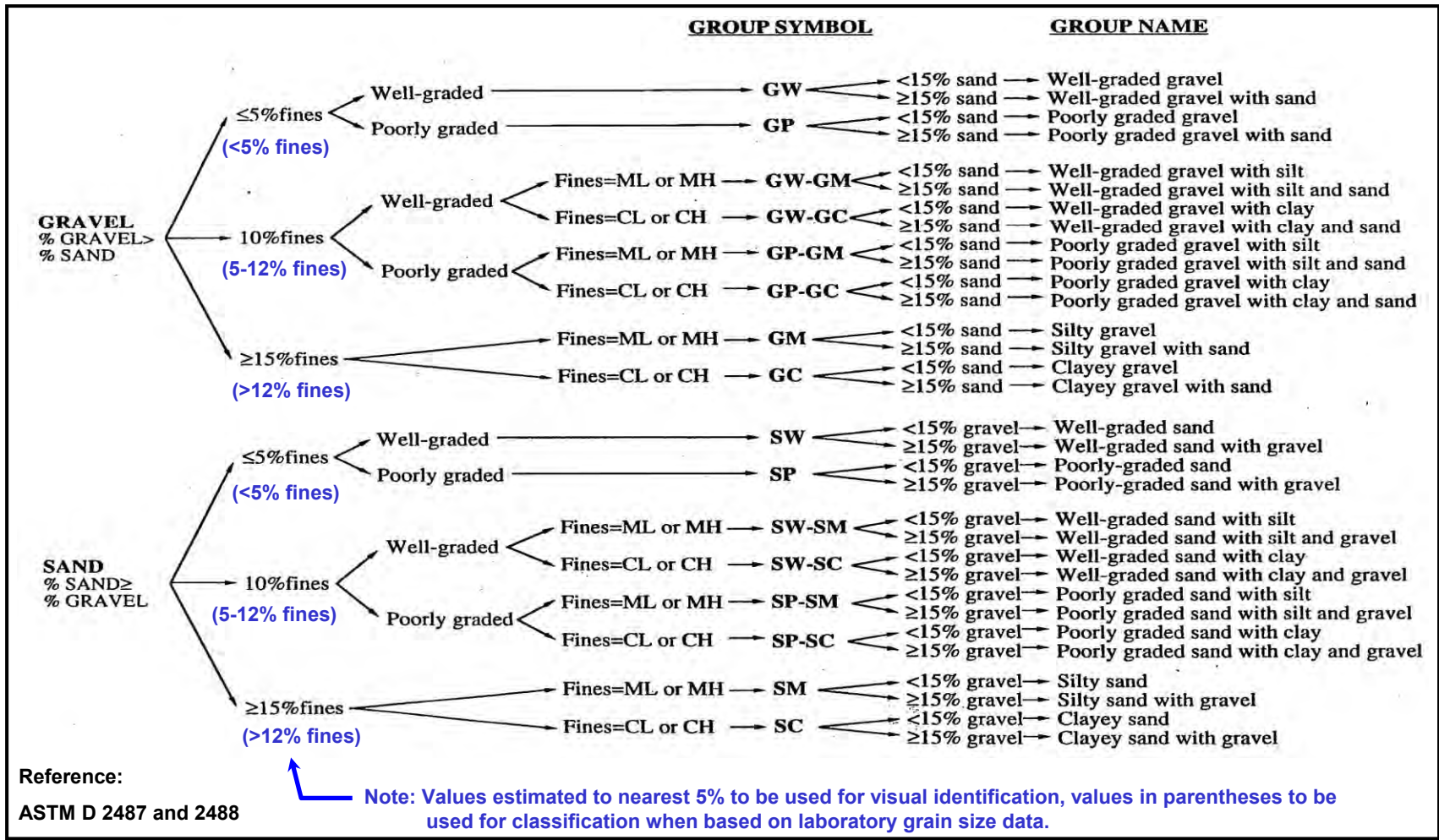
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Palo Comado Bridge OC (Widen)
Agoura Hills, CA

KEY FOR SOIL CLASSIFICATION #1

Figure A-1e

CLASSIFICATION OF COARSE-GRAINED SOILS (Soils with <50% “fines” passing No. 200 Sieve)



Granular Soil Gradation Parameters
 Coefficient of Uniformity: $C_u = D_{60}/D_{10}$
 Coefficient of Curvature: $C_c = D_{30}^2 / (D_{60} \times D_{10})$
 D_{10} = 10% of soil is finer than this diameter
 D_{30} = 30% of soil is finer than this diameter
 D_{60} = 60% of soil is finer than this diameter

Group Symbol	Gradation or Plasticity Requirement
SW.....	$C_u > 6$ and $1 \leq C_c \leq 3$
GW.....	$C_u > 4$ and $1 \leq C_c \leq 3$
GP or SP.....	Clean gravel or sand not meeting requirement for SW or GW
SM or GM.....	Non-plastic fines or below A-Line or $PI < 4$
SC or GC.....	Plastic fines or above A-Line and $PI > 7$



GDC Project No. LA1143
 Palo Comado Bridge OC (Widen)
 Agoura Hills, CA
KEY FOR SOIL CLASSIFICATION #2

Figure A-1f

BORING RECORD

PROJECT NAME Palo Comado Bridge Widening				PROJECT NUMBER LA-1143		HOLE ID A-13-001		
DIST. 07	CO. LA	ROUTE 101	POSTMILE 33.69	BRIDGE NO. 53 - 1678	CALTRANS ENCROACHMENT PERMIT NUMBER 0700001840	START 9/9/2013	FINISH 9/9/2013	SHEET NO. 1 of 2
SITE LOCATION Agoura Hills, CA				BOREHOLE LOCATION (Lat/Long or North/East and Datum) Boring Location Plan		BOREHOLE LOCATION (Offset, Station, Line) 22 ft left Sta. 16 + 22		
DRILLING COMPANY Choice			DRILL RIG CME 75		DRILLING METHOD Hollow Stem Auger		LOGGED BY S. Stone	CHECKED BY M.DiNicola
HAMMER TYPE (WEIGHT/DROP) Automatic, (140 lbs., 30")			HAMMER EFFICIENCY (ERi) 85%		BORING DIA. (in) 8"	TOTAL DEPTH (ft) 26.5	GROUND ELEV (ft) 934	DEPTH/ELEV. GW (ft) N/A
DRIVE SAMPLER TYPE(S) & SIZE (ID) SPT (1.4"), CAL (2.4")				NOTES (N)60 = 1.42Nspt = 0.95Ncal		BOREHOLE BACKFILL & COMPLETION Soil Cuttings		DURING DRILLING N/E / NE
								AFTER DRILLING N/E / NE

DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL:PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
															ASPHALT CONCRETE (9")
															AGGREGATE BASE (18")
5	930		B-1												Fat CLAY (CH); medium brown; moist; mostly fines; trace fine SAND; oxidation; high plasticity (ALLUVIUM, Qa)
			R-2	9 12 16	28	27			24.8	95	56:31				Very stiff; PP=3.0 tsf.
			S-3	3 3 4	7	10			27.4						Medium brown to gray; caliche; PP=3.0 tsf.
10	925		R-4	7 8 11	19	18			22.5	98					Rig chatter; hard drilling; PP=3.0 tsf.
15	920		S-5	3 4 5	9	13			21.3						Sandy Fat CLAY (CH); very stiff; dark gray; moist; mostly fines; some fine SAND; few GRAVEL; high plasticity; PP=3.5 tsf. #200: 7% GRAVEL; 38% SAND; 55% fines.
20	915		R-6	13 18 25	43	41			21.7	101					Fat CLAY (CH); very stiff; medium brown-gray; moist; mostly fines; few fine GRAVEL; high plasticity; PP=2.0 tsf.
	910														SEDIMENTARY ROCK (POORLY INDURATED CLAYSTONE); fine-grained; reddish

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GROUP DELTA CONSULTANTS, INC.
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Irvine, CA 92618

THIS SUMMARY APPLIES ONLY AT THE LOCATION OF THIS BORING AND AT THE TIME OF DRILLING. SUBSURFACE CONDITIONS MAY DIFFER AT OTHER LOCATIONS AND MAY CHANGE AT THIS LOCATION WITH THE PASSAGE OF TIME. THE DATA PRESENTED IS A SIMPLIFICATION OF THE ACTUAL CONDITIONS ENCOUNTERED.


FIGURE
A-2 a

BORING RECORD

PROJECT NAME Palo Comado Bridge Widening				PROJECT NUMBER LA-1143		HOLE ID A-13-001		
DIST. 07	CO. LA	ROUTE 101	POSTMILE 33.69	BRIDGE NO. 53 - 1678	CALTRANS ENCROACHMENT PERMIT NUMBER 0700001840	START 9/9/2013	FINISH 9/9/2013	SHEET NO. 2 of 2
SITE LOCATION Agoura Hills, CA				BOREHOLE LOCATION (Lat/Long or North/East and Datum) Boring Location Plan		BOREHOLE LOCATION (Offset, Station, Line) 22 ft left Sta. 16 + 22		
DRILLING COMPANY Choice			DRILL RIG CME 75		DRILLING METHOD Hollow Stem Auger		LOGGED BY S. Stone	CHECKED BY M.DiNicola
HAMMER TYPE (WEIGHT/DROP) Automatic, (140 lbs., 30")			HAMMER EFFICIENCY (ERI) 85%		BORING DIA. (in) 8"	TOTAL DEPTH (ft) 26.5	GROUND ELEV (ft) 934 N/A	DEPTH/ELEV. GW (ft) ∇ N/E / NE DURING DRILLING
DRIVE SAMPLER TYPE(S) & SIZE (ID) SPT (1.4"), CAL (2.4")				NOTES (N)60 = 1.42Nspt = 0.95Ncal		BOREHOLE BACKFILL & COMPLETION Soil Cuttings		AFTER DRILLING ▼ N/E / NE

DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL:PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
30	905	X	S-7	15 18 30	48	68			22.8						brown-medium gray; very soft; steeply dipping; some caliche; (Fat CLAY (CH); hard; moist; high plasticity; PP=4.0 tsf); (CALABASAS FORMATION, Tcb). Bottom of borehole at 26.5 feet. Boring terminated at planned depth. Groundwater not encountered. This Boring Record was prepared in accordance with the Caltrans Soil & Rock Logging, Classification, and Presentation Manual (2010).
35	900														
40	895														
45	890														
	885														

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	GROUP DELTA CONSULTANTS, INC. 32 Mauchly, Suite B Irvine, CA 92618	THIS SUMMARY APPLIES ONLY AT THE LOCATION OF THIS BORING AND AT THE TIME OF DRILLING. SUBSURFACE CONDITIONS MAY DIFFER AT OTHER LOCATIONS AND MAY CHANGE AT THIS LOCATION WITH THE PASSAGE OF TIME. THE DATA PRESENTED IS A SIMPLIFICATION OF THE ACTUAL CONDITIONS ENCOUNTERED.	FIGURE A-2 b
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BORING RECORD

PROJECT NAME Palo Comado Bridge Widening					PROJECT NUMBER LA-1143		HOLE ID A-13-002	
DIST. 07	CO. LA	ROUTE 101	POSTMILE 33.69	BRIDGE NO. 53 - 1678	CALTRANS ENCROACHMENT PERMIT NUMBER 0700001840	START 9/9/2013	FINISH 9/9/2013	SHEET NO. 1 of 3
SITE LOCATION Agoura Hills, CA				BOREHOLE LOCATION (Lat/Long or North/East and Datum) Boring Location Plan			BOREHOLE LOCATION (Offset, Station, Line) 25 ft left Sta. 18 + 72	
DRILLING COMPANY Choice			DRILL RIG CME 75		DRILLING METHOD Hollow Stem Auger		LOGGED BY S. Stone	CHECKED BY M.DiNicola
HAMMER TYPE (WEIGHT/DROP) Automatic, (140 lbs., 30")			HAMMER EFFICIENCY (ERi) 85%		BORING DIA. (in) 8"	TOTAL DEPTH (ft) 61	GROUND ELEV (ft) 936	DEPTH/ELEV. GW (ft) N/A
DRIVE SAMPLER TYPE(S) & SIZE (ID) SPT (1.4"), CAL (2.4")				NOTES (N)60 = 1.42Nspt = 0.95Ncal			BOREHOLE BACKFILL & COMPLETION Soil Cuttings	
								DURING DRILLING N/E / NE
								AFTER DRILLING N/E / NE

DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL:PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
	935														ASPHALT CONCRETE (6.5")
															AGGREGATE BASE (16")
5			B-1												Fat CLAY (CH); orange-brown; moist; high plasticity; (FILL, Qaf).
	930		S-2	3 4 4	8	11			23.8		53:30				Very stiff; orangish brown-gray; specks of volcanic ash; PP=3.5 tsf.
			R-3	7 10 12	22	21			19.9	102		CN			Orangish brown-gray and dark brown; PP=2.0 tsf.
10			S-4	3 3 4	7	10			23.4						Stiff; orange-gray; PP=1.0 tsf.
	925														
15			R-5	12 15 22	27	26			18.1	109		DS			Very stiff; few GRAVEL; PP=2.5 tsf.
20			S-6	5 5 6	11	16			25.7						Fat CLAY (CH); stiff; mottled orange-dark gray; moist; high plasticity; (ALLUVIUM, Qa); PP=1.5 tsf.
	915														

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BORING RECORD

PROJECT NAME Palo Comado Bridge Widening				PROJECT NUMBER LA-1143		HOLE ID A-13-002		
DIST. 07	CO. LA	ROUTE 101	POSTMILE 33.69	BRIDGE NO. 53 - 1678	CALTRANS ENCROACHMENT PERMIT NUMBER 0700001840	START 9/9/2013	FINISH 9/9/2013	SHEET NO. 2 of 3

SITE LOCATION Agoura Hills, CA			BOREHOLE LOCATION (Lat/Long or North/East and Datum) Boring Location Plan			BOREHOLE LOCATION (Offset, Station, Line) 25 ft left Sta. 18 + 72		
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DRILLING COMPANY Choice		DRILL RIG CME 75		DRILLING METHOD Hollow Stem Auger		LOGGED BY S. Stone		CHECKED BY M.DiNicola	
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HAMMER TYPE (WEIGHT/DROP) Automatic, (140 lbs., 30")		HAMMER EFFICIENCY (ER) 85%		BORING DIA. (in) 8"		TOTAL DEPTH (ft) 61		GROUND ELEV (ft) 936 N/A		DEPTH/ELEV. GW (ft) ∇ N/E / NE DURING DRILLING	
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DRIVE SAMPLER TYPE(S) & SIZE (ID) SPT (1.4"), CAL (2.4")				NOTES (N)60 = 1.42Nspt = 0.95Ncal				BOREHOLE BACKFILL & COMPLETION Soil Cuttings				AFTER DRILLING ∇ N/E / NE	
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DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL:PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
30	910	R-7		12 18 25	43	41			25.7	98	68:44	DS			SEDIMENTARY ROCK (POORLY INDURATED CLAYSTONE); fine-grained; mottled orange-grown; very soft; (Fat CLAY (CH); hard; slightly moist; high plasticity; PP>4.5 tsf); (CALABASAS FORMATION, Tcb).
	905	S-8		11 14 17	31	44			21.4						Thinly bedded; steeply dipping bedding plane; medium gray; (very stiff; weak cementation; oxidation; PP=2.5 tsf).
35	900	R-9		22 50/6"	50/6"	48/6"			24.9	104					(moist; PP=3.5 tsf).
40	895	S-10		12 20 26	46	65			22.4						Laminated; discontinuity; dark gray; friable; mineralization; (hard; dry; caliche; PP>4.5 tsf).
45	890	R-11		45 50/6"	50/6"	48/6"			17.7	112					Thickly bedded; medium gray; tuffaceous; (slightly moist; PP>4.5 tsf).

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BORING RECORD

PROJECT NAME Palo Comado Bridge Widening				PROJECT NUMBER LA-1143		HOLE ID A-13-002		
DIST. 07	CO. LA	ROUTE 101	POSTMILE 33.69	BRIDGE NO. 53 - 1678	CALTRANS ENCROACHMENT PERMIT NUMBER 0700001840	START 9/9/2013	FINISH 9/9/2013	SHEET NO. 3 of 3

SITE LOCATION Agoura Hills, CA			BOREHOLE LOCATION (Lat/Long or North/East and Datum) Boring Location Plan			BOREHOLE LOCATION (Offset, Station, Line) 25 ft left Sta. 18 + 72		
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DRILLING COMPANY Choice		DRILL RIG CME 75		DRILLING METHOD Hollow Stem Auger			LOGGED BY S. Stone	CHECKED BY M.DiNicola
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HAMMER TYPE (WEIGHT/DROP) Automatic, (140 lbs., 30")		HAMMER EFFICIENCY (ERi) 85%		BORING DIA. (in) 8"		TOTAL DEPTH (ft) 61	GROUND ELEV (ft) 936	N/A	DEPTH/ELEV. GW (ft) ▽ N/E / NE	DURING DRILLING
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DRIVE SAMPLER TYPE(S) & SIZE (ID) SPT (1.4"), CAL (2.4")			NOTES (N)60 = 1.42Nspt = 0.95Ncal			BOREHOLE BACKFILL & COMPLETION Soil Cuttings		AFTER DRILLING ▼ N/E / NE		
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DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL:PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
	885	⊗	S-12	16 28 36	64	91			16.4						SEDIMENTARY ROCK (POORLY INDURATED CLAYSTONE) (CALABASAS FORMATION, Tcb) (continued). (moist; PP>4.5 tsf).
55	880	⊗	R-13	50/6"	REF	REF			13.1	121					(PP>4.5 tsf).
60	875	⊗	S-14	29 50/6"	50/6"	71/6"			12.1						(slightly moist; moderate cementation; PP=4.0 tsf).
															Bottom of borehole at 61 feet. Boring terminated at planned depth.
															This Boring Record was prepared in accordance with the Caltrans Soil & Rock Logging, Classification, and Presentation Manual (2010)

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BORING RECORD

PROJECT NAME Palo Comado Bridge Widening					PROJECT NUMBER LA-1143		HOLE ID A-13-003	
DIST. 07	CO. LA	ROUTE 101	POSTMILE 33.69	BRIDGE NO. 53 - 1678	CALTRANS ENCROACHMENT PERMIT NUMBER 0700001840	START 9/12/2013	FINISH 9/13/2013	SHEET NO. 1 of 3
SITE LOCATION Agoura Hills, CA			BOREHOLE LOCATION (Lat/Long or North/East and Datum) Boring Location Plan			BOREHOLE LOCATION (Offset, Station, Line) 20 ft right Sta. 19 + 28		
DRILLING COMPANY Choice		DRILL RIG CME 75		DRILLING METHOD Hollow Stem Auger			LOGGED BY T. Latimer	CHECKED BY M.DiNicola
HAMMER TYPE (WEIGHT/DROP) Automatic, (140 lbs., 30")		HAMMER EFFICIENCY (ERi) 85%		BORING DIA. (in) 8"		TOTAL DEPTH (ft) 50.5	GROUND ELEV (ft) 910	DEPTH/ELEV. GW (ft) N/A
DRIVE SAMPLER TYPE(S) & SIZE (ID) SPT (1.4"), CAL (2.4")				NOTES (N)60 = 1.42Nspt = 0.95Ncal			BOREHOLE BACKFILL & COMPLETION Soil Cuttings	
							AFTER DRILLING N/A / NE	

DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL:PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
															ASPHALT CONCRETE (12")
															AGGREGATE BASE (9")
5	905		B-1												Fat CLAY (CH); moderately brown; moist; mostly fines; few GRAVEL; high plasticity; (FILL, Qaf / ALLUVIUM, Qa).
			R-2	12 21 25	46	44			27.9	94					SEDIMENTARY ROCK (POORLY INDURATED CLAYSTONE); fine-grained; mottled gray and orangish brown-brown; very soft; (Fat CLAY with SAND (CH); hard; moist; mostly fines; little fine SAND; high plasticity; PP>4.5 tsf). (CALABASAS FORMATION, Tcb). Mottled gray-brown; weathered; (Fat CLAY (CH); very stiff; mostly fines; few fine SAND; high plasticity; PP=3.75 tsf). (Hard; PP=4.5 tsf).
			S-3	4 6 11	17	24			25.3		65:39				
10	900		R-4	12 20 26	46	44			28.4	93					
			S-5	12 18 22	40	57			15.4						(Sandy Fat CLAY (CH); hard; gray; moist; mostly fines; some fine SAND; high plasticity; PP>4.5 tsf).
15	895														
			R-6	31 50/6"	50/6"	48/6"			13.6	114					(Fat CLAY with SAND (CH); hard; gray; moist; mostly fines; little fine SAND; high plasticity; PP>4.5 tsf).
20	890														Perched water at 23 feet.

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BORING RECORD

PROJECT NAME Palo Comado Bridge Widening					PROJECT NUMBER LA-1143		HOLE ID A-13-003	
DIST. 07	CO. LA	ROUTE 101	POSTMILE 33.69	BRIDGE NO. 53 - 1678	CALTRANS ENCROACHMENT PERMIT NUMBER 0700001840	START 9/12/2013	FINISH 9/13/2013	SHEET NO. 2 of 3
SITE LOCATION Agoura Hills, CA				BOREHOLE LOCATION (Lat/Long or North/East and Datum) Boring Location Plan			BOREHOLE LOCATION (Offset, Station, Line) 20 ft right Sta. 19 + 28	
DRILLING COMPANY Choice			DRILL RIG CME 75		DRILLING METHOD Hollow Stem Auger		LOGGED BY T. Latimer	CHECKED BY M.DiNicola
HAMMER TYPE (WEIGHT/DROP) Automatic, (140 lbs., 30")			HAMMER EFFICIENCY (ERI) 85%		BORING DIA. (in) 8"	TOTAL DEPTH (ft) 50.5	GROUND ELEV (ft) 910 N/A	DEPTH/ELEV. GW (ft) ▽ 23.0 / 887.0
DRIVE SAMPLER TYPE(S) & SIZE (ID) SPT (1.4"), CAL (2.4")				NOTES (N)60 = 1.42Nspt = 0.95Ncal			BOREHOLE BACKFILL & COMPLETION Soil Cuttings	
							AFTER DRILLING ▼ N/M / NE	

DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL;PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
		⊗	S-7	50/6"	REF	REF			23.4				CR		SEDIMENTARY ROCK (POORLY INDURATED CLAYSTONE) (CALABASAS FORMATION, Tcb) (continued). (Trace GRAVEL).
30	880	⊗	R-8	50/6"	REF	REF			17.1	120					(Fat CLAY (CH); hard; dark gray; moist to wet; mostly fines; few fine SAND; high plasticity; PP>4.5 tsf).
35	875	⊗	S-9	20 50/6"	50/6"	71/6"			20.4						(Sandy Fat CLAY (CH); hard; dark grayish brown; moist; mostly fines; some fine SAND; high plasticity; PP>4.5 tsf).
40	870	⊗	R-10	32 50/3"	50/3"	48/3"			21.4	101					(PP>4.5 tsf).
45	865	⊗	S-11	27 50/6"	50/6"	71/6"			22.1						

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FIGURE
A-4 b

BORING RECORD

PROJECT NAME Palo Comado Bridge Widening				PROJECT NUMBER LA-1143		HOLE ID A-13-003		
DIST. 07	CO. LA	ROUTE 101	POSTMILE 33.69	BRIDGE NO. 53 - 1678	CALTRANS ENCROACHMENT PERMIT NUMBER 0700001840	START 9/12/2013	FINISH 9/13/2013	SHEET NO. 3 of 3
SITE LOCATION Agoura Hills, CA				BOREHOLE LOCATION (Lat/Long or North/East and Datum) Boring Location Plan		BOREHOLE LOCATION (Offset, Station, Line) 20 ft right Sta. 19 + 28		
DRILLING COMPANY Choice		DRILL RIG CME 75		DRILLING METHOD Hollow Stem Auger		LOGGED BY T. Latimer		CHECKED BY M.DiNicola
HAMMER TYPE (WEIGHT/DROP) Automatic, (140 lbs., 30")		HAMMER EFFICIENCY (ERI) 85%		BORING DIA. (in) 8"	TOTAL DEPTH (ft) 50.5	GROUND ELEV (ft) 910	DEPTH/ELEV. GW (ft) ▽ 23.0 / 887.0	DRURING DRILLING
DRIVE SAMPLER TYPE(S) & SIZE (ID) SPT (1.4"), CAL (2.4")				NOTES (N)60 = 1.42Nspt = 0.95Ncal		BOREHOLE BACKFILL & COMPLETION Soil Cuttings		AFTER DRILLING ▼ N/M / NE

DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL:PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
55	855	R-12		50/5"	REF	REF			20	98					<p>SEDIMENTARY ROCK (POORLY INDURATED CLAYSTONE) (CALABASAS FORMATION, Tcb) (continued).</p> <p>Bottom of borehole at 50.5 feet. Boring terminated at planned depth. Perched water encountered at 23 feet.</p> <p>This Boring Record was prepared in accordance with the Caltrans Soil & Rock Logging, Classification, and Presentation Manual (2010)</p>
60	850														
65	845														
70	840														

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BORING RECORD

PROJECT NAME: Palo Comado Bridge Widening
 PROJECT NUMBER: LA-1143
 HOLE ID: A-13-004
 DIST. 07 CO. LA ROUTE 101 POSTMILE 33.69 BRIDGE NO. 53 - 1678
 CALTRANS ENCROACHMENT PERMIT NUMBER: 0700001840
 START: 9/12/2013 FINISH: 9/12/2013
 SHEET NO.: 1 of 3

SITE LOCATION: Agoura Hills, CA
 BOREHOLE LOCATION (Lat/Long or North/East and Datum): Boring Location Plan
 BOREHOLE LOCATION (Offset, Station, Line): 20 ft right Sta. 20 + 22
 DRILLING COMPANY: Choice
 DRILL RIG: CME 75
 DRILLING METHOD: Hollow Stem Auger
 LOGGED BY: S. Stone
 CHECKED BY: M. DiNicola
 HAMMER TYPE (WEIGHT/DROP): Automatic, (140 lbs., 30")
 HAMMER EFFICIENCY (ERI): 85%
 BORING DIA. (in): 8"
 TOTAL DEPTH (ft): 50.5
 GROUND ELEV (ft): 914
 N/A
 DEPTH/ELEV. GW (ft): ∇ N/E / NE DURING DRILLING
 DRIVE SAMPLER TYPE(S) & SIZE (ID): SPT (1.4"), CAL (2.4")
 NOTES: (N)60 = 1.42Nspt = 0.95Ncal
 BOREHOLE BACKFILL & COMPLETION: Soil Cuttings
 AFTER DRILLING: ∇ N/E / NE

DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL:PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
															ASPHALT CONCRETE (6") AGGREGATE BASE (15")
5	910		B-1												Sandy Fat CLAY (CH); reddish brown; moist; mostly fines; some fine SAND; high plasticity (ALLUVIUM, Qa).
			S-2	2 3 3	6	8			17.3						Very stiff; PP=3.25 tsf. #200: 33% SAND; 67% fines
	905		R-3	7 12 20	32	30			16.7	109					
10			S-4	4 7 8	15	21			18.5						Light reddish brown; little caliche; PP=2.75 tsf.
15	900		R-5	8 12 15	27	26			26.9	95					Reddish brown; PP=3.75 tsf.
20	895		S-6	7 10 20	30	42			23.1						SEDIMENTARY ROCK (POORLY INDURATED CLAYSTONE); fine-grained; reddish brown-light gray; weathered; very soft; (Fat CLAY (CH); hard; slightly moist; high plasticity; PP>4.5 tsf) (CALABASAS FORMATION, Tcb).
	890														

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BORING RECORD

PROJECT NAME Palo Comado Bridge Widening				PROJECT NUMBER LA-1143		HOLE ID A-13-004		
DIST. 07	CO. LA	ROUTE 101	POSTMILE 33.69	BRIDGE NO. 53 - 1678	CALTRANS ENCROACHMENT PERMIT NUMBER 0700001840	START 9/12/2013	FINISH 9/12/2013	SHEET NO. 2 of 3
SITE LOCATION Agoura Hills, CA				BOREHOLE LOCATION (Lat/Long or North/East and Datum) Boring Location Plan		BOREHOLE LOCATION (Offset, Station, Line) 20 ft right Sta. 20 + 22		
DRILLING COMPANY Choice			DRILL RIG CME 75		DRILLING METHOD Hollow Stem Auger		LOGGED BY S. Stone	CHECKED BY M.DiNicola
HAMMER TYPE (WEIGHT/DROP) Automatic, (140 lbs., 30")			HAMMER EFFICIENCY (ERi) 85%		BORING DIA. (in) 8"	TOTAL DEPTH (ft) 50.5	GROUND ELEV (ft) 914 N/A	DEPTH/ELEV. GW (ft) ∇ N/E / NE DURING DRILLING ∇ N/E / NE AFTER DRILLING
DRIVE SAMPLER TYPE(S) & SIZE (ID) SPT (1.4"), CAL (2.4")				NOTES (N)60 = 1.42Nspt = 0.95Ncal			BOREHOLE BACKFILL & COMPLETION Soil Cuttings	

DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (L:P)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
30	885	⊗	R-7	33 50/6"	50/6"	48/6"			21.5	104		CN			SEDIMENTARY ROCK (POORLY INDURATED CLAYSTONE) (CALABASAS FORMATION, Tcb) (continued). Thickly bedded; gray; (PP>4.5 tsf).
		⊗	S-8	11 15 19	34	48			20.2						Medium to dark gray; (PP >4.5 tsf).
35	880	⊗	R-9	34 50/6"	50/6"	48/6"			19.5	109					(PP >4.5 tsf).
40	875	⊗	S-10	14 21 25	46	65			20.5						Laminated; medium gray; (dry; PP>4.5 tsf).
45	870	⊗	R-11	50/6"	REF	REF			20.1	107					Medium to dark gray; (PP>4.5 tsf).
	865														

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BORING RECORD

PROJECT NAME Palo Comado Bridge Widening				PROJECT NUMBER LA-1143		HOLE ID A-13-004		
DIST. 07	CO. LA	ROUTE 101	POSTMILE 33.69	BRIDGE NO. 53 - 1678	CALTRANS ENCROACHMENT PERMIT NUMBER 0700001840	START 9/12/2013	FINISH 9/12/2013	SHEET NO. 3 of 3

SITE LOCATION Agoura Hills, CA			BOREHOLE LOCATION (Lat/Long or North/East and Datum) Boring Location Plan			BOREHOLE LOCATION (Offset, Station, Line) 20 ft right Sta. 20 + 22		
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DRILLING COMPANY Choice		DRILL RIG CME 75		DRILLING METHOD Hollow Stem Auger		LOGGED BY S. Stone		CHECKED BY M.DiNicola	
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HAMMER TYPE (WEIGHT/DROP) Automatic, (140 lbs., 30")		HAMMER EFFICIENCY (ERI) 85%		BORING DIA. (in) 8"		TOTAL DEPTH (ft) 50.5		GROUND ELEV (ft) 914 N/A		DEPTH/ELEV. GW (ft) ∇ N/E / NE DURING DRILLING	
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DRIVE SAMPLER TYPE(S) & SIZE (ID) SPT (1.4"), CAL (2.4")				NOTES (N)60 = 1.42Nspt = 0.95Ncal				BOREHOLE BACKFILL & COMPLETION Soil Cuttings				AFTER DRILLING ∇ N/E / NE	
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DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL:PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
55	860	×	S-12	50/6"	REF	REF			15.1						SEDIMENTARY ROCK (POORLY INDURATED CLAYSTONE) (CALABASAS FORMATION, Tcb) (continued). Steeply dipping beds; medium gray; (PP>4.5 tsf). Bottom of borehole at 50.5 feet Boring terminated at planned depth. Groundwater not encountered.
60	855														This Boring Record was prepared in accordance with the Caltrans Soil & Rock Logging, Classification, and Presentation Manual (2010)
65	850														
70	845														
840															

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BORING RECORD

PROJECT NAME Palo Comado Bridge Widening					PROJECT NUMBER LA-1143		HOLE ID A-13-005	
DIST. 07	CO. LA	ROUTE 101	POSTMILE 33.69	BRIDGE NO. 53 - 1678	CALTRANS ENCROACHMENT PERMIT NUMBER 0700001840	START 9/12/2013	FINISH 9/12/2013	SHEET NO. 1 of 3
SITE LOCATION Agoura Hills, CA				BOREHOLE LOCATION (Lat/Long or North/East and Datum) Boring Location Plan		BOREHOLE LOCATION (Offset, Station, Line) 25 ft right Sta. 20 + 83		
DRILLING COMPANY Choice			DRILL RIG CME 75		DRILLING METHOD Hollow Stem Auger		LOGGED BY S. Stone	CHECKED BY M.DiNicola
HAMMER TYPE (WEIGHT/DROP) Automatic, (140 lbs., 30")			HAMMER EFFICIENCY (ERi) 85%		BORING DIA. (in) 8"	TOTAL DEPTH (ft) 51	GROUND ELEV (ft) 917 N/A	DEPTH/ELEV. GW (ft) ▽ 45.5 / 871.5
DRIVE SAMPLER TYPE(S) & SIZE (ID) SPT (1.4"), CAL (2.4")				NOTES (N)60 = 1.42Nspt = 0.95Ncal			BOREHOLE BACKFILL & COMPLETION Soil Cuttings	
							AFTER DRILLING ▼ NM / NE	

DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL:PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
															ASPHALT CONCRETE (7")
															AGGREGATE BASE (8")
5	915		B-1												Fat CLAY (CH); reddish brown; moist; mostly fines; high plasticity; (ALLUVIUM Qa).
			R-2	18 18 24	42	40			18.9	105	58:31				Hard; dry; trace GRAVEL; PP>4.5 tsf.
10	910		S-3	7 12 17	29	41			25.8						SEDIMENTARY ROCK (POORLY INDURATED CLAYSTONE); fine-grained; thinly bedded; steeply dipping bedding planes; olive gray; weathered; very soft; (Fat CLAY (CH); hard; slightly moist; some oxidation; high plasticity; PP>4.5 tsf) (CALABASAS FORMATION, Tcb).
			R-4	13 26 34	60	57			26.0	98					Very thinly bedded to laminated; reddish brown-dark brown; (Caliche; PP>4.5 tsf).
15	905		S-5	5 9 11	20	28			25.3						Thinly bedded; medium brown; mineralized bedding planes; (PP>4.5 tsf).
20	900		R-6	35 21 36	57	54			21.4	104					Medium brown-gray (PP>4.5 tsf).
	895														

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FIGURE
A-6 a

BORING RECORD

PROJECT NAME Palo Comado Bridge Widening				PROJECT NUMBER LA-1143		HOLE ID A-13-005		
DIST. 07	CO. LA	ROUTE 101	POSTMILE 33.69	BRIDGE NO. 53 - 1678	CALTRANS ENCROACHMENT PERMIT NUMBER 0700001840	START 9/12/2013	FINISH 9/12/2013	SHEET NO. 2 of 3
SITE LOCATION Agoura Hills, CA				BOREHOLE LOCATION (Lat/Long or North/East and Datum) Boring Location Plan		BOREHOLE LOCATION (Offset, Station, Line) 25 ft right Sta. 20 + 83		
DRILLING COMPANY Choice			DRILL RIG CME 75		DRILLING METHOD Hollow Stem Auger		LOGGED BY S. Stone	CHECKED BY M.DiNicola
HAMMER TYPE (WEIGHT/DROP) Automatic, (140 lbs., 30")			HAMMER EFFICIENCY (ERI) 85%		BORING DIA. (in) 8"	TOTAL DEPTH (ft) 51	GROUND ELEV (ft) 917 N/A	DEPTH/ELEV. GW (ft) ▽ 45.5 / 871.5
DRIVE SAMPLER TYPE(S) & SIZE (ID) SPT (1.4"), CAL (2.4")				NOTES (N)60 = 1.42Nspt = 0.95Ncal		BOREHOLE BACKFILL & COMPLETION Soil Cuttings		AFTER DRILLING ▼ NM / NE

DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL:PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
890		⊗	S-7	6 12 15	27	38			19.1						SEDIMENTARY ROCK (POORLY INDURATED CLAYSTONE) (CALABASAS FORMATION, Tcb) (continued). Gray; (very stiff; dry; PP=3.5 tsf).
30		⊗	R-8	30 50/6"	50/6"	48/6"			20.8	106					Laminated; medium gray; (hard; slightly moist; PP>4.5 tsf).
35		⊗	S-9	8 10 12	22	31			20.4						(PP>4.5 tsf).
40		⊗	R-10	31 50/6"	50/6"	48/6"			18.4	110					(PP>4.5 tsf).
45		⊗	S-11	50/6"	REF	REF			15.0						▽ Very intensely fractured; (weak cementation). Perched water at 45.5 feet.

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FIGURE
A-6 b

BORING RECORD

PROJECT NAME Palo Comado Bridge Widening				PROJECT NUMBER LA-1143		HOLE ID A-13-005		
DIST. 07	CO. LA	ROUTE 101	POSTMILE 33.69	BRIDGE NO. 53 - 1678	CALTRANS ENCROACHMENT PERMIT NUMBER 0700001840	START 9/12/2013	FINISH 9/12/2013	SHEET NO. 3 of 3

SITE LOCATION Agoura Hills, CA			BOREHOLE LOCATION (Lat/Long or North/East and Datum) Boring Location Plan			BOREHOLE LOCATION (Offset, Station, Line) 25 ft right Sta. 20 + 83		
--	--	--	---	--	--	--	--	--


DRILLING COMPANY Choice		DRILL RIG CME 75		DRILLING METHOD Hollow Stem Auger			LOGGED BY S. Stone	CHECKED BY M.DiNicola
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HAMMER TYPE (WEIGHT/DROP) Automatic, (140 lbs., 30")		HAMMER EFFICIENCY (ERi) 85%		BORING DIA. (in) 8"	TOTAL DEPTH (ft) 51	GROUND ELEV (ft) 917	DEPTH/ELEV. GW (ft) N/A	DEPTH/ELEV. GW (ft) 45.5 / 871.5
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DRIVE SAMPLER TYPE(S) & SIZE (ID) SPT (1.4"), CAL (2.4")			NOTES (N)60 = 1.42Nspt = 0.95Ncal			BOREHOLE BACKFILL & COMPLETION Soil Cuttings		AFTER DRILLING NM / NE
--	--	--	---	--	--	--	--	----------------------------------

DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL:PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
865		R-12		29 50/6"	50/6"	48/6"			19.9	109					<p>SEDIMENTARY ROCK (POORLY INDURATED CLAYSTONE) (CALABASAS FORMATION, Tcb) (continued). Gray; (dry; PP>4.5 tsf). Bottom of borehole at 51 feet. Boring terminated at planned depth. Perched water encountered at 45 feet.</p> <p>This Boring Record was prepared in accordance with the Caltrans Soil & Rock Logging, Classification, and Presentation Manual (2010).</p>
55															
860															
60															
855															
65															
850															
70															
845															

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BORING RECORD					PROJECT NAME				PROJECT NUMBER		HOLE ID				
Palo Comado Bridge Widening <td colspan="4">LA-1143 <td colspan="2">A-13-006 <td colspan="2"></td> </td></td>					LA-1143 <td colspan="2">A-13-006 <td colspan="2"></td> </td>				A-13-006 <td colspan="2"></td>						
DIST.	CO.	ROUTE	POSTMILE	BRIDGE NO.	CALTRANS ENCROACHMENT PERMIT NUMBER			START	FINISH		SHEET NO.				
07	LA	101	33.69	53 - 1678	0700001840			9/9/2013	9/9/2013		1 of 3				
SITE LOCATION				BOREHOLE LOCATION (Lat/Long or North/East and Datum)				BOREHOLE LOCATION (Offset, Station, Line)							
Agoura Hills, CA				Boring Location Plan				17 ft right Sta. 21 + 75							
DRILLING COMPANY			DRILL RIG		DRILLING METHOD			LOGGED BY		CHECKED BY					
Choice			CME 75		Hollow Stem Auger			S. Stone		M.DiNicola					
HAMMER TYPE (WEIGHT/DROP)			HAMMER EFFICIENCY (ERi)		BORING DIA. (in)		TOTAL DEPTH (ft)	GROUND ELEV (ft)		DEPTH/ELEV. GW (ft)					
Automatic, (140 lbs., 30")			85%		8"		60.5	936		N/A					
DRIVE SAMPLER TYPE(S) & SIZE (ID)				NOTES				BOREHOLE BACKFILL & COMPLETION							
SPT (1.4"), CAL (2.4")				(N)60 = 1.42Nspt = 0.95Ncal				Soil Cuttings							
DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL:PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
5	935		B-1										CR		Fat CLAY (CH); medium reddish brown; slightly moist; mostly fines; few GRAVEL; high plasticity (FILL, Qaf).
	930		R-2	10 12 17	29	27			22.6	103			DS		Fat CLAY with SAND (CH); hard; medium brown-gray; slightly moist; mostly fines; little fine SAND; few GRAVEL; few oxidation; high plasticity; PP=4.0 tsf. Stiff; PP=1.5 tsf. #200: 21% SAND; 79% fines
			S-3	4 4 4	8	11			23.4						Brown-gray and orange; moist; PP=1.5 tsf.
10	925		R-4	8 11 14	25	24			21.3	101			DS		
15	920		S-5	3 4 6	10	14			22.1		57:39				Fat CLAY with SAND (CH); Very stiff; dark gray; oxidation; PP=3.5 tsf (ALLUVIUM, Qa).
20	915		R-6	13 19 28	47	45			29.9	93					SEDIMENTARY ROCK (POORLY INDURATED CLAYSTONE); fine-grained; laminated; brown-orange; very soft; weathered; (Fat CLAY (CH); hard; slightly moist; some caliche; high plasticity; PP=4 tsf) (CALABASAS FORMATION, Tcb).

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FIGURE
 A-7 a


BORING RECORD

PROJECT NAME Palo Comado Bridge Widening				PROJECT NUMBER LA-1143		HOLE ID A-13-006		
DIST. 07	CO. LA	ROUTE 101	POSTMILE 33.69	BRIDGE NO. 53 - 1678	CALTRANS ENCROACHMENT PERMIT NUMBER 0700001840	START 9/9/2013	FINISH 9/9/2013	SHEET NO. 2 of 3

SITE LOCATION Agoura Hills, CA			BOREHOLE LOCATION (Lat/Long or North/East and Datum) Boring Location Plan			BOREHOLE LOCATION (Offset, Station, Line) 17 ft right Sta. 21 + 75		
DRILLING COMPANY Choice		DRILL RIG CME 75		DRILLING METHOD Hollow Stem Auger			LOGGED BY S. Stone	CHECKED BY M.DiNicola
HAMMER TYPE (WEIGHT/DROP) Automatic, (140 lbs., 30")		HAMMER EFFICIENCY (ERi) 85%		BORING DIA. (in) 8"	TOTAL DEPTH (ft) 60.5	GROUND ELEV (ft) 936	DEPTH/ELEV. GW (ft) N/A	DEPTH/ELEV. GW (ft) N/E / NE
DRIVE SAMPLER TYPE(S) & SIZE (ID) SPT (1.4"), CAL (2.4")			NOTES (N)60 = 1.42Nspt = 0.95Ncal			BOREHOLE BACKFILL & COMPLETION Soil Cuttings		AFTER DRILLING N/E / NE

DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL:PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
30	910	X	S-7	3 3 4	7	10			28.5						SEDIMENTARY ROCK (POORLY INDURATED CLAYSTONE) (CALABASAS FORMATION, Tcb) (continued). Very thinly bedded; yellowish brown-orange; oxidation on bedding planes; (PP>4.5 tsf).
35	905	●	R-8	18 32 45	77	73			31.1	92		DS			Laminated; medium brown; (PP>4.5 tsf).
40	900	X	S-9	10 12 16	28	40			25.3						Thinly bedded; dark brown; caliche on some bedding planes; (slightly moist; PP>4.5 tsf).
45	895	●	R-10	50/6"	REF	REF			25.1	101					Tuffaceous; (PP>4.5 tsf).
45	890	X	S-11	43 50/6"	50/6"	71/6"			19.9						Thinly bedded; steeply dipping; gray; (PP>4.5 tsf).

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BORING RECORD

PROJECT NAME Palo Comado Bridge Widening				PROJECT NUMBER LA-1143		HOLE ID A-13-006		
DIST. 07	CO. LA	ROUTE 101	POSTMILE 33.69	BRIDGE NO. 53 - 1678	CALTRANS ENCROACHMENT PERMIT NUMBER 0700001840	START 9/9/2013	FINISH 9/9/2013	SHEET NO. 3 of 3
SITE LOCATION Agoura Hills, CA				BOREHOLE LOCATION (Lat/Long or North/East and Datum) Boring Location Plan		BOREHOLE LOCATION (Offset, Station, Line) 17 ft right Sta. 21 + 75		
DRILLING COMPANY Choice			DRILL RIG CME 75		DRILLING METHOD Hollow Stem Auger		LOGGED BY S. Stone	CHECKED BY M.DiNicola
HAMMER TYPE (WEIGHT/DROP) Automatic, (140 lbs., 30")			HAMMER EFFICIENCY (ERI) 85%		BORING DIA. (in) 8"	TOTAL DEPTH (ft) 60.5	GROUND ELEV (ft) 936	DEPTH/ELEV. GW (ft) N/A
DRIVE SAMPLER TYPE(S) & SIZE (ID) SPT (1.4"), CAL (2.4")				NOTES (N)60 = 1.42Nspt = 0.95Ncal		BOREHOLE BACKFILL & COMPLETION Soil Cuttings		DURING DRILLING N/E / NE
								AFTER DRILLING N/E / NE

DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL:PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
885		⊗	R-12	50/6"	REF	REF			17.7	113					SEDIMENTARY ROCK (POORLY INDURATED CLAYSTONE) (CALABASAS FORMATION, Tcb) (continued). (little caliche; PP>4.5 tsf).
55	880	⊗	S-13	30 50/6"	50/6"	71/6"			15.7						Dark gray; (PP>4.5 tsf).
60	875	⊗	R-14	50/6"	REF	REF			18.2	103					Medium to dark gray; (PP>4.5 tsf). Bottom of borehole at 60.5 feet. Boring terminated at planned depth. Groundwater not encountered.
65	870														This Boring Record was prepared in accordance with the Caltrans Soil & Rock Logging, Classification, and Presentation Manual (2010)
70	865														

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FIGURE
A-7 c

BORING RECORD

PROJECT NAME: Palo Comado Bridge Widening
 PROJECT NUMBER: LA-1143
 HOLE ID: HA-13-007
 DIST. 07 CO. LA ROUTE 101 POSTMILE 33.69 BRIDGE NO. 53 - 1678
 CALTRANS ENCROACHMENT PERMIT NUMBER: 0700001840
 START: 9/9/2013 FINISH: 9/9/2013
 SHEET NO.: 1 of 1

SITE LOCATION: Agoura Hills, CA
 BOREHOLE LOCATION (Lat/Long or North/East and Datum): Boring Location Plan
 BOREHOLE LOCATION (Offset, Station, Line): 14 ft left Sta. 25 + 43
 DRILLING COMPANY: Choice
 DRILL RIG: Hand Auger
 DRILLING METHOD: Hand Auger
 LOGGED BY: S. Stone
 CHECKED BY: M. DiNicola
 HAMMER TYPE (WEIGHT/DROP): NA
 HAMMER EFFICIENCY (ERi): NA
 BORING DIA. (in): 4"
 TOTAL DEPTH (ft): 5
 GROUND ELEV (ft): 928
 N/A
 DEPTH/ELEV. GW (ft): ∇ N/E / NE
 DURING DRILLING: N/A
 AFTER DRILLING: ∇ N/E / NE
 DRIVE SAMPLER TYPE(S) & SIZE (ID): Bag Sample
 NOTES: N/A
 BOREHOLE BACKFILL & COMPLETION: Soil Cuttings

DEPTH (feet)	ELEVATION (feet)	SAMPLE TYPE	SAMPLE NO.	PENETRATION RESISTANCE (BLOWS / 6 IN)	BLOWS/FT	SPT N ₆₀	RECOVERY (%)	RQD (%)	MOISTURE (%)	DRY DENSITY (pcf)	ATTERBERG LIMITS (LL:PI)	OTHER TESTS	DRILLING METHOD	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION
5	925	X	B-1										Hand Auger	Fat CLAY (CH); light brown; dry; high plasticity. Slightly moist. Laminations and black oxidation nodules.	
															Bottom of hand auger at 5 feet. Hand auger terminated at planned depth. Groundwater not encountered.
10	920														This Boring Record was prepared in accordance with the Caltrans Soil & Rock Logging, Classification, and Presentation Manual (2010).
15	915														
20	910														
	905														

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FIGURE
 A-8

SPT Hammer Energy Measurements

**Hammer Calibration done on:
October 27, 2012
in Canoga Park, CA**

**Choice Drilling Rig 1
Operator: Sean Pichinson
ETR = 85.2%**

Prepared for:

**Choice Drilling, Inc.
PO Box 299
Canoga Park, CA 91303**

Prepared by:

**Brian Serl
Calibration Engineer**

**SPT CAL
16254 Van Gogh Ct.
Chino Hills, CA 91709
<http://www.sptcal.com>
909-730-2161**

TABLE OF CONTENTS

1 INTRODUCTION

2 FIELD EQUIPMENT & PROCEDURES

3 INSTRUMENTATION

4 OBSERVATIONS

5 RESULTS

TABLE 1

REFERENCES

Presentation of SPT Analyzer Test Data

1. Introduction

This report presents the results of SPT Hammer Energy Measurements recorded with an SPT Analyzer from Pile Dynamics carried out on October 27, 2012 in Canoga Park, CA.

2. Field Equipment and Procedures

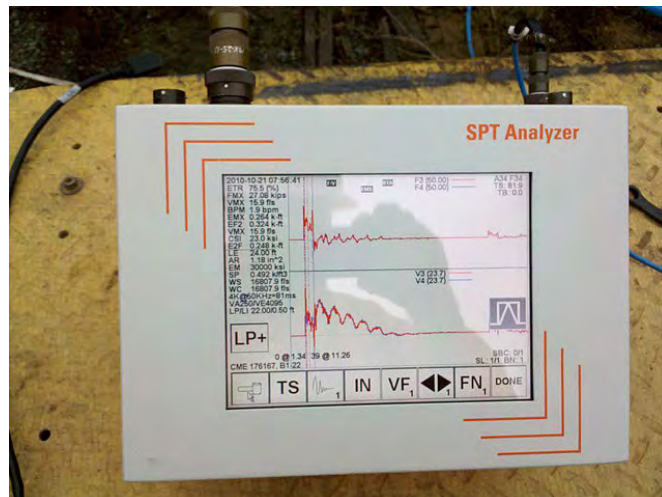
The drill used is referred to at Choice Drilling as Rig 1. The operator of this drill and attached hydraulic Landa automatic trip hammer was Sean Pichinson of Choice Drilling, Inc. The Landa auto hammer has the same specifications and dimensions as the CME automatic trip hammer.

The Landa Auto Hammer uses a 140 lb. weight dropped 30" on to an anvil above the bore hole. AWJ drill rod connects the anvil to a split spoon type soil sampler inside an 8" o.d. hollow stem auger at the designated sample depth. After a seeding blow the sampler is driven 18". The number of blows required to penetrate the last 12" is referred to as the "N value", which is related to soil strength.

The first recording was taken at 5' below ground surface and then every 5' to final recording at 50'.

3. Instrumentation

An SPT Analyzer from Pile Dynamics was used to record and the process the data. The raw data was stored directly in the SPT Analyzer computer with subsequent analysis in the office with PDA-W and PDIPlot software. The measurements and analysis were conducted in general accordance with ASTM D4945 and ASTM D6066 test standards.



The SPT Analyzer is fully compliant with the minimum digital sampling frequency requirements of ASTM D4633-05 (50 kHz) and EN ISO 22476-3:2005 (100 kHz), as well as with the low pass filter, (cutoff frequency of 5000 Hz instead of 3000 Hz) requirements of ASTM D4633-05. All equipment and analysis also conform to ASTM D6066.

Figure 9C



A 2' instrumented section of AWJ rod, with two sets of accelerometers and strain transducers mounted on opposite sides of the drill rod, was placed below the anvil. It measured strain and acceleration of every hammer blow. The SPT Analyzer then calculates the amount of energy transferred to the rod by force and velocity measurements.

4. Observations

The the drill rig motor is diesel fueled. The throttle control is a push pull locking type. The drill and sample equipment looked to be well operated and maintained. The operator Sean Pichinson has been drilling in the geotechnical field with similar equipment for over 13 years. His professionalism, experience and expertise were evident during the drilling process.

5. Results

Results from the SPT Hammer Energy Measurements are summarized in Table 1. It shows the Energy Transfer Ratio (ETR) at each sampling depth. ETR is the ratio of the measured maximum transferred energy to rated energy of the hammer which is the product of the weight of the hammer times the height of the fall. $140 \text{ lb} \times 30'' = 4200 \text{ lb-in} = 0.350 \text{ kip-ft}$.

The ETR for all of the blow counts averaged **85.2%**

Figure 9D

Table 1 – Summary of SPT Hammer Energy Measurements

B1-05	84.9
B1-10	85.2
B1-15	84.0
B1-20	80.9
B1-25	82.5
B1-30	85.4
B1-35	86.9
B1-40	86.3
B1.45	90.3
B1-50	85.7
Average ETR%	85.2

References

- [Stress Wave Methods in Civil Engineering. Proceedings of The Fifth Highway Geophysics - NDE Conference: Charlotte, NC; 472-480.](#)
- [Abou-matar, H., Goble, G. G., October, 1997. SPT Dynamic Analysis and Measurements. Journal of Geotechnical and Geoenvironmental Engineering, ASCE, October 1997: Reston, VA; 921-926.](#)
- [Rausche, F., Thendean, G., Abou-matar, H., Likins, G. E., Goble, G. G., September, 1995. Robinson, B., Webster, S., Alvarez, C., December, 2008. . PDA Users Day: Cleveland, OH.](#)
- [Batchelor, C., Goble, G. G., Berger, J. A., Miner, R., May, 1995. Standard Penetration Test Energy Measurements on the Seattle ASCE Field Testing Program. Seminar In Situ Testing for Seismic Evaluation: University of Washington.](#)
- [Goble, G. G., Abou-matar, H., September, 1992. Determination of wave equation soil constants from the standard penetration test. Proceedings of the Fourth International Conference on the Application of Stress-Wave Theory to Piles: The Netherlands; 99-103.](#)
- [Morgano, C.M., Liang, R., September, 1992. Energy transfer in SPT - Rod length effect. Proceedings of the Fourth International Conference on the Application of Stress-Wave Theory to Piles: The Netherlands; 121-127.](#)
- [Check out our website at <http://www.sptcal.com> for more information and references.](#)

Appendix B Laboratory Testing

APPENDIX B

LABORATORY TESTING

B.1 General

The laboratory testing was performed using appropriate American Society for Testing and Materials (ASTM) and Caltrans Test Methods (CTM).

Modified California drive samples, Standard Penetration Test (SPT) drive samples, and bulk samples collected during the field investigation were carefully sealed in the field to prevent moisture loss. The samples of earth materials were then transported to the laboratory for further examination and testing. Tests were performed on selected samples as an aid in classifying the earth materials and to evaluate their physical properties and engineering characteristics. Laboratory testing for this investigation included:

- Soil and Rock Classification: USCS (ASTM D 2487) and Visual Manual (ASTM D 2488), (ISRM) (1981) standards and the Bureau of Reclamation (2001) standards;
- Moisture content (ASTM D 2216) and Dry Unit Weight (ASTM D 2937);
- Atterberg Limits (ASTM D 4318);
- Percent Passing No. 200 Sieve (ASTM D 1140);
- Direct Shear (ASTM D 3080);
- One-Dimensional Consolidation (ASTM D 2435);
- Expansion Index (D 4829);
- Soil Corrosivity (Caltrans Methods 643, 422, and 417);
- Resistance R-Value (CTM 301).

A summary of laboratory test results is presented in Table B-1. Brief descriptions of the laboratory testing program and test results are presented below.

B.2 Soil and Rock Classification

Earth materials recovered from subsurface explorations were classified in general accordance with Caltrans' "Soil and Rock Logging Classification Manual, 2010". The subsurface soils were classified visually / manually in the field in accordance with the Unified Soil Classification System (USCS) following ASTM D 2488; soil classifications were modified as necessary based on testing in the laboratory in accordance with ASTM D 2487. Rock materials were classified using a hybrid of the International Society of Rock Mechanics (ISRM) (1981) standards and the Bureau of Reclamation (2001) standards, and modified where necessary on the basis of laboratory test results. The details of the soil and rock

classification systems and boring records presenting the classifications are presented in Appendix A.

B.3 Moisture Content and Dry Unit Weight

The in-situ moisture content of selected bulk, SPT, and ring samples was determined by oven drying in general accordance with ASTM D 2216. Selected California Ring samples were trimmed flush in the metal rings and wet weight was measured. After drying, the dry weight of each sample was measured, volume and weight of the metal containers was measured, and moisture content and dry density were calculated in general accordance with ASTM D 2216 and D 2937. Results of these tests are presented in Table B-1 and on the boring records in Appendix A.

B.4 Atterberg Limits

Characterization of the fine-grained fractions of soils was evaluated using the Atterberg Limits. This test includes Liquid Limit and Plastic Limit tests to determine the Plasticity Index in accordance with ASTM D 4318. Results of these tests are presented on the boring records in Appendix A, are summarized in Table B-1, and are plotted on a Plasticity Chart in Figure B-1 of this Appendix.

B.5 Percent Passing No. 200 Sieve

Representative samples were dried, weighed, soaked in water until individual soil particles were separated, and then washed on the No. 200 sieve. The percentage of fines (soil passing No. 200 sieve) was determined for selected samples in accordance with ASTM D 1140. For selected samples the washed fraction retained on the No. 200 sieve was then screened on a No. 4 sieve, and the fraction retained on No. 4 was weighed to determine the percentage of gravel. For selected samples, the washed material retained on No. 200 sieve was shaken through a standard stack of sieves in accordance with ASTM D 422 to determine the grain size distribution. For selected samples, the grain size distribution of the fraction finer than No. 200 sieve was determined by Hydrometer Analysis in accordance with ASTM D 422. The relative proportion (or percentage) by dry weight of gravel (retained on No. 4 sieve), sand (passing No. 4 and retained on No. 200 sieve), and fines (passing No. 200 sieve) are listed on the boring records in Appendix A and summarized in Table B-1.

B.6 Direct Shear Test

To determine the drained shear strength parameters of the on-site soils, direct shear tests were performed on selected in situ samples and compacted remolded samples in accordance with ASTM D 3080. After the initial weight and volume measurements were made, the sample was placed in the shear machine, and a selected normal load was applied. The sample was saturated or kept at field moisture (to model worst case field conditions), allowed to consolidate under the selected normal load, and then sheared to failure. Shear rate was selected to maintain drained conditions. Shear stress and vertical/horizontal sample deformations were monitored throughout the test. The process was repeated on additional samples of the same soil material at two additional normal loads. The test results are presented in Figures B-2a through B-2e of this appendix.

B.7 One-Dimensional Consolidation

The consolidation characteristics of representative soil samples under incremental loading were evaluated by performing one-dimensional consolidation in general accordance with ASTM D 2435, using a floating ring consolidometer and dead weight system. Results of the tests are presented in Figures B-3a and B-3b.

B.8 Expansion Index

The expansion potential of the site soils was estimated using the Expansion Index Test in accordance with ASTM D 4829. The results of this test are illustrated in Figure B-4.

B.9 R-Value

Resistance “R” Value tests were performed by stabilometer method on selected bulk samples of the subgrade soils. The tests were conducted in general accordance with CTM 301. The test results are presented in Figures B-5a through B-5d.

B.10 Soil Corrosivity

Tests were performed in order to determine corrosion potential of site soils on concrete and ferrous metals. Corrosivity testing included minimum resistivity and soil pH (Caltrans Method 643), water-soluble chlorides (Caltrans Method 422), water-soluble sulfates (Caltrans Method 417) and electrical resistivity (Caltrans Method 643). The test results are summarized in Table B-2.

B.11 List of Attached Table and Figures

The following tables and figures are attached and complete this appendix:

List of Table

Table B-1	Summary of Laboratory Test Results
Table B-2	Summary of Corrosion Test Results

List of Figures

Figure B-1	Atterberg Limits Test Results
Figures B-2a through B-2e	Direct Shear Test Results
Figures B-3a and B-3b	Consolidation Test Results
Figure B-4	Expansion Index Test Results
Figures B-5a through B-5d	R-Value Test Results

GDC TABLE B-1 CALTRANS BORING LOGS.GPJ GDC2013.GDT 6/17/14

Boring No.	Sample No.	Depth (ft)	Sample Type	Geologic Unit	USCS Group Symbol	SPT N*60 (blows/ft)	Undrained Shear Strength, Su (ksf)			Moisture Content (%)	Dry Unit Weight (pcf)	Total Unit Wt (pcf)	Atterberg Limits			Grain Size Distribution (%) by dry weight			Clay	Other Tests
							Pocket Pen.	Mini Vane	UU Test				LL	PL	PI	Gravel	Sand	Fines		
A-13-001	B-1	2.0	BULK		CH															
A-13-001	R-2	5.0	MC		CH	27	3		24.8	95	119	56	25	31						
A-13-001	S-3	7.5	SPT		CH	10	3		27.4											
A-13-001	R-4	10.0	MC		CH	18	3		22.5	98	120									
A-13-001	S-5	15.0	SPT		CL	13	3.5		21.3						7	38	55			
A-13-001	R-6	20.0	MC		CH	41	2		21.7	101	123									
A-13-001	S-7	25.0	SPT		ML	68	4		22.8											
A-13-002	B-1	2.0	BULK		CH															
A-13-002	S-2	5.0	SPT		CH	11	3.5		23.8			53	23	30						
A-13-002	R-3	7.5	MC		CH	21	2.0		19.9	102	122									CN
A-13-002	S-4	10.0	SPT		CH	10	1.0		23.4											
A-13-002	R-5	15.0	MC		CH	26	2.5		18.1	109	129									DS
A-13-002	S-6	20.0	SPT		CH	16	1.5		25.7											
A-13-002	R-7	25.0	MC		Tcb	41	4.5		25.7	98	123	68	24	44						DS
A-13-002	S-8	30.0	SPT		Tcb	44	2.5		21.4											
A-13-002	R-9	35.0	MC		Tcb	48/6"	3.5		24.9	104	130									
A-13-002	S-10	40.0	SPT		Tcb	65	>4.5		22.4											
A-13-002	R-11	45.0	MC		Tcb	48/6"	>4.5		17.7	112	132									
A-13-002	S-12	50.0	SPT		Tcb	91	>4.5		16.4											
A-13-002	R-13	55.0	MC		Tcb	REF	>4.5		13.1	121	137									
A-13-002	S-14	60.0	SPT		Tcb	71/6"	4.0		12.1											
A-13-003	B-1	2.0	BULK		CH															
A-13-003	R-2	5.0	MC		CH	44	4.5		27.9	94	120									
A-13-003	S-3	7.5	SPT		Tcb	24	3.75		25.3			65	26	39						
A-13-003	R-4	10.0	MC		Tcb	44	4.5		28.4	93	119									
A-13-003	S-5	15.0	SPT		Tcb	57	>4.5		15.4											
A-13-003	R-6	20.0	MC		Tcb	48/6"	>4.5		13.6	114	130									
A-13-003	S-7	25.0	SPT		Tcb	REF	1.5		23.4											Corrosivity
A-13-003	R-8	30.0	MC		Tcb	REF	4.5		17.1	120	141									
A-13-003	S-9	35.0	SPT		Tcb	71/6"	>4.5		20.4											



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TABLE B-1: Summary of Laboratory Results

Project: Palo Comado Bridge Widening
 Location: Agoura Hills, CA
 Number: LA-1143

GDC TABLE B-1 CALTRANS BORING LOGS.GPJ GDC2013.GDT 6/17/14

Boring No.	Sample No.	Depth (ft)	Sample Type	Geologic Unit	USCS Group Symbol	SPT N*60 (blows/ft)	Undrained Shear Strength, Su (ksf)			Moisture Content (%)	Dry Unit Weight (pcf)	Total Unit Wt (pcf)	Atterberg Limits			Grain Size Distribution (%) by dry weight			Clay	Other Tests
							Pocket Pen.	Mini Vane	UU Test				LL	PL	PI	Gravel	Sand	Fines		
A-13-003	R-10	40.0	MC		Tcb	48/3"	>4.5			21.4	101	123								
A-13-003	S-11	45.0	SPT		Tcb	71/6"	>4.5			22.1										
A-13-003	R-12	50.0	MC		Tcb	REF	>4.5			20.0	98	118								
A-13-004	B-1	2.5	BULK		CH															
A-13-004	S-2	6.0	SPT		CH	8	3.25			17.3						0	33	67		
A-13-004	R-3	7.5	MC		CH	30	3.75			16.7	109	127								
A-13-004	S-4	10.0	SPT		CH	21	2.75			18.5										
A-13-004	R-5	15.0	MC		Tcb	26	3.75			26.9	95	121								
A-13-004	S-6	20.0	SPT		Tcb	42	>4.5			23.1										
A-13-004	R-7	25.0	MC		Tcb	48/6"	>4.5			21.5	104	126								CN
A-13-004	S-8	30.0	SPT		Tcb	48	>4.5			20.2										
A-13-004	R-9	35.0	MC		Tcb	48/6"	>4.5			19.5	109	130								
A-13-004	S-10	40.0	SPT		Tcb	65	>4.5			20.5										
A-13-004	R-11	45.0	MC		Tcb	REF	>4.5			20.1	107	129								
A-13-004	S-12	50.0	SPT		Tcb	REF	>4.5			15.1										
A-13-005	B-1	1.5	BULK		CH															
A-13-005	R-2	5.0	MC		CH	40	>4.5			18.9	105	125	58	27	31					
A-13-005	S-3	7.5	SPT		Tcb	41	>4.5			25.8										
A-13-005	R-4	10.0	MC		Tcb	57	>4.5			26.0	98	123								
A-13-005	S-5	15.0	SPT		Tcb	28	>4.5			25.3										
A-13-005	R-6	20.0	MC		Tcb	54	>4.5			21.4	104	126								
A-13-005	S-7	25.0	SPT		Tcb	38	3.5			19.1										
A-13-005	R-8	30.0	MC		Tcb	48/6"	>4.5			20.8	106	128								
A-13-005	S-9	35.0	SPT		Tcb	31	>4.5			20.4										
A-13-005	R-10	40.0	MC		Tcb	48/6"	>4.5			18.4	110	130								
A-13-005	S-11	45.0	SPT		Tcb	REF	>4.5			15.0										
A-13-005	R-12	50.0	MC		Tcb	48/6"	>4.5			19.9	109	131								
A-13-006	B-1	0.0	BULK		CH															Corrosivity, R
A-13-006	R-2	5.0	MC		CH	27	4.0			22.6	103	126								DS
A-13-006	S-3	7.5	SPT		CH	11	1.5			23.4					0	21	79			



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TABLE B-1: Summary of Laboratory Results

Project: Palo Comado Bridge Widening
 Location: Agoura Hills, CA
 Number: LA-1143

Boring No.	Sample No.	Depth (ft)	Sample Type	Geologic Unit	USCS Group Symbol	SPT N*60 (blows/ft)	Undrained Shear Strength, Su (ksf)			Moisture Content (%)	Dry Unit Weight (pcf)	Total Unit Wt (pcf)	Atterberg Limits			Grain Size Distribution (%) by dry weight			Clay	Other Tests
							Pocket Pen.	Mini Vane	UU Test				LL	PL	PI	Gravel	Sand	Fines		
A-13-006	R-4	10.0	MC		CH	24	1.5			21.3	101	123								DS
A-13-006	S-5	15.0	SPT		CH	14	3.5			22.1			57	18	39					
A-13-006	R-6	20.0	MC		Tcb	45	4.0			29.9	93	121								
A-13-006	S-7	25.0	SPT		Tcb	10	>4.5			28.5										
A-13-006	R-8	30.0	MC		Tcb	73	>4.5			31.1	92	121								DS
A-13-006	S-9	35.0	SPT		Tcb	40	>4.5			25.3										
A-13-006	R-10	40.0	MC		Tcb	REF	>4.5			25.1	101	126								
A-13-006	S-11	45.0	SPT		Tcb	71/6"	>4.5			19.9										
A-13-006	R-12	50.0	MC		Tcb	REF	>4.5			17.7	113	133								
A-13-006	S-13	55.0	SPT		Tcb	71/6"	>4.5			15.7										
A-13-006	R-14	60.0	MC		Tcb	REF	>4.5			18.2	103	122								
A-13-007	B-1	0.0	BULK		CH															R, EI

GDC TABLE B-1 CALTRANS BORING LOGS.GPJ GDC2013.GDT 6/17/14



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TABLE B-1: Summary of Laboratory Results

Project: Palo Comado Bridge Widening

Location: Agoura Hills, CA

Number: LA-1143

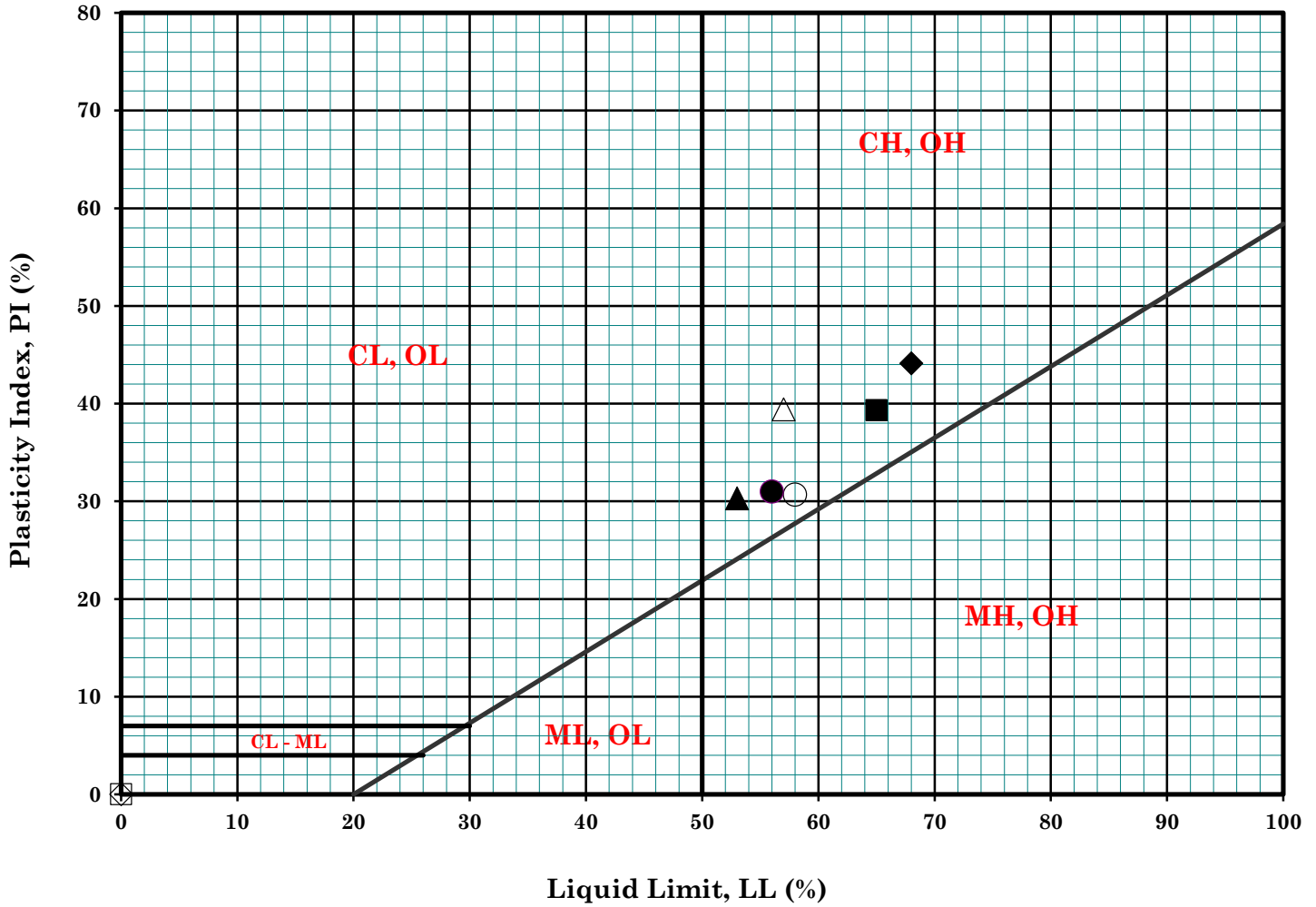
Sheet 3 of 3

TABLE B-2: SUMMARY OF CORROSION TEST RESULTS

Boring No	Sample No.	Depth (ft)	USCS Soil Type	Resistivity CTM 643 (ohm-cm)	pH CTM 643	Soluble Sulfate Content CTM 417 (ppm)	Soluble Chloride CTM 422 (ppm)
A-13-003	S-7	25	Tcb	NM	7.29	13250	< 0.01
A-13-006	B-1	0-5	CH	423	7.09	10500	< 0.01



PLASTICITY CHART



Symbol	Boring No.	Sample No.	Depth				MC (%)	LL (%)	PL (%)	PI (%)	Description
			(ft)	(m)	(ft)	(m)					
●	A-13-001	R2	5.0	6.5	1.5	2.0	24.8	56	25	31	Fat Clay (CH)
▲	A-13-002	S-2	5.0	6.5	1.5	2.0	23.8	53	23	30	Fat Clay (CH)
◆	A-13-002	R-7	25.0	26.5	7.6	8.1	25.7	68	24	44	Calabasas Formation (Tcb)
■	A-13-003	S-3	7.5	9.0	2.3	2.7	25.3	65	26	39	Calabasas Formation (Tcb)
○	A-13-005	R-2	5.0	6.5	1.5	2.0	18.9	58	27	31	Fat Clay (CH)
△	A-13-006	S-5	15.0	16.5	4.6	5.0	22.1	57	18	39	Fat Clay (CH)

Remark : _____



Palo Comado Bridge Widening

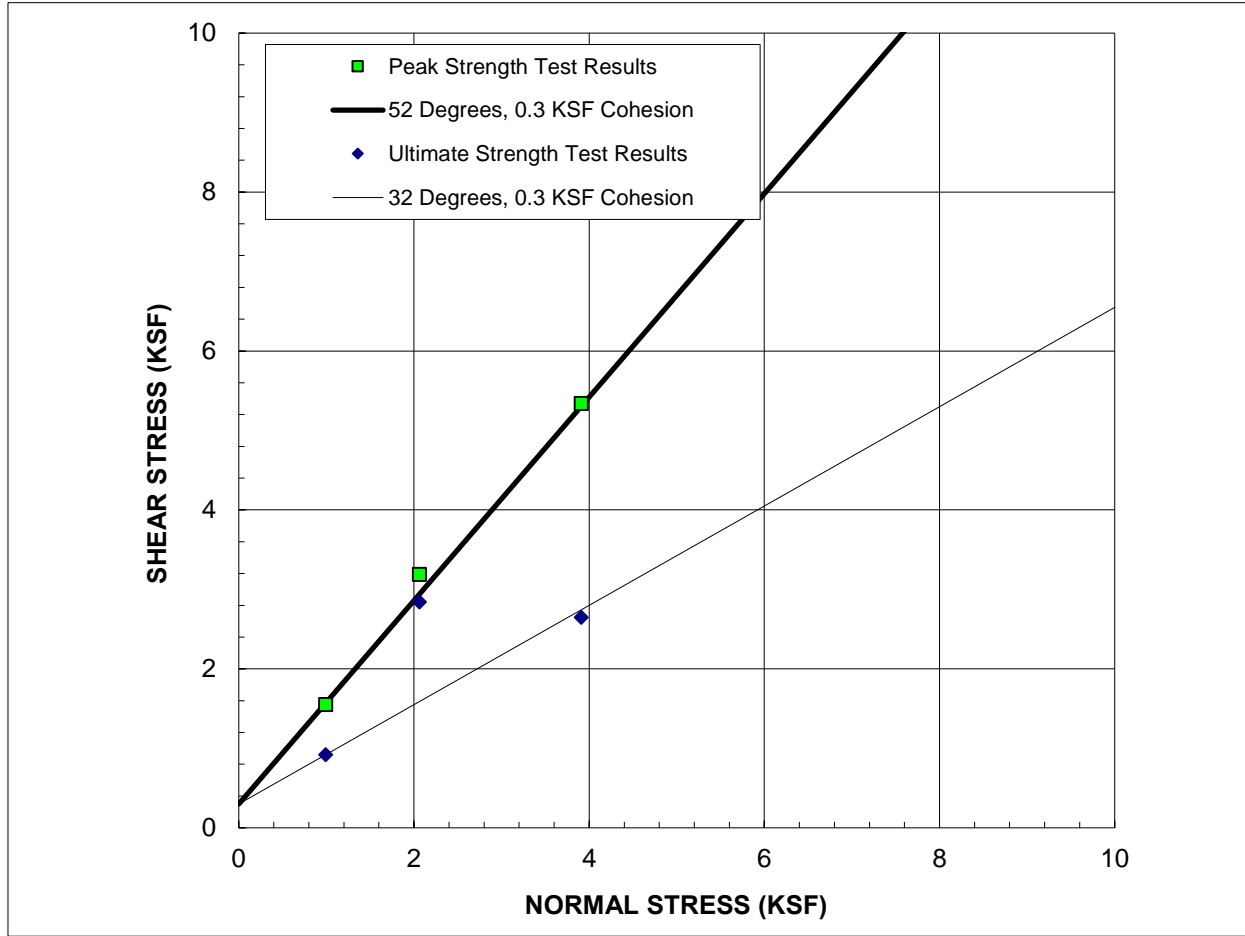
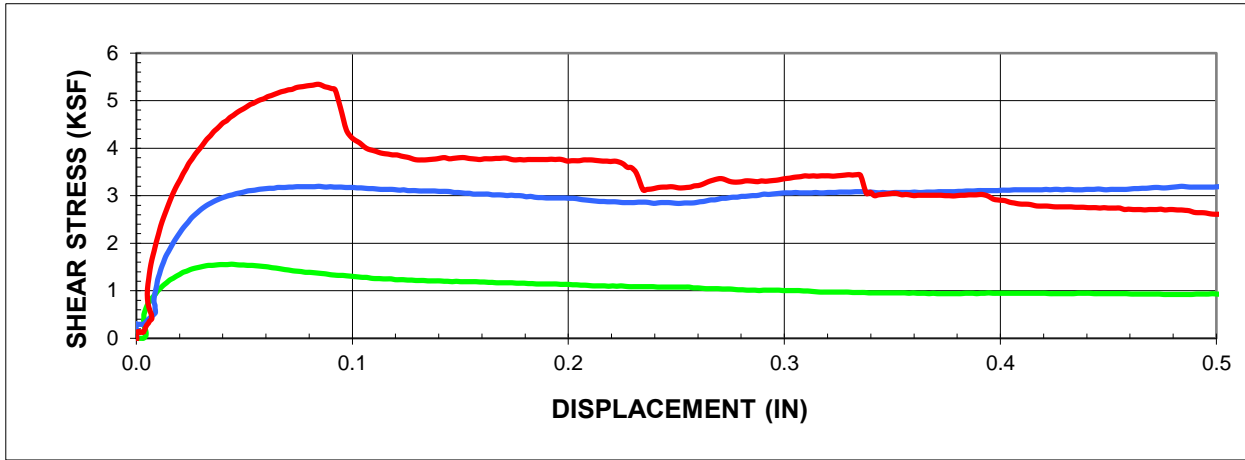
Project No. : LA-1143

Date : 9/30/13

ATTERBERG LIMITS

(ASTM D-4318-84)

FIGURE B-1



SAMPLE: A-13-002 R5@15'

Description: CH

PEAK

ϕ'	52 °
c'	0.30 KSF

ULTIMATE

	32 °
	0.30 KSF

STRAIN RATE: 0.0025 IN/MIN
(Sample was consolidated and drained)

IN-SITU

γ_d	109.0 PCF
w_c	18.1 %

AS-TESTED

	109.0 PCF
	28.8 %

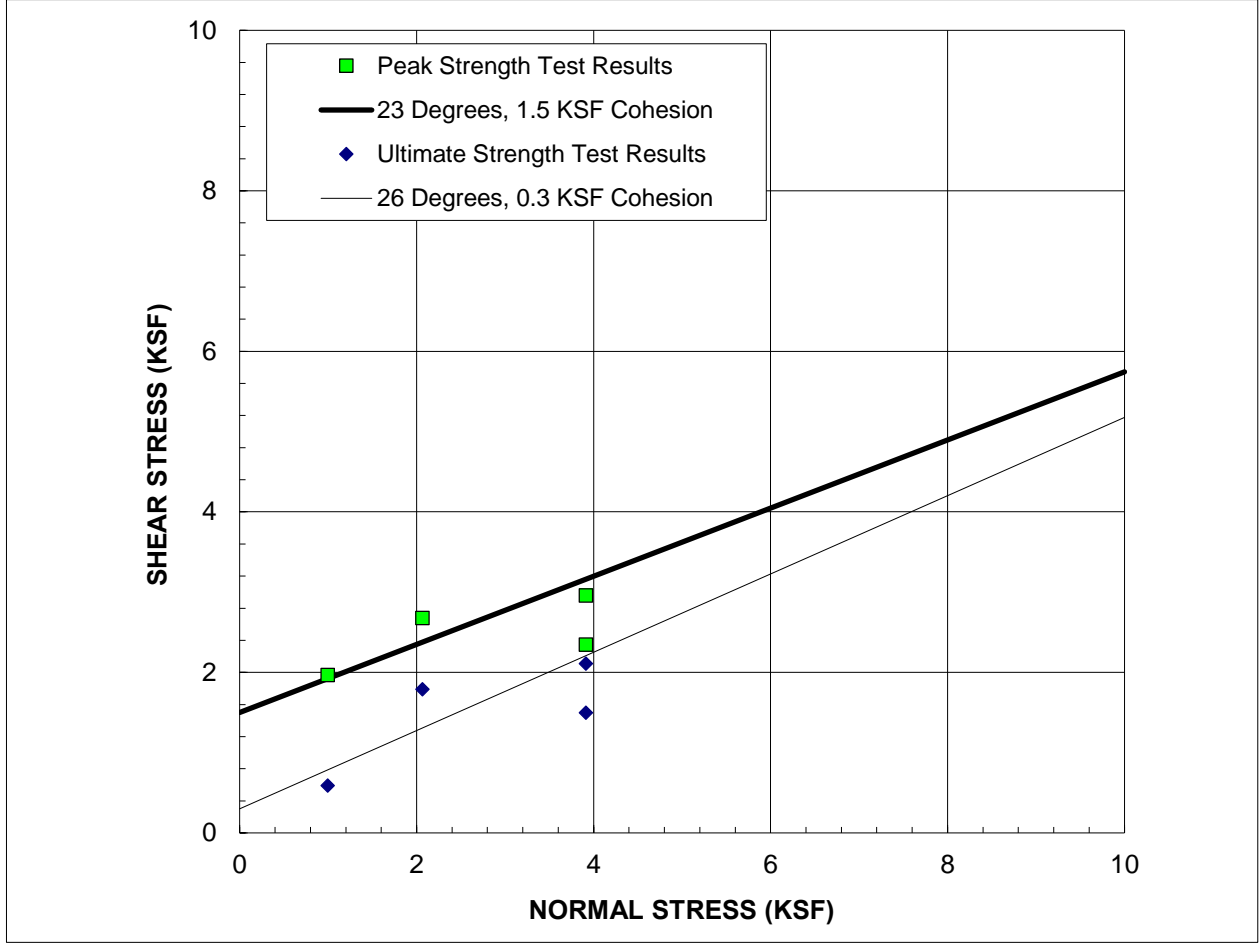
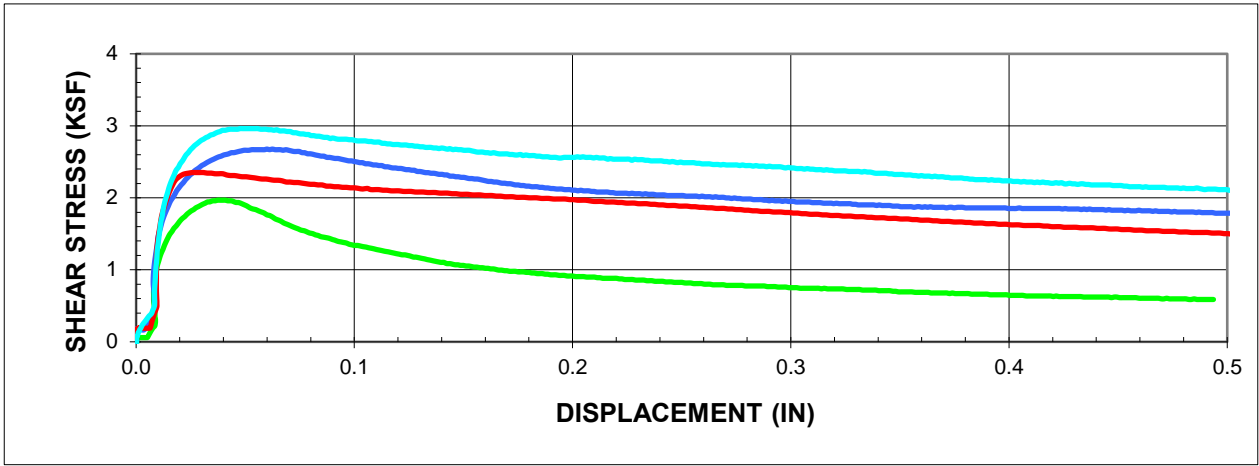


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DIRECT SHEAR TEST RESULTS

Project No.: LA - 1143

FIGURE B-2a



SAMPLE: A-13-002 R7@25'

Description: Tcb- Calabasas Formation

STRAIN RATE: 0.0025 IN/MIN
(Sample was consolidated and drained)

PEAK

ϕ'	23 °
c'	1.50 KSF

IN-SITU

γ_d	98.0 PCF
w_c	25.7 %

ULTIMATE

ϕ'	26 °
c'	0.30 KSF

AS-TESTED

γ_d	98.0 PCF
w_c	30.9 %

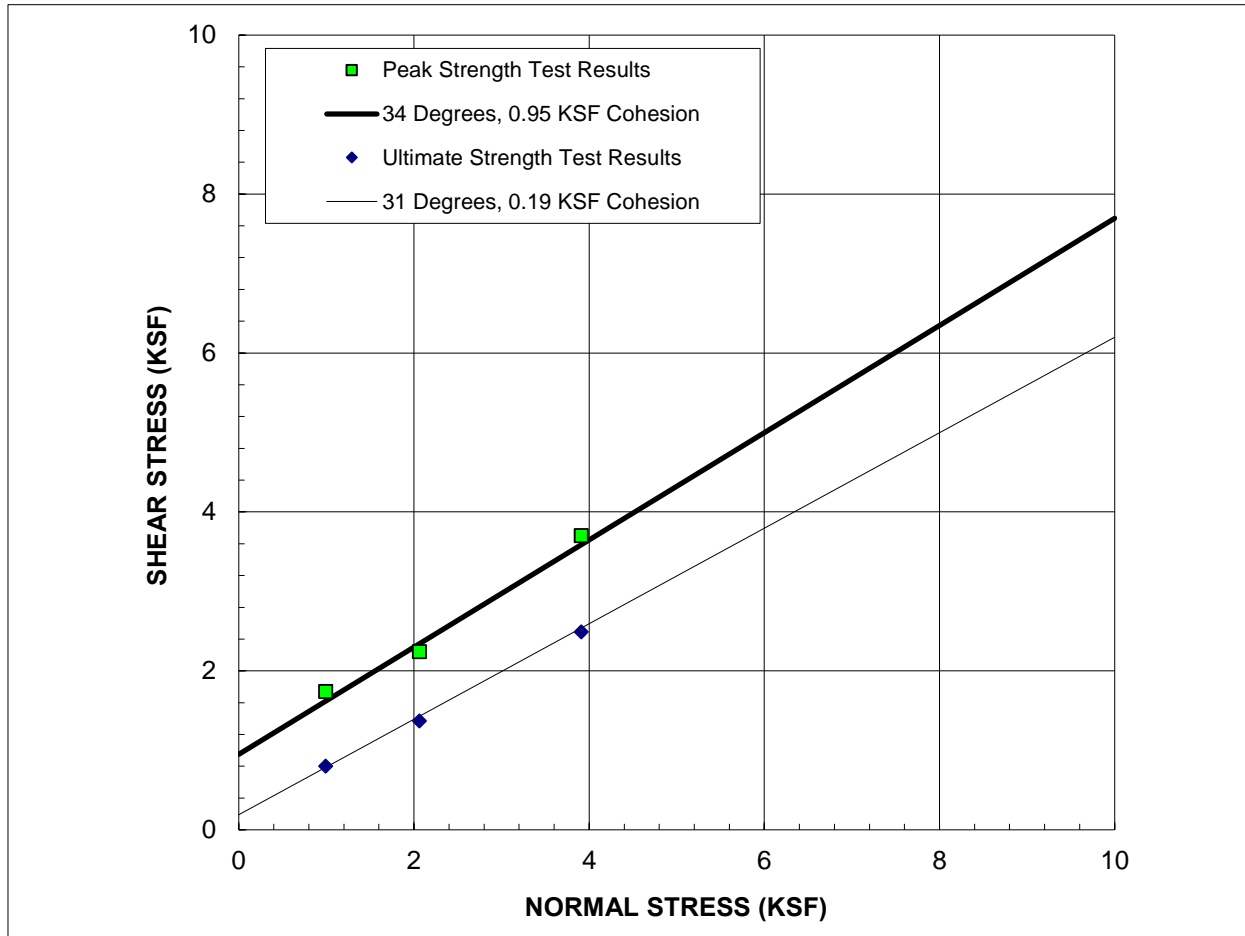
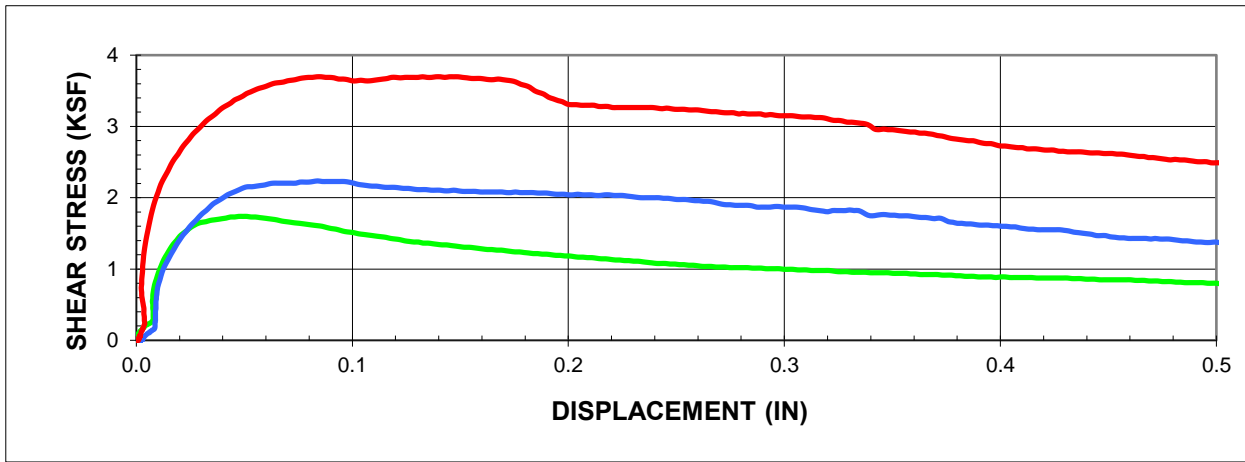


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DIRECT SHEAR TEST RESULTS

Project No.: LA-1143

FIGURE B-2b



SAMPLE: A-13-006 R2@5'

Description: CH

PEAK

ϕ'	34 °
c'	0.95 KSF

ULTIMATE

ϕ'	31 °
c'	0.19 KSF

STRAIN RATE: 0.0025 IN/MIN
(Sample was consolidated and drained)

IN-SITU

γ_d	103.0 PCF
w_c	22.6 %

AS-TESTED

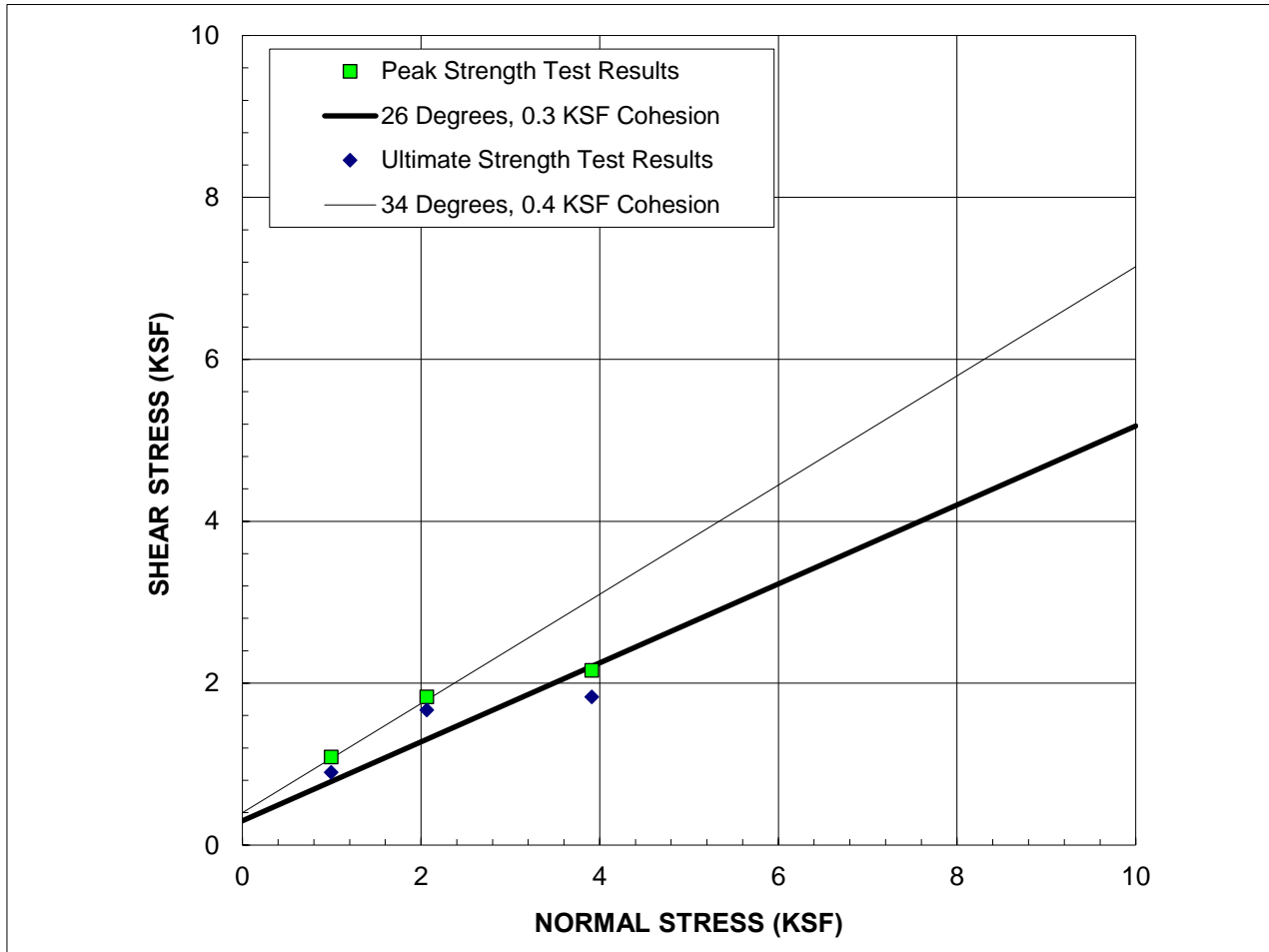
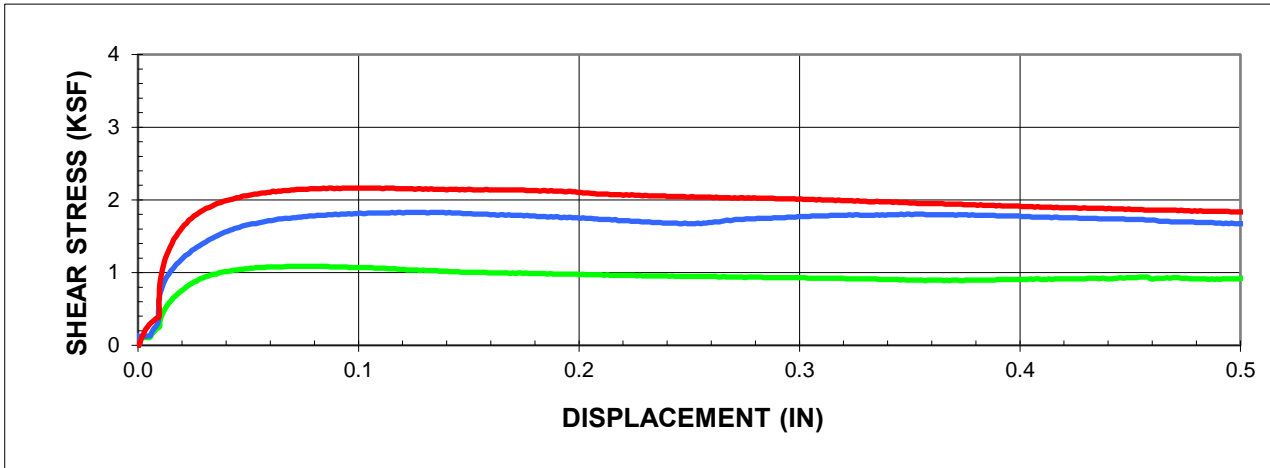
γ_d	104.5 PCF
w_c	26.3 %



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DIRECT SHEAR TEST RESULTS

Project LA- 1143
FIGURE B-2c



SAMPLE: A-13-006 R4@10'

Description: CH

PEAK

ϕ'	26 °
c'	0.30 KSF

ULTIMATE

	34 °
	0.40 KSF

STRAIN RATE: 0.0025 IN/MIN
(Sample was consolidated and drained)

IN-SITU

γ_d	101 PCF
w_c	21.3 %

AS-TESTED

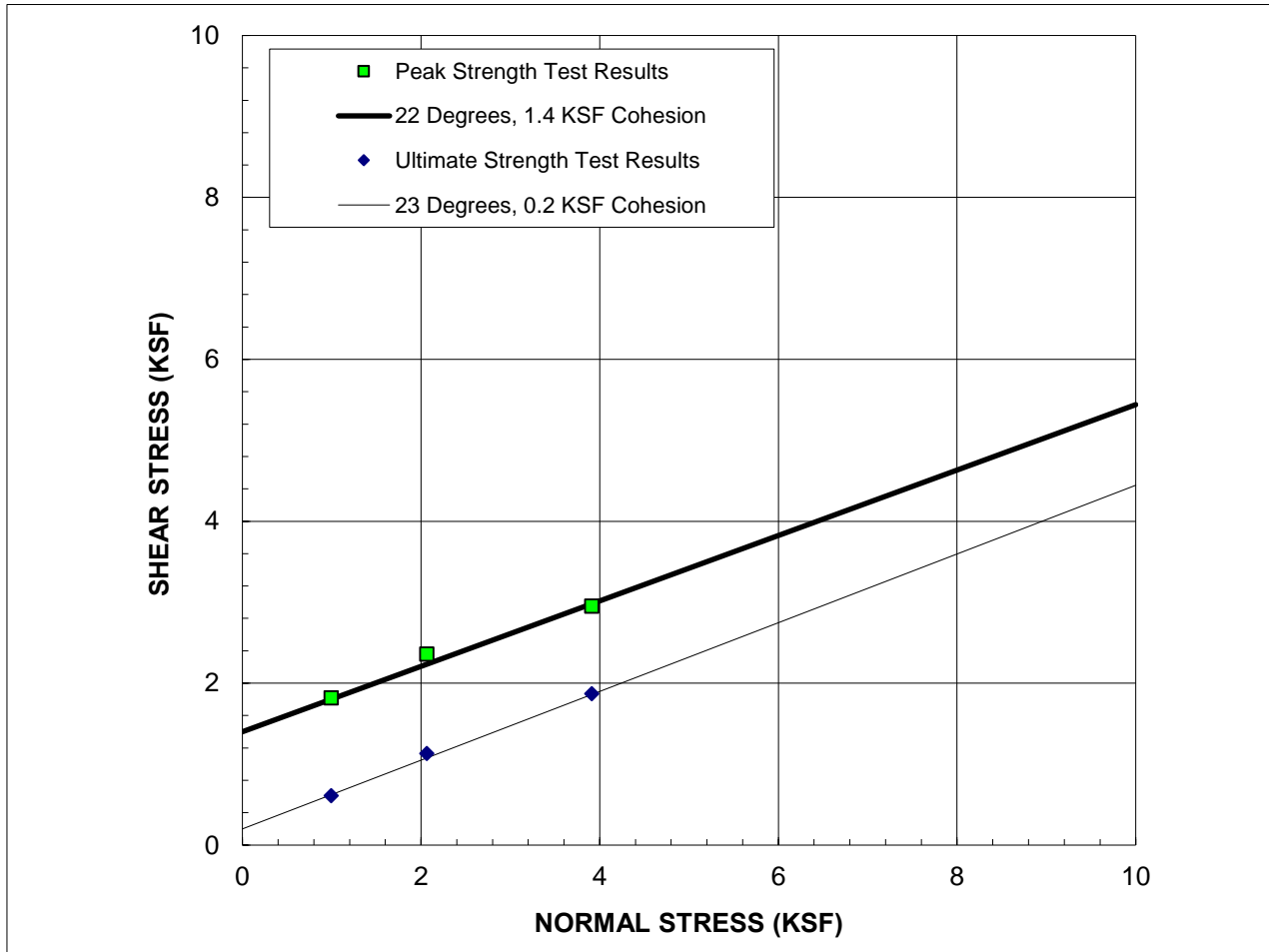
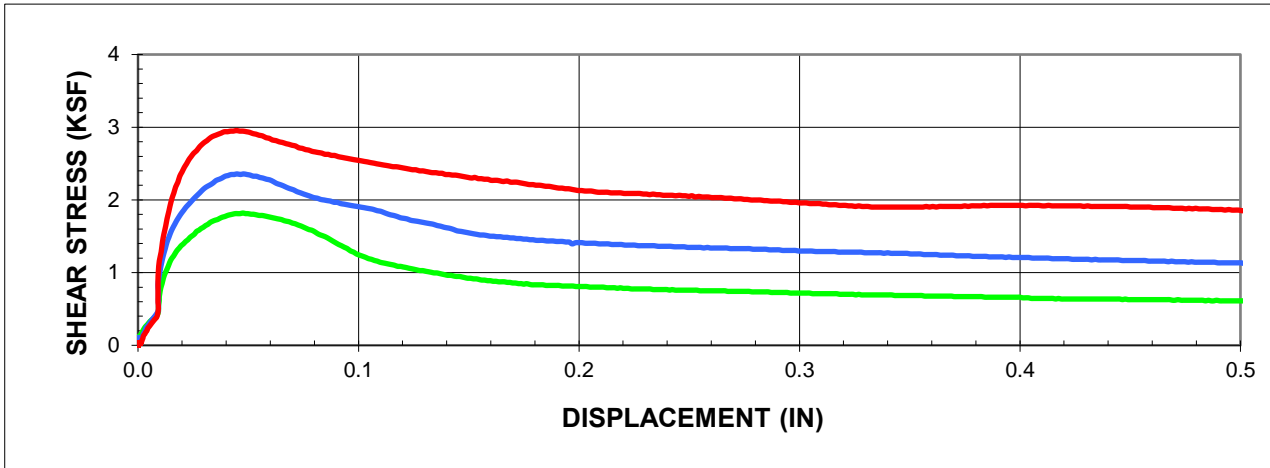
	101 PCF
	26.2 %



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DIRECT SHEAR TEST RESULTS

Project No.: LA1143
FIGURE B-2d



SAMPLE: A-13-006 R8@30'

Description: Calabasas Formation (Tcb)

PEAK

ϕ'	22 °
c'	1.40 KSF

ULTIMATE

ϕ'	23 °
c'	0.20 KSF

STRAIN RATE: 0.0025 IN/MIN
(Sample was consolidated and drained)

IN-SITU

γ_d	92.0 PCF
w_c	31.1 %

AS-TESTED

γ_d	92.0 PCF
w_c	33.1 %

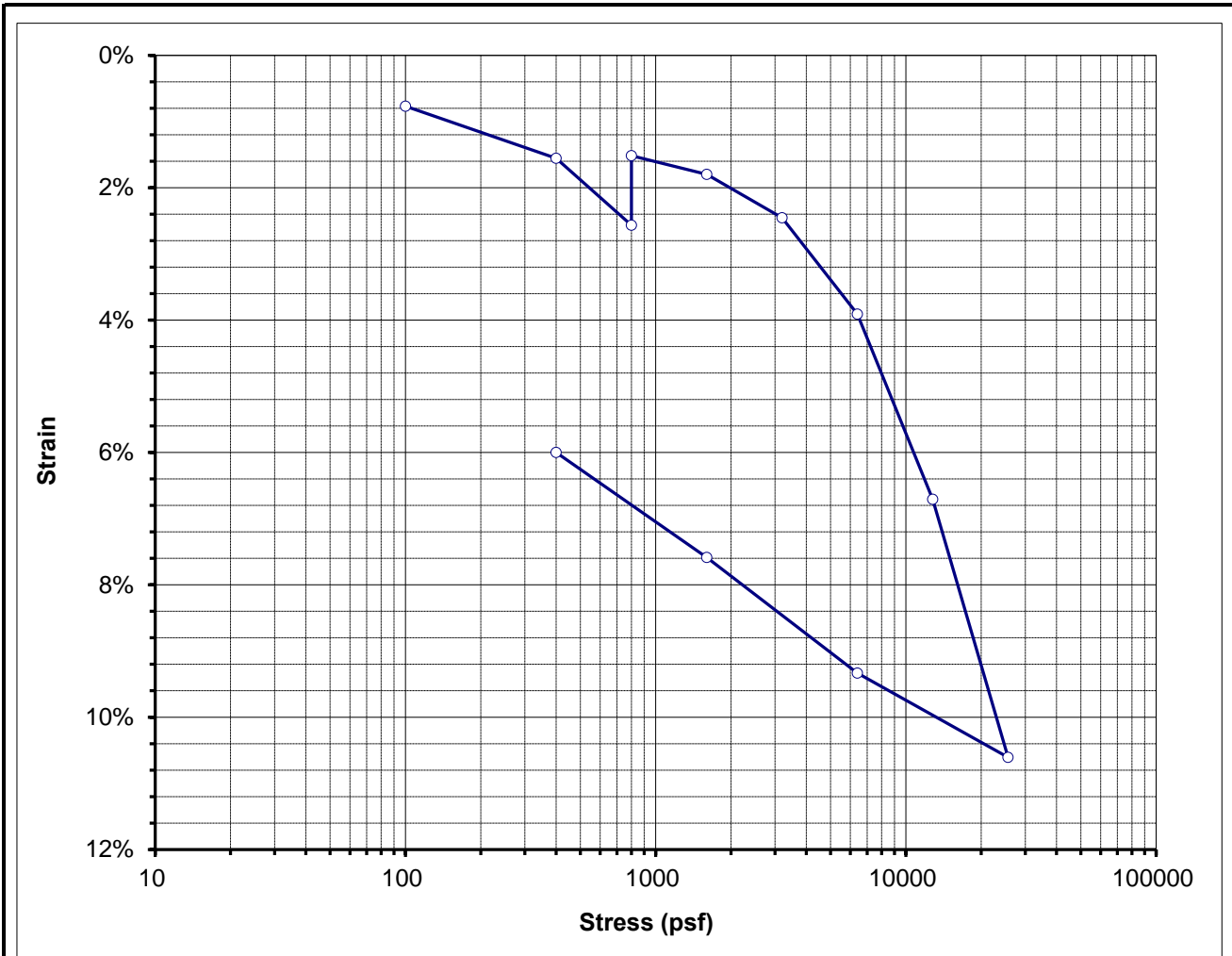


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DIRECT SHEAR TEST RESULTS

Project No.: LA-1143
FIGURE B-2e

CONSOLIDATION TEST RESULTS ASTM D-2435



Boring No.	A-13-002	Sample Depth	7.5 ft
Sample No.	R3	USCS	CH
Depth (feet)			

BEFORE TEST	Initial Moisture Content:	25.6%	
	Initial Dry Unit Wt.:	96.8	pcf
	Initial Total Unit Wt.:	121.7	pcf
	Initial Void Ratio:	0.8202	
	Initial Degree of Saturation:	88.3%	
AFTER TEST	Final Moisture Content:	25.8%	
	Final Dry Unit Wt.:	102.0	pcf
	Final Total Unit Wt.:	128.3	pcf
	Final Void Ratio:	0.7282	
	Final Degree of Saturation:	100.0%	
	Water Added at:	800	psf

PRESSURE (psf)	SAMPLE STRAIN	VOID RATIO
100	0.77%	0.8062
400	1.56%	0.7919
800	2.57%	0.7735
800	1.52%	0.7926
1600	1.80%	0.7874
3200	2.45%	0.7755
6400	3.91%	0.7490
12800	6.71%	0.6981
25600	10.61%	0.6271
6400	9.33%	0.6503
1600	7.59%	0.6821
400	6.00%	0.7110

ATTERBERG LIMITS					
LL=	53	PL=	23	PI=	30

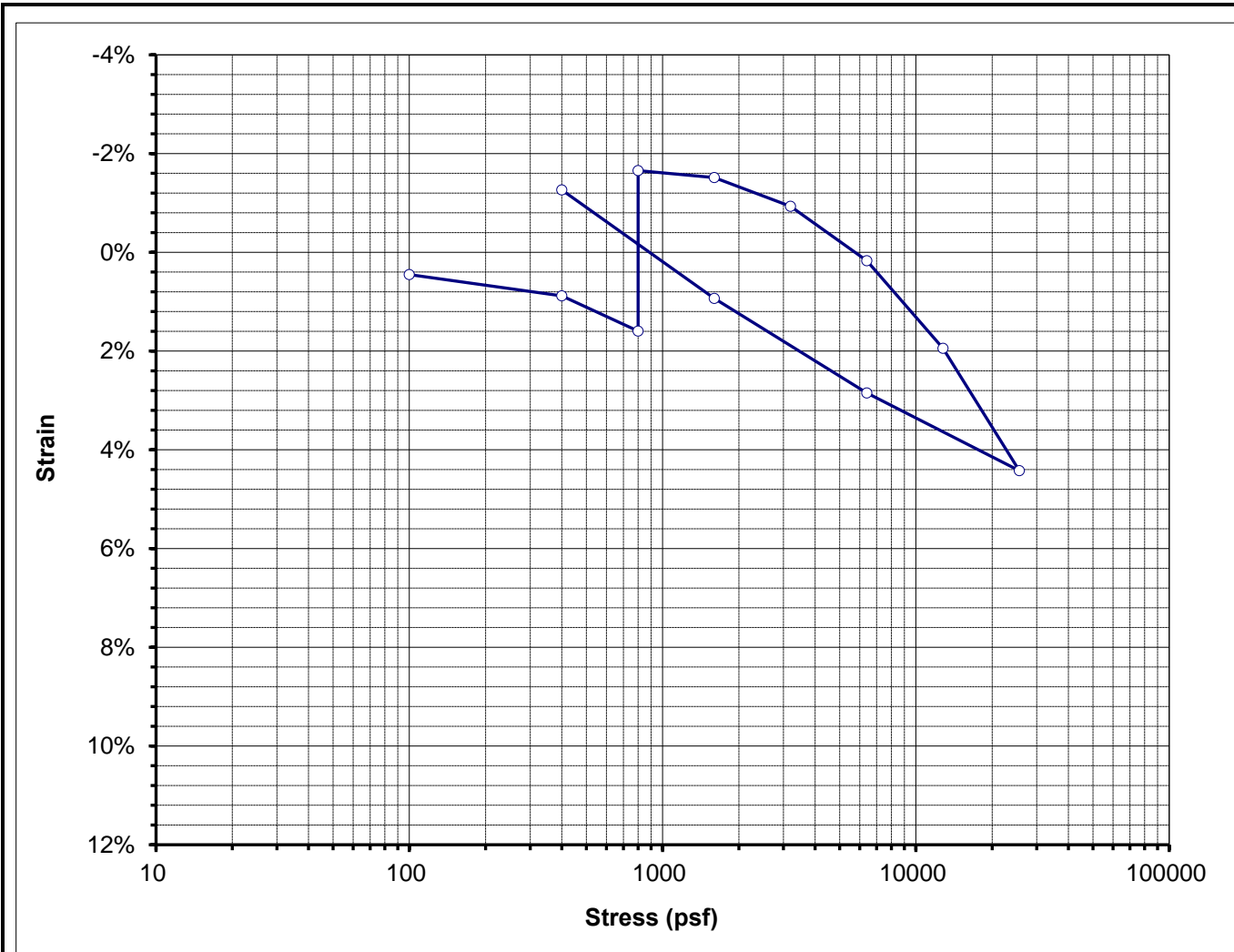
Assumed Specific Gravity of Solids, G_s: 2.83

PROJECT NUMBER: LA - 1143 PROJECT NAME: Palo Comado Bridge Widening

FIGURE B-3a



CONSOLIDATION TEST RESULTS ASTM D-2435



Boring No. A-13-004 Sample Depth 25 ft
 Sample No. R7 USCS Tcb

BEFORE TEST

Initial Moisture Content:	22.7%
Initial Dry Unit Wt.:	103.4 pcf
Initial Total Unit Wt.:	126.8 pcf
Initial Void Ratio:	0.9441
Initial Degree of Saturation:	77.3%

AFTER TEST

Final Moisture Content:	26.9%
Final Dry Unit Wt.:	107.6 pcf
Final Total Unit Wt.:	136.6 pcf
Final Void Ratio:	0.8673
Final Degree of Saturation:	99.9%

Water Added at: 800 psf

ATTERBERG LIMITS					
LL=	N/M	PL=	N/M	PI=	N/M

Assumed Specific Gravity of Solids, Gs: 3.22

PRESSURE (psf)	SAMPLE STRAIN	VOID RATIO
100	0.45%	0.9353
400	0.88%	0.9269
800	1.59%	0.9131
800	-1.65%	0.9763
1600	-1.51%	0.9735
3200	-0.93%	0.9622
6400	0.17%	0.9408
12800	1.95%	0.9063
25600	4.42%	0.8581
6400	2.85%	0.8887
1600	0.93%	0.9259
400	-1.26%	0.9687

PROJECT NUMBER: LA-1143

PROJECT NAME: Palo Comado Bridge Widening

FIGURE B-3b



EXPANSION INDEX OF SOIL

ASTM D-4829-10 / UBC 29-2

Project Name : <u>Palo Comado Bridge Widening</u>	Sampled By : <u>Steve S.</u>	Date : _____
Project No. : <u>LA-1143</u>	Prepared By : <u>Eric Y.</u>	Date : <u>09/21/13</u>
Boring No. : <u>HA-13-007</u>	Test By : <u>Eric Y.</u>	Date : <u>09/23/13</u>
Sample No. : <u>B-1</u>	Calculated By : <u>Eric Y.</u>	Date : <u>09/24/13</u>
Depth (ft/m) : <u>0-5</u> ###	Checked By : _____	Date : _____
Location : _____		
Description : <u>Fat Clay (CH)</u>		

Sample Preparation						
Weight of Total Soil	3271.50	Weight of Soil Retained on No. 4 Sieve	50.70	% Passing No. 4 Sieve	98.45	
Trail	Field	2	3	4	Tested	M & D After Test
Container No.	SP3	SP3				Container No.
Weight of Wet Soil + Container (gm)	577.60	411.70				Wet Soil+Cont.+Ring
Weight of Dry Soil + Container (gm)	512.60	381.10				Dry Soil+Cont.+Ring
Weight of Container (gm)	192.10	192.10				Wt. of Container
Moisture Content (%)	20.28	16.19			16.19	Moisture Content
Weight of Wet Soil + Ring (gm)	565.20	552.90				
Weight of Ring (gm) No. 1.0	202.58	202.58			202.58	
Weight of Wet Soil (gm)	362.62	350.32				
Wet Density of Soil (pcf)	109.38	105.67				Wet Density (pcf)
Dry Density of Soil (pcf)	90.94	90.95				Dry Density (pcf)
Precent Saturation of Soil S _(Meas.)	64.15	51.22			51.22	(%) Saturation

Loading Machine No.				
Date	Reading Time	Elapsed Time	Dial Reading	Expansion
09/23/13	8:50:00	0:10:00		0.0000
09/23/13				
09/23/13	9:00:00	0:00:00	0.5000	0.0000
Add Distilled Water to Sample				
			0.5000	0.0000
	10:00:00	1:00:00	0.5770	0.0770
	11:00:00	2:00:00	0.5800	0.0800
	12:00:00	3:00:00	0.5820	0.0820
	14:00:00	5:00:00	0.5830	0.0830
	17:00:00	8:00:00	0.5840	0.0840
09/24/13	7:30:00	22:30:00	0.5850	0.0850
09/24/13	9:00:00	0:00:00	0.5850	0.0850
Remark :				

1. Screen sample through **No. 4** Sieve

2. Sample should be compacted into a metal ring of the Degree of Saturation of **50 +/- 2% (48 - 52)**.

3. Inundated sample in distilled water to 24 h, or until the rate of expansion > (0.0002 in./h), no less than 3 h.

Volume of Mold (ft ³)	0.00731	Specific Gravity	2.70
Rammer Weight (lb.)	5.0	Blows/Layer	15
Vertical Confining Pressure	1.0 (lb/in ²) / 6.9 (kPa)		

(%) S = $\frac{S.G. \times W \times Dd}{Wd \times S.G. - Dd}$ S.G.=Specific Gravity, W=Water Content
 Dd=Dry Soil Density, Wd=Unit Wt. of Water

E.I. _(meas) = $\frac{\text{Change in High}}{\text{Initial Thickness}} \times 1000 = 85.00$

$$\text{Expansion Index}_{(50)} = EI_{(meas.)} - (50 - S_{(meas.)}) \times \frac{65 + EI_{(meas.)}}{220 - S_{(meas.)}}$$

86	Medium
-----------	---------------

Expansion Index	Potential Expansion
0 - 20	Very Low
21 - 50	Low
51 - 90	Medium
91 - 130	High
> 130	Very High

SAMPLE NO.: HA-13-007

SAMPLE DATE: 9/9/13

SAMPLE LOCATION: B-1 @ 0' - 5'

TEST DATE: 9/27/13

SAMPLE DESCRIPTION: Dark yellow brown lean clay (CL)

LABORATORY TEST DATA

TEST SPECIMEN	1	2	3	4	5	
A COMPACTOR PRESSURE	130	160	200			[PSI]
B INITIAL MOISTURE	16.9	16.9	16.9			[%]
C BATCH SOIL WEIGHT	1200	1200	1200			[G]
D WATER ADDED	120	112	104			[ML]
E WATER ADDED (D*(100+B)/C)	11.7	10.9	10.1			[%]
F COMPACTION MOISTURE (B+E)	28.6	27.8	27.0			[%]
G MOLD WEIGHT	2111.6	2114.6	2099.0			[G]
H TOTAL BRIQUETTE WEIGHT	3151.1	3110.0	3087.2			[G]
I NET BRIQUETTE WEIGHT (H-G)	1039.5	995.4	988.2			[G]
J BRIQUETTE HEIGHT	2.65	2.52	2.48			[IN]
K DRY DENSITY (30.3*I/((100+F)*J))	92.4	93.6	95.0			[PCF]
L EXUDATION LOAD	3200	4479	5976			[LB]
M EXUDATION PRESSURE (L/12.54)	255	357	477			[PSI]
N STABILOMETER AT 1000 LBS	53	48	42			[PSI]
O STABILOMETER AT 2000 LBS	123	112	103			[PSI]
P DISPLACEMENT FOR 100 PSI	4.46	4.34	4.27			[Turns]
Q R VALUE BY STABILOMETER	14	20	24			
R CORRECTED R-VALUE (See Fig. 14)	16	20	24			
S EXPANSION DIAL READING	0.0031	0.0046	0.0069			[IN]
T EXPANSION PRESSURE (S*43,300)	134	199	299			[PSF]
U COVER BY STABILOMETER	1.55	1.48	1.40			[FT]
V COVER BY EXPANSION	1.03	1.53	2.30			[FT]

TRAFFIC INDEX:

7.5

GRAVEL FACTOR:

1.30

UNIT WEIGHT OF COVER [PCF]:

130

R-VALUE BY EXUDATION:

17

R-VALUE BY EXPANSION:

20

R-VALUE AT EQUILIBRIUM:

17

*Note: Gravel factor estimated from pavement section using CTM 301, Section C, Part b.



370 Amapola Ave., Suite 212, Torrance, CA 90501
32 Mauchly, Suite B, Irvine, CA 92618
4201 Santa Ana St., Suite F, Ontario, CA 91761
9245 Activity Road, Suite 103, San Diego, CA 92126

R-VALUE TEST RESULTS

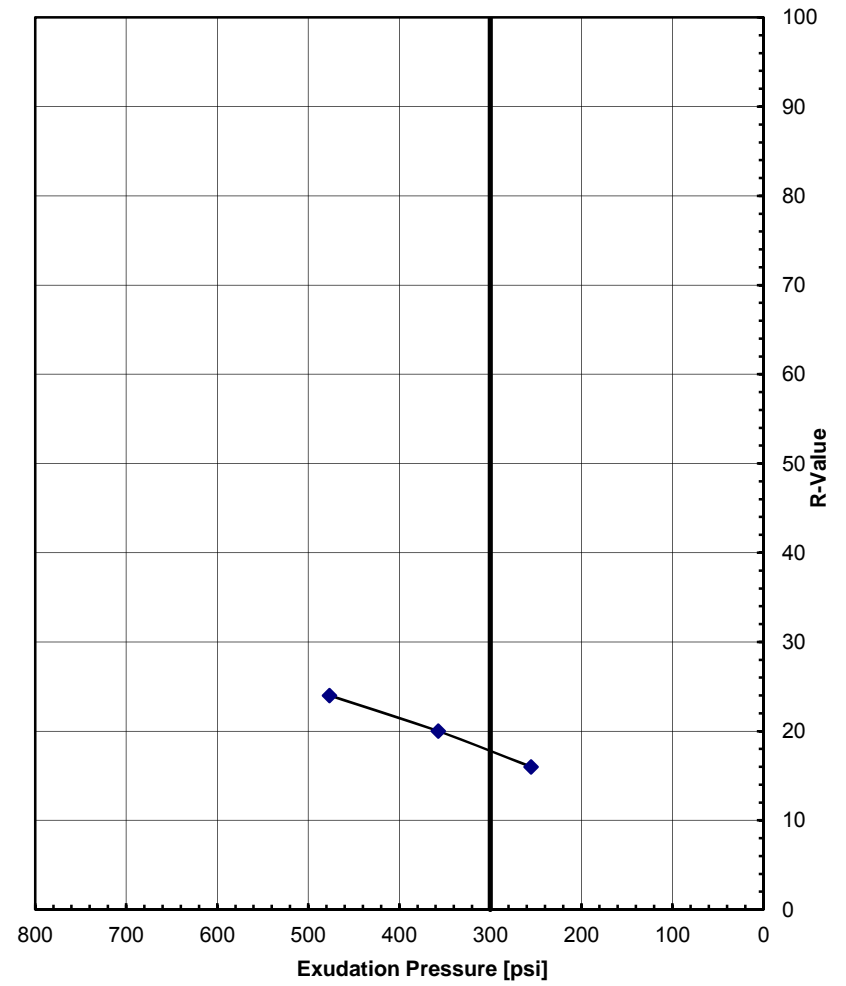
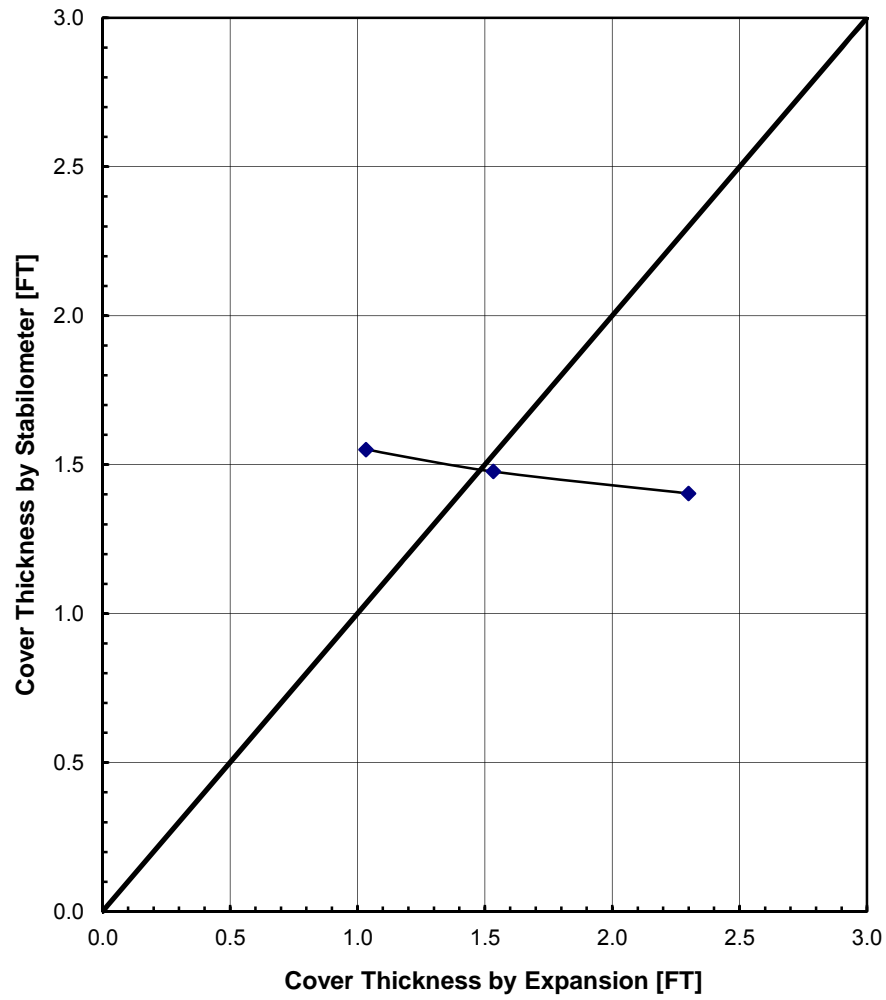
Document No. 13-0194

Project No. LA1143

FIGURE B-5a

Sample: HA-13-007, B-1 @ 0' - 5'

R-Value at Equilibrium: 17



370 Amapola Ave., Suite 212, Torrance, CA 90501
32 Mauchly, Suite B, Irvine, CA 92618
4201 Santa Ana St., Suite F, Ontario, CA 91761
9245 Activity Road, Suite 103, San Diego, CA 92126

COVER AND EXUDATION CHARTS

Document No. 13-0194

Project No. LA1143

FIGURE B-5b

BORING NO.: A-13-006, B-1

SAMPLE DATE: 6/23/14

BORING LOCATION: 0-5'

TEST DATE: 6/26/14

SAMPLE DESCRIPTION: Dark yellow brown fat clay (CH)

LABORATORY TEST DATA

TEST SPECIMEN	1	2	3	4	5	
A COMPACTOR PRESSURE	145	100	80			[PSI]
B INITIAL MOISTURE	6.0	6.0	6.0			[%]
C BATCH SOIL WEIGHT	1100	1100	1100			[G]
D WATER ADDED	140	160	185			[ML]
E WATER ADDED (D*(100+B)/C)	13.5	15.4	17.8			[%]
F COMPACTION MOISTURE (B+E)	19.5	21.4	23.8			[%]
G MOLD WEIGHT	2108.0	2113.3	2111.5			[G]
H TOTAL BRIQUETTE WEIGHT	3162.0	3136.6	3167.3			[G]
I NET BRIQUETTE WEIGHT (H-G)	1054.0	1023.3	1055.8			[G]
J BRIQUETTE HEIGHT	2.53	2.51	2.64			[IN]
K DRY DENSITY (30.3*I/((100+F)*J))	105.6	101.7	97.9			[PCF]
L EXUDATION LOAD	7795	5567	3427			[LB]
M EXUDATION PRESSURE (L/12.54)	622	444	273			[PSI]
N STABILOMETER AT 1000 LBS	50	59	66			[PSI]
O STABILOMETER AT 2000 LBS	121	135	144			[PSI]
P DISPLACEMENT FOR 100 PSI	3.94	4.47	5.72			[Turns]
Q R VALUE BY STABILOMETER	17	9	5			
R CORRECTED R-VALUE (See Fig. 14)	17	9	5			
S EXPANSION DIAL READING	0.0041	0.0022	0.0010			[IN]
T EXPANSION PRESSURE (S*43,300)	178	95	43			[PSF]
U COVER BY STABILOMETER	0.80	0.88	0.92			[FT]
V COVER BY EXPANSION	1.37	0.73	0.33			[FT]

TRAFFIC INDEX:	4.5
GRAVEL FACTOR:	1.49
UNIT WEIGHT OF COVER [PCF]:	130
R-VALUE BY EXUDATION:	6
R-VALUE BY EXPANSION:	10
R-VALUE AT EQUILIBRIUM:	6

*Note: Gravel factor estimated from required AC pavement section using CT301, Part 6.B.2.



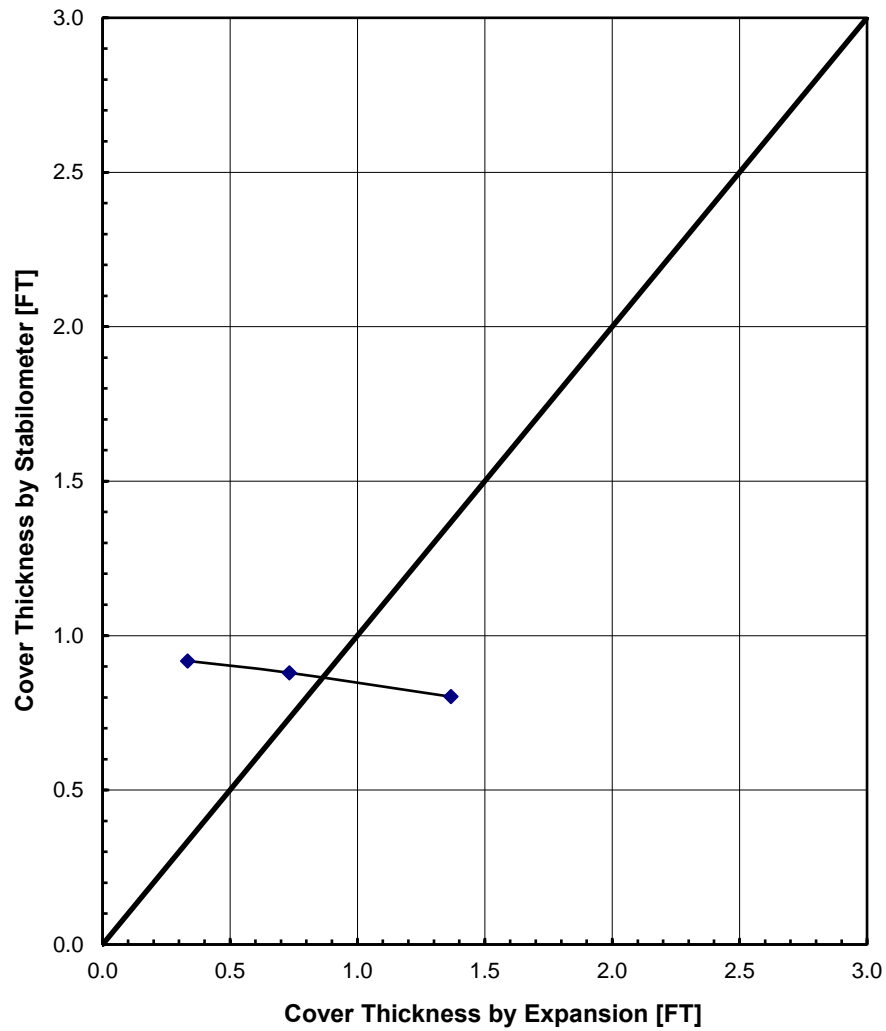
GROUP DELTA

R-VALUE TEST RESULTS

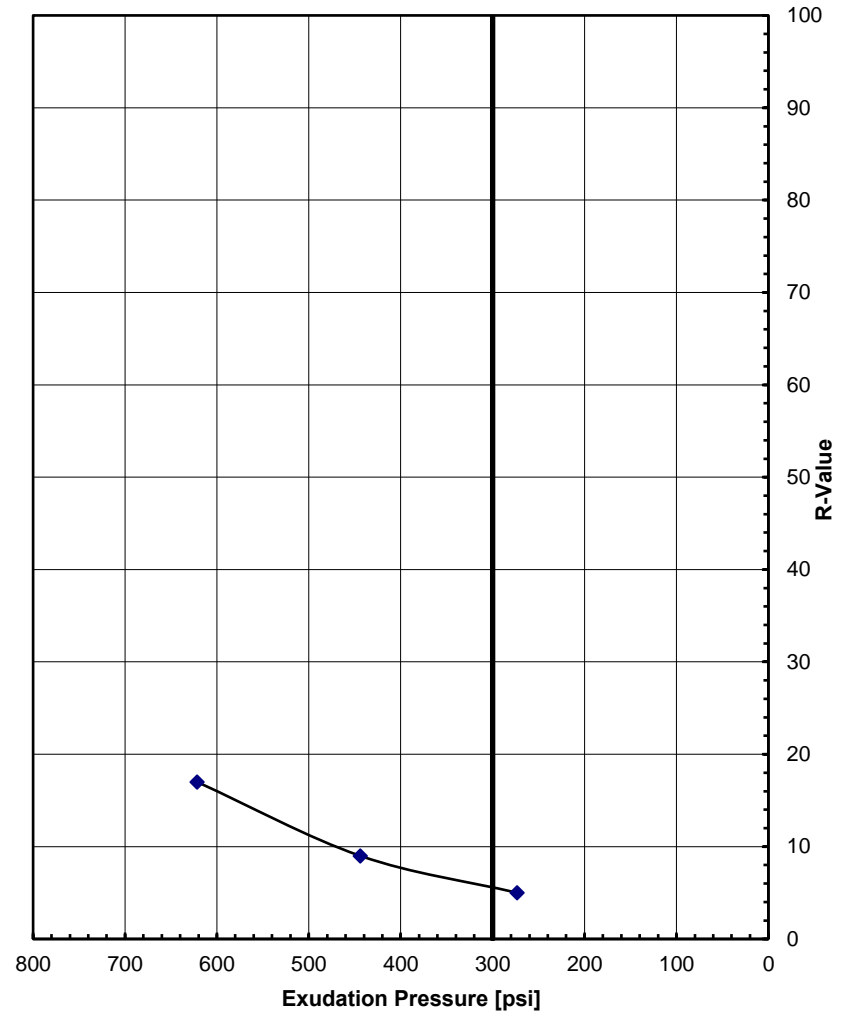
Document No.
Project No. LA1143

FIGURE B-5c

Sample A-13-006, B-1



R-Value at Equilibrium: 6

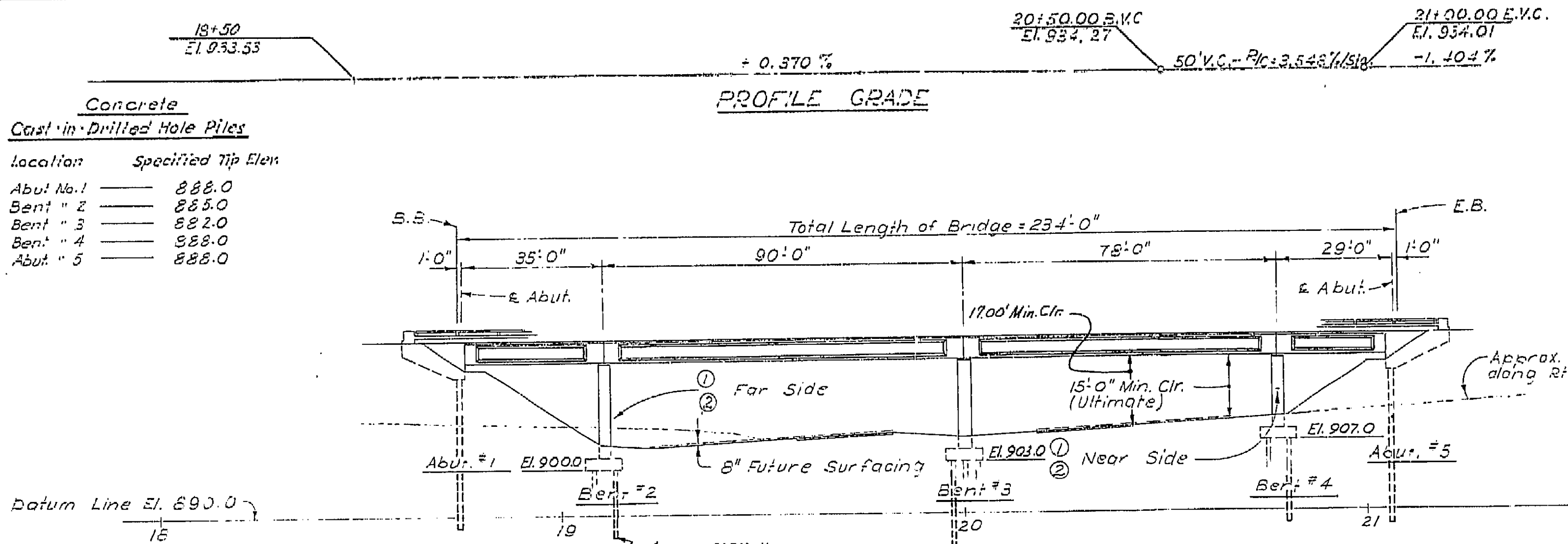


Appendix C As-Built Plans and LOTB

FED. ROAD DIST. NO.	STATE	PROJ. NO.	SHEET NO.	TOTAL SHEETS
7	CALIF.		57	151

DIST.	COUNTY	ROUTE	SECTION	POST MILE	TOTAL MILES
VII	LA	5		101	15

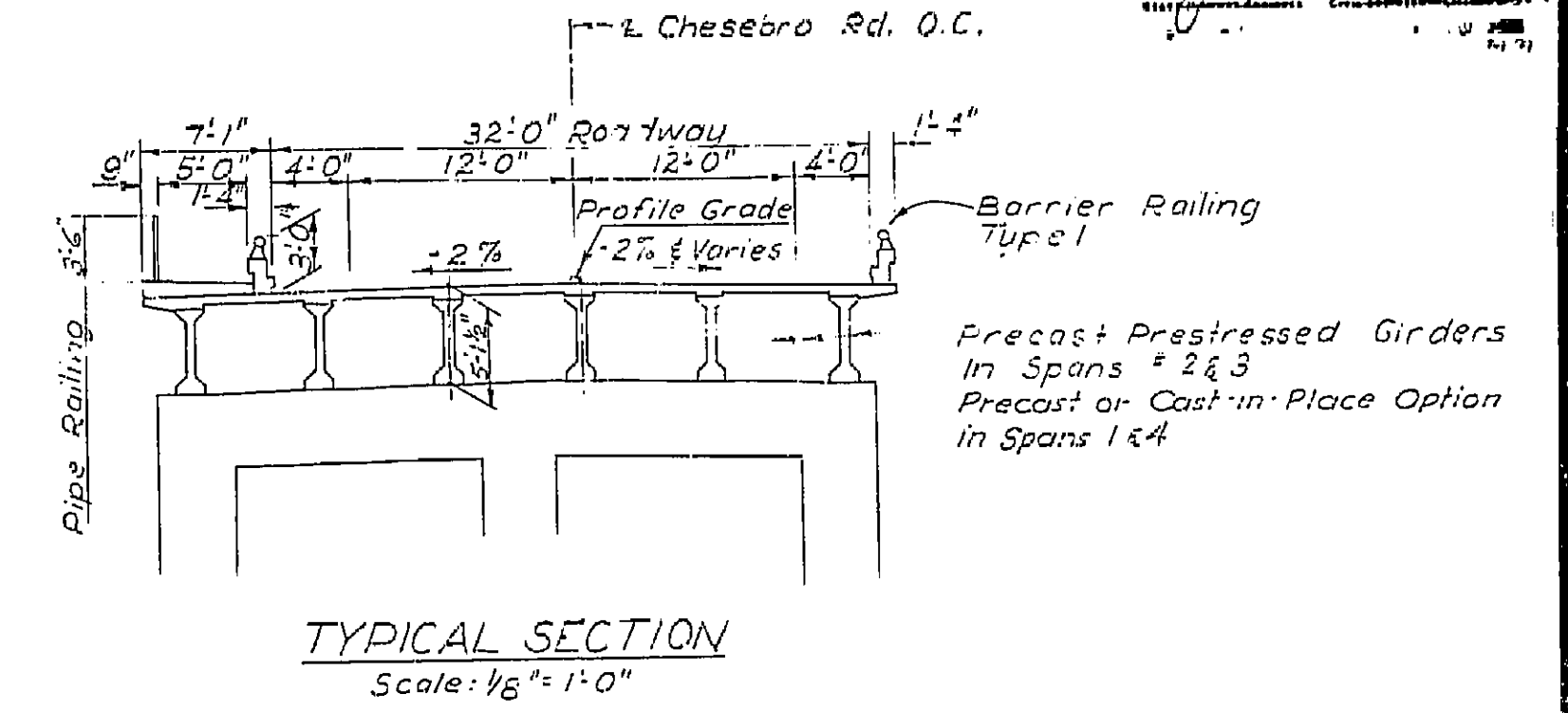
101
 DATE APPROVED: 12/22/63
 ENGINEER: [Signature]
 CHECKED: [Signature]



Concrete Cast-in-Drilled Hole Piles
 location Specified Tip Elev.
 Abut. #1 888.0
 Bent #2 885.0
 Bent #3 882.0
 Bent #4 888.0
 Abut. #5 888.0

ELEVATION
 Scale: 1" = 20'-0"

- ① = Point Bridge No. & Date
- ② = Point Chesebro Rd. O.C.
- ⊙ Indicates point of minimum vertical clearance.



TYPICAL SECTION
 Scale: 1/8" = 1'-0"

AS BUILT PLANS
 Contract No. 63-7V13C58
 Date Completed
 Document No. 7000 2373

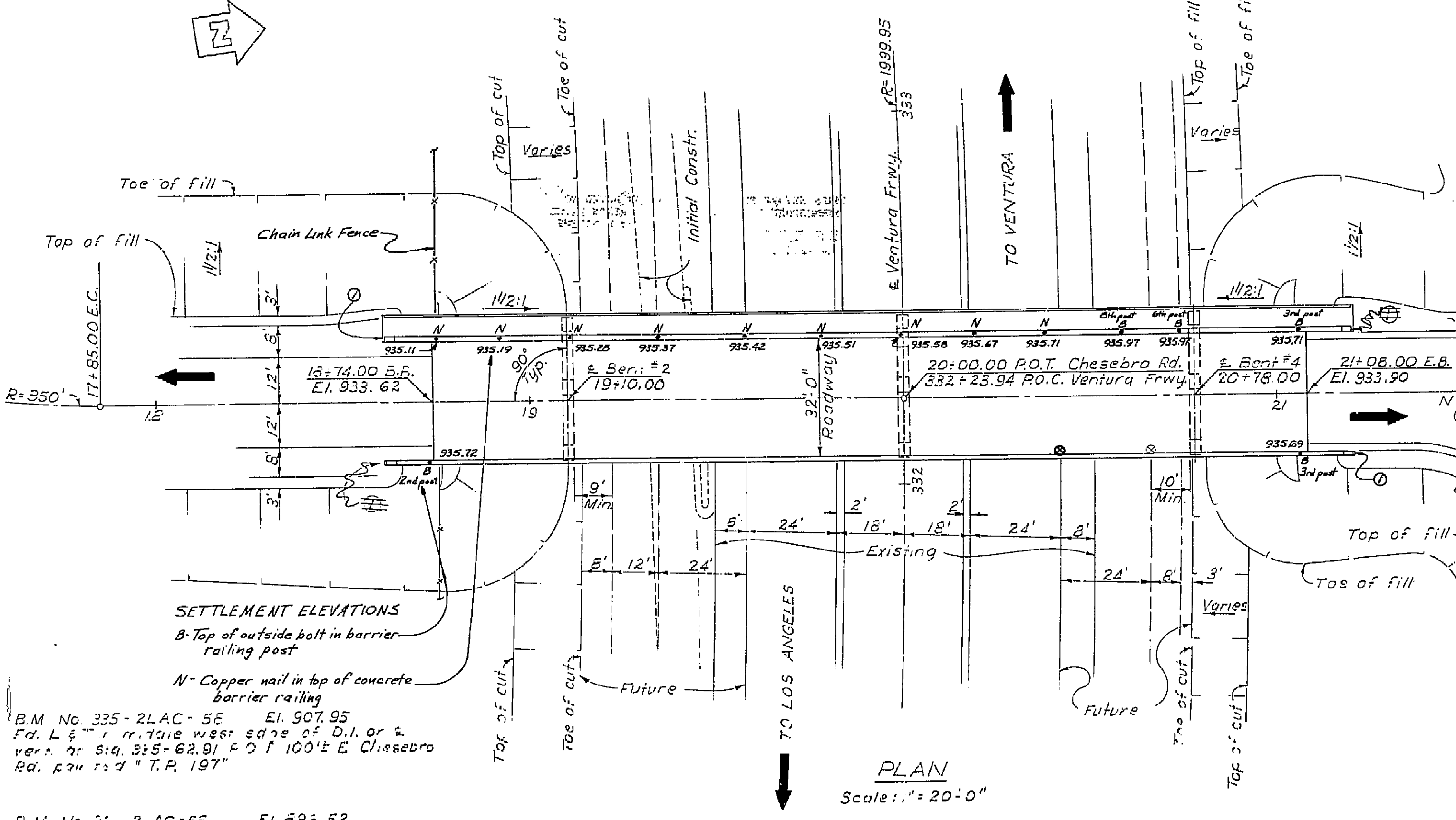
INDEX TO PLANS

Sheet No.	Title
1	General Plan
2	Grid Grades
3	Foundation Plan
4	Abutment Details
5	Bent Details
6	Typical Sections
7	Girder Layout
8	Girder Details Spans 1 & 4 - Precast Alternative
9	Girder Details Spans 1 & 4 - Cast-in-Place Alternative
10	Girder Details Spans 2 & 3
11	Diaphragm Details
12	Barrier Railing Sheet 1
13	Barrier Railing Sheet 2
14	Pipe Railing
15	Log of Test Borings

APPROXIMATE QUANTITIES

*STRUCTURE EXCAVATION (BRIDGE)	310 C.Y.
*STRUCTURE BACKFILL (BRIDGE)	180 C.Y.
16" C.I.D.H. CONCRETE PILING	1,210 L.F.
FURNISHING PC/PS CONCRETE GIRDERS (90'-0")	6 EA.
FURNISHING PC/PS CONCRETE GIRDERS (78'-0")	6 EA.
ERECTING PC/PS CONCRETE GIRDERS	12 EA.
*CLASS "A" CONCRETE (BRIDGE)	540 C.Y.
RUBBER WATERSTOPS	128 L.F.
JOINT SEALER	128 L.F.
*BAR REINFORCING STEEL (BRIDGE)	109,000 LBS.
MISCELLANEOUS METAL (BRIDGE)	400 LBS.
BARRIER RAILING (TYPE 1)	528 L.F.
PIPE BRIDGE RAILING (3'-6")	262 L.F.

*FINAL QUANTITIES
 Contract # 63-7V13C58
 Note: Route Change (VII-LA-5)



PLAN
 Scale: 1" = 20'-0"

B.M. No. 335-2-LAC-58 El. 907.95
 Fd. L. 1/2" r. 1/2" west edge of D.I. or a
 vert. nr Sta. 335+62.91 ± 3' 100'± E Chesebro
 Rd. from T.P. 197'

B.M. N-21-2-LAC-55 El. 893.52
 Fd. on top of T.P. in cor. 0.2'± below
 F.L. Median strip or 1/2 Ver. or sta 321+39.63 B.C.

For General Notes See Sheet No. 2

BRIDGE DEPARTMENT
 ... DESIGN SECTION ... 4
 Project Designer: [Signature]
 Chief Designer: [Signature]

DESIGN	[Signature]
DETAILS	[Signature]
QUANTITIES	[Signature]
SPECIFICATIONS	[Signature]

Approval Recommended by: [Signature]
 District Engineer

STATE OF CALIFORNIA
 DEPARTMENT OF PUBLIC WORKS
 DIVISION OF HIGHWAYS

CHESERO ROAD OVERCROSSING
 LOCATED ABOUT 400 FEET EAST OF THE INTERSECTION OF
 EXISTING CHESERO RD. AND VENTURA FRWY IN
 LOS ANGELES COUNTY

GENERAL PLAN

SCALE AS NOTED BRIDGE 53-1878 FILE DRAWING C-531678-1

PREL. DRAWING NO. P-531678-1

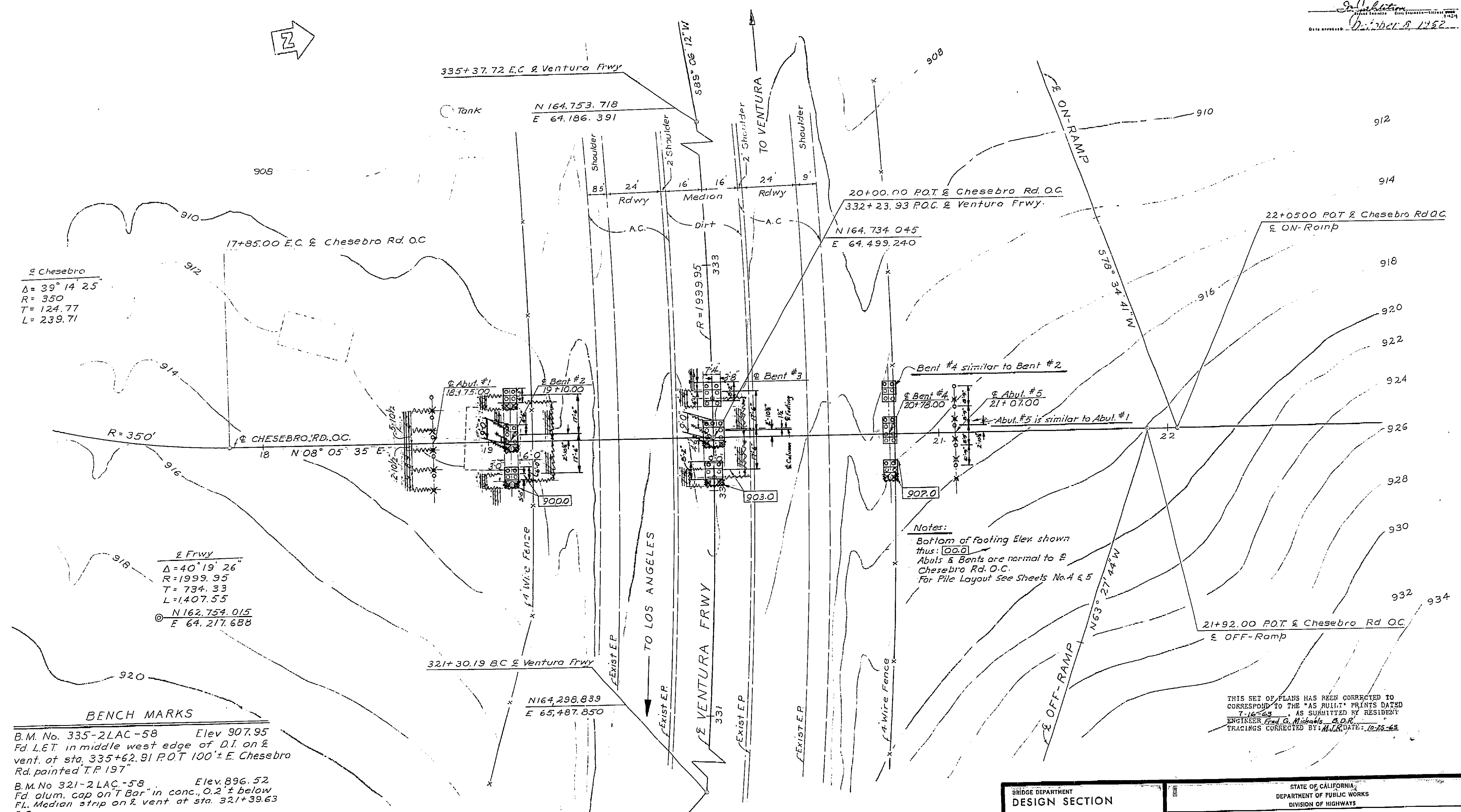
I HEREBY CERTIFY THAT THIS IS A TRUE AND ACCURATE COPY OF THE ABOVE DOCUMENT TAKEN
 UNDER MY DIRECTION AND CONTROL ON THIS DATE IN SACRAMENTO, CALIFORNIA PURSUANT TO
 AUTHORIZATION BY THE DIRECTOR OF PUBLIC WORKS.
 DATE: 11/22 SIGNATURE: [Signature] TITLE: [Title]



FED. ROAD DIST. NO.	STATE	F. & PROJECT NO.	SHEET NO.	TOTAL SHEETS
7	CALIF.		53	91

VII LA 5

J. A. Johnston
 DATE APPROVED: Dec 18, 1952



& Chesebro
 $\Delta = 39^\circ 14' 25''$
 $R = 350$
 $T = 124.77$
 $L = 239.71$

& Frwy
 $\Delta = 40^\circ 19' 26''$
 $R = 1999.95$
 $T = 734.33$
 $L = 1407.55$
 N 162.754.015
 E 64.217.688

BENCH MARKS
 B.M. No. 335-2LAC-58 Elev. 907.95
 Fd. L&T in middle west edge of D.I. on &
 vent. of sta. 335+62.91 P.O.T. 100' E. Chesebro
 Rd. painted T.P. 197
 B.M. No. 321-2LAC-58 Elev. 896.52
 Fd. alum. cap on T Bar in conc. 0.2' below
 P.L. Median strip on & vent at sta. 321+39.63
 B.C.

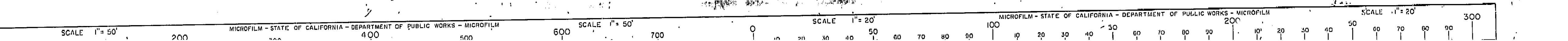
AS BUILT PLANS
 Contract No. 63-7V13CS8
 Date Completed _____
 Document No. 7000 2373

CONTOURS CHECKED &
 VERIFIED IN FIELD
 Date: June 1961
 by: J.E.B.

Drawn By H.R. Mariscal 6-26-61
 Checked By F.C.M.L. 8-5-61

BRIDGE DEPARTMENT DESIGN SECTION Section Supervisor: <i>R. E. Foster</i>	STATE OF CALIFORNIA DEPARTMENT OF PUBLIC WORKS DIVISION OF HIGHWAYS
DESIGN BY: <i>F. L. ...</i>	CHESEBRO ROAD OVERCROSSING
DETAILS BY: <i>...</i>	
QUANTITIES BY: <i>...</i>	
SCALE 1"=20'	BRIDGE 53-1676 FILE 63 DRAWING C-531678-3

I HEREBY CERTIFY THAT THIS IS A TRUE AND ACCURATE COPY OF THE ABOVE DOCUMENT TAKEN UNDER MY DIRECTION AND CONTROL ON THIS DATE IN SACRAMENTO, CALIFORNIA PURSUANT TO AUTHORIZATION BY THE DIRECTOR OF PUBLIC WORKS.
 DATE 1-13-72 SIGNATURE *...* TITLE

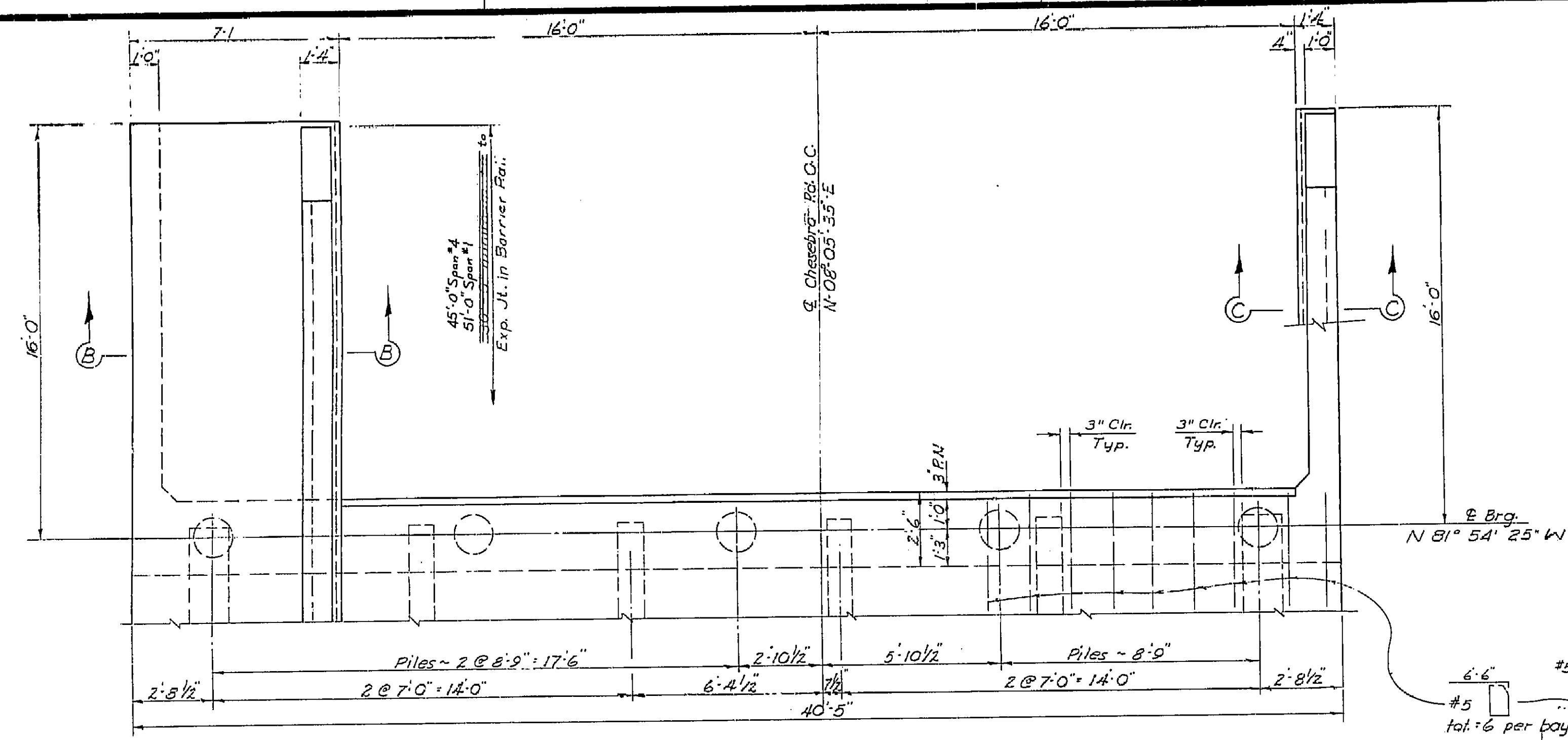


59

FED. ROAD DIST. NO.	STATE	P. A. PROJECT NO.	SHEET NO.	TOTAL SHEETS
7	CALIF.		60	21

DATE	COUNTY	ROUTE	SECTION	POST MILE	TOTAL MILES
11/14	LA	5	3	4	115

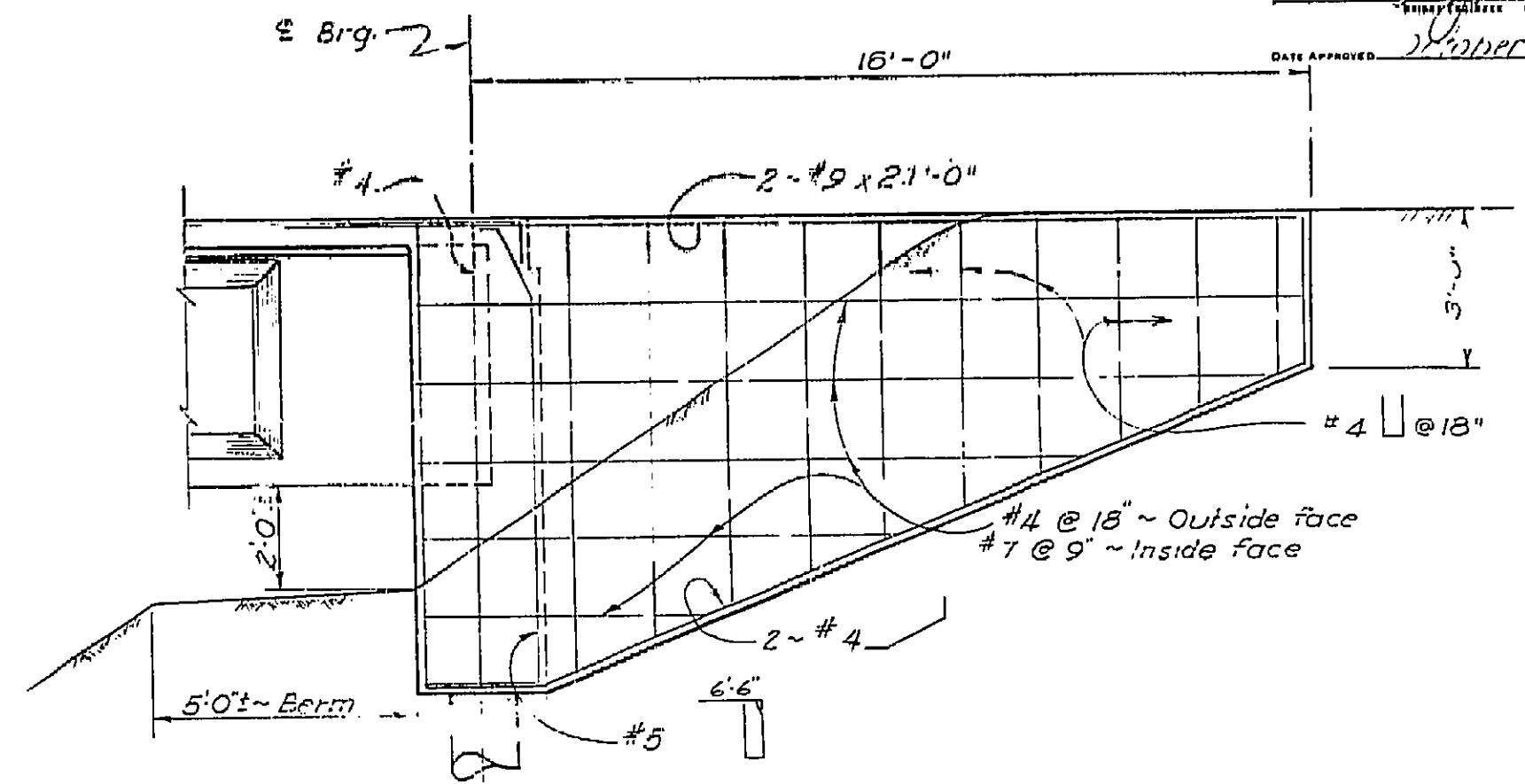
DATE APPROVED: *[Signature]*
 11/14/62



PLAN

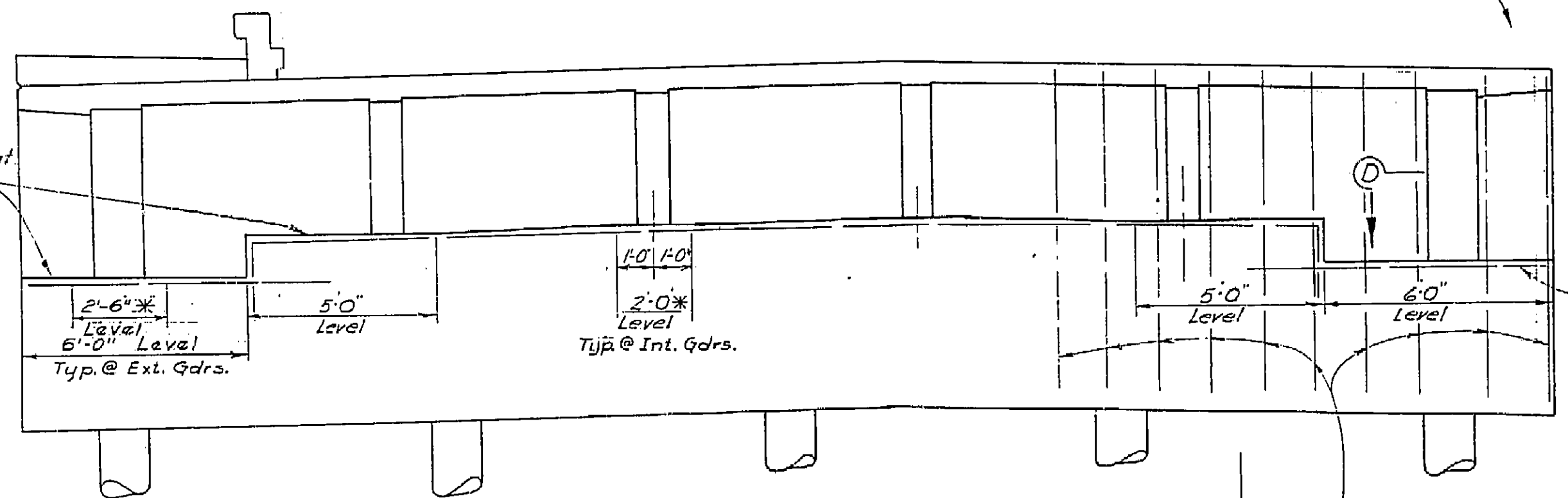
Scale: 3/8" = 1'-0"

Note: Abutment #5 shown, Abutment #1 is similar



WINGWALL ELEVATION

Scale: 3/8" = 1'-0"

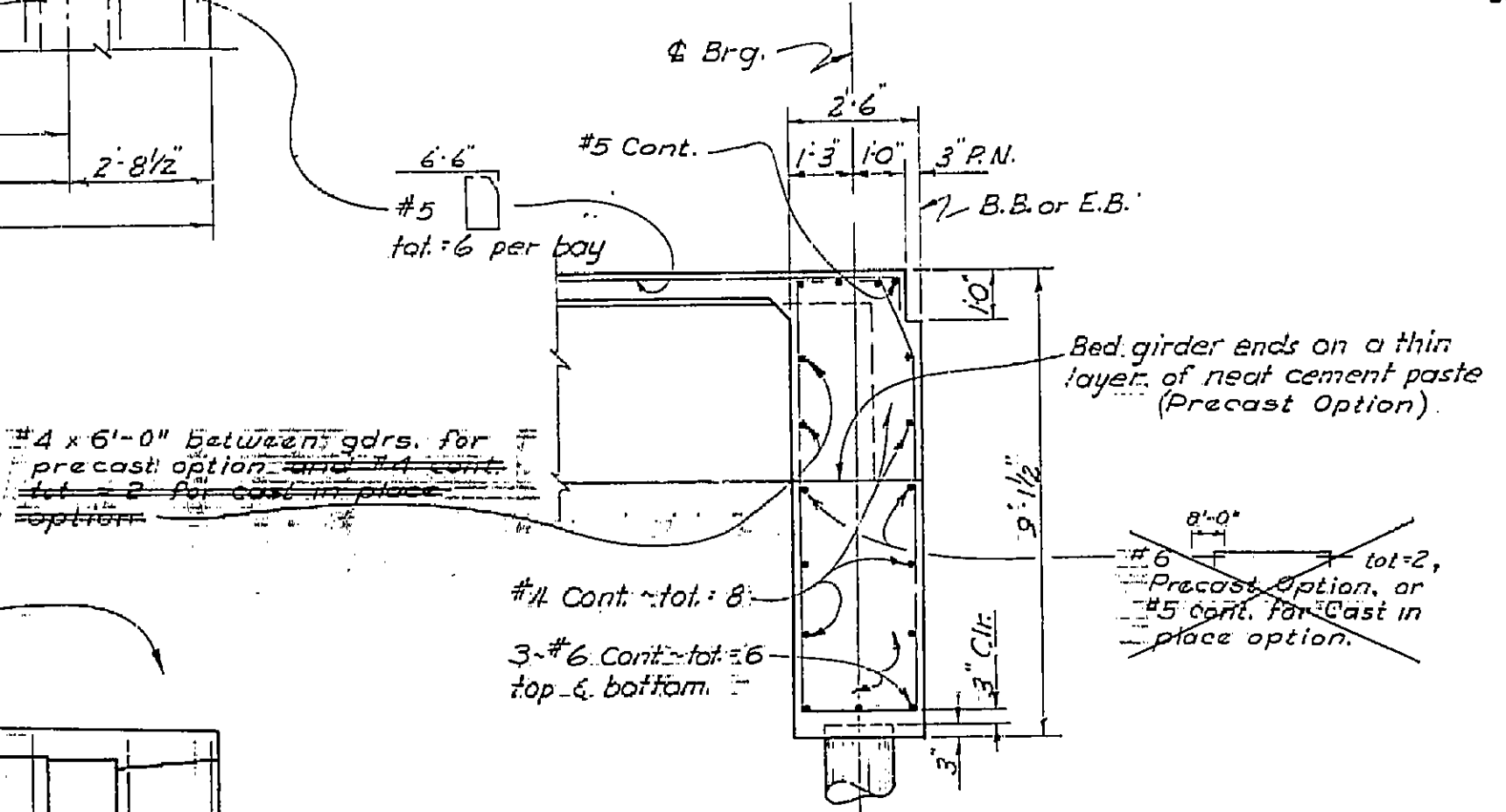


ELEVATION

Scale: 3/8" = 1'-0"

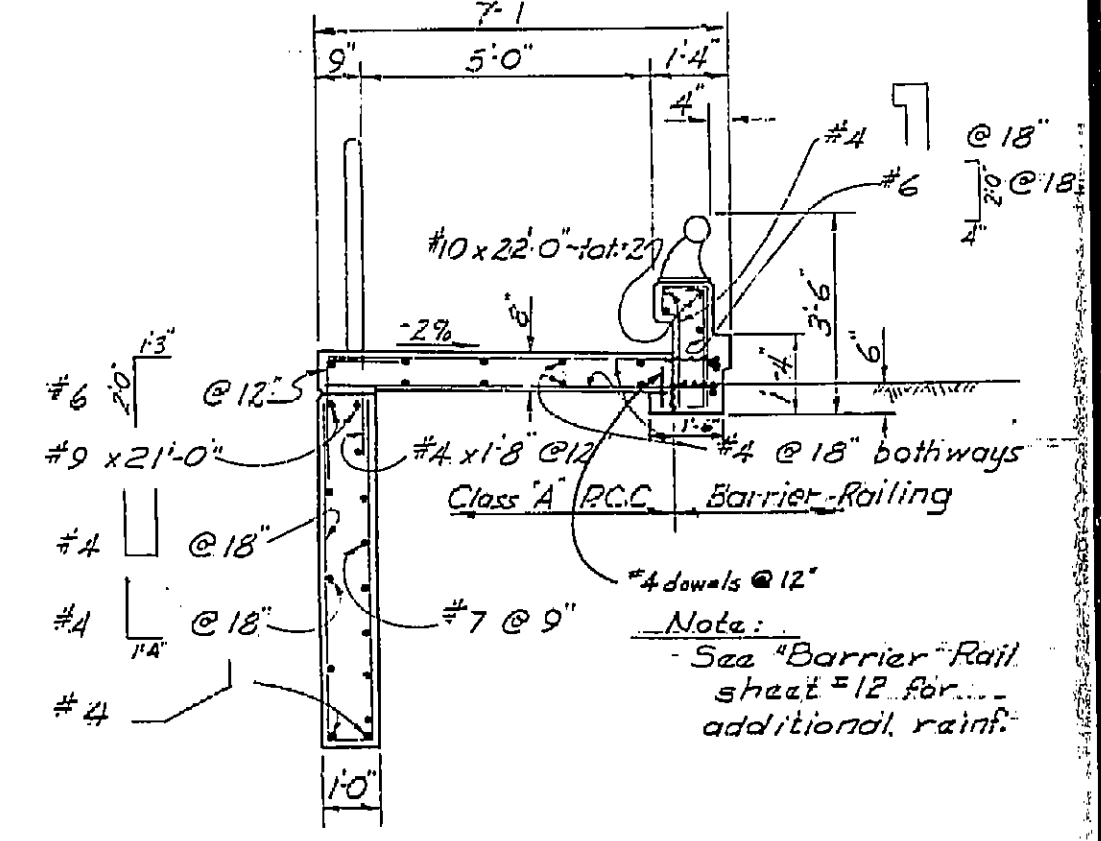
* For Precast Option - Finish or grind to a smooth surface, (level normal to E. Gdr., and at slope of gdr. length. to W. gdr.) set girders in a thin layer of neat cement grout.

AS BUILT PLANS
 Contract No. 63-7V13C58
 Date Completed _____
 Document No. 7000 2373



SECTION A-A

Scale: 3/8" = 1'-0"

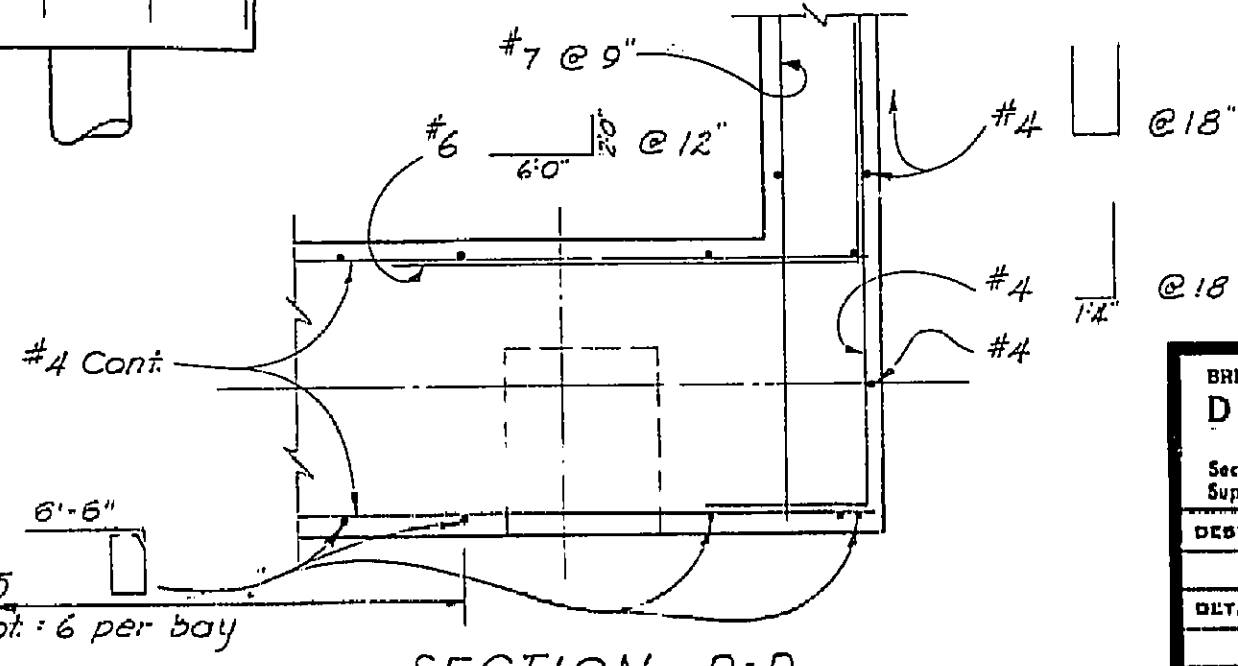


SECTION B-B

Scale: 3/8" = 1'-0"

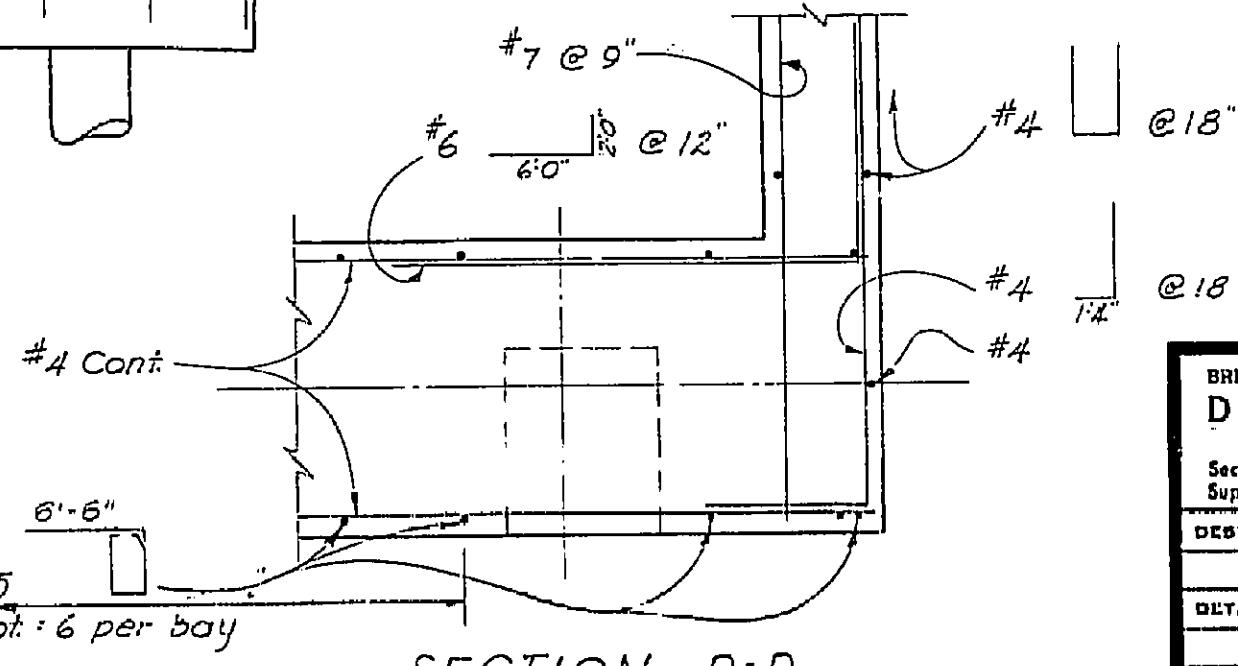
Note: For Barrier Railing Details not shown See Sheets #12 & 13

THIS SET OF PLANS HAS BEEN CORRECTED TO CORRESPOND TO THE "AS BUILT" PRINTS DATED 7-16-63 AS SUBMITTED BY RESIDENT ENGINEER Fred C. Michaels - B.D.R. REVISIONS CORRECTED BY: M.J.C. DATE: 10-25-63



SECTION C-C

Scale: 3/8" = 1'-0"



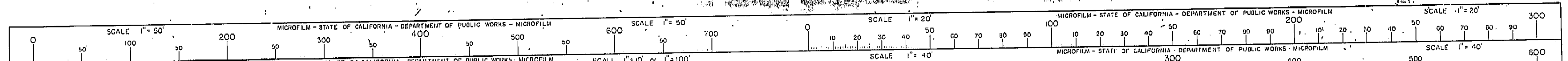
SECTION D-D

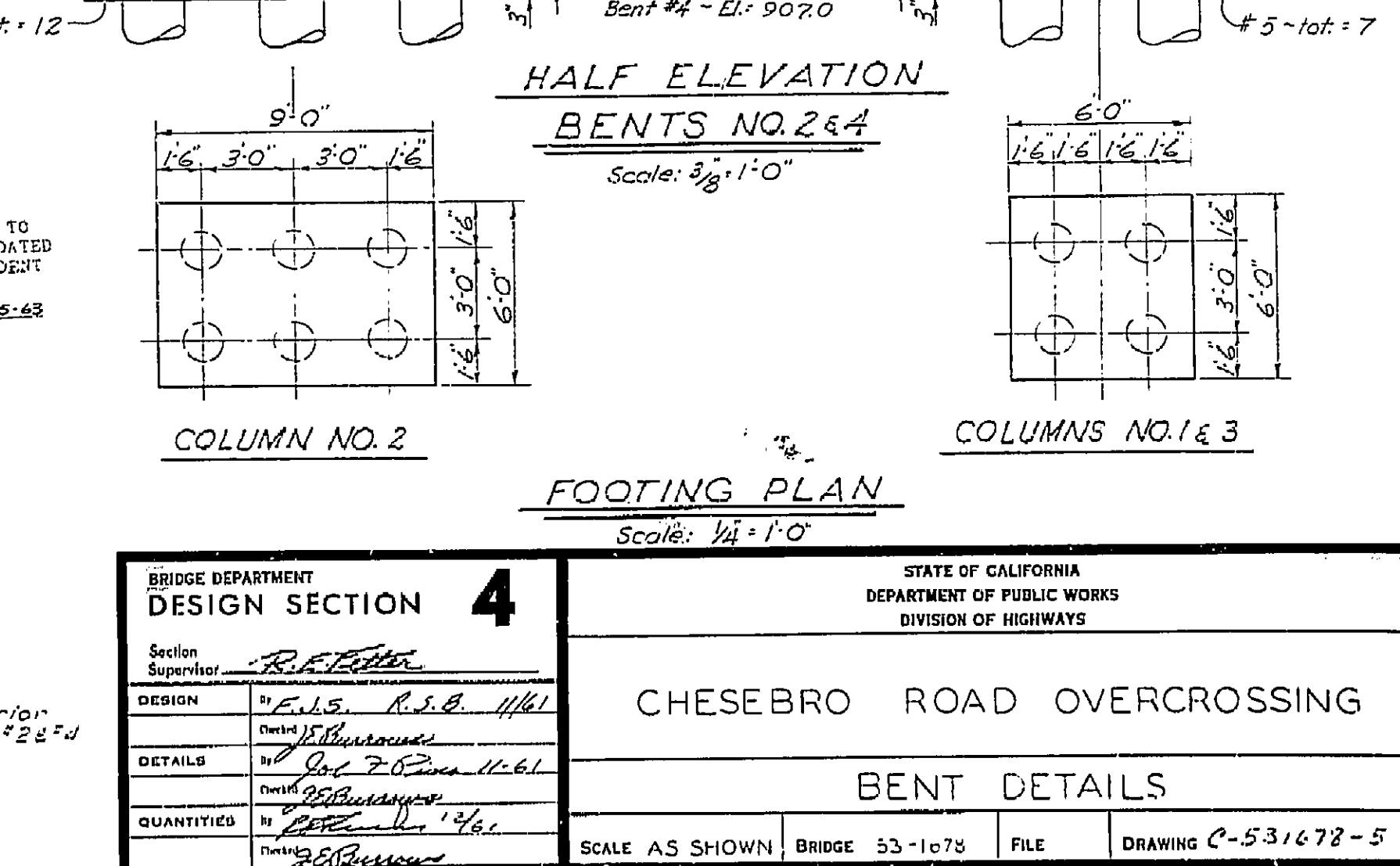
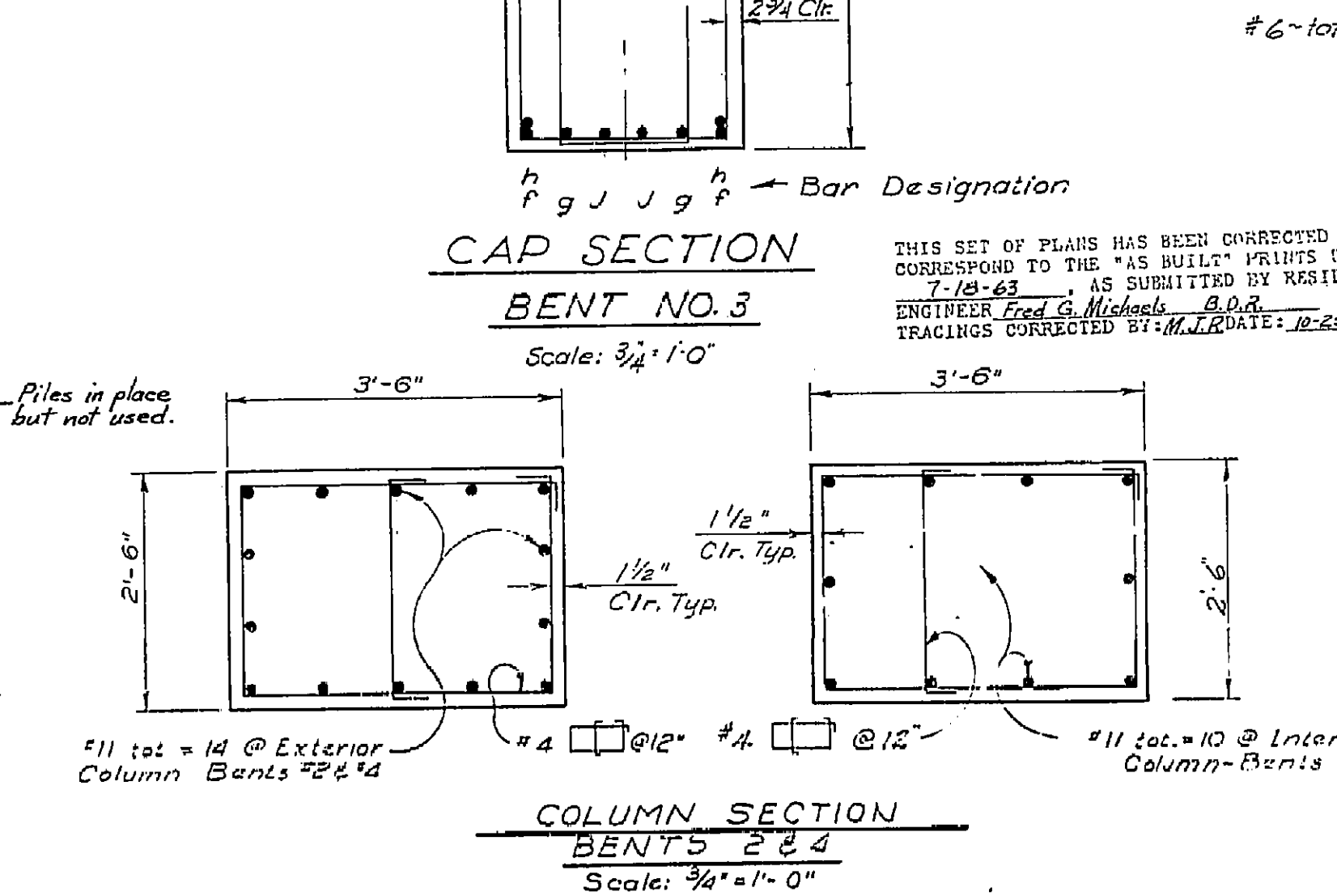
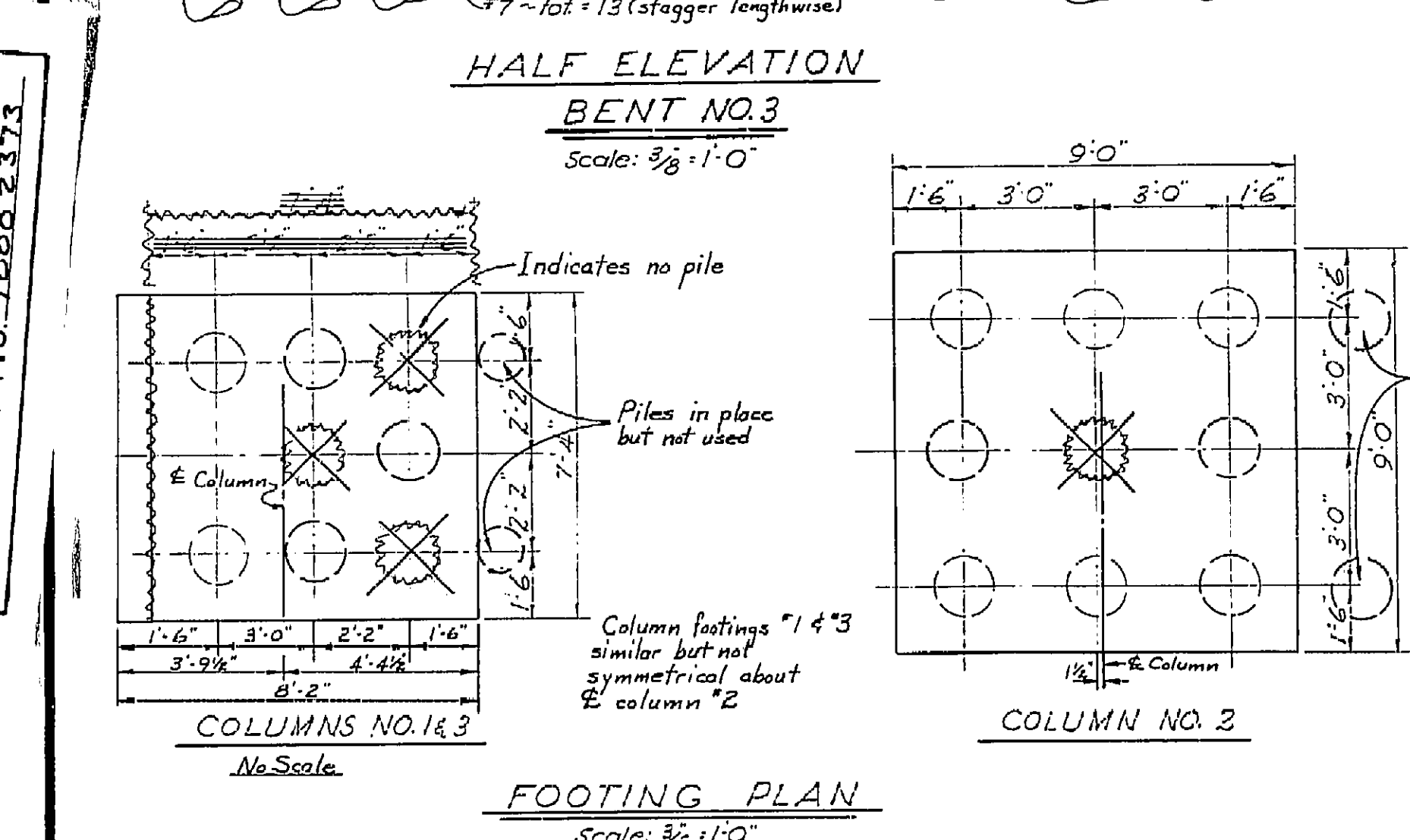
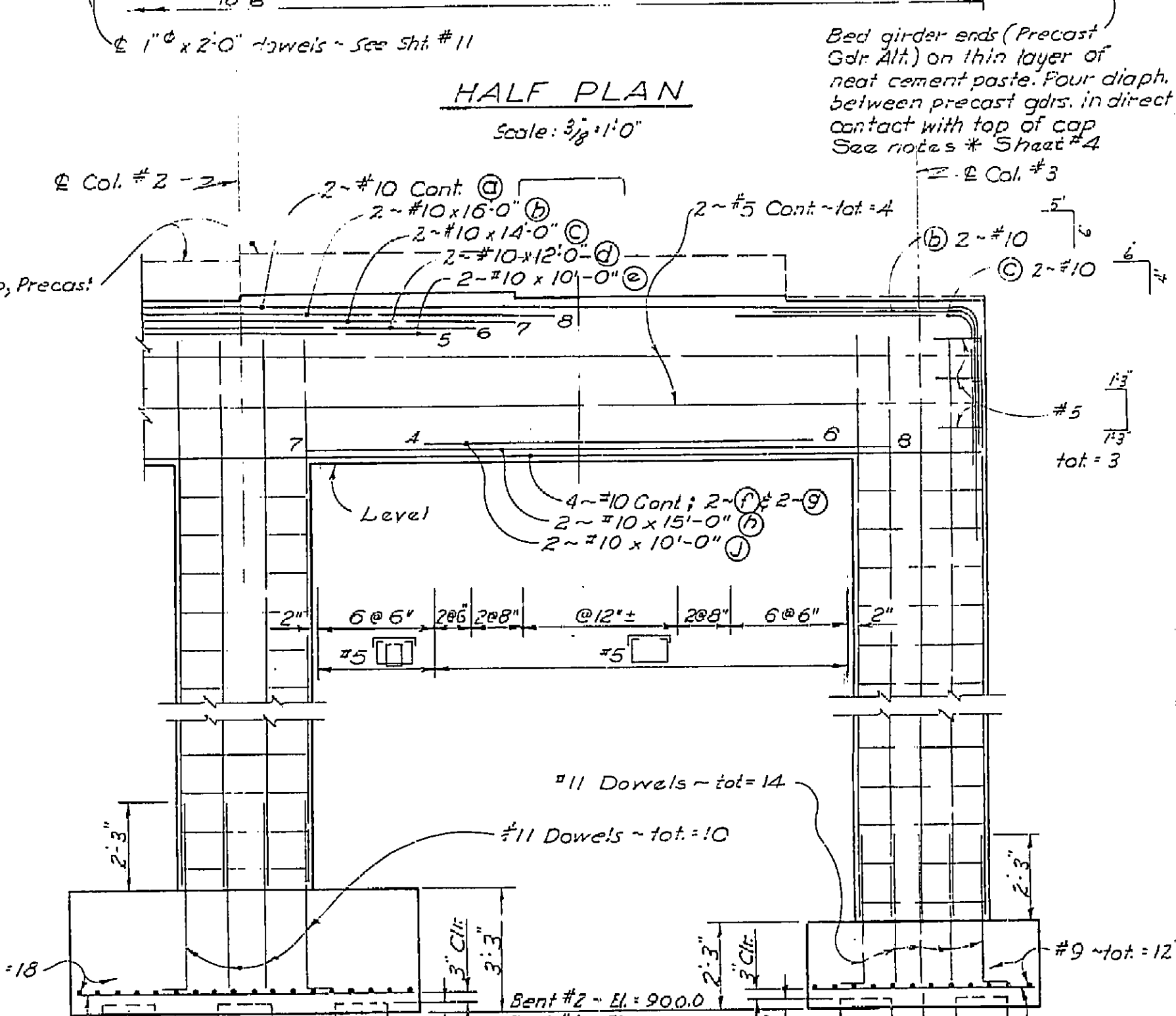
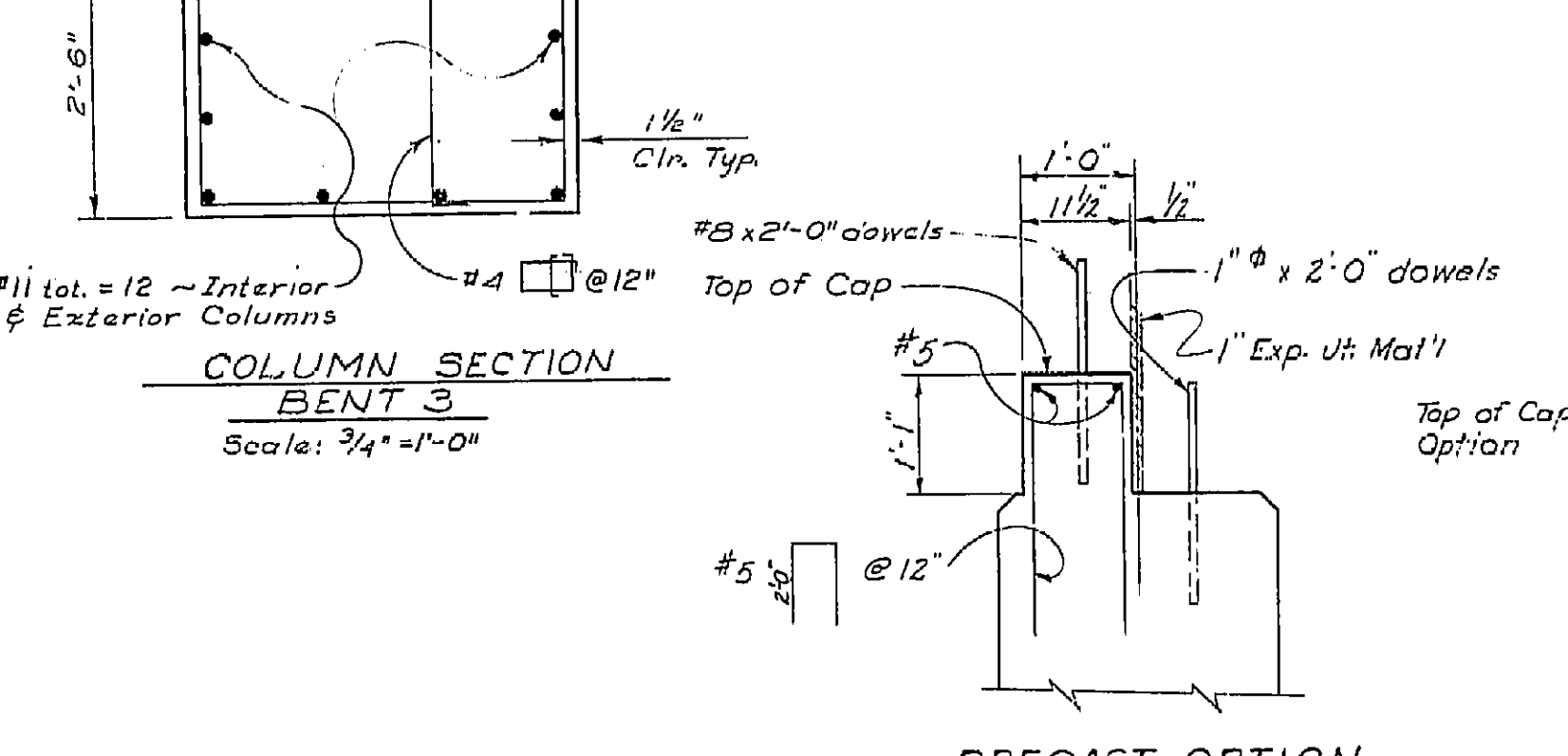
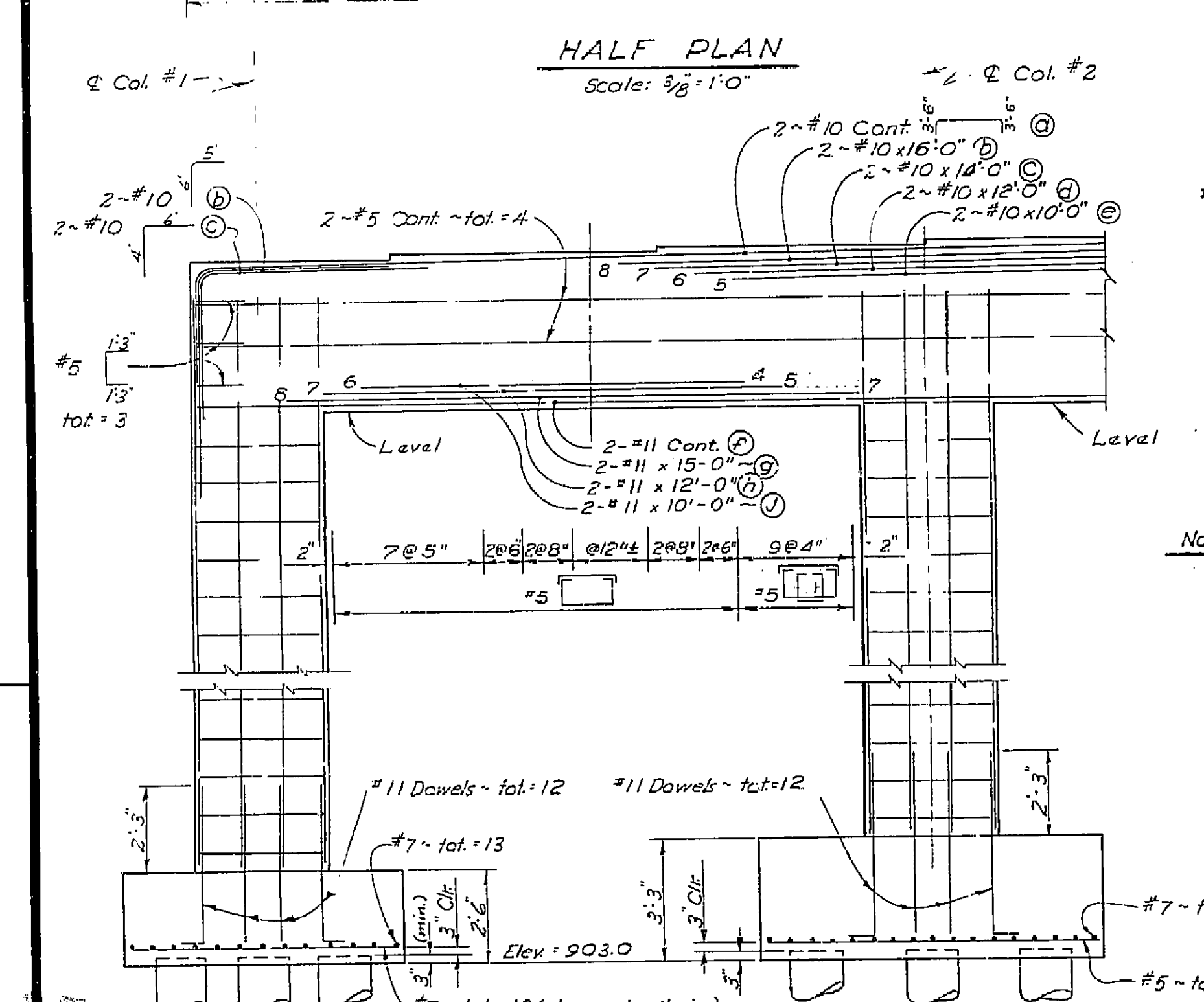
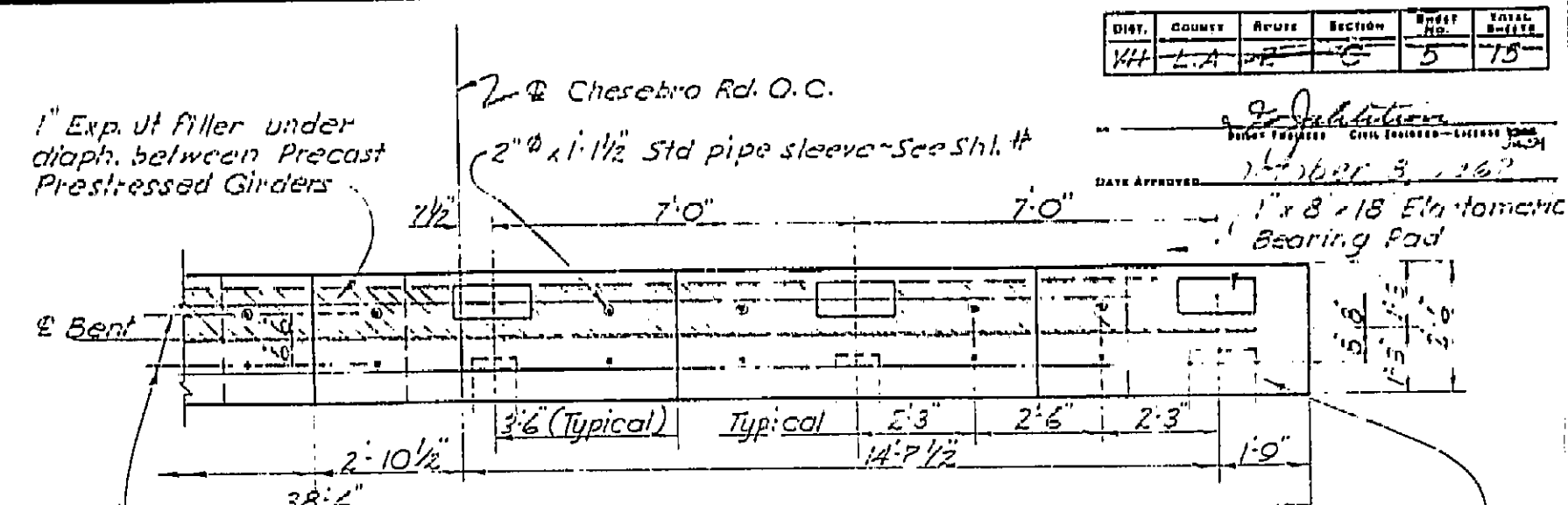
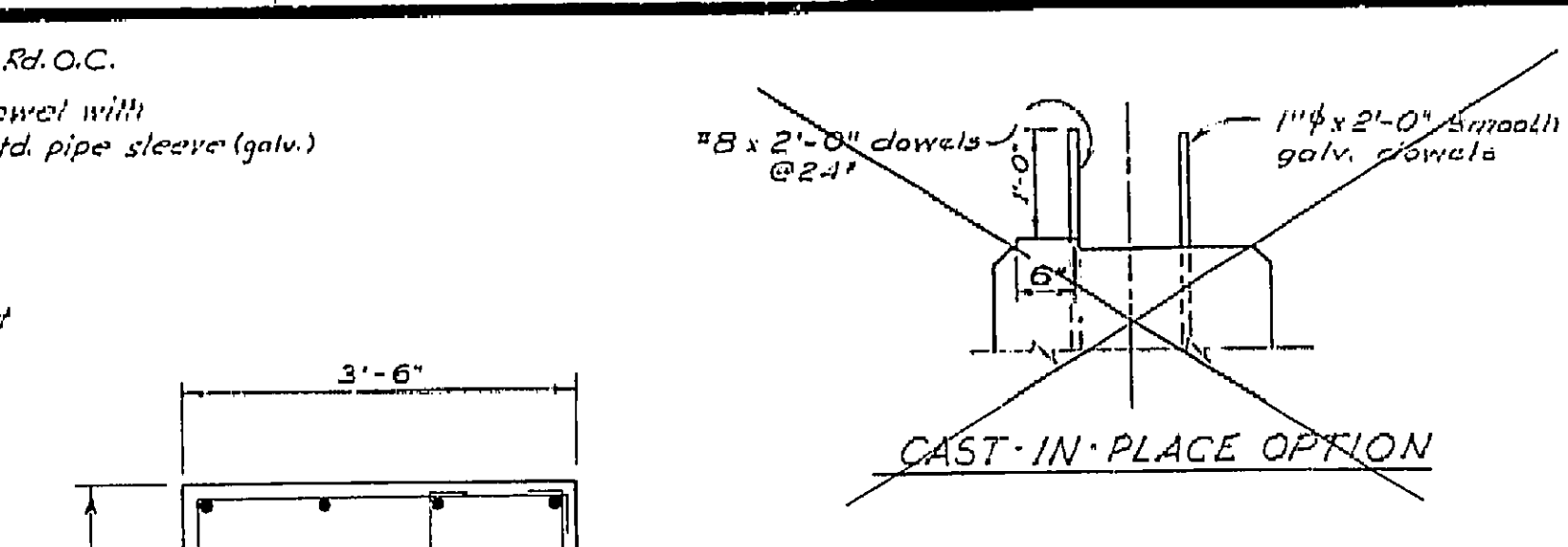
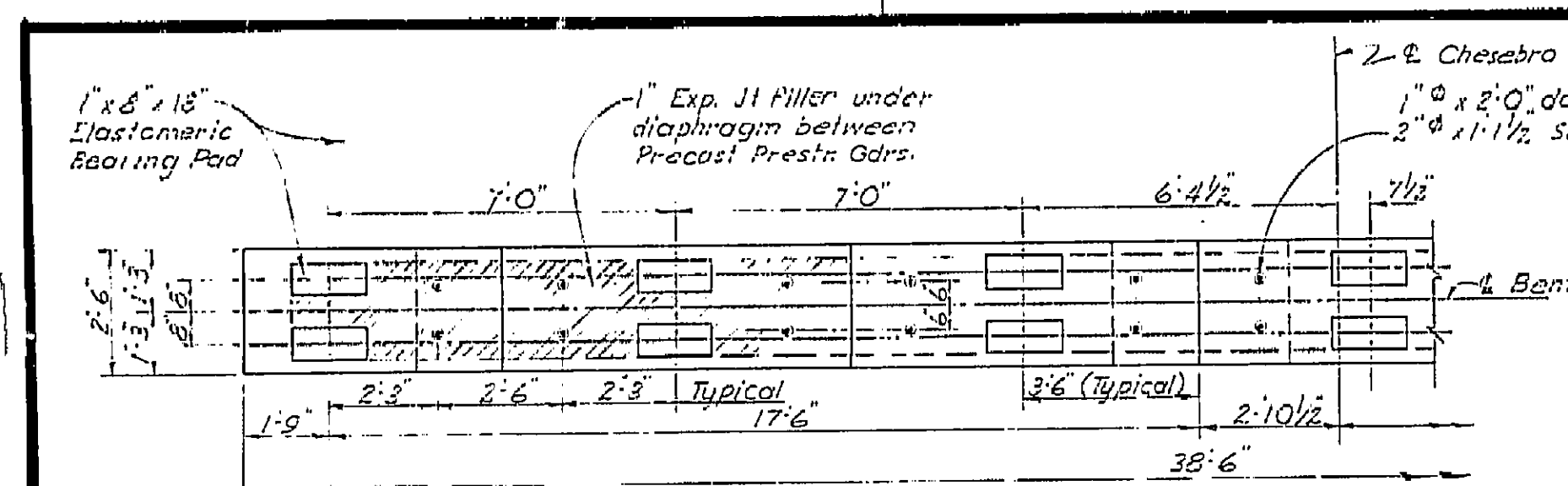
Scale: 3/8" = 1'-0"

BRIDGE DEPARTMENT	
DESIGN SECTION 4	
Section Supervisor	<i>[Signature]</i>
DESIGN	By E.L.S. R.S.B. 11/61
DETAILS	By Fred C. Michaels 11-61
QUANTITIES	By Fred C. Michaels 12-61

STATE OF CALIFORNIA DEPARTMENT OF PUBLIC WORKS DIVISION OF HIGHWAYS			
CHESEBRO ROAD OVERCROSSING			
ABUTMENT DETAILS			
SCALE AS SHOWN	BRIDGE 53-1678	FILE	DRAWING C-531678-4
PRELIMINARY DRAWING NO.	P-531678-3	REVISION DATES	

I HEREBY CERTIFY THAT THIS IS A TRUE AND ACCURATE COPY OF THE ABOVE DOCUMENT TAKEN UNDER MY DIRECTION AND CONTROL ON THIS DATE IN SACRAMENTO, CALIFORNIA PURSUANT TO AUTHORIZATION BY THE DIRECTOR OF PUBLIC WORKS.
 DATE 1-11-72 SIGNATURE *[Signature]* TITLE _____





Note:
Number at ends of bars indicate distance in feet from & Col. for top reinf. and from & between Col. for bottom reinf.

THIS SET OF PLANS HAS BEEN CORRECTED TO CORRESPOND TO THE "AS BUILT" PRINTS DATED 7-18-63 AS SUBMITTED BY RESIDENT ENGINEER Fred G. Michaels, O.R.S. TRACINGS CORRECTED BY: M.J.R. DATE: 10-25-63

AS BUILT PLANS
Contract No. 63-7V13C58
Date Completed
Document No. 7000 2373

BRIDGE DEPARTMENT DESIGN SECTION 4		STATE OF CALIFORNIA DEPARTMENT OF PUBLIC WORKS DIVISION OF HIGHWAYS	
Section Supervisor <i>R.H. Fisher</i>	DESIGN BY: <i>F.L.S. R.S.B. 11/61</i>	CHESEBRO ROAD OVERCROSSING	
DETAILS BY: <i>John F. Brown 11/61</i>	QUANTITIES BY: <i>John F. Brown 11/61</i>	BENT DETAILS	
SCALE AS SHOWN BRIDGE 53-1078 FILE		DRAWING C-531678-5	
PRELIMINARY DRAWING NO. P-531678-9		REVISION DATES	

I HEREBY CERTIFY THAT THIS IS A TRUE AND ACCURATE COPY OF THE ABOVE DOCUMENT TAKEN UNDER MY DIRECTION AND CONTROL ON THIS DATE IN SACRAMENTO, CALIFORNIA PURSUANT TO AUTHORIZATION BY THE DIRECTOR OF PUBLIC WORKS.
DATE: 11 72 SIGNATURE: *James C. ...* TITLE: *...*

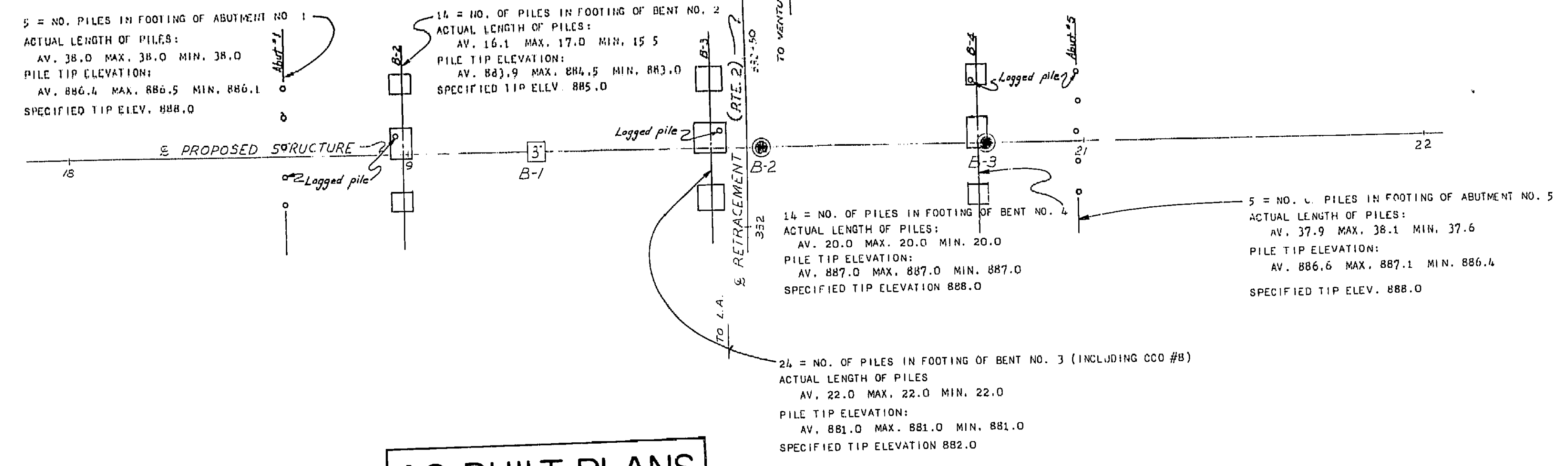
FED. ROAD DIST. NO.	STATE	PROJECT NO.	FISCAL YEAR	SHEET NO.	TOTAL SHEETS
7	CAL.			1	1

DIST.	COUNTY	PROJECT	SHEET NO.	TOTAL SHEETS
VII	LA	5	1	1

DATE APPROVED: 2/22/63

BENCH MARK #335-2LAC-58
 Fd 1, 47 in middle West edge of D1 on E. Ven. at Sta 335+62.91
 P.O.T. 100' ± E. Chasebro Rd. pointed "TR 197"

ELEV. 907.95



AS BUILT PLANS
 Contract No. 63-7V13C58
 Date Completed _____
 Document No. 70002373

PILE DATA
 TYPE OF PILE - C.I.D.H.
 HAMMER DATA -
 PILE DIAMETER: TIP 16" BUTT 15"
 PILE DESIGN LOAD = 45 TONS
 FOR THE STRUCTURE:
 NUMBER OF PILES = 55 + 7 IN CCO #8
 EST. LENGTH OF PILING = 1,213 L.F.
 ACTUAL LENGTH OF PILING = 1,259.2 + 154.0 L.F. CCO #8

THIS SET OF PLANS HAS BEEN CORRECTED TO CORRESPOND TO THE "AS BUILT" PRINTS DATED 3-22-63 AS SUBMITTED BY RESIDENT ENGINEER Fred G. Michaels, B.S.C.E. TRACINGS CORRECTED BY: M.J.R. DATE: 10-29-63

NO GROUND WATER ENCOUNTERED DURING THIS INVESTIGATION BY BRIDGE DEPT. GEOLOGY SECTION DATE: June 1961

NOTES

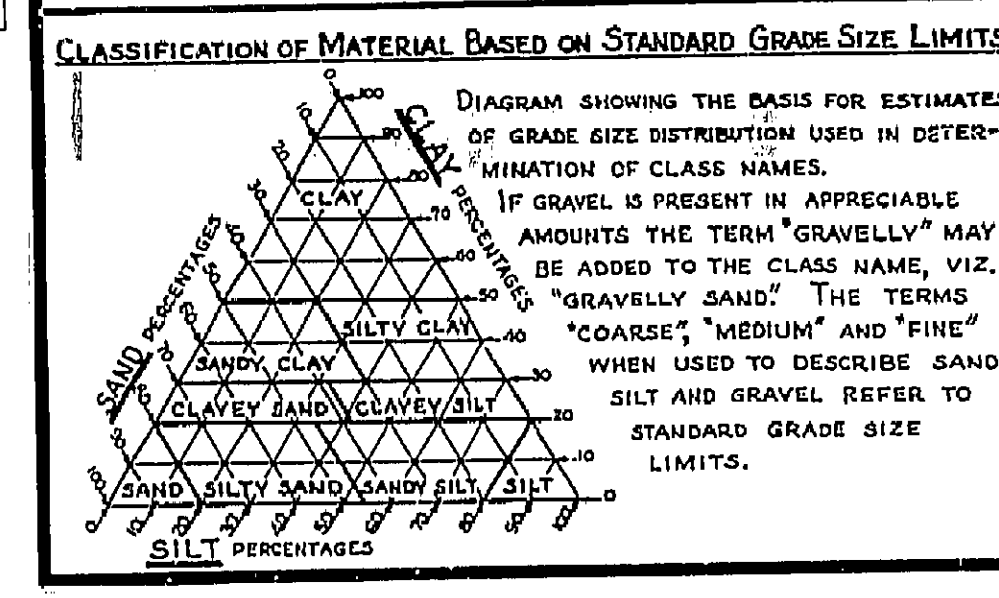
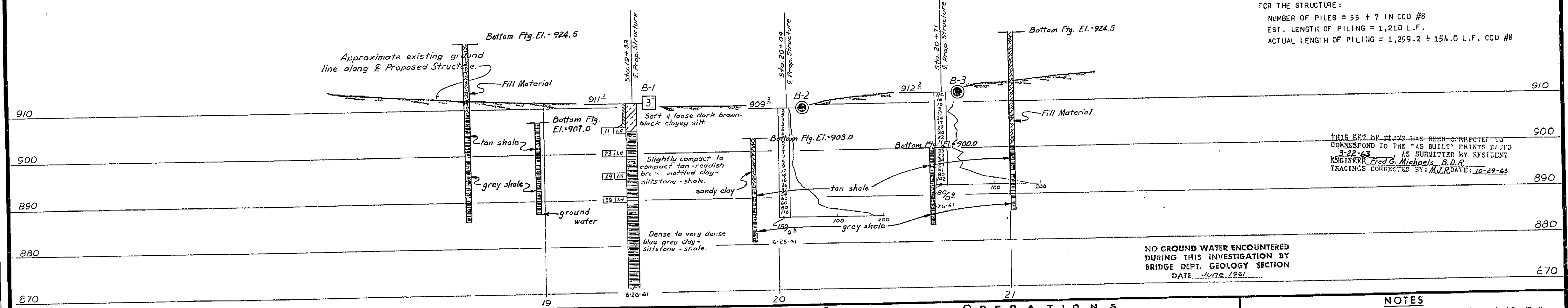
The contractor's attention is directed to Section 2, Article (c) of the Standard Specifications and to the Special Provisions accompanying this set of plans. Classification of earth material as shown on this sheet is based upon field inspection and is not to be construed to imply mechanical analysis.

STATE OF CALIFORNIA
 DEPARTMENT OF PUBLIC WORKS
 DIVISION OF HIGHWAYS

CHESEBRO RD. OVERCROSSING

LOG OF TEST BORINGS

Scale: Horiz 1"=20', Vert 1"=10'
 BRIDGE 53-1678 FILE DRAWING C-531678-15
 P.E.L. DRAWING P-531678-15



LEGEND OF EARTH MATERIALS

GRAVEL	SILTY CLAY OR CLAYEY SILT
SAND	PEAT AND/OR ORGANIC MATTER
SILT	FILL MATERIAL
CLAY	IGNEOUS ROCK
SANDY CLAY OR CLAYEY SAND	SEDIMENTARY ROCK
SANDY SILT OR SILTY SAND	METAMORPHIC ROCK

LEGEND OF BORING OPERATIONS

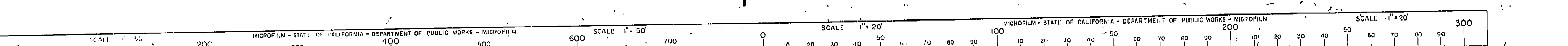
PENETROMETER
 2 1/4" CONE PENETROMETER
 SAMPLER BORING (DRY)
 ROTARY BORING (WET)
 AUGER BORING (DRY)
 JET BORING
 CORE BORING
 TEST PIT

1" SOIL TUBE

ROTARY BORING
 Top Hole El. Location
 Casing driven
 Description of material (Unit weight (pcf), % Moisture, Consolidation Test, etc.)
 Estimated material change
 Unconformable material change

PENETRATION BORING
 Top Hole El. Location
 Pushed
 No count
 Seconds per Foot (Using a 140 lb. Miskin-Terry Air Hammer @ 115 psi or as noted)
 Average skin friction (lb/ft)
 Friction above this point (lb/ft)

I HEREBY CERTIFY THAT THIS IS A TRUE AND ACCURATE COPY OF THE ABOVE DOCUMENT TAKEN UNDER MY DIRECTION AND CONTROL ON THIS DATE IN SACRAMENTO, CALIFORNIA PURSUANT TO AUTHORIZATION BY THE DIRECTOR OF PUBLIC WORKS.
 DATE _____ SIGNATURE _____ TITLE _____



Appendix D Analysis and Calculations

- D-1 Seismic Analyses**
- D-2 Axial Pile Capacity Calculations**
- D-3 Lateral Pile Capacity Calculations**
- D-4 Retaining Wall Calculations**

APPENDIX D-1
SEISMIC ANALYSES

Shear Wave Velocity Calculation Summary

CPT No.	Computed Vs30 (m/s)
A-13-002	321
A-13-003	373
A-13-004	361
A-13-005	384
A-13-006	345

Average
Vs30 for the
site= **357** m/s

Design= 360 m/s



SHEAR WAVE VELOCITY CALCULATIONS

Boring: **A-13-002**
 Boring Depth 100

Depth (feet)		layer thickness, Di (feet)	soil type	N ₆₀	Su (psf)	Vs		Di (ft) / Vs (fps)	
from	to					m/s	ft/sec		
0	6.25	6.25	clay		3500	265	869	0.007	soil
6.25	8.75	2.5	clay		2000	203	666	0.004	
8.75	12.5	3.75	clay		1000	146	479	0.008	
12.5	17.5	5	clay		2500	226	740	0.007	
17.5	22.5	5	clay		1500	177	581	0.009	
22.5	27.5	5	clay		4500	298	979	0.005	
27.5	32.5	5	clay		8170	396	1300	0.004	rock
32.5	37.5	5	clay		8170	396	1300	0.004	
37.5	42.5	5	clay		8170	396	1300	0.004	
42.5	47.5	5	clay		8170	396	1300	0.004	
47.5	52.5	5	clay		8170	396	1300	0.004	
52.5	57.5	5	clay		8170	396	1300	0.004	
57.5	60	2.5	clay		8170	396	1300	0.002	
60	65	5	clay		8170	396	1300	0.004	
65	70	5	clay		8170	396	1300	0.004	
70	75	5	clay		8170	396	1300	0.004	
75	80	5	clay		8170	396	1300	0.004	
80	90	10	clay		8170	396	1300	0.008	
90	100	10	clay		8170	396	1300	0.008	
						Vs(d) = 321	1052		
						Vs30 = 318			

REFERENCES

Cohesionless Soil, Sykora (1987): $V_s = 100.5(N_{60})^{0.29}$

V_s=shear wave velocity (m/s)
 N₆₀=SPT blowcount corrected for hammer energy only

Cohesive Soil, Dickenson (1994): $V_s = 203(S_u/2000)^{0.475}$

V_s=shear wave velocity (m/s)
 S_u=undrained shear strength (psf)

Averaging method (Geotechnical Services Design Manual Version 1.0 August 2009 Section 1.1.7) $V_{s30} = 100 \text{ feet} / (D_1/V_{s1} + D_2/V_{s2} + \dots + D_n/V_{sn})$

V_{s30}= average shear wave velocity in ft/sec upper 30 m (100 feet)
 D_i= layer thickness (feet) for individual layers
 V_{s_i}= shear wave velocity (ft/sec) for individual layers



SHEAR WAVE VELOCITY CALCULATIONS

Boring: **A-13-003**
 Boring Depth 100

Depth (feet)		layer thickness, Di (feet)	soil type	N ₆₀	Su (psf)	Vs		Di (ft) / Vs (fps)	
from	to					m/s	ft/sec		
0	5	5	clay		1500	177	581	0.009	soil
5	8.75	3.75	clay		8170	396	1300	0.003	rock
8.75	10.625	1.875	clay		8170	396	1300	0.001	
10.625	13.125	2.5	clay		8170	396	1300	0.002	
13.125	17.5	4.375	clay		8170	396	1300	0.003	
17.5	22.5	5	clay		8170	396	1300	0.004	
22.5	27.5	5	clay		8170	396	1300	0.004	
27.5	32.5	5	clay		8170	396	1300	0.004	
32.5	37.5	5	clay		8170	396	1300	0.004	
37.5	42.5	5	clay		8170	396	1300	0.004	
42.5	47.5	5	clay		8170	396	1300	0.004	
47.5	50	2.5	clay		8170	396	1300	0.002	
50	55	5	clay		8170	396	1300	0.004	
55	60	5	clay		8170	396	1300	0.004	
60	65	5	clay		8170	396	1300	0.004	
65	70	5	clay		8170	396	1300	0.004	
70	75	5	clay		8170	396	1300	0.004	
75	80	5	clay		8170	396	1300	0.004	
80	90	10	clay		8170	396	1300	0.008	
90	100	10	clay		8170	396	1300	0.008	
						Vs(d) =	373	1224	
						Vs30 =	370		

REFERENCES

Cohesionless Soil, Sykora (1987): $V_s = 100.5(N_{60})^{0.29}$

V_s=shear wave velocity (m/s)

N₆₀=SPT blowcount corrected for hammer energy only

Cohesive Soil, Dickenson (1994): $V_s = 203(S_u/2000)^{0.475}$

V_s=shear wave velocity (m/s)

S_u=undrained shear strength (psf)

Averaging method (Geotechnical Services Design Manual Version 1.0 August 2009 Section 1.1.7) $V_{s30} = 100 \text{ feet} / (D_1/V_{s1} + D_2/V_{s2} + \dots + D_n/V_{sn})$

Manual Version 1.0 August 2009 Section 1.1.7)

V_{s30}= average shear wave velocity in ft/sec upper 30 m (100 feet)

D_i= layer thickness (feet) for individual layers

V_{s_i}= shear wave velocity (ft/sec) for individual layers



SHEAR WAVE VELOCITY CALCULATIONS

Boring: **A-13-004**
 Boring Depth 100

Depth (feet)		layer thickness, Di (feet)	soil type	N ₆₀	Su (psf)	Vs		Di (ft) / Vs (fps)	
from	to					m/s	ft/sec		
0	5	5	clay		3250	256	839	0.006	soil
5	10.5	5.5	clay		3250	256	839	0.007	
10.5	13.5	3	clay		2750	236	775	0.004	
13.5	17.5	4	clay		3750	274	898	0.004	
17.5	22.5	5	clay		8170	396	1300	0.004	rock
22.5	27.5	5	clay		8170	396	1300	0.004	
27.5	32.5	5	clay		8170	396	1300	0.004	
32.5	37.5	5	clay		8170	396	1300	0.004	
37.5	42.5	5	clay		8170	396	1300	0.004	
42.5	47.75	5.25	clay		8170	396	1300	0.004	
47.75	50	2.25	clay		8170	396	1300	0.002	
50	55	5	clay		8170	396	1300	0.004	
55	60	5	clay		8170	396	1300	0.004	
60	65	5	clay		8170	396	1300	0.004	
65	70	5	clay		8170	396	1300	0.004	
70	75	5	clay		8170	396	1300	0.004	
75	80	5	clay		8170	396	1300	0.004	
80	85	5	clay		8170	396	1300	0.004	
85	90	5	clay		8170	396	1300	0.004	
90	95	5	clay		8170	396	1300	0.004	
95	100	5	clay		8170	396	1300	0.004	
						Vs(d) = 361	1186		
						Vs30 = 359			

REFERENCES

Cohesionless Soil, Sykora (1987): $V_s = 100.5(N_{60})^{0.29}$

V_s=shear wave velocity (m/s)

N₆₀=SPT blowcount corrected for hammer energy only

Cohesive Soil, Dickenson (1994): $V_s = 203(S_u/2000)^{0.475}$

V_s=shear wave velocity (m/s)

S_u=undrained shear strength (psf)

Averaging method (Geotechnical Services Design Manual Version 1.0 August 2009 Section 1.1.7) $V_{s30} = 100 \text{ feet} / (D_1/V_{s1} + D_2/V_{s2} + \dots + D_n/V_{sn})$

Manual Version 1.0 August 2009 Section 1.1.7)

V_{s30}= average shear wave velocity in ft/sec upper 30 m (100 feet)

Di= layer thickness (feet) for individual layers

V_{si}= shear wave velocity (ft/sec) for individual layers



SHEAR WAVE VELOCITY CALCULATIONS

Boring: **A-13-005**
 Boring Depth 100

Depth (feet)		layer thickness, Di (feet)	soil type	N ₆₀	Su (psf)	Vs		Di (ft) / Vs (fps)	
from	to					m/s	ft/sec		
0	6.25	6.25	clay		4500	298	979	0.006	soil
6.25	9.375	3.125	clay		4500	298	979	0.003	
9.375	13.125	3.75	clay		8170	396	1300	0.003	rock
13.125	17.5	4.375	clay		8170	396	1300	0.003	
17.5	22.5	5	clay		8170	396	1300	0.004	
22.5	27.5	5	clay		8170	396	1300	0.004	
27.5	32.5	5	clay		8170	396	1300	0.004	
32.5	37.5	5	clay		8170	396	1300	0.004	
37.5	42.5	5	clay		8170	396	1300	0.004	
42.5	47.5	5	clay		8170	396	1300	0.004	
47.5	50	2.5	clay		8170	396	1300	0.002	
50	55	5	clay		8170	396	1300	0.004	
55	60	5	clay		8170	396	1300	0.004	
60	65	5	clay		8170	396	1300	0.004	
65	70	5	clay		8170	396	1300	0.004	
70	75	5	clay		8170	396	1300	0.004	
75	80	5	clay		8170	396	1300	0.004	
80	85	5	clay		8170	396	1300	0.004	
85	90	5	clay		8170	396	1300	0.004	
90	100	10	clay		8170	396	1300	0.008	
						Vs(d) = 384	1261		
						Vs30 = 382			

REFERENCES

Cohesionless Soil, Sykora (1987): $V_s = 100.5(N_{60})^{0.29}$

V_s=shear wave velocity (m/s)

N₆₀=SPT blowcount corrected for hammer energy only

Cohesive Soil, Dickenson (1994): $V_s = 203(S_u/2000)^{0.475}$

V_s=shear wave velocity (m/s)

S_u=undrained shear strength (psf)

Averaging method (Geotechnical Services Design Manual Version 1.0 August 2009 Section 1.1.7) $V_{s30} = 100 \text{ feet} / (D_1/V_{s1} + D_2/V_{s2} + \dots + D_n/V_{sn})$

Manual Version 1.0 August 2009 Section 1.1.7

V_{s30}= average shear wave velocity in ft/sec upper 30 m (100 feet)

D_i= layer thickness (feet) for individual layers

V_{s_i}= shear wave velocity (ft/sec) for individual layers



SHEAR WAVE VELOCITY CALCULATIONS

Boring: **A-13-006**
 Boring Depth 100

Depth (feet)		layer thickness, Di (feet)	soil type	N ₆₀	Su (psf)	Vs		Di (ft) / Vs (fps)	
from	to					m/s	ft/sec		
0	6.25	6.25	clay		4000	282	926	0.007	soil
6.25	8.75	2.5	clay		1500	177	581	0.004	
8.75	12.5	3.75	clay		1500	177	581	0.006	
12.5	17.5	5	clay		3500	265	869	0.006	
17.5	22.5	5	clay		4000	282	926	0.005	
22.5	27.5	5	clay		8170	396	1300	0.004	rock
27.5	32.5	5	clay		8170	396	1300	0.004	
32.5	37.5	5	clay		8170	396	1300	0.004	
37.5	42.5	5	clay		8170	396	1300	0.004	
42.5	47.5	5	clay		8170	396	1300	0.004	
47.5	50	2.5	clay		8170	396	1300	0.002	
50	55	5	clay		8170	396	1300	0.004	
55	60	5	clay		8170	396	1300	0.004	
60	65	5	clay		8170	396	1300	0.004	
65	70	5	clay		8170	396	1300	0.004	
70	75	5	clay		8170	396	1300	0.004	
75	80	5	clay		8170	396	1300	0.004	
80	85	5	clay		8170	396	1300	0.004	
85	90	5	clay		8170	396	1300	0.004	
90	100	10	clay		8170	396	1300	0.008	
						Vs(d) = 345		1132	
						Vs30 = 343			

REFERENCES

Cohesionless Soil, Sykora (1987): $V_s = 100.5(N_{60})^{0.29}$

V_s=shear wave velocity (m/s)

N₆₀=SPT blowcount corrected for hammer energy only

Cohesive Soil, Dickenson (1994): $V_s = 203(S_u/2000)^{0.475}$

V_s=shear wave velocity (m/s)

S_u=undrained shear strength (psf)

Averaging method (Geotechnical Services Design Manual Version 1.0 August 2009 Section 1.1.7) $V_{s30} = 100 \text{ feet} / (D_1/V_{s1} + D_2/V_{s2} + \dots + D_n/V_{sn})$

Manual Version 1.0 August 2009 Section 1.1.7

V_{s30}= average shear wave velocity in ft/sec upper 30 m (100 feet)

D_i= layer thickness (feet) for individual layers

V_{s_i}= shear wave velocity (ft/sec) for individual layers



SITE DATA (ARS Online Version 2.3.06)

Shear Wave Velocity, V_{s30} : 360 m/s
Latitude: 34.143300
Longitude: -118.737900
Depth to $V_s = 1.0$ km/s: N/A
Depth to $V_s = 2.5$ km/s: N/A

DETERMINISTIC

Anacapa-Dume alt 1

Fault ID: 348
Maximum Magnitude (MMax): 7.2
Fault Type: Rev
Fault Dip: 45 Deg
Dip Direction: N
Bottom of Rupture Plane: 15.60 km
Top of Rupture Plane(Ztor): 0.00 km
Rrup: 12.99 km
Rjb: 2.77 km
Rx: 18.37 km
Fnorm: 0
Frev: 1

Period	SA(Base Spectrum)	Basin Factor	Near Fault Factor(Applied)	SA(Final Spectrum)
0.01	0.432	1.000	1.000	0.432
0.05	0.550	1.000	1.000	0.550
0.1	0.783	1.000	1.000	0.783
0.15	0.933	1.000	1.000	0.933
0.2	0.978	1.000	1.000	0.978
0.25	0.962	1.000	1.000	0.962
0.3	0.930	1.000	1.000	0.930
0.4	0.843	1.000	1.000	0.843
0.5	0.759	1.000	1.000	0.759
0.6	0.671	1.000	1.040	0.697
0.7	0.601	1.000	1.080	0.649
0.85	0.516	1.000	1.140	0.588
1	0.447	1.000	1.200	0.536
1.2	0.370	1.000	1.200	0.444
1.5	0.284	1.000	1.200	0.341
2	0.183	1.000	1.200	0.219
3	0.092	1.000	1.200	0.111
4	0.058	1.000	1.200	0.070
5	0.045	1.000	1.200	0.054

Santa Monica fault

Fault ID: 341
Maximum Magnitude (MMax): 7
Fault Type: SS
Fault Dip: 75 Deg
Dip Direction: N
Bottom of Rupture Plane: 17.90 km
Top of Rupture Plane(Ztor): 0.00 km
Rrup 14.25 km
Rjb: 9.95 km
Rx: 14.75 km
Fnorm: 0
Frev: 0

Period	SA(Base Spectrum)	Basin Factor	Near Fault Factor(Applied)	SA(Final Spectrum)
0.01	0.257	1.000	1.000	0.257
0.05	0.322	1.000	1.000	0.322
0.1	0.471	1.000	1.000	0.471
0.15	0.562	1.000	1.000	0.562
0.2	0.584	1.000	1.000	0.584
0.25	0.568	1.000	1.000	0.568
0.3	0.545	1.000	1.000	0.545
0.4	0.489	1.000	1.000	0.489
0.5	0.437	1.000	1.000	0.437
0.6	0.383	1.000	1.040	0.399
0.7	0.342	1.000	1.080	0.369
0.85	0.293	1.000	1.140	0.334
1	0.255	1.000	1.200	0.306
1.2	0.214	1.000	1.200	0.257
1.5	0.170	1.000	1.200	0.204
2	0.119	1.000	1.200	0.143
3	0.069	1.000	1.200	0.083
4	0.047	1.000	1.200	0.057
5	0.036	1.000	1.200	0.043

Malibu Coast alt 2

Fault ID: 346
Maximum Magnitude (MMax): 6.6
Fault Type: SS
Fault Dip: 74 Deg
Dip Direction: N
Bottom of Rupture Plane: 16.30 km
Top of Rupture Plane(Ztor): 0.00 km
Rrup 11.82 km
Rjb: 7.62 km
Rx: 12.29 km

Fnorm: 0
Frev: 0

Period	SA(Base Spectrum)	Basin Factor	Near Fault Factor(Applied)	SA(Final Spectrum)
0.01	0.267	1.000	1.000	0.267
0.05	0.335	1.000	1.000	0.335
0.1	0.494	1.000	1.000	0.494
0.15	0.587	1.000	1.000	0.587
0.2	0.608	1.000	1.000	0.608
0.25	0.587	1.000	1.000	0.587
0.3	0.561	1.000	1.000	0.561
0.4	0.502	1.000	1.000	0.502
0.5	0.440	1.000	1.000	0.440
0.6	0.378	1.000	1.040	0.393
0.7	0.332	1.000	1.080	0.358
0.85	0.278	1.000	1.140	0.317
1	0.237	1.000	1.200	0.285
1.2	0.195	1.000	1.200	0.234
1.5	0.151	1.000	1.200	0.181
2	0.102	1.000	1.200	0.122
3	0.057	1.000	1.200	0.068
4	0.038	1.000	1.200	0.045
5	0.028	1.000	1.200	0.034

PROBABILISTIC

**Probabilistic Model
USGS Seismic Hazard Map(2008) 975 Year Return Period**

Period	SA(Base Spectrum)	Basin Factor	Near Fault Factor(Applied)	SA(Final Spectrum)
0.01	0.567	1.000	1.000	0.567
0.05	0.872	1.000	1.000	0.872
0.1	1.049	1.000	1.000	1.049
0.15	1.192	1.000	1.000	1.192
0.2	1.305	1.000	1.000	1.305
0.25	1.282	1.000	1.000	1.282
0.3	1.263	1.000	1.000	1.263
0.4	1.137	1.000	1.000	1.137
0.5	1.048	1.000	1.000	1.048
0.6	0.935	1.000	1.040	0.972
0.7	0.849	1.000	1.080	0.917
0.85	0.726	1.000	1.140	0.828
1	0.627	1.000	1.200	0.752
1.2	0.512	1.000	1.200	0.614

1.5	0.399	1.000	1.200	0.479
2	0.290	1.000	1.200	0.348
3	0.175	1.000	1.200	0.209
4	0.122	1.000	1.200	0.147
5	0.101	1.000	1.200	0.121

MINIMUM DETERMINISTIC SPECTRUM

Period	SA
0.01	0.225
0.05	0.283
0.1	0.422
0.15	0.504
0.2	0.522
0.25	0.505
0.3	0.482
0.4	0.430
0.5	0.375
0.6	0.320
0.7	0.280
0.85	0.233
1	0.198
1.2	0.162
1.5	0.125
2	0.086
3	0.050
4	0.034
5	0.025

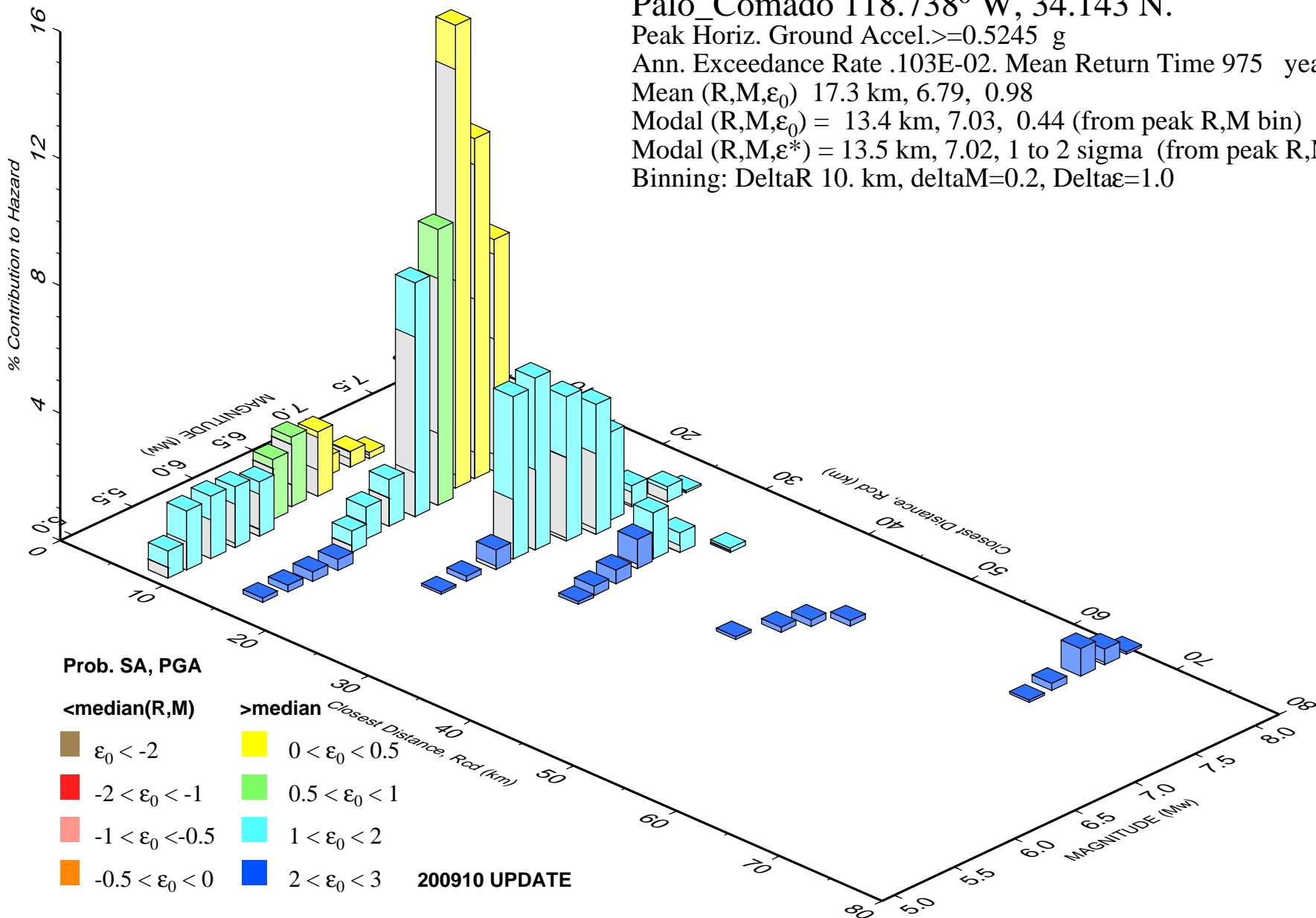
Envelope Data

Period	SA
0.01	0.567
0.05	0.872
0.1	1.049
0.15	1.192
0.2	1.305
0.25	1.282
0.3	1.263
0.4	1.137
0.5	1.048
0.6	0.972
0.7	0.917
0.85	0.828
1	0.752

1.2	0.614
1.5	0.479
2	0.348
3	0.209
4	0.147
5	0.121

PSH Deaggregation on NEHRP CD soil Palo_Comado 118.738° W, 34.143 N.

Peak Horiz. Ground Accel. ≥ 0.5245 g
 Ann. Exceedance Rate .103E-02. Mean Return Time 975 years
 Mean (R,M, ϵ_0) 17.3 km, 6.79, 0.98
 Modal (R,M, ϵ_0) = 13.4 km, 7.03, 0.44 (from peak R,M bin)
 Modal (R,M, ϵ^*) = 13.5 km, 7.02, 1 to 2 sigma (from peak R,M, ϵ bin)
 Binning: DeltaR 10. km, deltaM=0.2, Delta ϵ =1.0



PSH Deaggregation on NEHRP CD soil

Palo_Comado 118.738° W, 34.143 N.

SA period 0.30 sec. Accel. \geq 1.1812 g

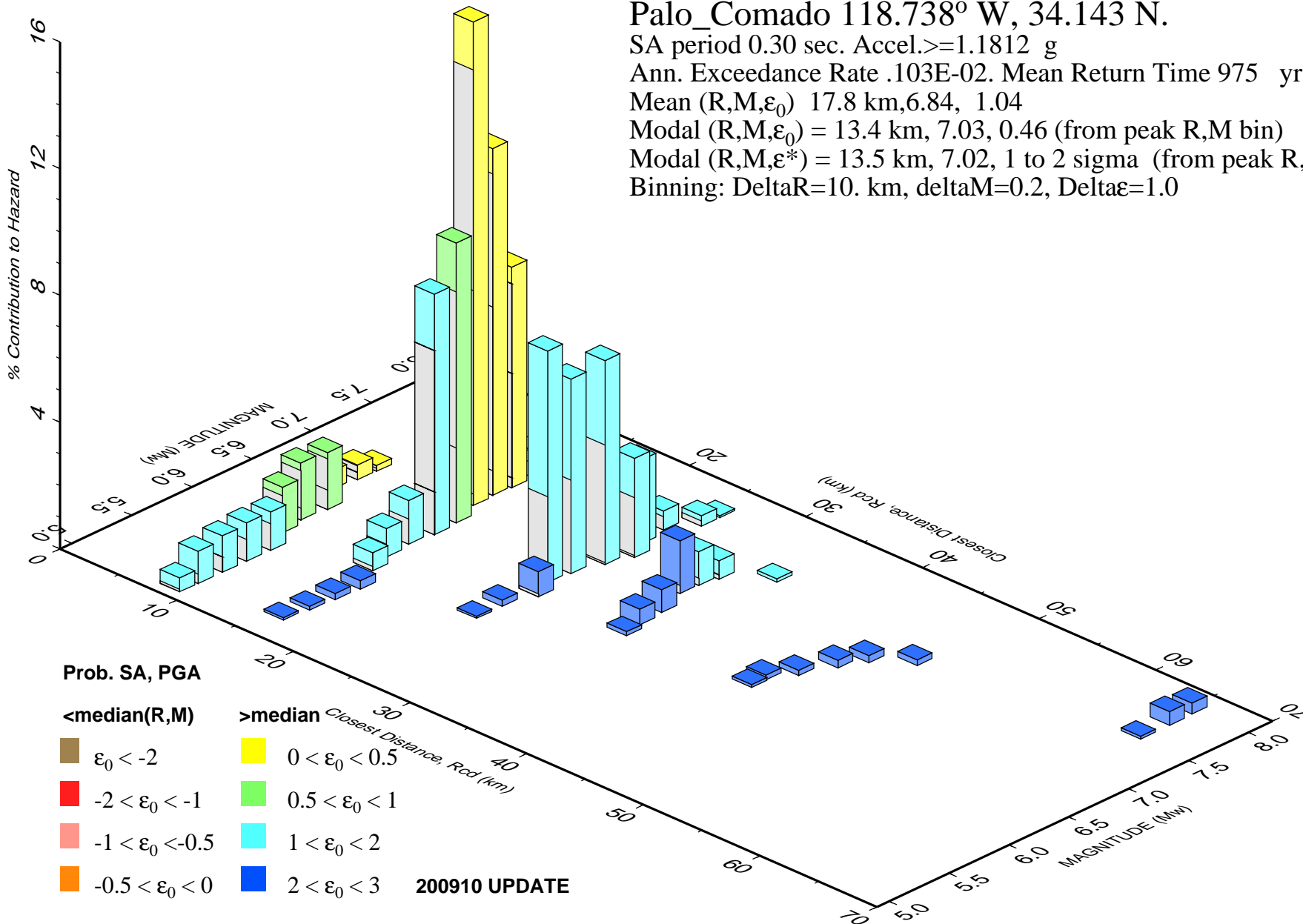
Ann. Exceedance Rate .103E-02. Mean Return Time 975 yrs

Mean (R,M, ϵ_0) 17.8 km,6.84, 1.04

Modal (R,M, ϵ_0) = 13.4 km, 7.03, 0.46 (from peak R,M bin)

Modal (R,M, ϵ^*) = 13.5 km, 7.02, 1 to 2 sigma (from peak R,M, ϵ bin)

Binning: DeltaR=10. km, deltaM=0.2, Delta ϵ =1.0



PSH Deaggregation on NEHRP CD soil

Palo_Comado 118.738° W, 34.143 N.

SA period 1.00 sec. Accel. \geq 0.5801 g

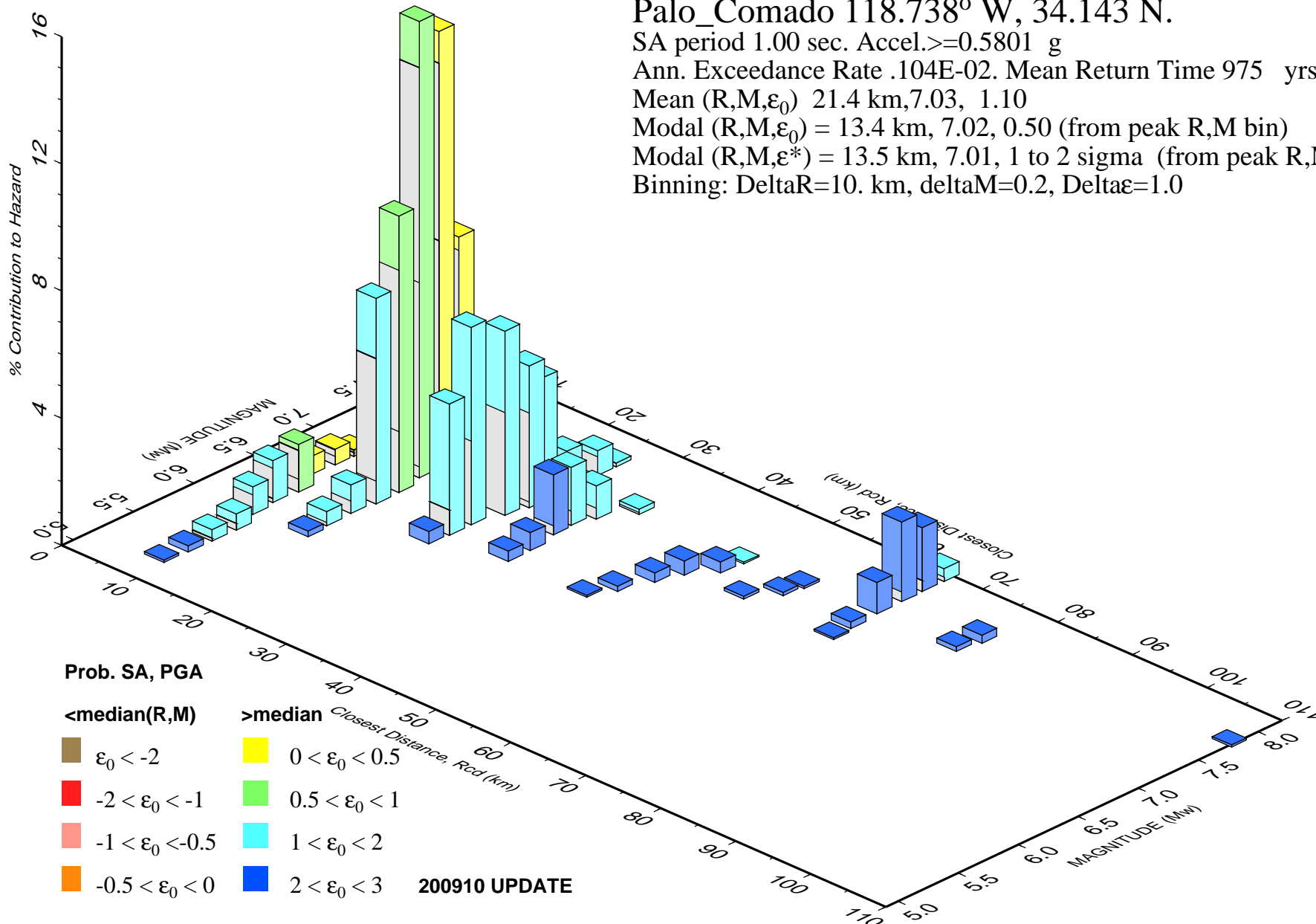
Ann. Exceedance Rate .104E-02. Mean Return Time 975 yrs

Mean (R,M, ϵ_0) 21.4 km,7.03, 1.10

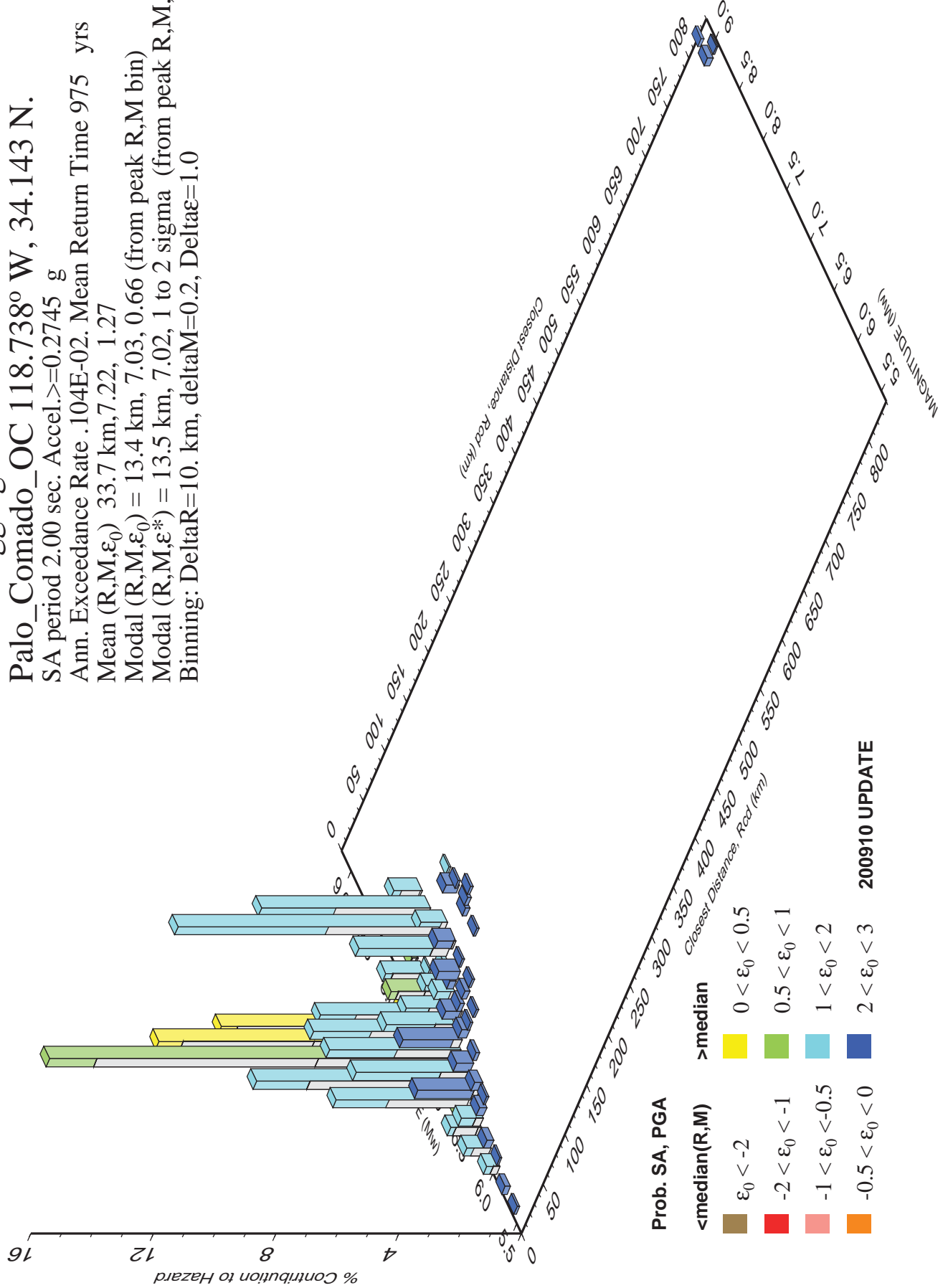
Modal (R,M, ϵ_0) = 13.4 km, 7.02, 0.50 (from peak R,M bin)

Modal (R,M, ϵ^*) = 13.5 km, 7.01, 1 to 2 sigma (from peak R,M, ϵ bin)

Binning: DeltaR=10. km, deltaM=0.2, Delta ϵ =1.0



PSH Deaggregation on NEHRP CD soil
 Palo_Comado_OC 118.738° W, 34.143 N.
 SA period 2.00 sec. Accel.>=0.2745 g
 Ann. Exceedance Rate .104E-02. Mean Return Time 975 yrs
 Mean (R,M, ϵ_0) 33.7 km, 7.22, 1.27
 Modal (R,M, ϵ_0) = 13.4 km, 7.03, 0.66 (from peak R,M bin)
 Modal (R,M, ϵ^*) = 13.5 km, 7.02, 1 to 2 sigma (from peak R,M, ϵ bin)
 Binning: DeltaR=10. km, deltaM=0.2, Delta ϵ =1.0



PSH Deaggregation on NEHRP CD soil

Palo_Comado 118.738° W, 34.143 N.

SA period 3.00 sec. Accel.>=0.1674 g

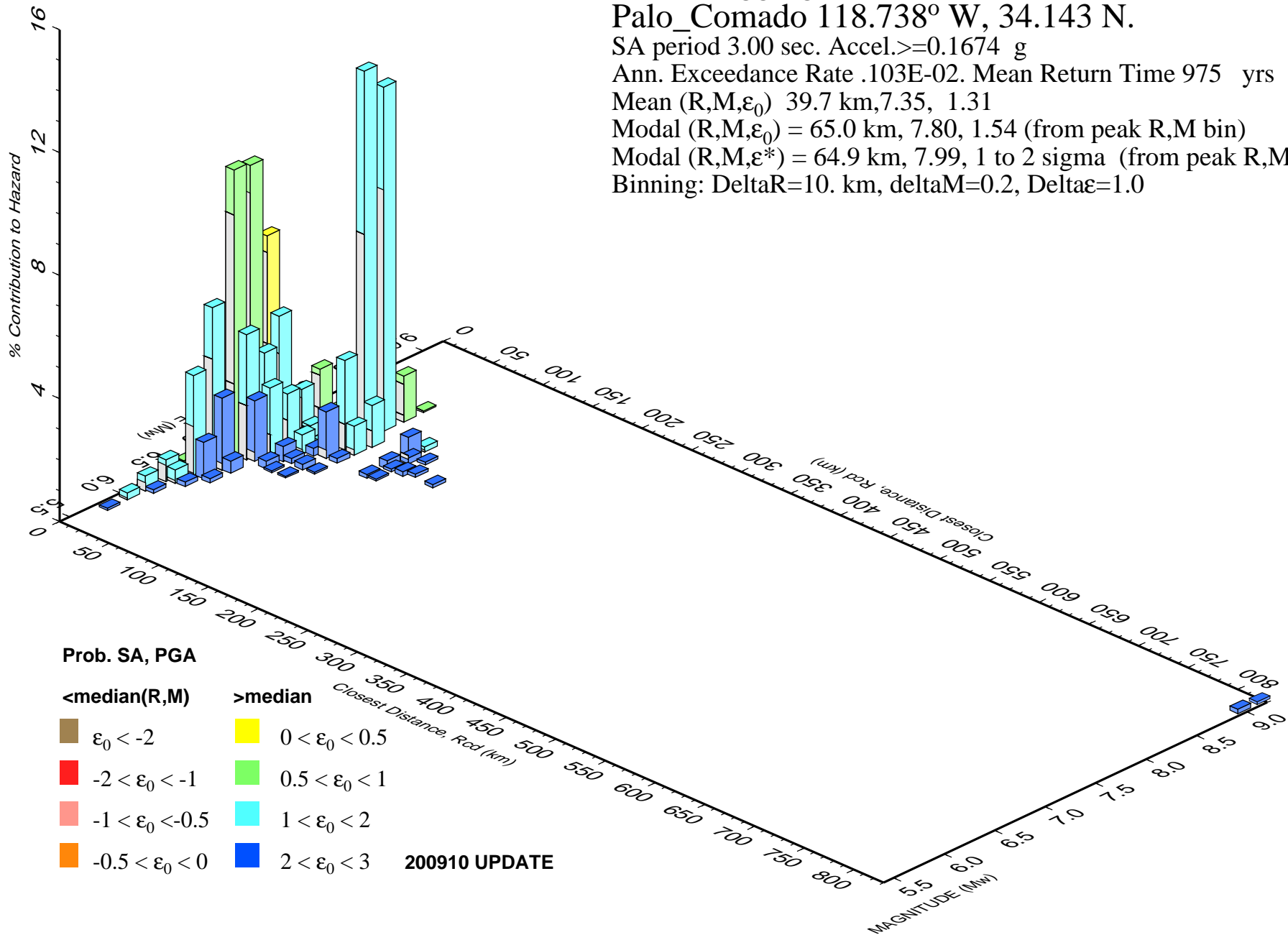
Ann. Exceedance Rate .103E-02. Mean Return Time 975 yrs

Mean (R,M, ϵ_0) 39.7 km,7.35, 1.31

Modal (R,M, ϵ_0) = 65.0 km, 7.80, 1.54 (from peak R,M bin)

Modal (R,M, ϵ^*) = 64.9 km, 7.99, 1 to 2 sigma (from peak R,M, ϵ bin)

Binning: DeltaR=10. km, deltaM=0.2, Delta ϵ =1.0



Prob. SA, PGA

<median(R,M)

>median

$\epsilon_0 < -2$

$0 < \epsilon_0 < 0.5$

$-2 < \epsilon_0 < -1$

$0.5 < \epsilon_0 < 1$

$-1 < \epsilon_0 < -0.5$

$1 < \epsilon_0 < 2$

$-0.5 < \epsilon_0 < 0$

$2 < \epsilon_0 < 3$

200910 UPDATE

APPENDIX D-2

AXIAL PILE CAPACITY CALCULATIONS

PROJECT NUMBER / NAME: LA-1143/Palo Comado OC

CALCULATION NAME: 16 inch CIHD Abutment 1L

Req. Nom. = N/A kips

Factored= 140 kips

Req. Nom. T= N/A kips

File Diameter= 1.33333 ft
Perimeters= 4.189 ft
End Area= 1.396 ft^2

Group Efficiency Factor= 1.0
SPT= 0.80 inch
Limiting Settlement for Obse= 0.00 inch
Overburden at pile cutoff= 0.21735 ksf
Depth of overburden= 1.89 ft

Pile head below ground surface (ft) 1.89
Groundwater below ground surface (ft) 0
Groundwater below pile head (ft) 98.11

Nominal Comp Plot Depth (ft) 0
Nominal Resistance (kips) 0
N/A

Strength Plot Depth (ft) 0
Factored Load (kips) 140
35 140 0

Nominal Tension Plot Depth (ft) 0
Nominal Load (kips) 0
N/A N/A 0

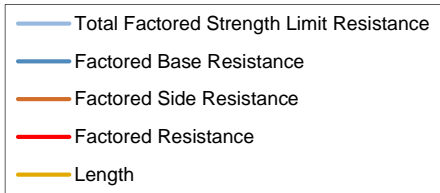
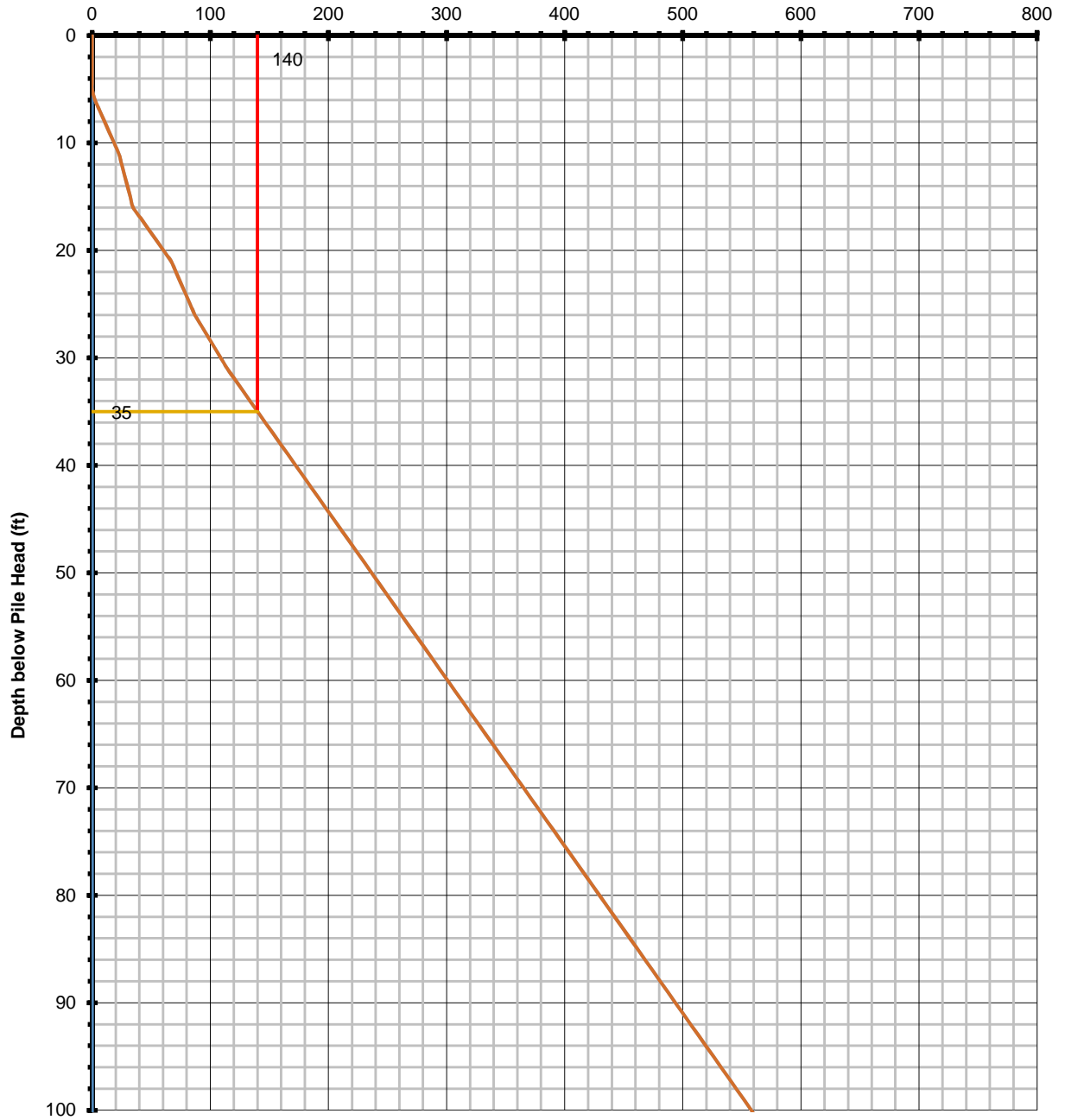
Table with columns: Elevation (ft), Layer Bottom Depth (ft), Layer Bottom below ground (ft), SAND or CLAY, SAND SPT or CLAY U (ksf), EFFECTIVE UNIT WEIGHT (pcf), Mid-Layer (kSF), User Input Friction Factor, SAND Friction Factor for SPT N60, Friction Factor for Group Efficiency, beta, alpha, fs (ksf), Pile Depth (ft), A (ft^2), fs * As (kips), Qs = 1/2 * fs * As (kips), Strength Limit State Factored, User Input Factor on Base Resistance, Undrained Modulus Es (ksf), Nominal Resistance at 5%Q (kips), Nominal Base Resistance at 5%Q (kips), Nominal Base Resistance at Specified Settlement (kips), Strength Limit State Factored Base Resistance (kips), Factored Compression Resistance State 0.5*QB+0.7*QS (kips), Compression Resistance Extreme Event QB-QS (kips), Tension Extreme Event QSP-QS (kips)



LA-1143/Palo Comado OC

16 inch CIDH Abutment 1L

Strength Limit Factored Nominal Resistance (kips)



PROJECT NUMBER / NAME: LA-1143/Palo Comado OC

CALCULATION NAME: 16 inch CIHD Abutment 1R

Req. Nom. = N/A kips

Factored = 160 kips

Req. Nom. T_e = N/A kips

File Diameter = 1.333333 ft
Perimeter = 4.189 ft
End Area = 1.396 ft²

Group Efficiency Factor = 1
5% D = 0.80 inch
Limiting Settlement for Overturbled at pile cutoff = 0.000 inch ksf
Depth of overburden = 1.17 ft

Pile head below ground surface (ft) = 1.17
Groundwater below ground surface (ft) = 1.00
Groundwater below pile head (ft) = 98.83

Nominal Comp Plot Depth (ft) = 0
Load (kips) = 0
N/A

Strength Plot Depth (ft) = 0
Factored Load (kips) = 160
N/A

Nominal Tension Plot Depth (ft) = 0
Load (kips) = 0
N/A

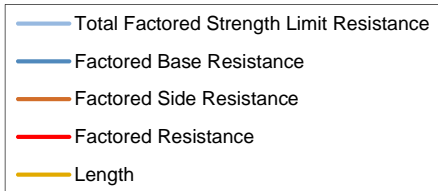
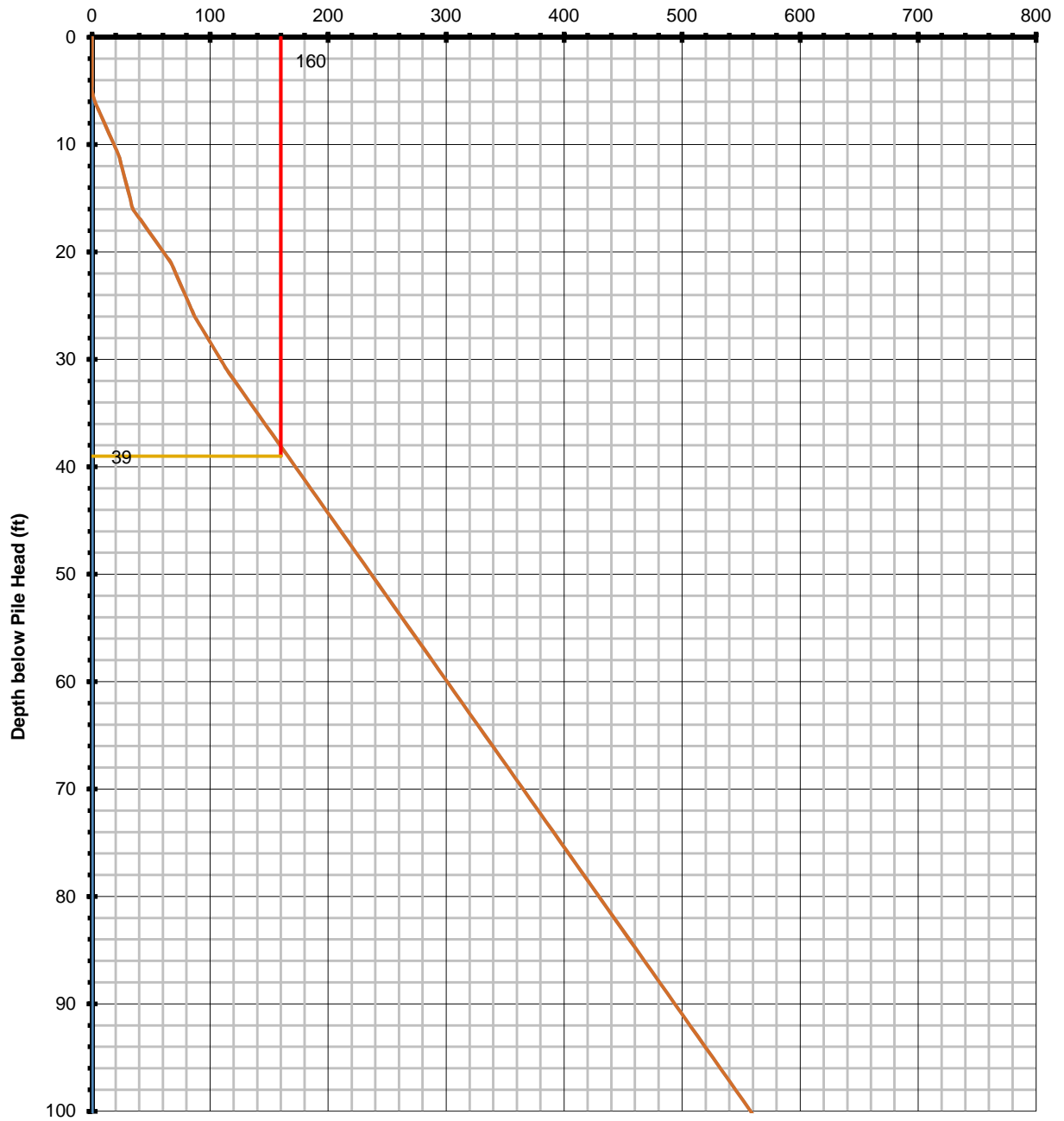
Table with columns: Elevation (ft), Layer Bottom Depth below Pile Head (ft), Layer Depth below ground (ft), SAND or CLAY, SAND SPT N₆₀ or CLAY γ (pcf), EFFECTIVE UNIT WEIGHT γ (pcf), Mid-Layer γ_{mid} (pcf), User Input Friction Factor, SAND Friction Factor SPT N₆₀, Friction Group Efficiency, β, α, fs (ksf), Pile Depth (ft), A (ft²), Q = γ As (kips), R_s (kips), Strength Limit State Factored Side Compression inResistance 0.7*Q_s (kips), User Input on Base Resistance, Undrained Modulus Es (ksf), Nominal Unit Base Resistance at 5MD (ksf), Nominal Side Base Resistance at 5MD (kips), Nominal Base Resistance at Specified Settlement (kips), Strength Limit State Factored Base Resistance (kips), Factored Compression Resistance Limit State 0.5*Q_{ub}+0.7Q_s (kips), Compression Extreme Event Limit-Q_s (kips), Tension Extreme Event Q_s+0.7*Q_s (kips)



LA-1143/Palo Comado OC

16 inch CIDH Abutment 1R

Strength Limit Factored Nominal Resistance (kips)



PROJECT NUMBER / NAME: LA-1143/Palo Comado CC

CALCULATION NAME: 24 inch CI/DH Bent 2L

Req. Nom. = 300 kips

Factored = 260 kips

Req. Nom. T_c = 140 kips

File Diameter: 2 ft
Perimeters: 6.283 ft
End Area: 3.142 ft²

Group Efficiency Factor: 1
5% D = 1.20 inch
Limiting Settlement for Base-Overburden at pile cutoff: 0.00 inch
Depth of overburden: 2 ft

Head below ground surface (ft): 8.91
Groundwater below ground surface (ft): 1.00
Groundwater below pile head (ft): 91.09

Nominal Comp Plot
Depth (ft) Load (kips)
0 300
27 0
27 300

Strength Plot
Depth (ft) Factored Load (kips)
0 260
32 0
32 260

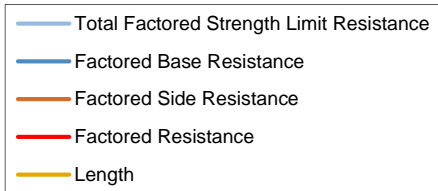
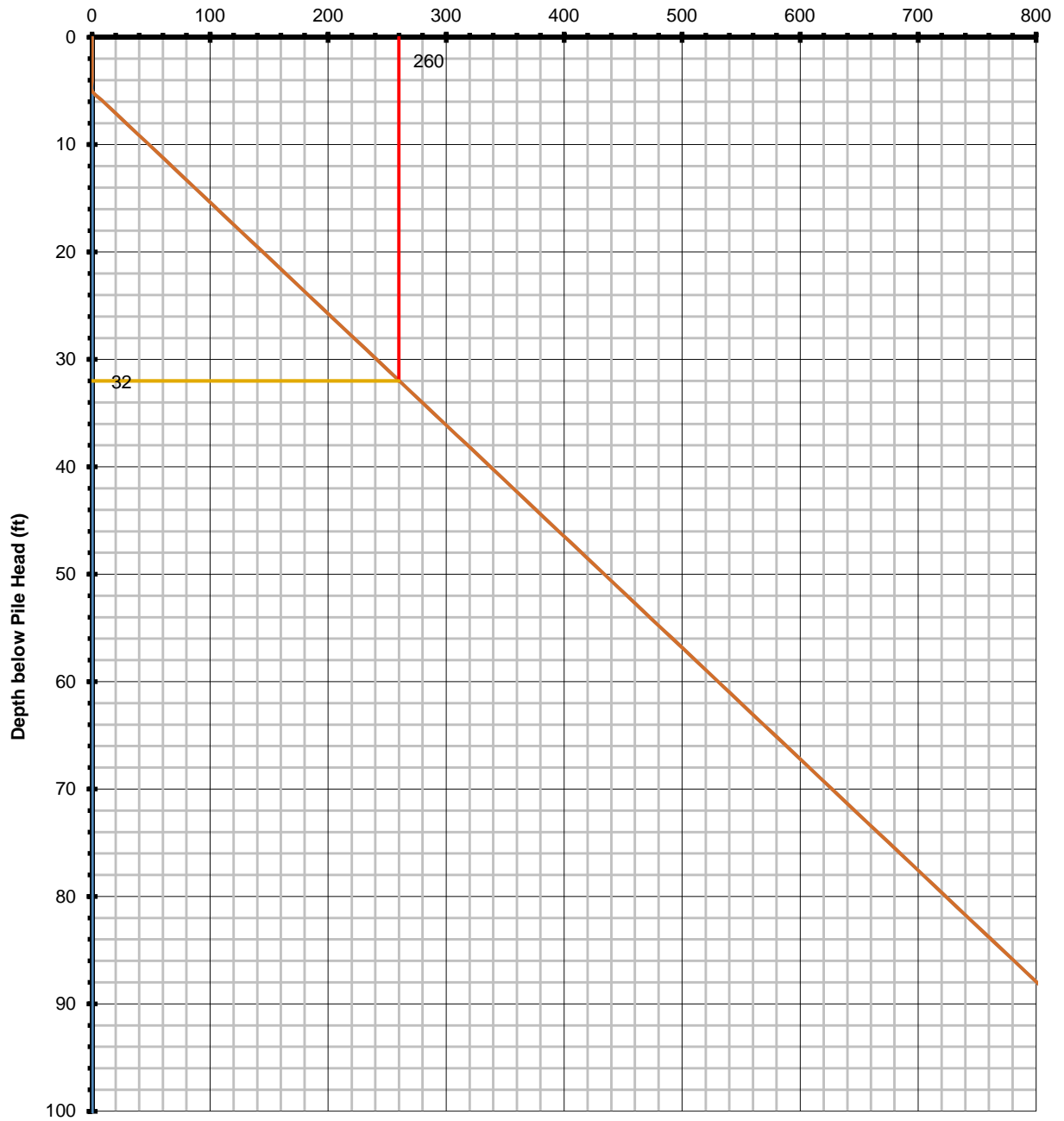
Nominal Tension Plot
Depth (ft) Load (kips)
0 140
20 0
20 140

Table with columns: Elevation (ft), Layer Bottom Depth (ft), Layer Depth (ft), SAND or CLAY, SAND SPT N₆₀ (ksf), EFFECTIVE UNIT WEIGHT γ (pcf), Mid-Layer Friction Factor, User Input Friction Factor, SAND Friction Factor SPT N₆₀, Friction Group Efficiency, β, α, fs (ksf), Pile Depth (ft), α (ft²), Q_s + Q_u (kips), Q_s (kips), Q_u (kips), Strength Limit State Factored Resistance Q_s + Q_u (kips), User Input on Base Resistance, Undrained Modulus E_s (ksf), Nominal Unit Base Resistance at 5MD (ksf), Nominal Side Base Resistance at 5MD (kips), Nominal Base Resistance at Specified Settlement (kips), Strength Limit State Factored Base Resistance (kips), Factored Compression Resistance Strength Limit State 0.5*Q_u+0.7Q_s (kips), Compression Extreme Event Q_u+Q_s (kips), Tension Extreme Event Q_u+0.7Q_s (kips).

LA-1143/Palo Comado OC

24 inch CIDH Bent 2L

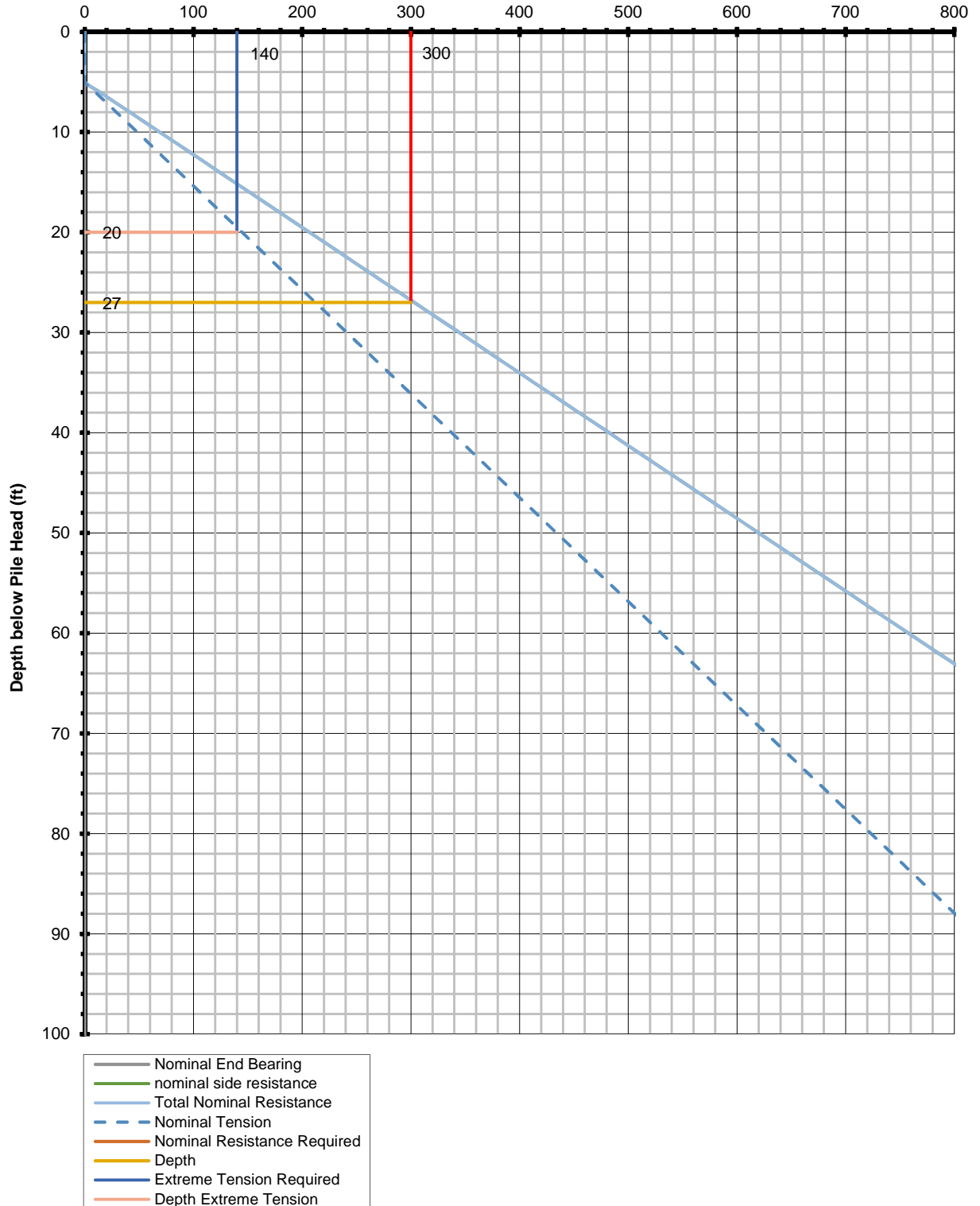
Strength Limit Factored Nominal Resistance (kips)



LA-1143/Palo Comado OC

24 inch CIDH Bent 2L

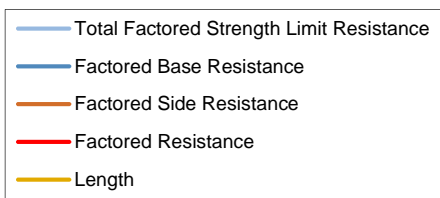
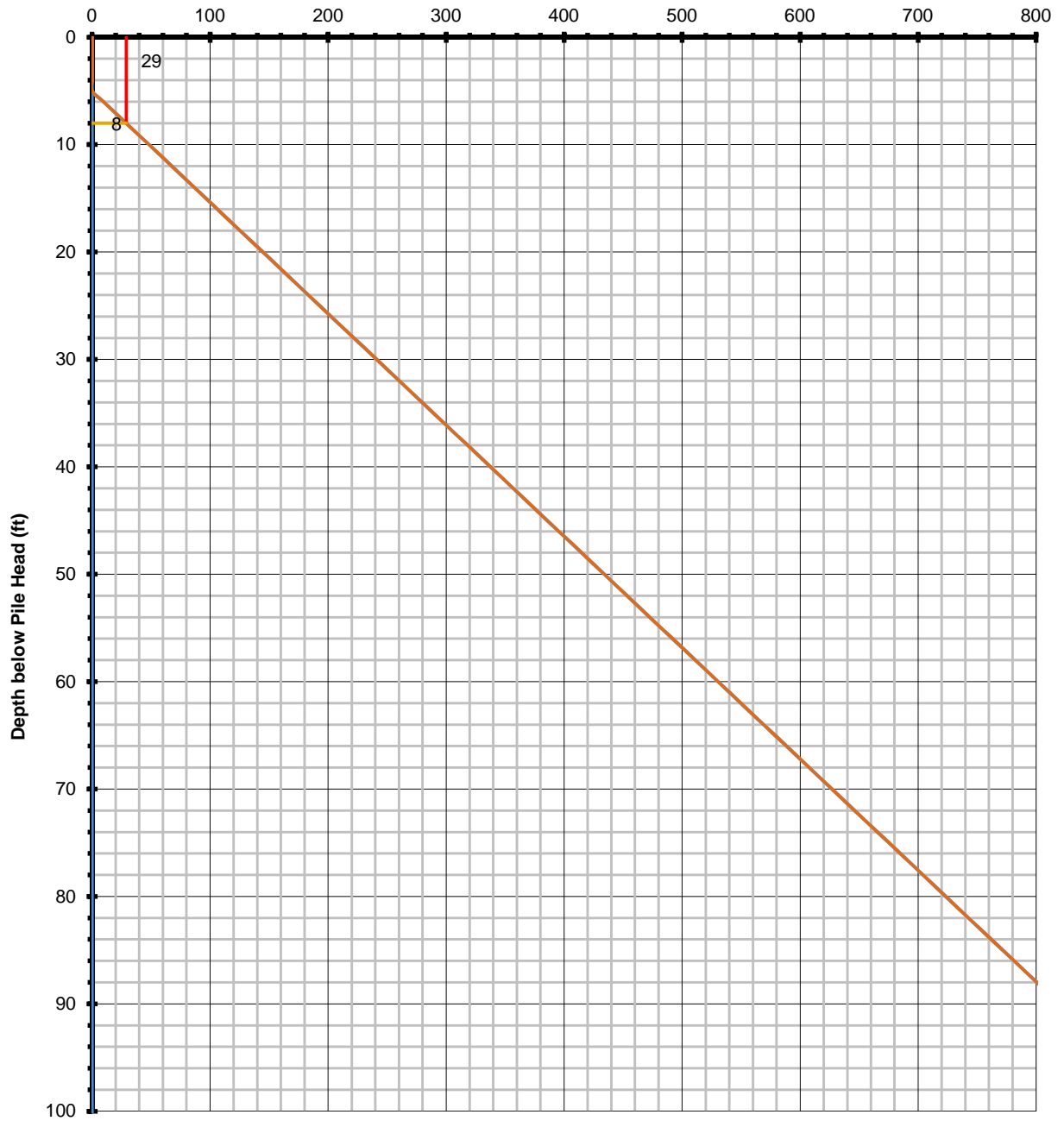
Nominal Resistance (kips)



LA-1143/Palo Comado OC

24 inch CIDH Bent 2L

Strength Limit Factored Nominal Resistance (kips)



PROJECT NUMBER / NAME: LA-1143/Palo Comado CC

CALCULATION NAME: 24 inch CI/DH Bent 2R

Req. Nom. = 320 kips

Factored = 180 kips

Req. Nom. T_e = 180 kips

Summary table with columns: File Diameter, Perimeters, End Area, Group Efficiency Factor, Limiting Settlement, Depth of overburden, Headwater below ground surface (ft), Groundwater below ground surface (ft), Groundwater below pile head (ft), Nominal Comp Plot, Depth (ft), Load (kips), Strength Plot, Depth (ft), Factored Load (kips), Nominal Tension Plot, Depth (ft), Load (kips).

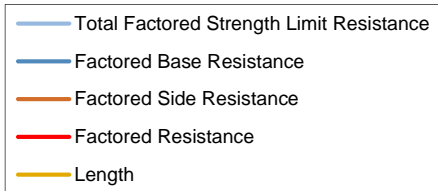
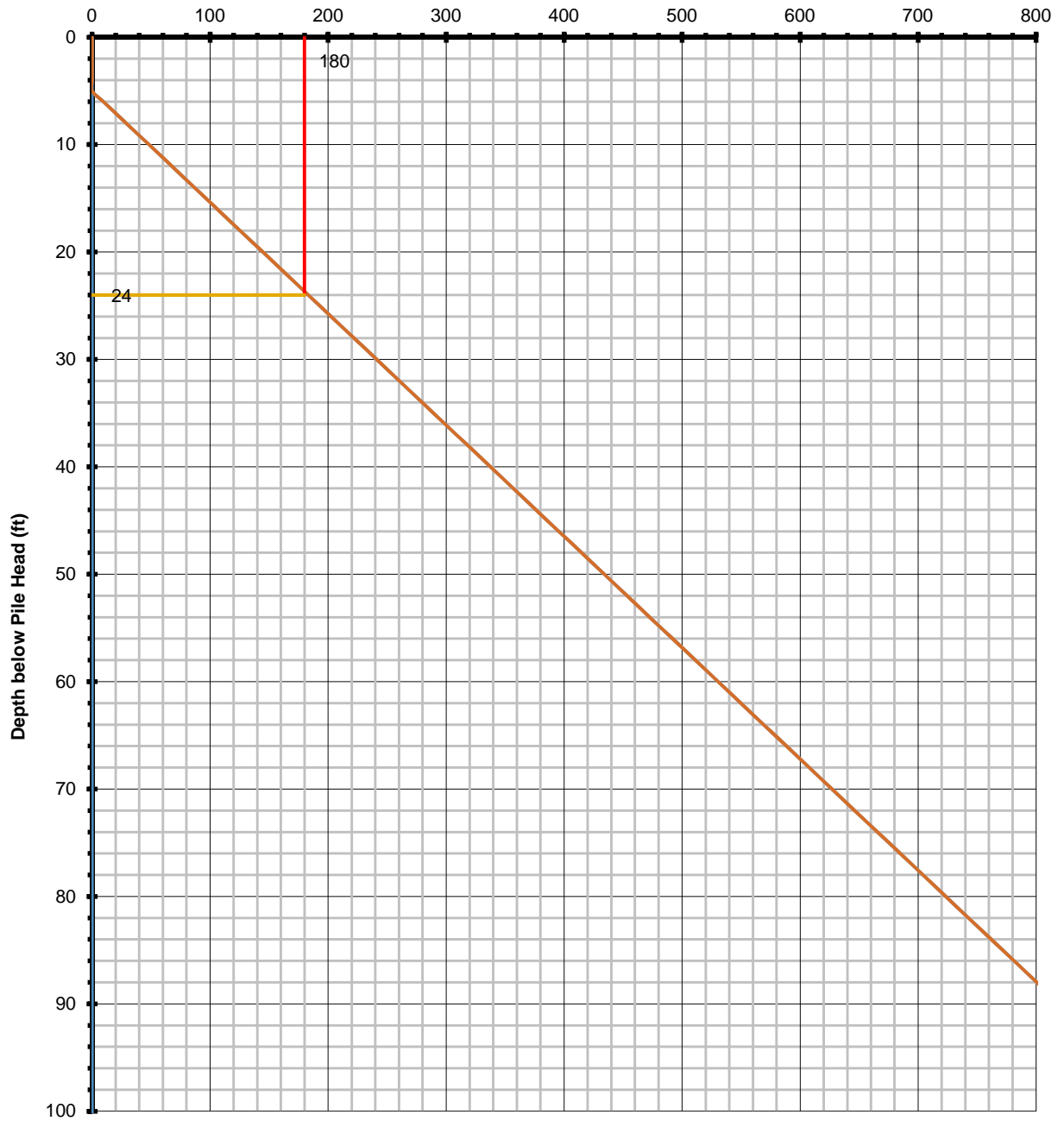
Main data table with columns: Elevation (ft), Layer Bottom Depth below Pile Head (ft), Layer Depth below Pile Head (ft), SAND or CLAY, SAND SPT N₆₀ or CLAY γ (pcf), EFFECTIVE UNIT WEIGHT γ (pcf), Mid-Layer Friction Factor, User Input Friction Factor, SAND Friction Factor SPT N₆₀, Friction Factor Group Efficiency, β, α, fs (ksf), Pile Depth (ft), α (ft²), fs + As (kips), fs + As (kips), Strength Limit State Factored Resistance Q_s = 2 fs * A_s (kips), User Input on Base Resistance, Undrained Modulus E_s (ksf), Nominal Unit Base Resistance at 5MD (ksf), Nominal Side Base Resistance at 5MD (kips), Nominal Side Resistance at Specified Settlement (kips), Strength Limit State Factored Base Resistance (kips), Factored Resistance Strength Limit State 0.5*Q₈₀-0.7Q₂₅, Compression Resistance Extreme Event Q₈₀-Q₂₅ (kips), Tension Extreme Event Q₈₀-Q₂₅ (kips).



LA-1143/Palo Comado OC

24 inch CIDH Bent 2R

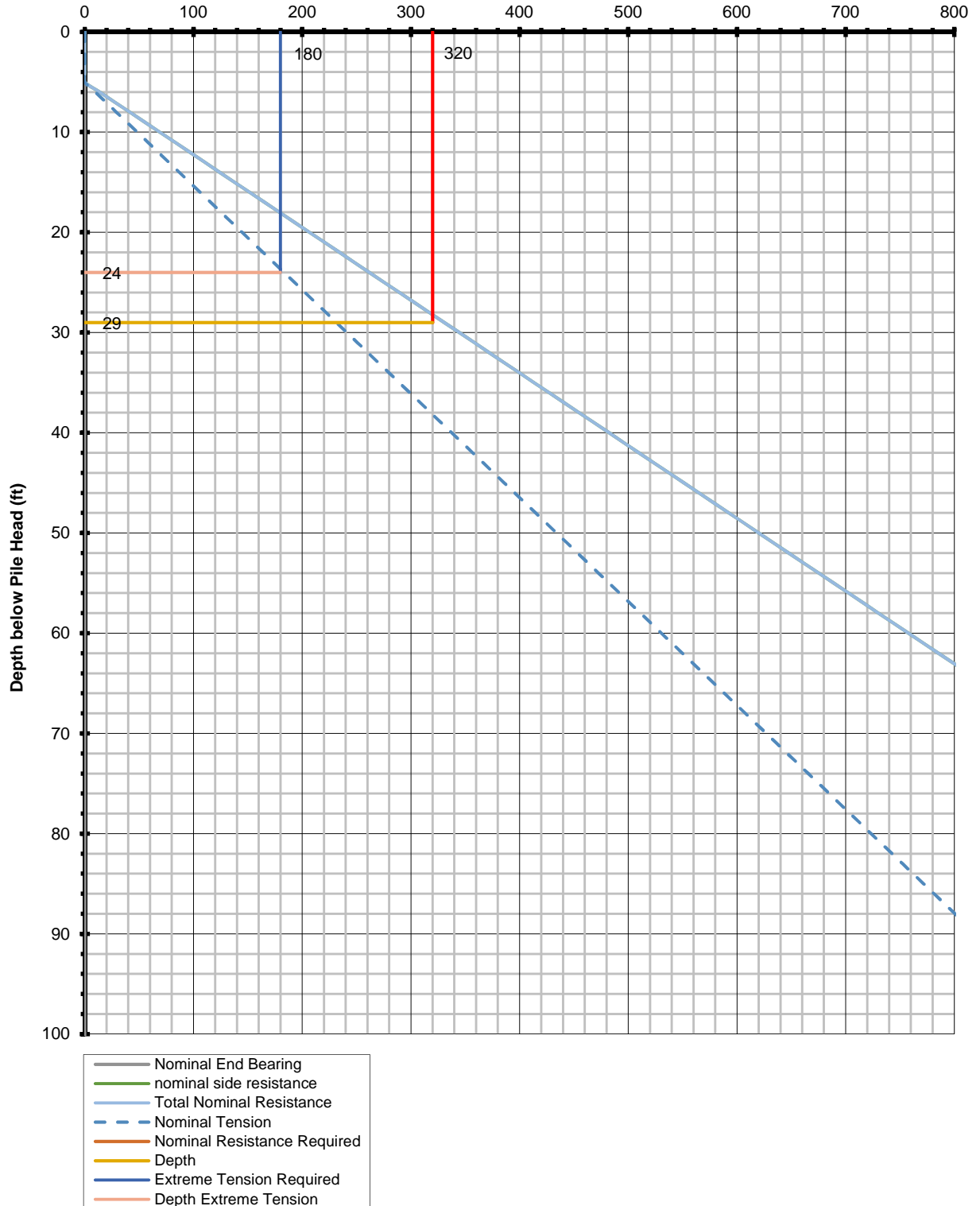
Strength Limit Factored Nominal Resistance (kips)



LA-1143/Palo Comado OC

24 inch CIDH Bent 2R

Nominal Resistance (kips)



PROJECT NUMBER / NAME: LA-1143/Palo Comado CO

CALCULATION NAME: 24 inch CIH Bent 3L

Req. Nom. = 320 kips

Factored = 280 kips

Req. Nom. T_e = 120 kips

File Diameter: 2 ft
Perimeters: 6.283 ft
End Area: 3.142 ft²

Group Efficiency Factor: 1
5% D= 1.20 inch
Limiting Settlement for Obse- Overburden at pile cutoff: 0.00 0.23 inch ksf
Depth of overburden: 2 ft

Pile head below ground surface (ft): 9.66
Groundwater below ground surface (ft): 100
Groundwater below pile head (ft): 90.34

Nominal Comp Plot Depth (ft) Load (kips)
0 320
29 0 320
29 0 320

Strength Plot Depth (ft) Factored Load (kips)
0 280
35 0 280
35 0 280

Nominal Tension Plot Depth (ft) Load (kips)
0 120
18 0 120
18 0 120

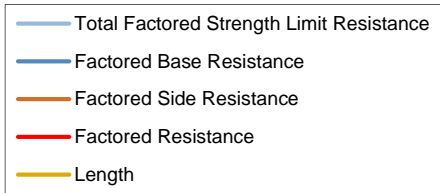
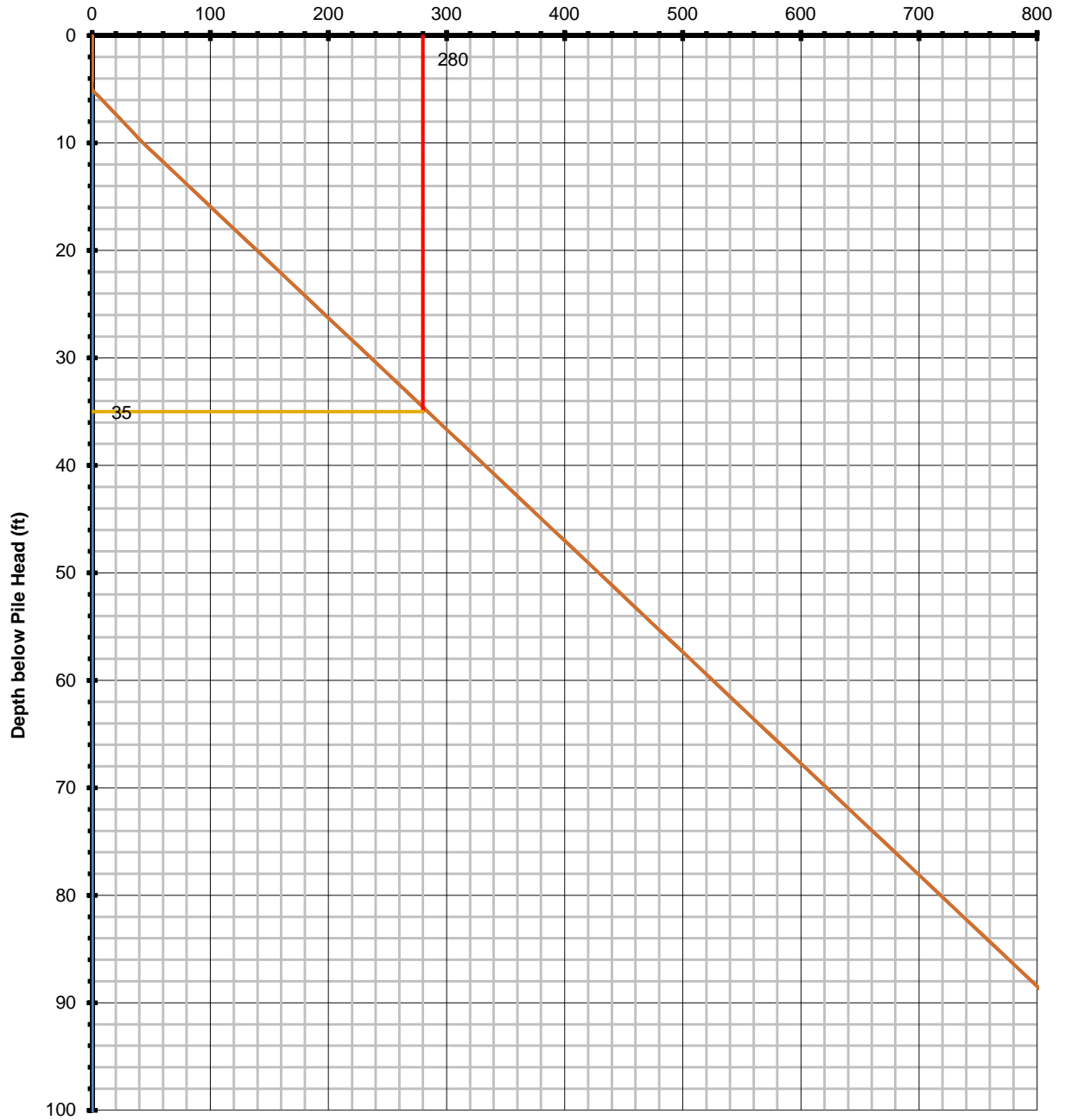
Table with columns: Elevation (ft), Layer Bottom Depth below Pile Head (ft), Layer Depth below ground (ft), SAND or CLAY, SAND SPT N₆₀ or CLAY S₆₀, EFFECTIVE UNIT WEIGHT γ (pcf), Mid-Layer γ_{av} (pcf), User Input Friction Factor, SAND Friction Factor SPT N₆₀, Friction Group Efficiency, β, α, f_s (ksf), Pile Depth (ft), A (ft²), f_s * A (kips), Q_s * A (kips), Strength Limit State Factored Resistance Q_s*A (kips), User Input on Base Resistance, Undrained Modulus E_s (ksf), Nominal Unit Base Resistance at 5MD (ksf), Nominal Side Base Resistance at 5MD (kips), Nominal Side Resistance at Specified Settlement (kips), Strength Limit State Factored Base Resistance (kips), Factored Compression Resistance Limit State 0.5*Q_{08-0.7Q₀₅} (kips), Compression Resistance Extreme Event Q_{08-GS} (kips), Tension Extreme Event Q_{05-0.7Q₀₅} (kips)



LA-1143/Palo Comado OC

24 inch CIDH Bent 3L

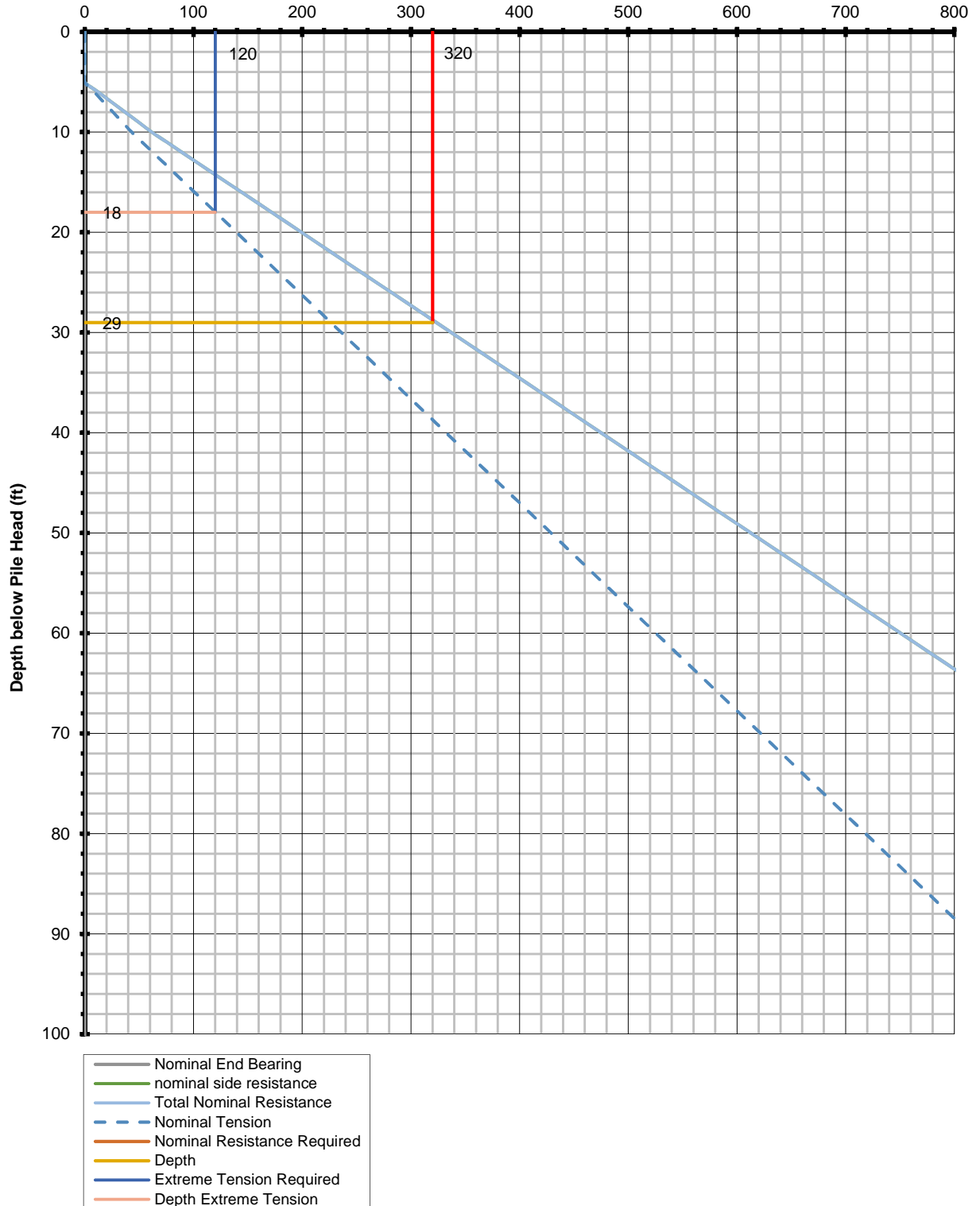
Strength Limit Factored Nominal Resistance (kips)



LA-1143/Palo Comado OC

24 inch CIDH Bent 3L

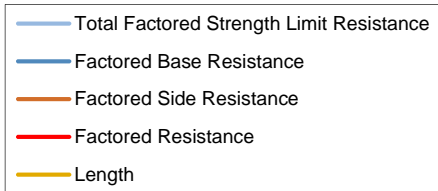
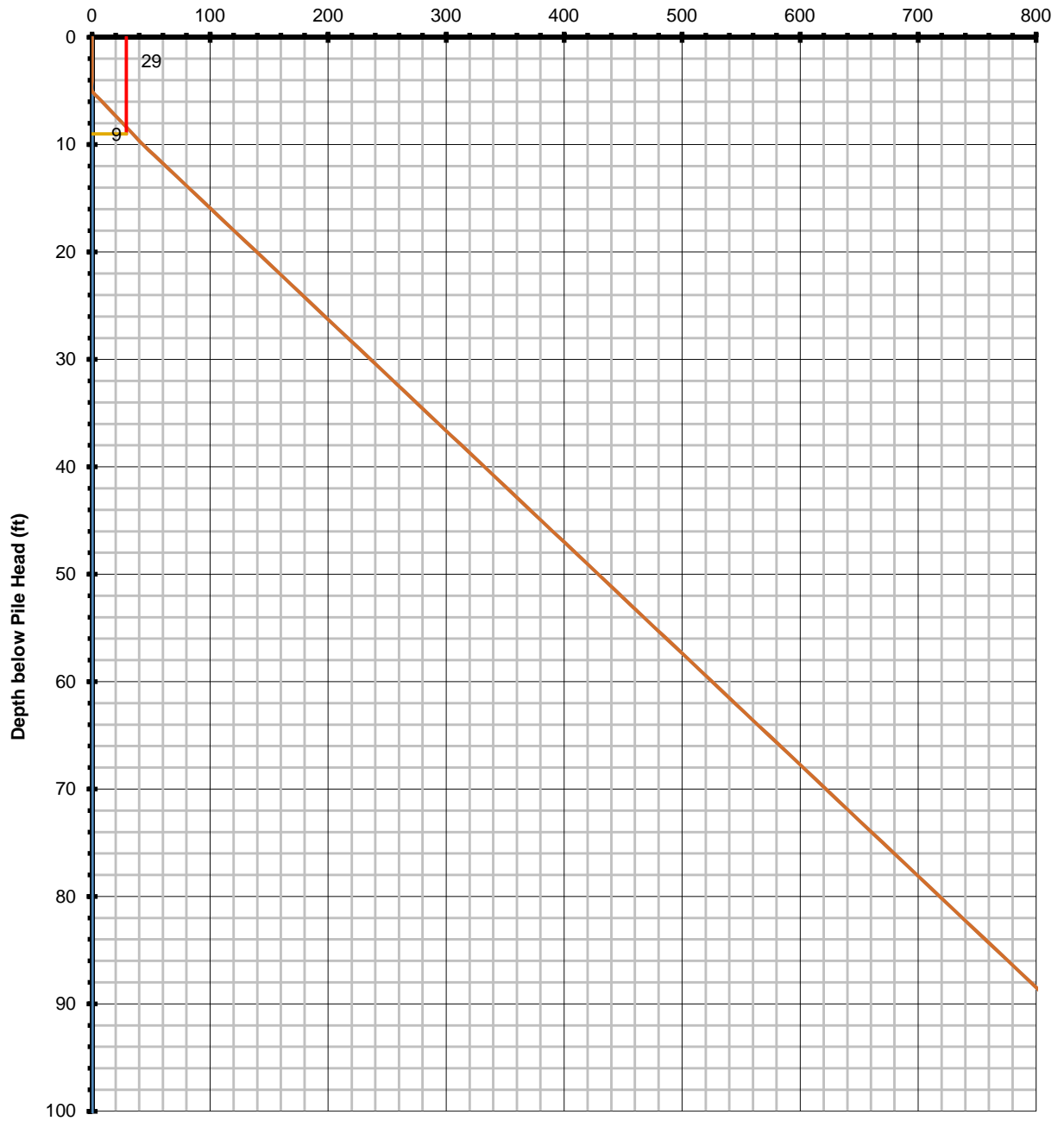
Nominal Resistance (kips)



LA-1143/Palo Comado OC

24 inch CIDH Bent 3L

Strength Limit Factored Nominal Resistance (kips)



PROJECT NUMBER / NAME: LA-1143/Palo Comado CO

CALCULATION NAME: 24 inch C10H Bent 3R

Req. Nom. = 340 kips

Factored = 200 kips

Req. Nom. T_e = 180 kips

File Diameter: 2 ft
Perimeters: 6.283 ft
End Area: 3.142 ft^2

Group Efficiency Factor: 1
5% D = 1.20 inch
Limiting Settlement for Obse- Overburden at pile cutoff: 0.00 0.23 inch ksf
Depth of overburden: 2 ft

Pile head below ground surface (ft): 9.66
Groundwater below ground surface (ft): 100
Groundwater below pile head (ft): 90.34

Nominal Comp Plot Depth (ft) Load (kips)
0 340
31 340
31 0
31 340

Strength Plot Depth (ft) Factored Load (kips)
0 200
27 200
27 0
27 200

Nominal Tension Plot Depth (ft) Load (kips)
0 180
25 180
25 0
25 180

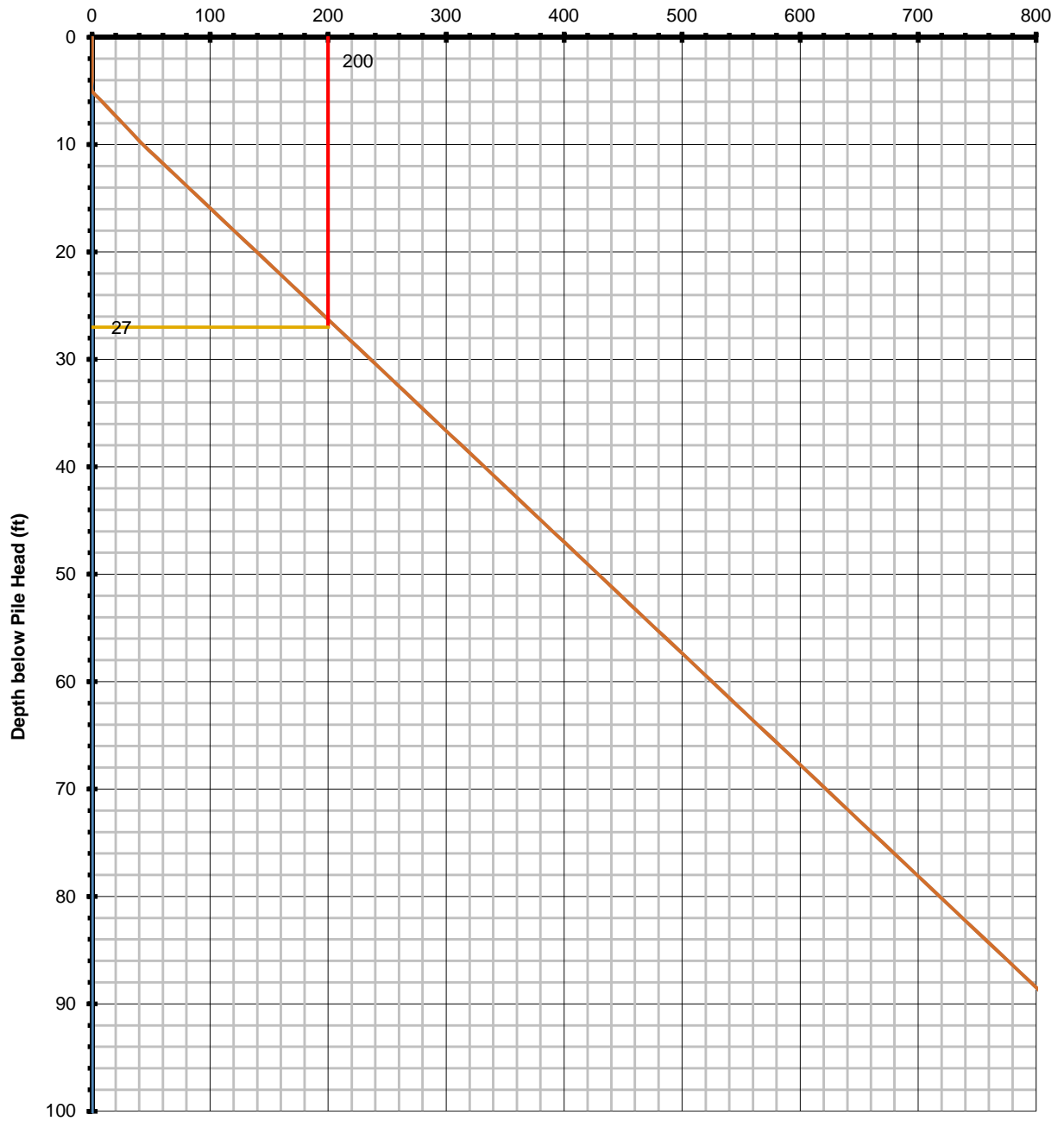
Table with columns: Elevation (ft), Layer Bottom Depth below Pile Head (ft), Layer Depth below ground (ft), SAND or CLAY, SAND SPT N₆₀ or CLAY S₆₀, EFFECTIVE UNIT WEIGHT γ (pcf), Mid-Layer γ₁ (pcf), User Input Friction Factor, SAND Friction Factor SPT N₆₀, Friction Group Efficiency, β, α, γ (ksf), Pile Depth (ft), α (ft^2), f_s As (kips), Q_u (kips), Strength Limit State Factored Resistance Q_s = Q_u * As (kips), User Input on Base Resistance, Undrained Modulus E_s (ksf), Nominal Unit Base Resistance at 5MD (ksf), Nominal Side Base Resistance at 5MD (kips), Nominal Side Resistance at Specified Settlement (kips), Strength Limit State Factored Base Resistance (kips), Factored Compression Resistance Limit State 0.5*Q_u (kips), Compression Resistance Extreme Event Q_u-GS (kips), Tension Extreme Event Q_u-GS (kips).



LA-1143/Palo Comado OC

24 inch CIDH Bent 3R

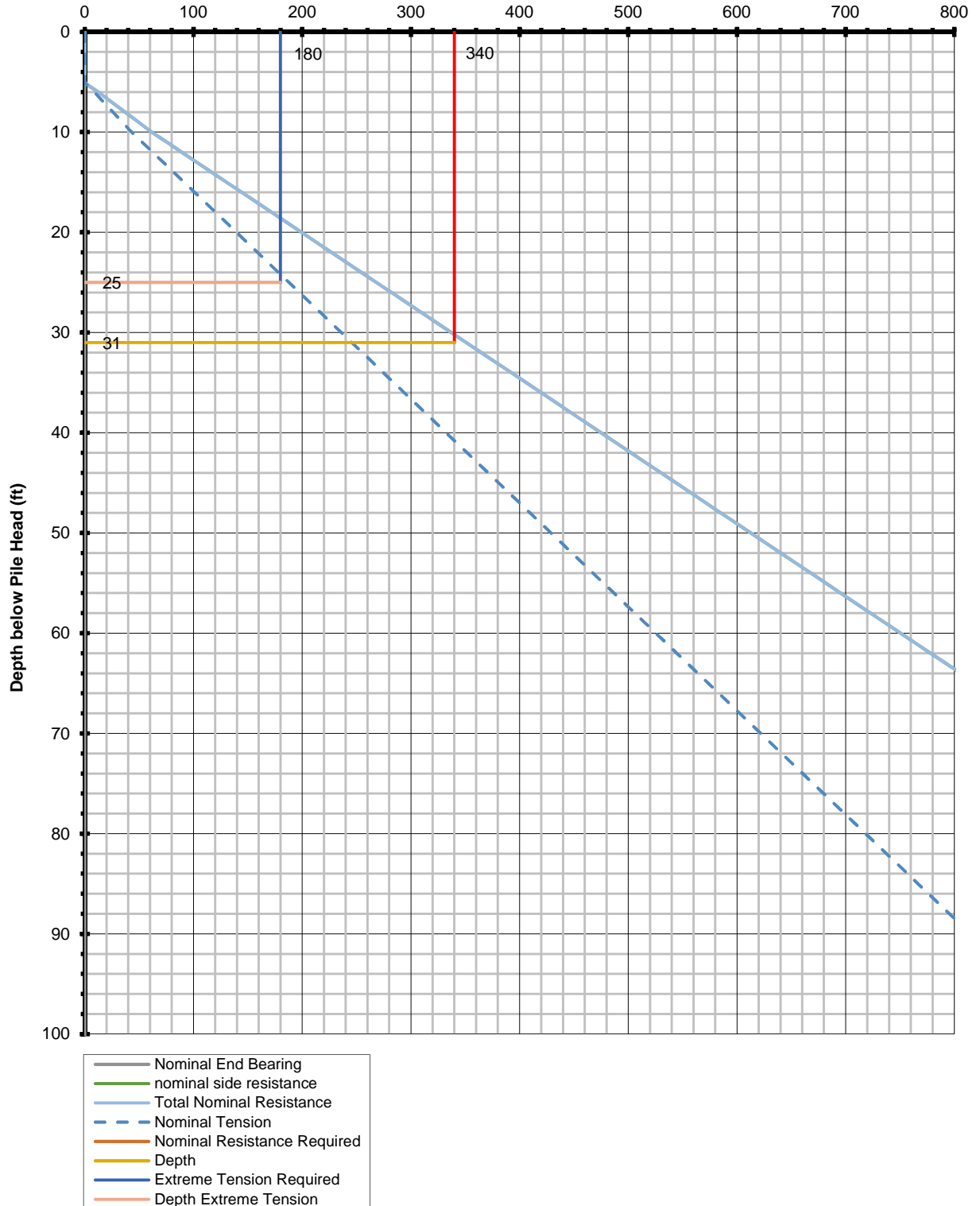
Strength Limit Factored Nominal Resistance (kips)



LA-1143/Palo Comado OC

24 inch CIDH Bent 3R

Nominal Resistance (kips)



PROJECT NUMBER / NAME: LA-1143/Palo Comado CC

CALCULATION NAME: 24 inch CIH Bent 4L

Req. Nom. = 300 kips

Factored = 220 kips

Req. Nom. T_e = 140 kips

Summary table with columns: File Diameter, Perimeters, End Area, Group Efficiency Factor, Limiting Settlement at Base, Overburden per unit of base cut-off, Depth of overburden, Head below ground surface (ft), Groundwater below ground surface (ft), Groundwater below pile head (ft), Nominal Comp Plot, Strength Plot, Nominal Tension Plot.

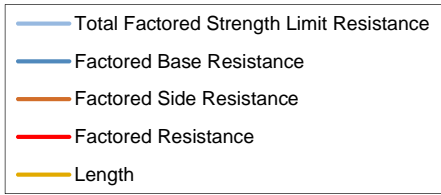
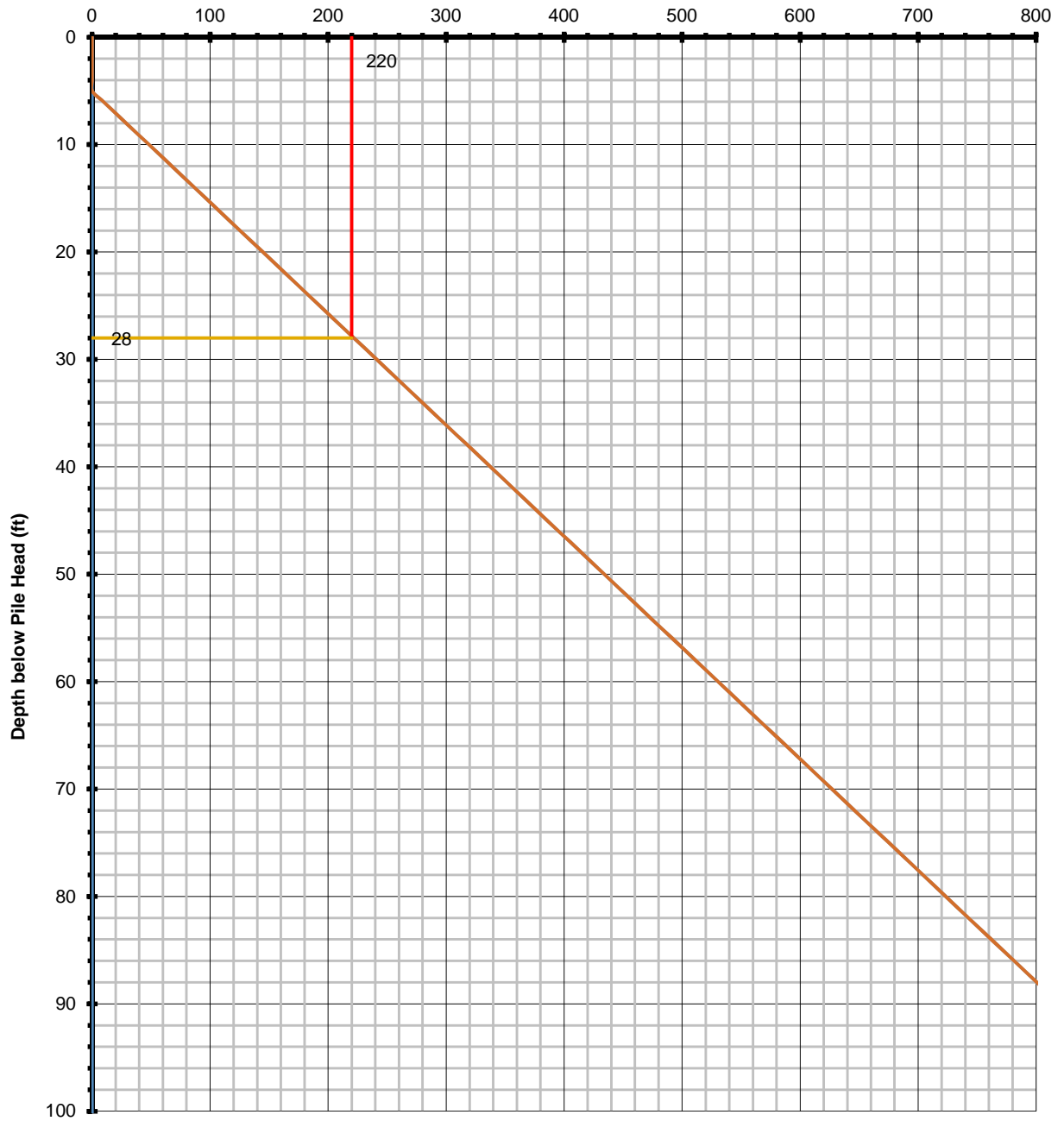
Main data table with columns: Elevation (ft), Layer Bottom Depth below Pile Head (ft), Layer Depth below Pile Head (ft), SAND or CLAY, SAND SPT N₆₀ or CLAY S_u (ksf), EFFECTIVE UNIT WEIGHT γ (pcf), Mid-Layer γ_{av} (pcf), User Input Friction Factor, SAND Friction Factor SPT N₆₀, Friction Group Efficiency, β, α, fs (ksf), Pile Depth (ft), A (ft²), Q_s + A_s (kips), Compressive Resistance (kips), User Input on Base Resistance, Undrained Modulus E_s (ksf), Nominal Unit Base Resistance at 5MD (ksf), Nominal Side Base Resistance at 5MD (kips), Nominal Base Resistance at Specified Settlement (kips), Strength Limit State Factored Resistance (kips), Factored Resistance Strength Limit State 0.5*Q_u+0.7Q_s (kips), Compression Extreme Event Q_u+Q_s (kips), Tension Extreme Event Q_u-0.7Q_s (kips).



LA-1143/Palo Comado OC

24 inch CIDH Bent 4L

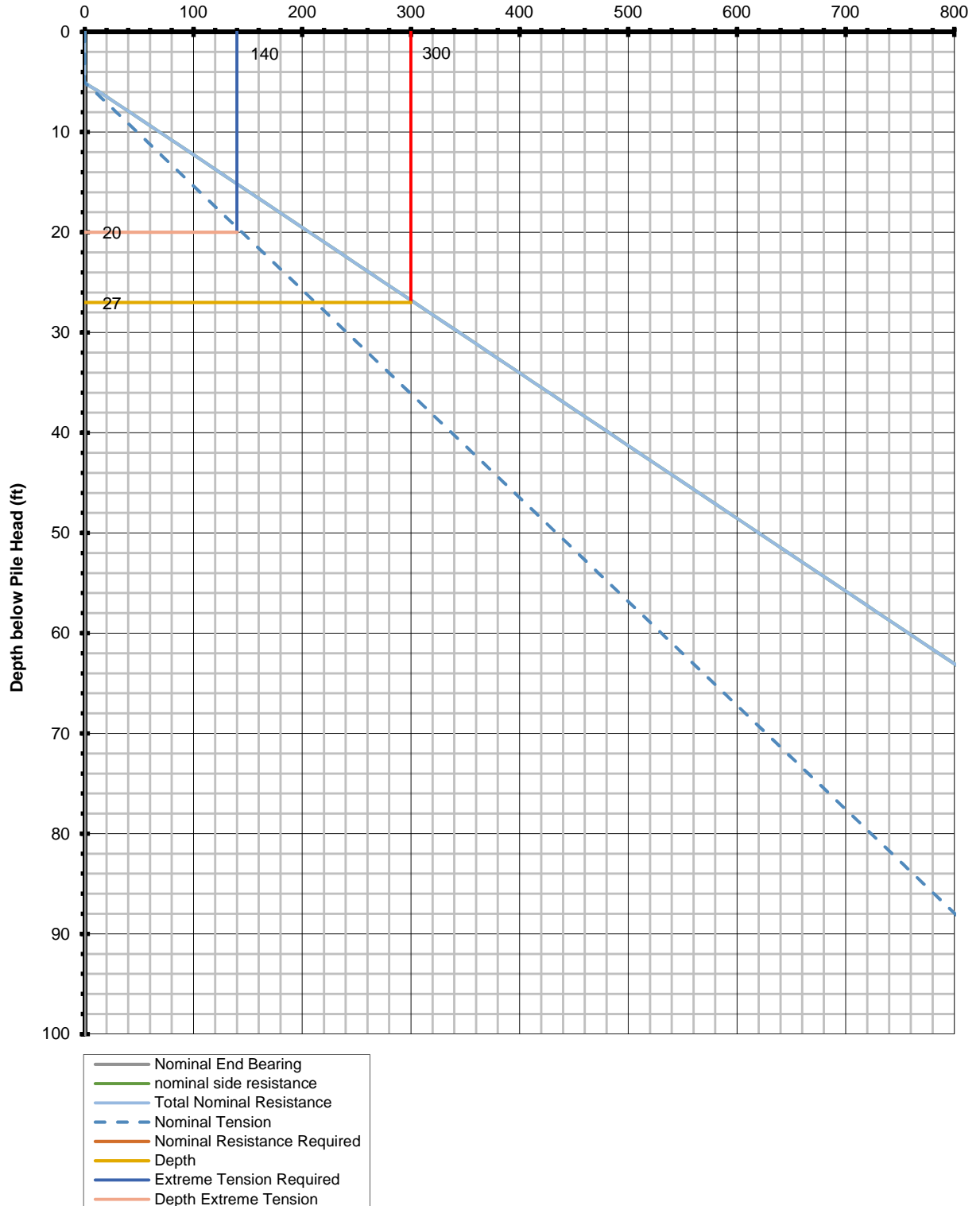
Strength Limit Factored Nominal Resistance (kips)



LA-1143/Palo Comado OC

24 inch CIDH Bent 4L

Nominal Resistance (kips)



PROJECT NUMBER / NAME: LA-1143/Palo Comado CC

CALCULATION NAME: 24 inch C10H Bent 4R

Req. Nom. = 320 kips

Factored = 150 kips

Req. Nom. T_e = 200 kips

File Diameter: 2 ft
Perimeters: 6.283 ft
End Area: 3.142 ft²

Group Efficiency Factor: 1
5% D = 1.20 inch
Limiting Settlement for Pile-Overburden at pile cutoff: 0.00 inch ksf
Depth of overburden: 2 ft

File head below ground surface (ft): 8.91
Groundwater below ground surface (ft): 1.00
Groundwater below pile head (ft): 91.09

Normal Comp Plot
Depth (ft) Load (kips)
0 320
29 0
29 320
29 320

Strength Plot
Depth (ft) Factored Load (kips)
0 150
21 0
21 150
21 150

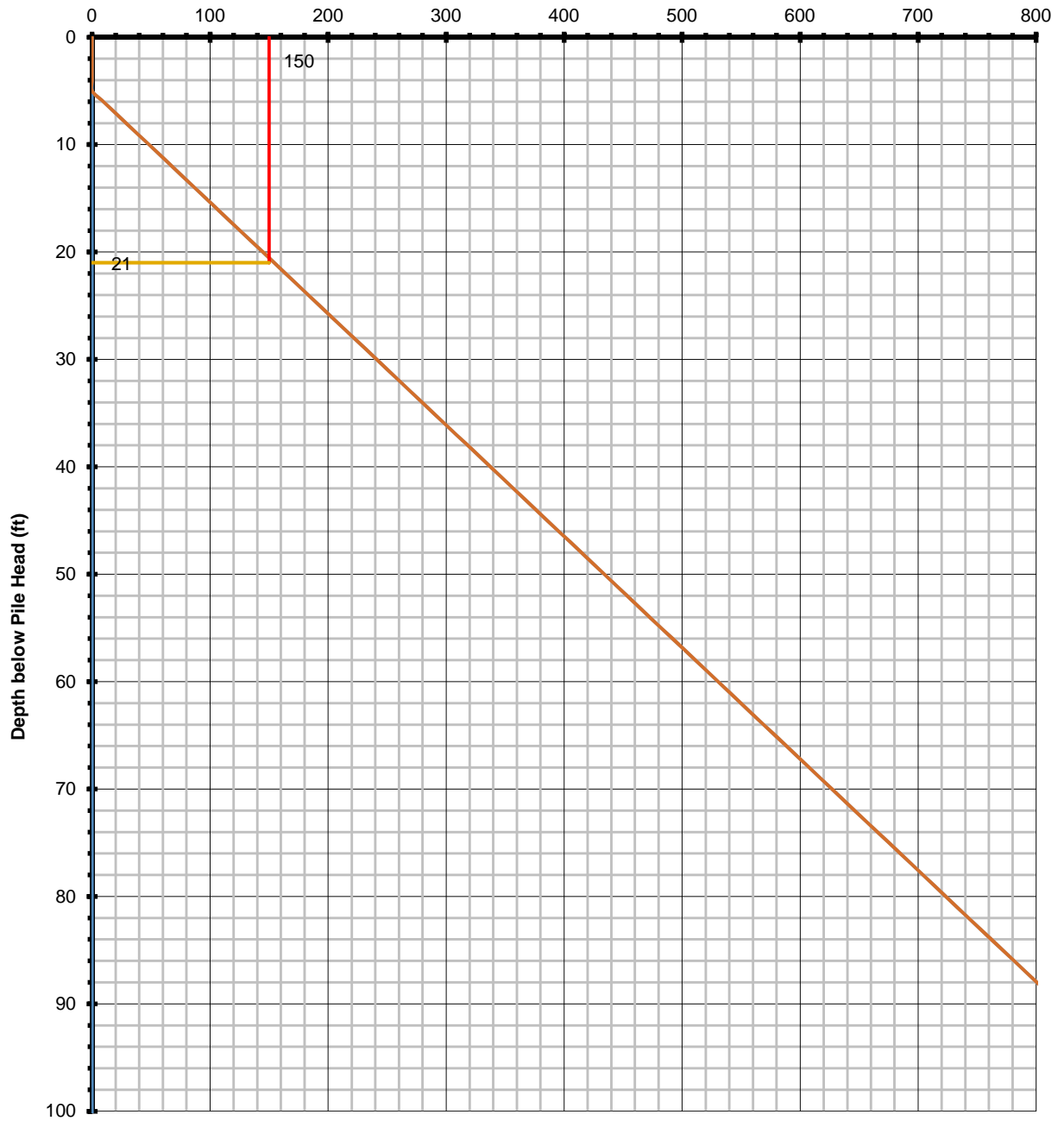
Nominal Tension Plot
Depth (ft) Load (kips)
0 200
26 0
26 200
26 200

Table with columns: Elevation (ft), Layer Bottom Depth below Pile Head (ft), Layer Depth below Pile Head (ft), SAND or CLAY, SAND SPT N₆₀ or CLAY S_u (ksf), EFFECTIVE UNIT WEIGHT γ (pcf), Mid-Layer γ_{av} (pcf), User Input Friction Factor, SAND Friction Factor SPT N₆₀, Friction Group Efficiency, β, α, γ (ksf), Pile Depth (ft), A (ft²), Q_s + Aγ (kips), Pile Resistance (kips), Strength Limit State Factored Resistance Q_s + Aγ (kips), User Input on Base Resistance, Undrained Modulus E_s (ksf), Nominal Unit Base Resistance at 5MD (ksf), Nominal Side Base Resistance at 5MD (kips), Nominal Base Resistance at Specified Settlement (kips), Strength Limit State Factored Base Resistance (kips), Factored Compression Resistance Strength Limit State 0.5*Q₈+0.7Q₅ (kips), Compression Resistance Extreme Event Q₈+Q₅ (kips), Tension Extreme Event Q₅+0.7Q₈ (kips).

LA-1143/Palo Comado OC

24 inch CIDH Bent 4R

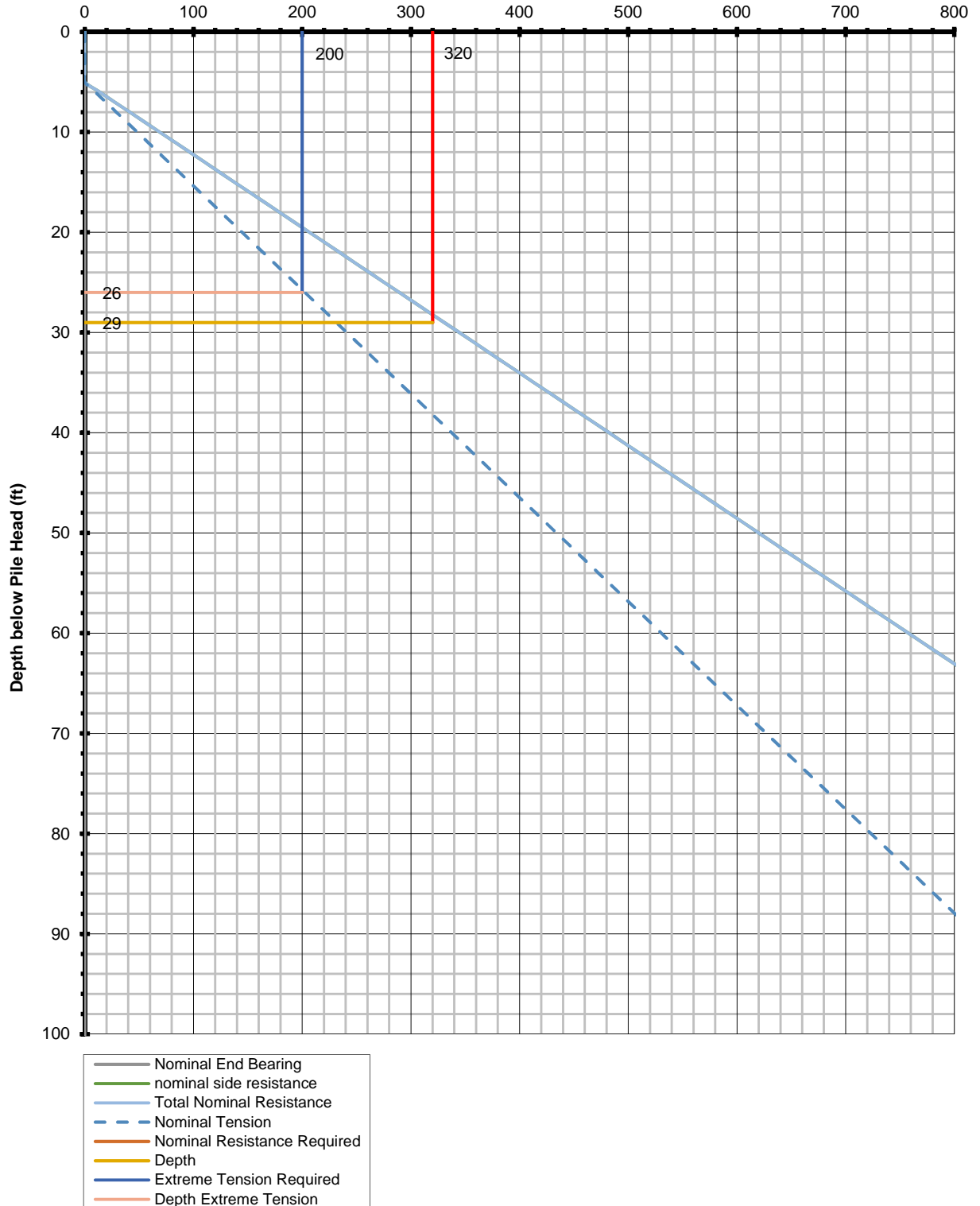
Strength Limit Factored Nominal Resistance (kips)



LA-1143/Palo Comado OC

24 inch CIDH Bent 4R

Nominal Resistance (kips)



PROJECT NUMBER / NAME: LA-1143/Palo Comado CC

CALCULATION NAME: 16 inch CDRH Abut 5L

Req. Nom. = N/A kips

Factored = 140 kips

Req. Nom. Tc = N/A kips

File Diameter: 1.33333 ft
Perimeter: 4.189 ft
End Area: 1.396 ft^2

Group Efficiency Factor: 1.0
5% D= 1 inch
Limiting Settlement for Obe- Overburden at pile cutoff: 0.00 0.23 inch ksf
Depth of overburden: 2 ft

Pile head below ground surface (ft): 3.6
Groundwater below ground surface (ft): 100
Groundwater below pile head (ft): 96.4

Nominal Comp Plot Depth (ft) Load (kips)
0 N/A
30 0
140 0
30 140
30 140

Strength Plot Depth (ft) Factored Load (kips)
0 0
140 0
30 140
30 140

Nominal Tension Plot Depth (ft) Load (kips)
0 0
30 0
140 0
30 0

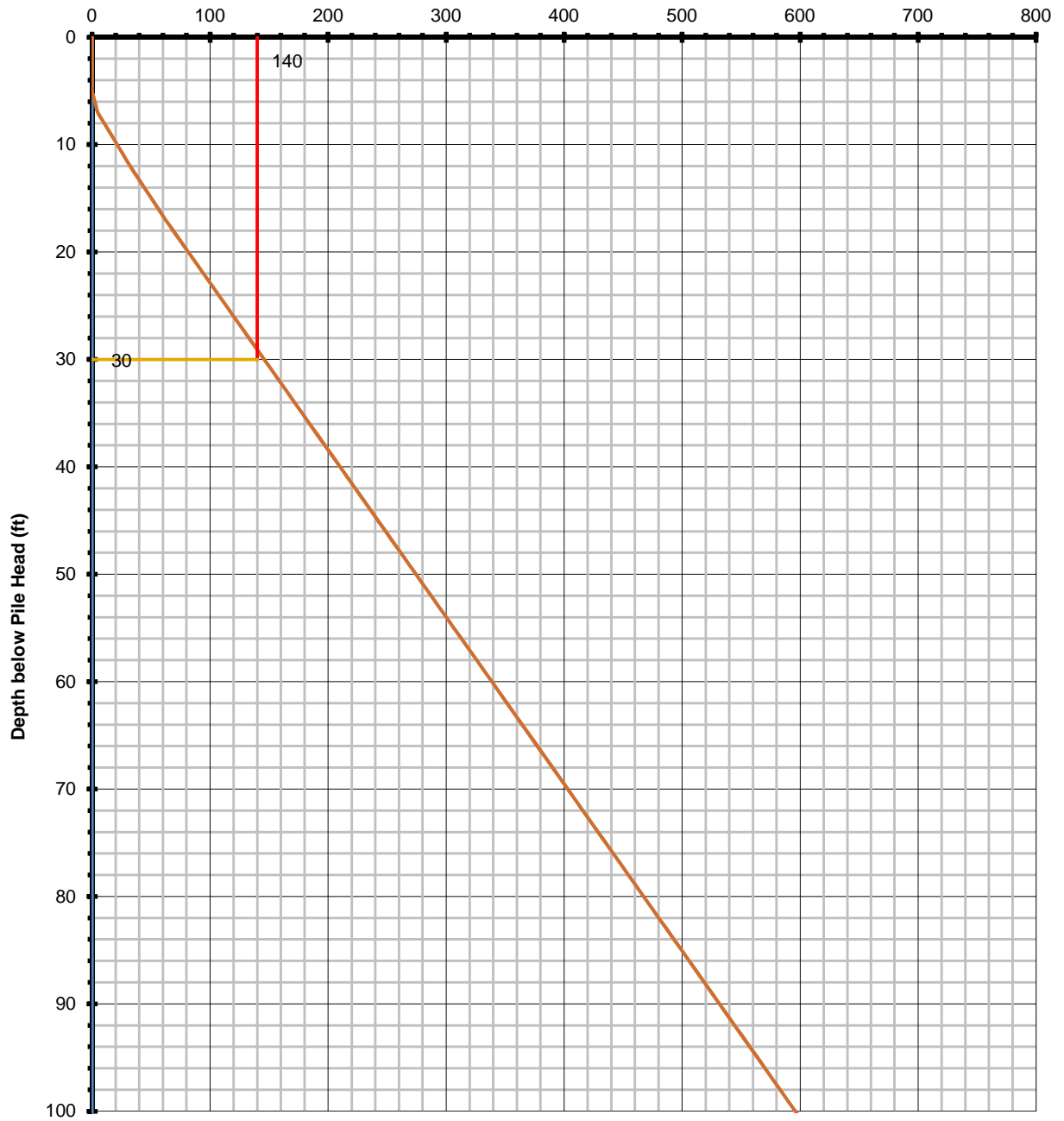
Table with columns: Elevation (ft), Layer Bottom Depth below Pile Head (ft), Layer Depth below Pile Head (ft), SAND or CLAY, SAND SPT N60 or CLAY Y (pcf), EFFECTIVE UNIT WEIGHT gamma (pcf), Mid-Layer SPT N60 (pcf), User Input Friction Factor, SAND Friction Factor SPT N60, Friction Group Efficiency, beta, alpha, phi (ksf), Pile Depth (ft), A (ft^2), Qs = 2 fs * As (kips), Nominal Side Resistance in 0.7' QS (kips), User Input on Base Resistance, Undrained Modulus Es (ksf), Nominal Unit Base Resistance at 5MD (ksf), Nominal Side Base Resistance at 5MD (kips), Nominal Base Resistance at Specified Settlement (kips), Strength Limit State Resistance (kips), Factored Resistance Limit State 0.5*Q08+0.7QS (kips), Compression Extreme Event Limit QS (kips), Tension Extreme Event Qs0.7*QS (kips)



LA-1143/Palo Comado OC

16 inch CIDH Abut 5L

Strength Limit Factored Nominal Resistance (kips)



PROJECT NUMBER / NAME: LA-1143/Palo Comado CC

CALCULATION NAME: 36 inch CDH Abut SR

Req. Nom. = N/A kips

Factored = 150 kips

Req. Nom. Tension = N/A kips

File Diameter: 1.3333 ft
Perimeter: 4.189 ft
End Area: 1.396 ft²

Group Efficiency Factor: 1.0
5% D = 0.80 inch
Limiting Settlement for Overturb: 0.00 inch
Overburden at pile cutoff: 0.23 inch
Depth of overburden: 2 ft

Pile head below ground surface (ft): 3.56
Groundwater below ground surface (ft): 100
Groundwater below pile head (ft): 96.44

Nominal Comp Plot Depth (ft) (kips) 0
Strength Plot Depth (ft) (kips) 0
Nominal Tension Plot Depth (ft) (kips) 0

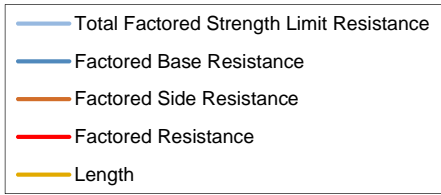
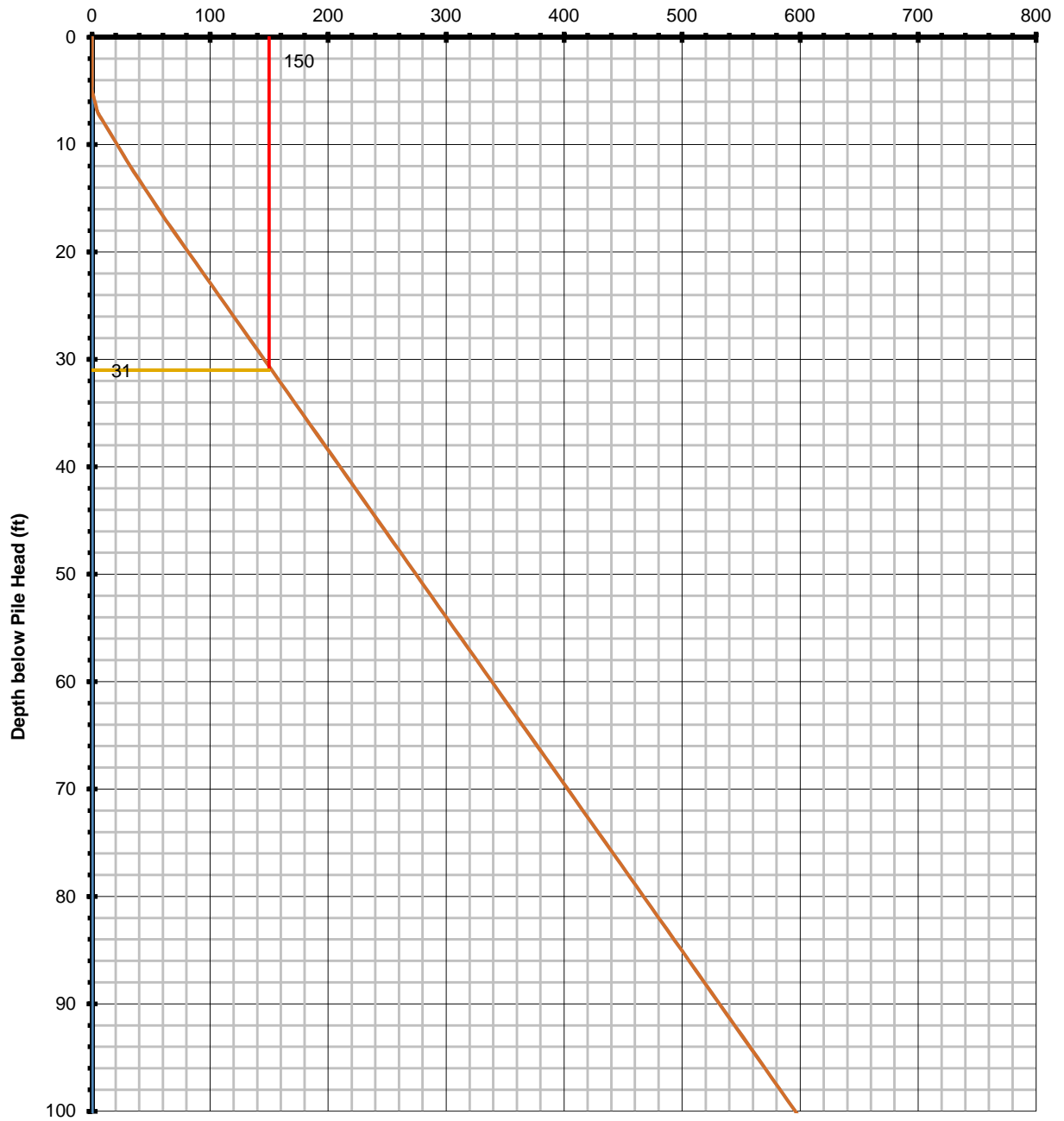
Table with columns: Elevation (ft), Layer Bottom Depth (ft), Layer Top Depth (ft), SAND or CLAY, SAND SPT N60 (ksf), EFFECTIVE UNIT WEIGHT (pcf), Mid-Layer (ksf), User Input Friction Factor, SAND Friction Factor (ksf), Friction Group Efficiency, β, α, (fs) (ksf), Pile Depth (ft), A (ft²), Qs (kips), Qs + As (kips), Strength Limit State Factored Resistance (kips), User Input on Base Resistance, Undrained Modulus (ksf), Nominal Unit Base Resistance at 5MD (ksf), Nominal Side Base Resistance at 5MD (kips), Nominal Side Resistance at Specified Settlement (kips), Strength Limit State Factored Base Resistance (kips), Factored Compression Resistance Limit State (kips), Compression Extreme Event Limit State (kips), Tension Extreme Event Qs+0.7Qs (kips).



LA-1143/Palo Comado OC

16 inch CIDH Abut 5R

Strength Limit Factored Nominal Resistance (kips)



PROJECT NUMBER / NAME: LA-1143/Palo Comado OC

CALCULATION NAME: 16 inch CDH Abut 5 Pilester

Req. Nom. = 150 kips

Factored = 60 kips

Req. Nom. T_e = 70 kips

Pile Diameter = 1.33333 ft
Perimeter = 4.189 ft
End Area = 1.396 ft²

Group Efficiency Factor = 1.0
5% D = 1.0 inch
Limiting Settlement for Obse- Overburden at pile cutoff = 0.00 0.23 inch ksf

Pile head below ground surface (ft) = 5
Groundwater below ground surface (ft) = 100
Groundwater below pile head (ft) = 95

Nominal Comp Plot Depth (ft) = 150
Nominal Tension Plot Depth (ft) = 150

Strength Plot Depth (ft) = 60
Factored Load (kips) = 60

Nominal Tension Plot Depth (ft) = 70
Nominal Tension Load (kips) = 70

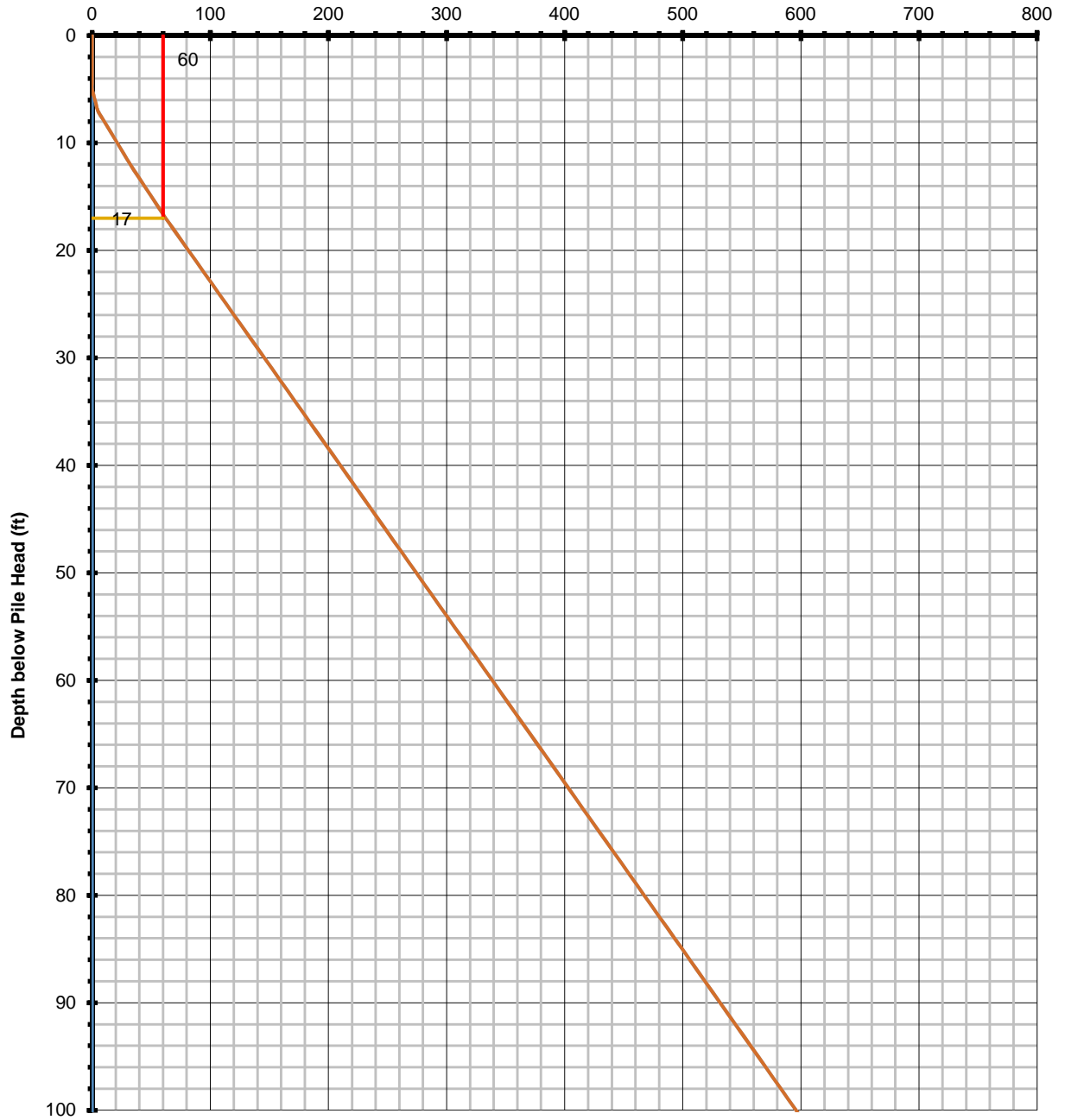
Table with 20 columns: Elevation (ft), Layer Bottom Depth below Pile Head (ft), Layer Bottom Depth below Ground (ft), SAND or CLAY, SAND SPT N₆₀ or CLAY γ (pcf), EFFECTIVE UNIT WEIGHT γ (pcf), Mid-Layer γ_{cr} (pcf), User Input Friction Factor, SAND Friction Factor SPT N₆₀, Friction Group Efficiency, β, α, f_s (ksf), Pile Depth (ft), A (ft²), f_s * A_s (kips), Q_s = 2 * f_s * A_s (kips), Compressive Resistance 0.7*Q_s (kips), User Input on Base Resistance, Undrained Modulus E_s (ksf), Nominal Unit Base Resistance at 5MD (ksf), Nominal Side Base Resistance at 5MD (kips), Nominal Side Resistance at Specified Settlement (kips), Strength Limit State Factored Base Resistance (kips), Factored Compression Resistance Limit State 0.5*Q_u (kips), Compression Extreme Event Limit State Q_u (kips), Tension Extreme Event Q_u (kips).



LA-1143/Palo Comado OC

16 inch CIDH Abut 5 Pilaster

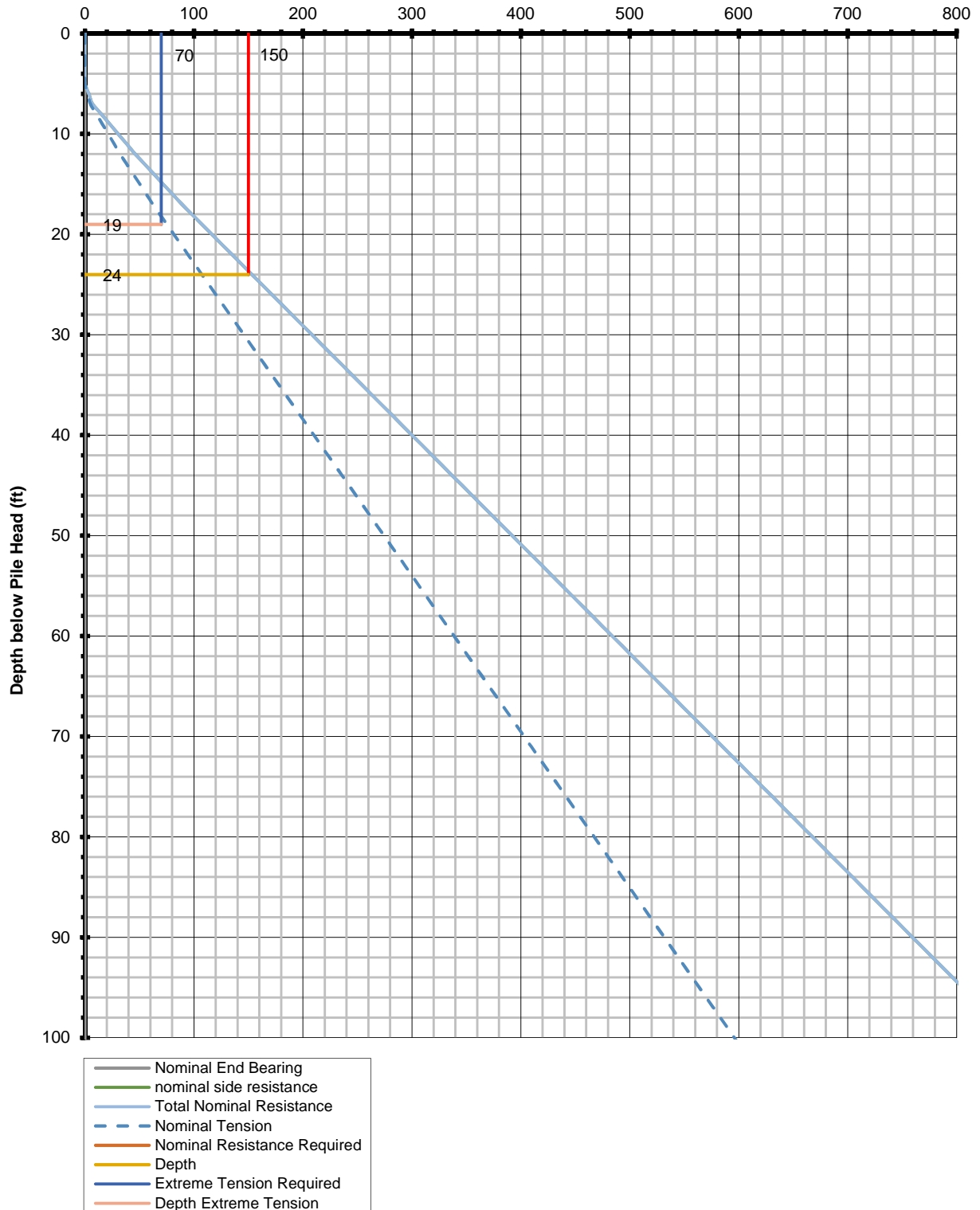
Strength Limit Factored Nominal Resistance (kips)



LA-1143/Palo Comado OC

16 inch CIDH Abut 5 Pilaster

Nominal Resistance (kips)



APPENDIX D-3

LATERAL PILE CAPACITY CALCULATIONS

SUPPORT: ABUTMENT 1R

LOAD DIRECTION: LONGITUDE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE

Layer 1, Depth -2.00 to 0.10 ft = Stiff Clay without Free Water

Layer 2, Depth 0.10 to 3.00 ft = Stiff Clay without Free Water

Layer 3, Depth 3.00 to 8.00 ft = Stiff Clay without Free Water

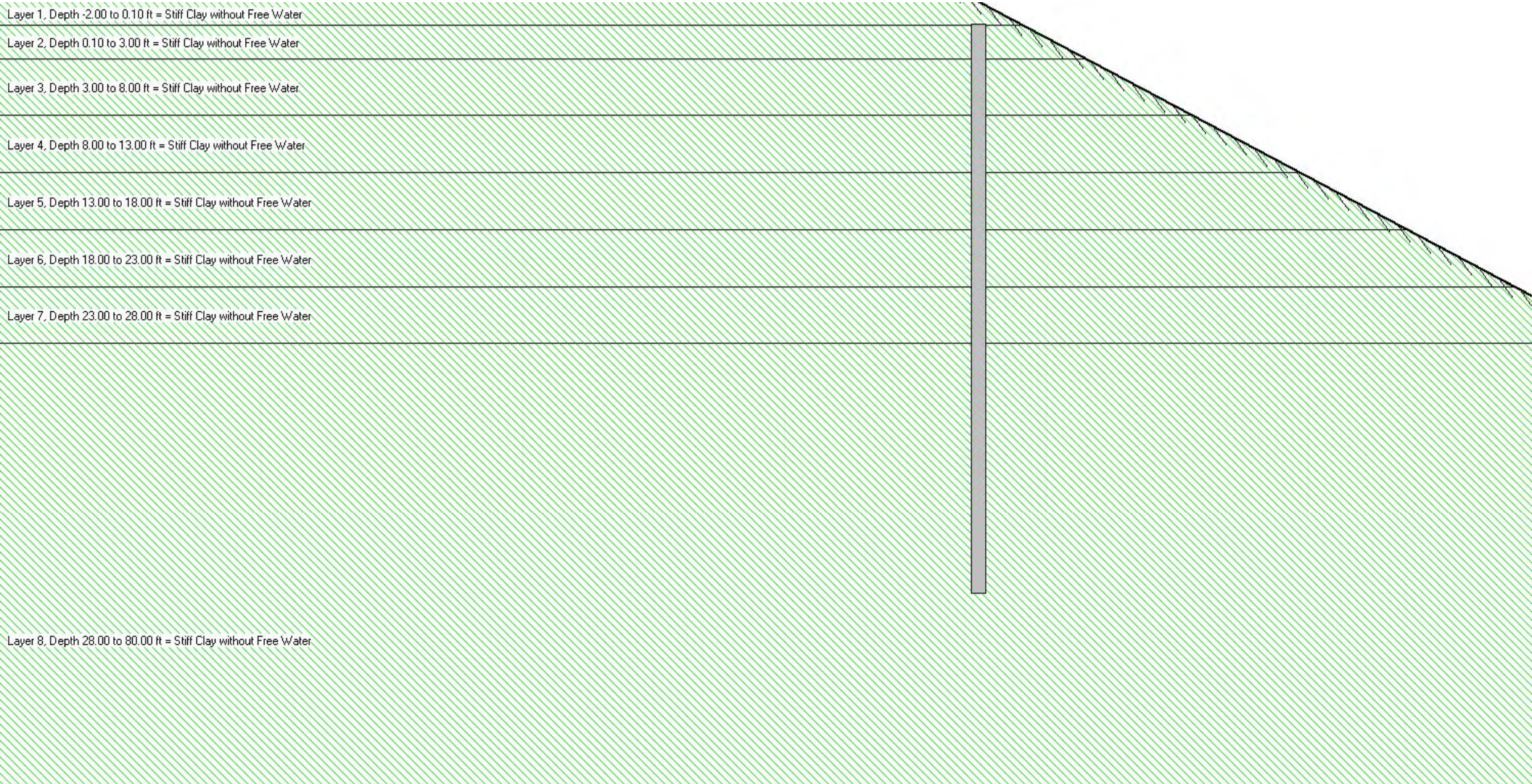
Layer 4, Depth 8.00 to 13.00 ft = Stiff Clay without Free Water

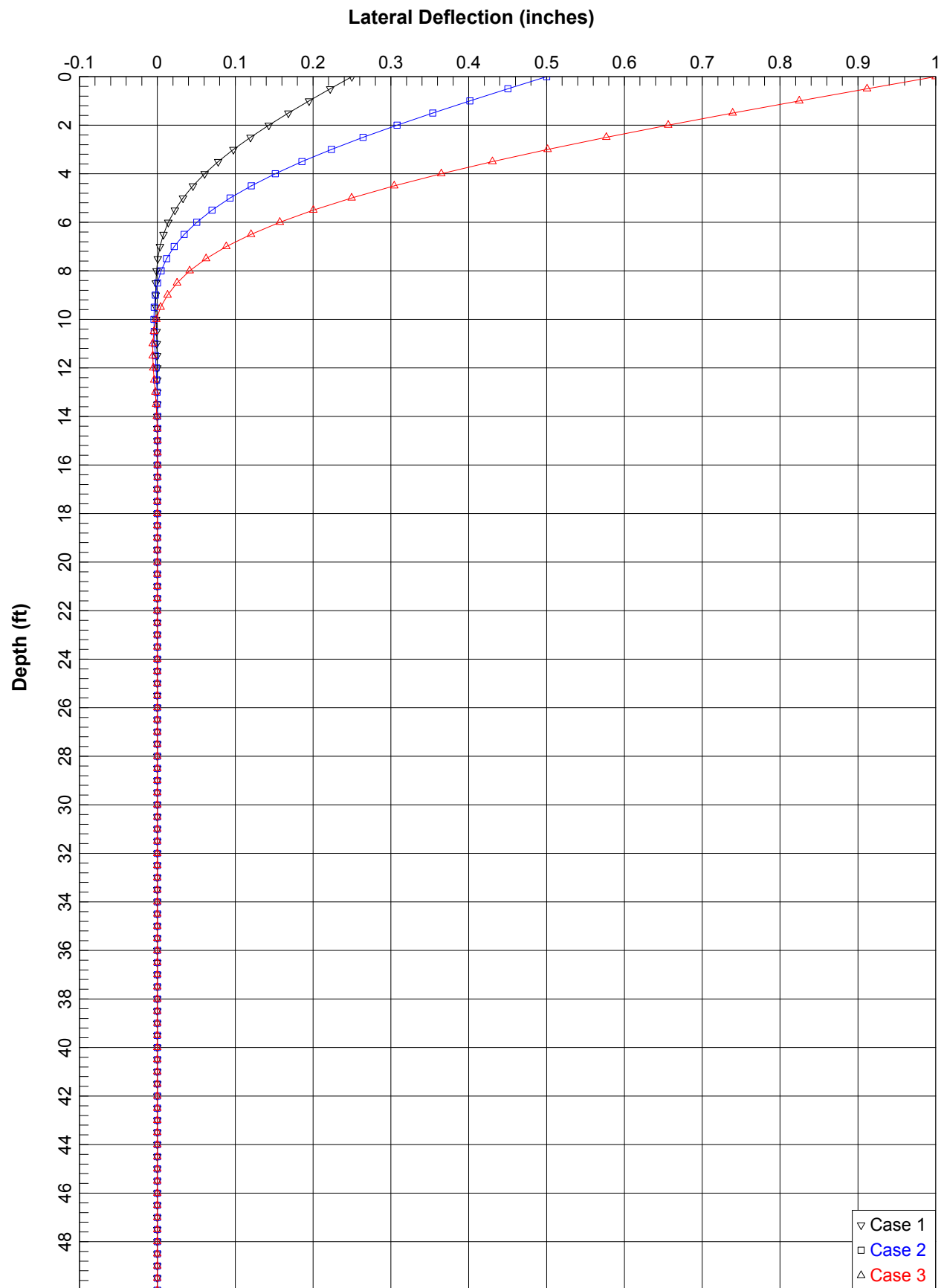
Layer 5, Depth 13.00 to 18.00 ft = Stiff Clay without Free Water

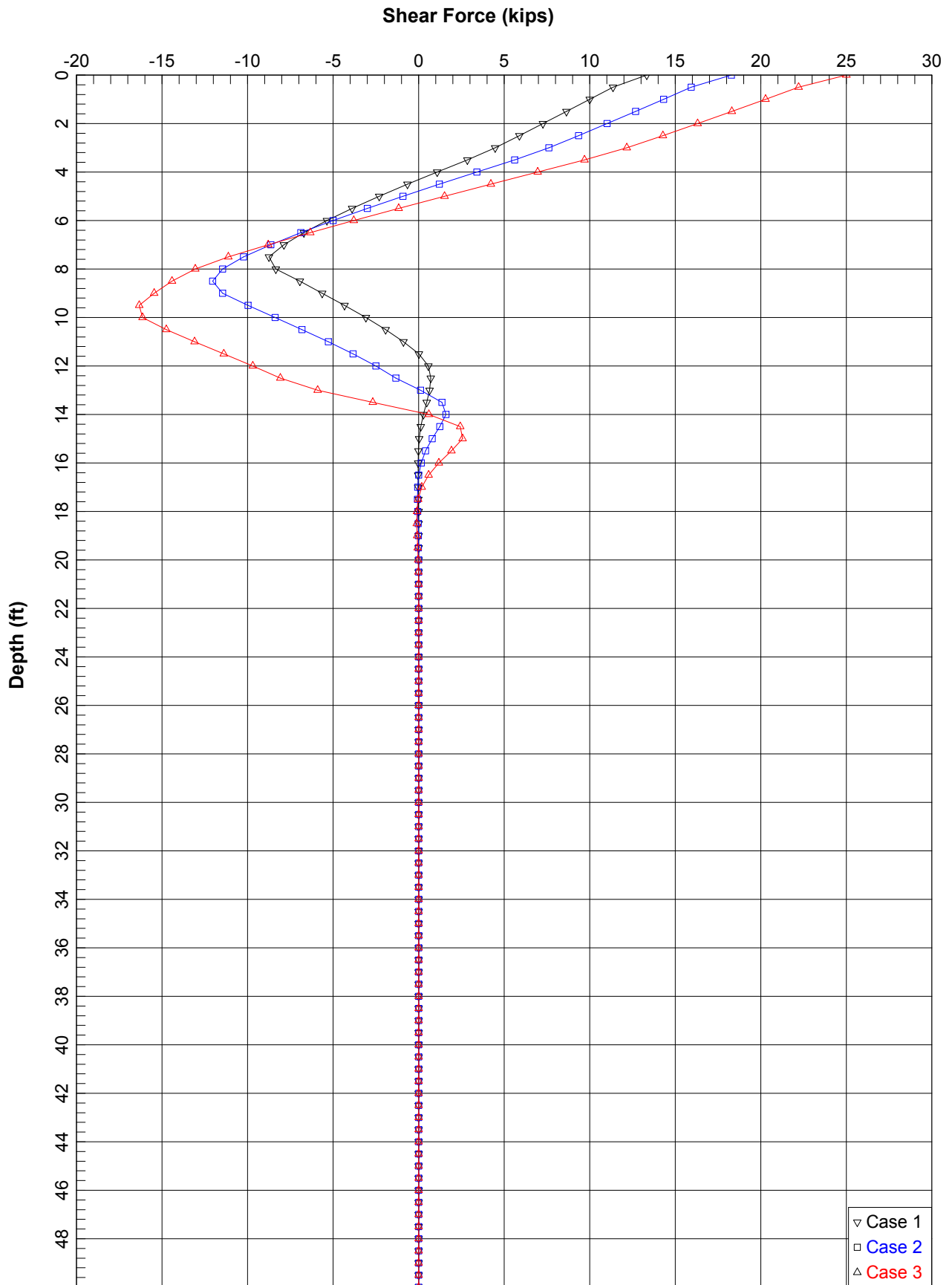
Layer 6, Depth 18.00 to 23.00 ft = Stiff Clay without Free Water

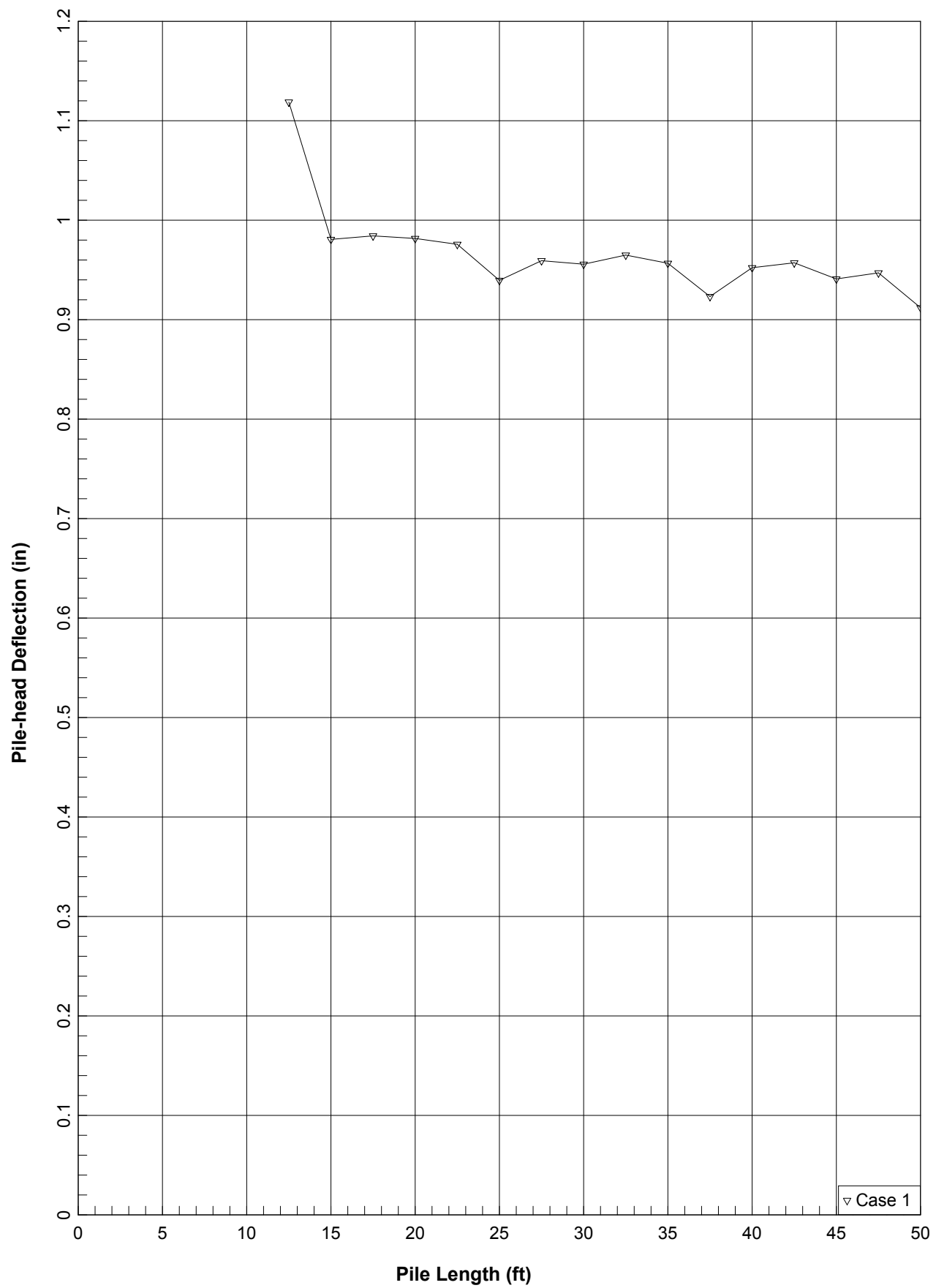
Layer 7, Depth 23.00 to 28.00 ft = Stiff Clay without Free Water

Layer 8, Depth 28.00 to 80.00 ft = Stiff Clay without Free Water









NOTE: LPILE output print shows the undrained shear strength value of individual layers in "psi" - This is an error from LPILE output format. It should be in "psf" as shown in Summary of Soil Properties (LPILE output)

 Abut 1R_long_Critical Length

 Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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This copy of LPILE is licensed to:

gdc
 gdc
 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

 Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 1\
 Name of input data file: Abut 1R_long_Critical Length.lp6d
 Name of output report file: Abut 1R_long_Critical Length.lp6o
 Name of plot output file: Abut 1R_long_Critical Length.lp6p
 Name of runtime message file: Abut 1R_long_Critical Length.lp6r

 Date and Time of Analysis

Date: September 13, 2014 Time: 8:56:30

 Problem Title

Project Name: Palo Comado OC Bridge Widen

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

 Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

 Pile Structural Properties and Geometry

Page 1

 Abut 1R_long_Critical Length

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

 Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 16.0000000 in
 Bottom Width = 16.0000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

 Ground Slope and Pile Batter Angles

Ground Slope Angle = 33.700 degrees
 = 0.588 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

 Soil and Rock Layering Information

The soil profile is modelled using 8 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer	=	-2.00000 ft
Distance from top of pile to bottom of layer	=	0.10000 ft
Effective unit weight at top of layer	=	120.00000 pcf
Effective unit weight at bottom of layer	=	120.00000 pcf
Undrained cohesion at top of layer	=	3500.00000 psi
Undrained cohesion at bottom of layer	=	3500.00000 psi
Epsilon-50 at top of layer	=	0.00700
Epsilon-50 at bottom of layer	=	0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer	=	0.10000 ft
Distance from top of pile to bottom of layer	=	3.00000 ft
Effective unit weight at top of layer	=	120.00000 pcf
Effective unit weight at bottom of layer	=	120.00000 pcf
Undrained cohesion at top of layer	=	1500.00000 psi
Undrained cohesion at bottom of layer	=	1500.00000 psi
Epsilon-50 at top of layer	=	0.00700
Epsilon-50 at bottom of layer	=	0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer	=	3.00000 ft
Distance from top of pile to bottom of layer	=	8.00000 ft
Effective unit weight at top of layer	=	120.00000 pcf
Effective unit weight at bottom of layer	=	120.00000 pcf
Undrained cohesion at top of layer	=	2500.00000 psi
Undrained cohesion at bottom of layer	=	2500.00000 psi

Page 2

NOTE: LPILE output print shows the undrained shear strength value of individual layers in "psi" - This is an error from LPILE output format. It should be in "psf" as shown in Summary of Soil Properties (LPILE output)

Abut 1R_long_Critical Length
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water
 Distance from top of pile to top of layer = 8.00000 ft
 Distance from top of pile to bottom of layer = 13.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water
 Distance from top of pile to top of layer = 13.00000 ft
 Distance from top of pile to bottom of layer = 18.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 6 is stiff clay without free water
 Distance from top of pile to top of layer = 18.00000 ft
 Distance from top of pile to bottom of layer = 23.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 2500.00000 psi
 Undrained cohesion at bottom of layer = 2500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 7 is stiff clay without free water
 Distance from top of pile to top of layer = 23.00000 ft
 Distance from top of pile to bottom of layer = 28.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 8 is stiff clay without free water
 Distance from top of pile to top of layer = 28.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type	Rock Mass Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Elastic Mod.	ROD %
Num.	Epsilon on 50	(p-y Curve Criteria)	Rock Mass Depth	pcf	psi	deg.	psi	GSI
1	0.00700	Stiff Clay w/o Free Water	-2.000	120.000	3500.000	--	--	--
	0.00700	--	0.10000	120.000	3500.000	--	--	--
2	0.00700	Stiff Clay w/o Free Water	0.10000	120.000	1500.000	--	--	--
	0.00700	--	3.000	120.000	1500.000	--	--	--
3	0.00700	Stiff Clay w/o Free Water	3.000	120.000	2500.000	--	--	--
	0.00700	--	8.000	120.000	2500.000	--	--	--

		Abut 1R_long_Critical Length			
4	0.00700	Stiff Clay w/o Free Water	8.000	120.000	1500.000
	0.00700	--	13.000	120.000	1500.000
5	0.00700	Stiff Clay w/o Free Water	13.000	125.000	4500.000
	0.00700	--	18.000	125.000	4500.000
6	0.00700	Stiff Clay w/o Free Water	18.000	125.000	2500.000
	0.00700	--	23.000	125.000	2500.000
7	0.00700	Stiff Clay w/o Free Water	23.000	125.000	3500.000
	0.00700	--	28.000	125.000	3500.000
8	0.00500	Stiff Clay w/o Free Water	28.000	125.000	4500.000
	0.00500	--	80.000	125.000	4500.000

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	1.0000	1.0000
2	50.000	1.0000	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of Loads specified = 1

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	1	V = 24000. lbs	M = 0.0000 in-lbs	154000.	True

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head = 24000.000 lbs
 Applied moment at pile head = 0.000 in-lbs
 Axial thrust load on pile head = 154000.000 lbs

Abut 1R_long_Critical Length

Abut 1R_long_Ave P

Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 1\
 Name of input data file: Abut 1R_long_Ave P.lpd
 Name of output report file: Abut 1R_long_Ave P.lpo
 Name of plot output file: Abut 1R_long_Ave P.lpp
 Name of runtime message file: Abut 1R_long_Ave P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 8:58:47

Problem Title

Project Name: Palo Comado OC Bridge Widened

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario DiNicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Abut 1R_long_Ave P

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 16.0000000 in
 Bottom Width = 16.0000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 33.700 degrees
 = 0.588 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 8 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 3.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 3.00000 ft
 Distance from top of pile to bottom of layer = 8.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2500.00000 psi
 Undrained cohesion at bottom of layer = 2500.00000 psi

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 8.00000 ft
 Distance from top of pile to bottom of layer = 13.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 13.00000 ft
 Distance from top of pile to bottom of layer = 18.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 6 is stiff clay without free water

Distance from top of pile to top of layer = 18.00000 ft
 Distance from top of pile to bottom of layer = 23.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 2500.00000 psi
 Undrained cohesion at bottom of layer = 2500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 7 is stiff clay without free water

Distance from top of pile to top of layer = 23.00000 ft
 Distance from top of pile to bottom of layer = 28.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 8 is stiff clay without free water

Distance from top of pile to top of layer = 28.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 125.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type	Rock Mass Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Uniaxial Subgrade Mod.	ROD %
Num.	Epsilon 50	(p-y Curve Criteria)	ft	pcf	psf	deg.	psi	GSI
1	0.00700	Stiff Clay w/o Free Water	-2.000	120.000	3500.000	--	--	--
	0.00700	--	0.10000	120.000	3500.000	--	--	--
2	0.00700	Stiff Clay w/o Free Water	0.10000	120.000	1500.000	--	--	--
	0.00700	--	3.000	120.000	1500.000	--	--	--
3	0.00700	Stiff Clay w/o Free Water	3.000	120.000	2500.000	--	--	--
	0.00700	--	8.000	120.000	2500.000	--	--	--

		Abut 1R_long_Ave P						
4	0.00700	Stiff Clay w/o Free Water	8.000	120.000	1500.000	--	--	--
	0.00700	--	13.000	120.000	1500.000	--	--	--
5	0.00700	Stiff Clay w/o Free Water	13.000	125.000	4500.000	--	--	--
	0.00700	--	18.000	125.000	4500.000	--	--	--
6	0.00700	Stiff Clay w/o Free Water	18.000	125.000	2500.000	--	--	--
	0.00700	--	23.000	125.000	2500.000	--	--	--
7	0.00700	Stiff Clay w/o Free Water	23.000	125.000	3500.000	--	--	--
	0.00700	--	28.000	125.000	3500.000	--	--	--
8	0.00500	Stiff Clay w/o Free Water	28.000	125.000	4500.000	--	--	--
	0.00500	--	80.000	125.000	125.000	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	1.0000	1.0000
2	50.000	1.0000	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4 y =	0.25000 in	M = 0.0000 in-lbs	154000.	False
2	4 y =	0.50000 in	M = 0.0000 in-lbs	154000.	False
3	4 y =	1.00000 in	M = 0.0000 in-lbs	154000.	False

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Page 4

		Abut		1R_Long_Ave P					
516.000	0.000	-5.659E-09	4.475E-09	0.000	765.9332	5.799E+09	-6.234E-10	6071214.	0.000
522.000	0.000	1.001E-08	1.542E-09	0.000	765.9332	5.799E+09	-3.543E-10	5992338.	0.000
528.000	0.000	1.291E-08	1.917E-11	0.000	765.9332	5.799E+09	-1.533E-10	5913462.	0.000
534.000	0.000	1.029E-08	-5.469E-10	0.000	765.9332	5.799E+09	-3.543E-11	5834585.	0.000
540.000	0.000	6.377E-09	-5.992E-10	0.000	765.9332	5.799E+09	1.800E-11	5755709.	0.000
546.000	0.000	3.108E-09	-4.476E-10	0.000	765.9332	5.799E+09	3.252E-11	5676833.	0.000
552.000	0.000	1.007E-09	-2.642E-10	0.000	765.9332	5.799E+09	2.862E-11	5597957.	0.000
558.000	0.000	-6.503E-11	-1.211E-10	0.000	765.9332	5.799E+09	1.908E-11	5519081.	0.000
564.000	0.000	-4.499E-10	-3.342E-11	0.000	765.9332	5.799E+09	1.016E-11	5440204.	0.000
570.000	0.000	-4.685E-10	9.032E-12	0.000	765.9332	5.799E+09	3.989E-12	5361328.	0.000
576.000	0.000	-3.431E-10	2.267E-11	0.000	765.9332	5.799E+09	0.000	5282452.	0.000
582.000	0.000	-1.974E-10	2.155E-11	0.000	765.9332	5.799E+09	0.000	5203576.	0.000
588.000	0.000	-8.483E-11	1.481E-11	0.000	765.9332	5.799E+09	-1.321E-12	5124700.	0.000
594.000	0.000	-1.976E-11	7.066E-12	0.000	765.9332	5.799E+09	-1.259E-12	5045823.	0.000
600.000	0.000	0.000	0.000	0.000	765.9332	5.799E+09	-1.096E-12	2483474.	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

Pile-head deflection = 1.0000000 inches
 Computed slope at pile head = -0.0146990 radians
 Maximum bending moment = 948521. inch-lbs
 Maximum shear force = 24997. lbs
 Depth of maximum bending moment = 66.0000000 inches below pile head
 Depth of maximum shear force = 0.0000000 inches below pile head
 Number of iterations = 24
 Number of zero deflection points = 12

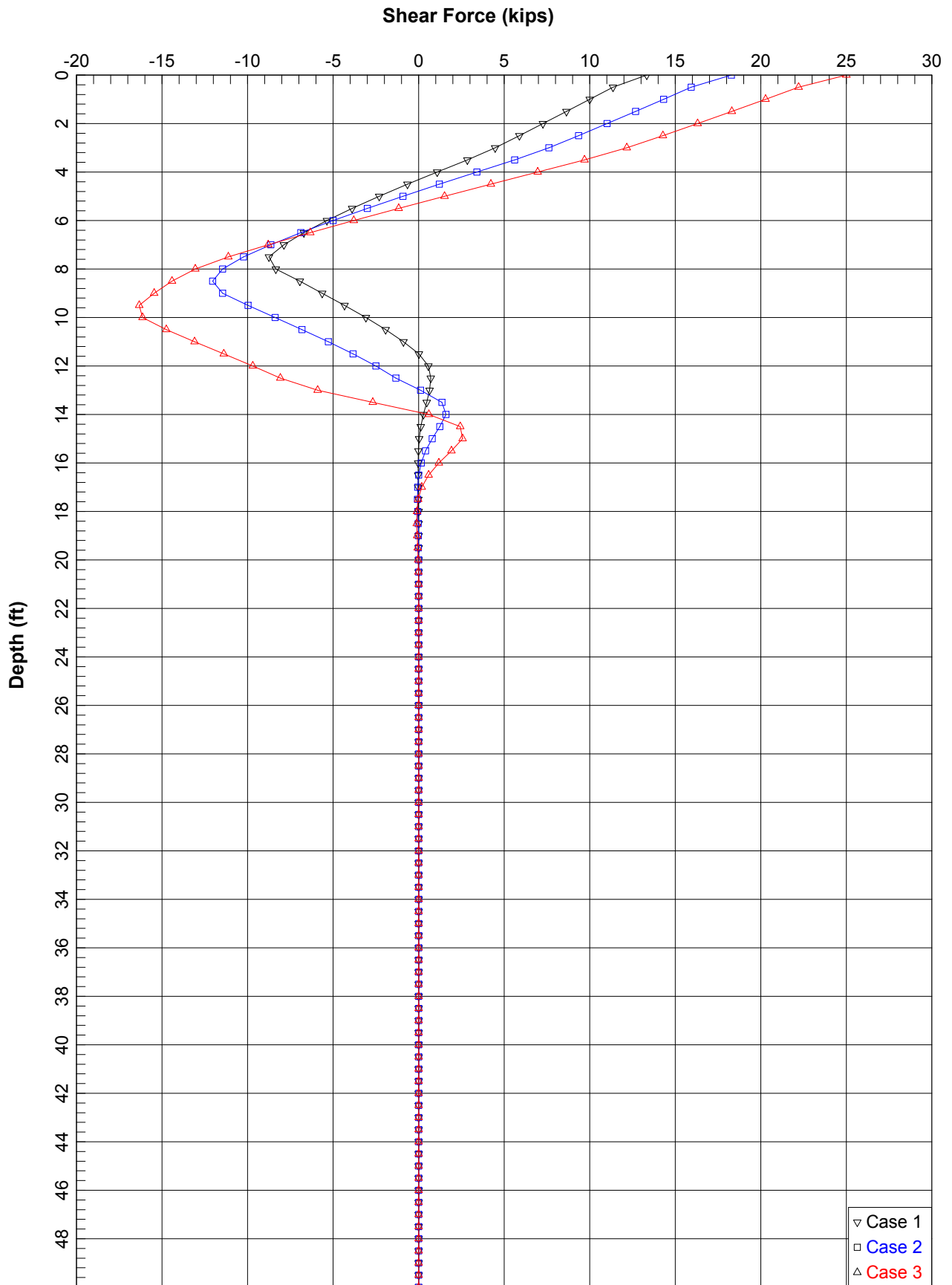
 Summary of Pile Response(s)

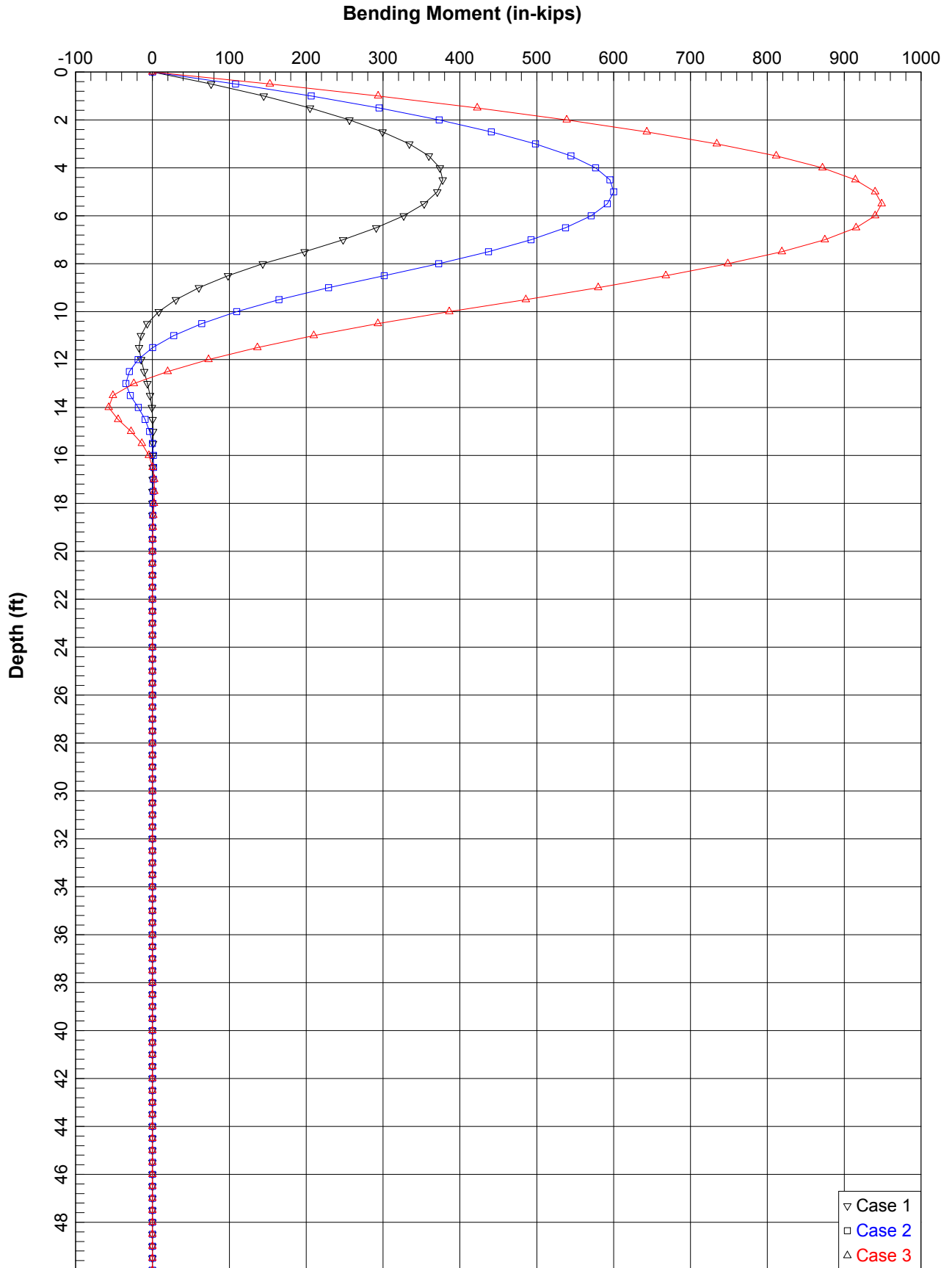
Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.		Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 M = in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y =	0.2500	M = 0.000	154000.	0.25000000	377472.	13327.	-0.00463902
2	4	sy =	0.5000	M = 0.000	154000.	0.50000000	600061.	18283.	-0.00827470
3	4	y =	1.0000	M = 0.000	154000.	1.00000000	948521.	24997.	-0.01469901

The analysis ended normally.





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Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 1\
 Name of input data file: Abut 1R_long_Ave P.lpd
 Name of output report file: Abut 1R_long_Ave P.lpo
 Name of plot output file: Abut 1R_long_Ave P.lpp
 Name of runtime message file: Abut 1R_long_Ave P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 8:58:47

Problem Title

Project Name: Palo Comado OC Bridge Widened

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

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Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 16.0000000 in
 Bottom Width = 16.0000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 33.700 degrees
 = 0.588 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 8 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 3.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 3.00000 ft
 Distance from top of pile to bottom of layer = 8.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2500.00000 psi
 Undrained cohesion at bottom of layer = 2500.00000 psi

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 8.00000 ft
 Distance from top of pile to bottom of layer = 13.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 13.00000 ft
 Distance from top of pile to bottom of layer = 18.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 6 is stiff clay without free water

Distance from top of pile to top of layer = 18.00000 ft
 Distance from top of pile to bottom of layer = 23.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 2500.00000 psi
 Undrained cohesion at bottom of layer = 2500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 7 is stiff clay without free water

Distance from top of pile to top of layer = 23.00000 ft
 Distance from top of pile to bottom of layer = 28.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 8 is stiff clay without free water

Distance from top of pile to top of layer = 28.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 125.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type	Rock Mass Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Uniaxial Subgrade Mod.	RQD %
Num.	Epsilon 50	(p-y Curve Criteria) Factor	ft	pcf	psf	deg.	psi	or GSI
1	0.00700	Stiff Clay w/o Free Water	-2.000	120.000	3500.000	--	--	--
	0.00700	--	0.10000	120.000	3500.000	--	--	--
2	0.00700	Stiff Clay w/o Free Water	0.10000	120.000	1500.000	--	--	--
	0.00700	--	3.000	120.000	1500.000	--	--	--
3	0.00700	Stiff Clay w/o Free Water	3.000	120.000	2500.000	--	--	--
	0.00700	--	8.000	120.000	2500.000	--	--	--

		Abut 1R_long_Ave P						
4	0.00700	Stiff Clay w/o Free Water	8.000	120.000	1500.000	--	--	--
	0.00700	--	13.000	120.000	1500.000	--	--	--
5	0.00700	Stiff Clay w/o Free Water	13.000	125.000	4500.000	--	--	--
	0.00700	--	18.000	125.000	4500.000	--	--	--
6	0.00700	Stiff Clay w/o Free Water	18.000	125.000	2500.000	--	--	--
	0.00700	--	23.000	125.000	2500.000	--	--	--
7	0.00700	Stiff Clay w/o Free Water	23.000	125.000	3500.000	--	--	--
	0.00700	--	28.000	125.000	3500.000	--	--	--
8	0.00500	Stiff Clay w/o Free Water	28.000	125.000	4500.000	--	--	--
	0.00500	--	80.000	125.000	125.000	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	1.0000	1.0000
2	50.000	1.0000	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4 y =	0.25000 in	M = 0.0000 in-lbs	154000.	False
2	4 y =	0.50000 in	M = 0.0000 in-lbs	154000.	False
3	4 y =	1.00000 in	M = 0.0000 in-lbs	154000.	False

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Page 4

Table with columns: Displacement of pile head, Moment at pile head, Axial load at pile head, Depth X inches, Deflect. Y inches, Bending Moment in-lbs, Shear Force lbs, Slope S radians, Total Stress psi, Bending Stiffness lb-in^2, Soil Res. p lb/in, Soil Spr. Es h lb/inch, Distrib. Lat. Load lb/inch. Rows include Abut 1R_ong_Ave P and Abut 2S_ong_Ave P.

Table with columns: Displacement of pile head, Moment at pile head, Axial load at pile head, Depth X inches, Deflect. Y inches, Bending Moment in-lbs, Shear Force lbs, Slope S radians, Total Stress psi, Bending Stiffness lb-in^2, Soil Res. p lb/in, Soil Spr. Es h lb/inch, Distrib. Lat. Load lb/inch. Rows include Abut 1R_ong_Ave P and Abut 2S_ong_Ave P.

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

- Pile-head deflection = 0.2500000 inches
Computed slope at pile head = -0.0046390 radians
Maximum bending moment = 377472 inch-lbs
Maximum shear force = 372994 lbs
Depth of maximum bending moment = 54.000000 inches below pile head
Depth of maximum shear force = 0.000000 inches below pile head
Number of iterations = 17
Number of zero deflection points = 13

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 2

Table with columns: Displacement of pile head, Moment at pile head, Axial load at pile head, Depth X inches, Deflect. Y inches, Bending Moment in-lbs, Shear Force lbs, Slope S radians, Total Stress psi, Bending Stiffness lb-in^2, Soil Res. p lb/in, Soil Spr. Es h lb/inch, Distrib. Lat. Load lb/inch. Rows include Abut 1R_ong_Ave P and Abut 2S_ong_Ave P.

		Abut		1R_Long_Ave P					
516.000	0.000	-5.659E-09	4.475E-09	0.000	765.9332	5.799E+09	-6.234E-10	6071214.	0.000
522.000	0.000	1.001E-08	1.542E-09	0.000	765.9332	5.799E+09	-3.543E-10	5992338.	0.000
528.000	0.000	1.291E-08	1.917E-11	0.000	765.9332	5.799E+09	-1.533E-10	5913462.	0.000
534.000	0.000	1.029E-08	-5.469E-10	0.000	765.9332	5.799E+09	-3.543E-11	5834585.	0.000
540.000	0.000	6.377E-09	-5.992E-10	0.000	765.9332	5.799E+09	1.800E-11	5755709.	0.000
546.000	0.000	3.108E-09	-4.476E-10	0.000	765.9332	5.799E+09	3.252E-11	5676833.	0.000
552.000	0.000	1.007E-09	-2.642E-10	0.000	765.9332	5.799E+09	2.862E-11	5597957.	0.000
558.000	0.000	-6.503E-11	-1.211E-10	0.000	765.9332	5.799E+09	1.908E-11	5519081.	0.000
564.000	0.000	-4.499E-10	-3.342E-11	0.000	765.9332	5.799E+09	1.016E-11	5440204.	0.000
570.000	0.000	-4.685E-10	9.032E-12	0.000	765.9332	5.799E+09	3.989E-12	5361328.	0.000
576.000	0.000	-3.431E-10	2.267E-11	0.000	765.9332	5.799E+09	0.000	5282452.	0.000
582.000	0.000	-1.974E-10	2.155E-11	0.000	765.9332	5.799E+09	0.000	5203576.	0.000
588.000	0.000	-8.483E-11	1.481E-11	0.000	765.9332	5.799E+09	-1.321E-12	5124700.	0.000
594.000	0.000	-1.976E-11	7.066E-12	0.000	765.9332	5.799E+09	-1.259E-12	5045823.	0.000
600.000	0.000	0.000	0.000	0.000	765.9332	5.799E+09	-1.096E-12	2483474.	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

Pile-head deflection = 1.0000000 inches
 Computed slope at pile head = -0.0146990 radians
 Maximum bending moment = 948521. inch-lbs
 Maximum shear force = 24997. lbs
 Depth of maximum bending moment = 66.0000000 inches below pile head
 Depth of maximum shear force = 0.0000000 inches below pile head
 Number of iterations = 24
 Number of zero deflection points = 12

 Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

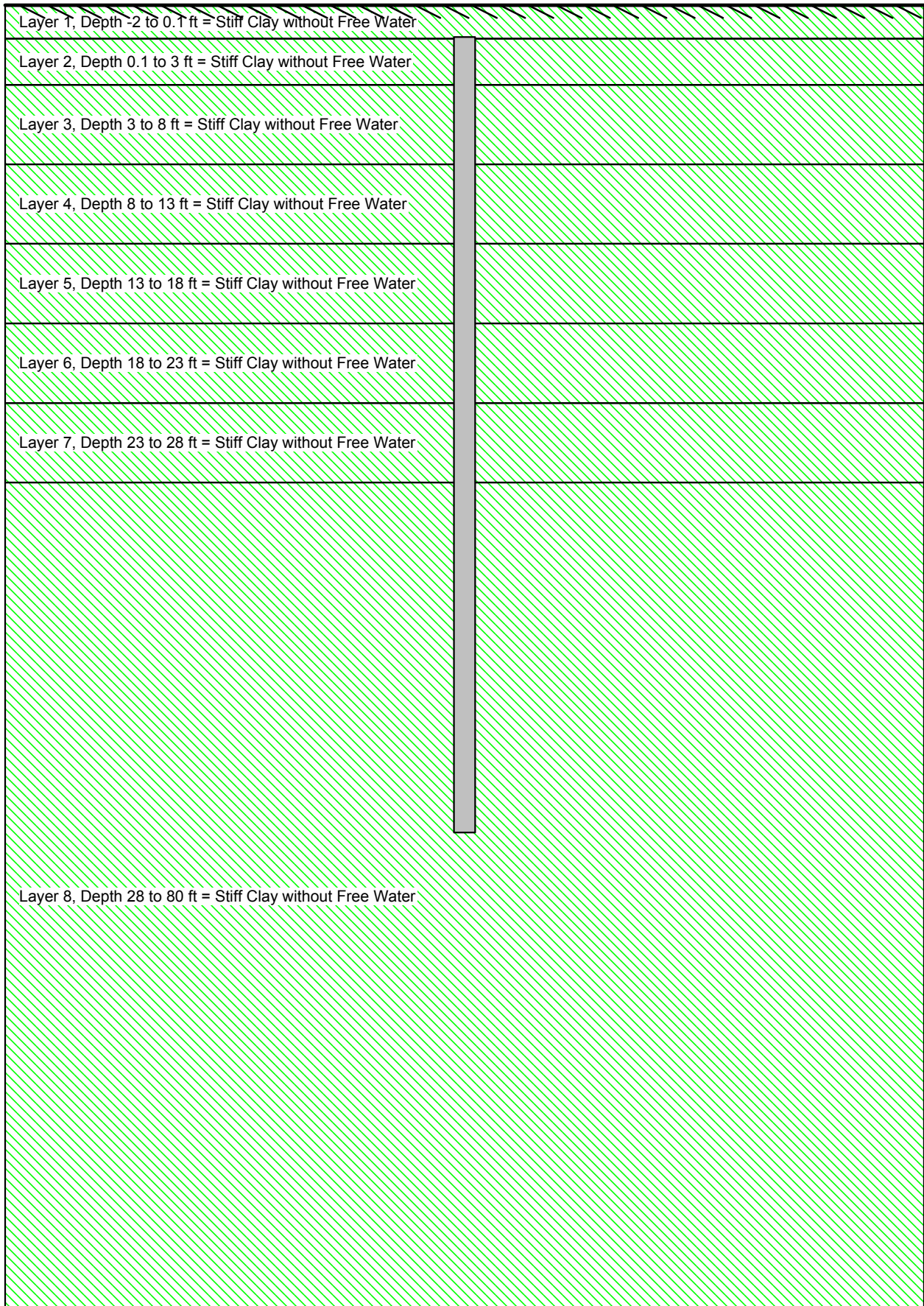
Load Case No.	Load Type No.		Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians	
1	4	y =	0.2500	M =	0.000	154000.	0.25000000	377472.	13327.	-0.00463902
2	4	sy =	0.5000	M =	0.000	154000.	0.50000000	600061.	18283.	-0.00827470
3	4	y =	1.0000	M =	0.000	154000.	1.00000000	948521.	24997.	-0.01469901

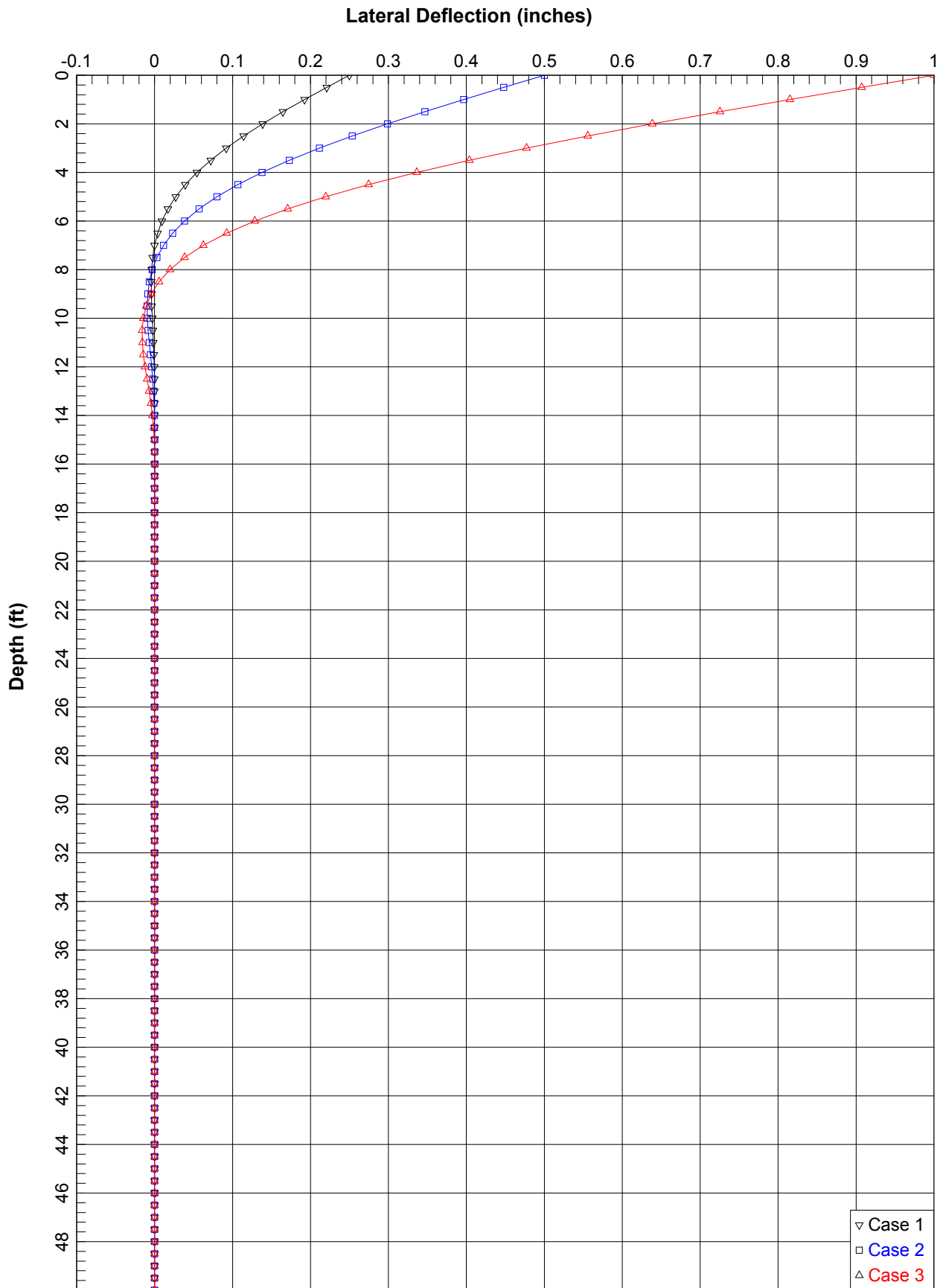
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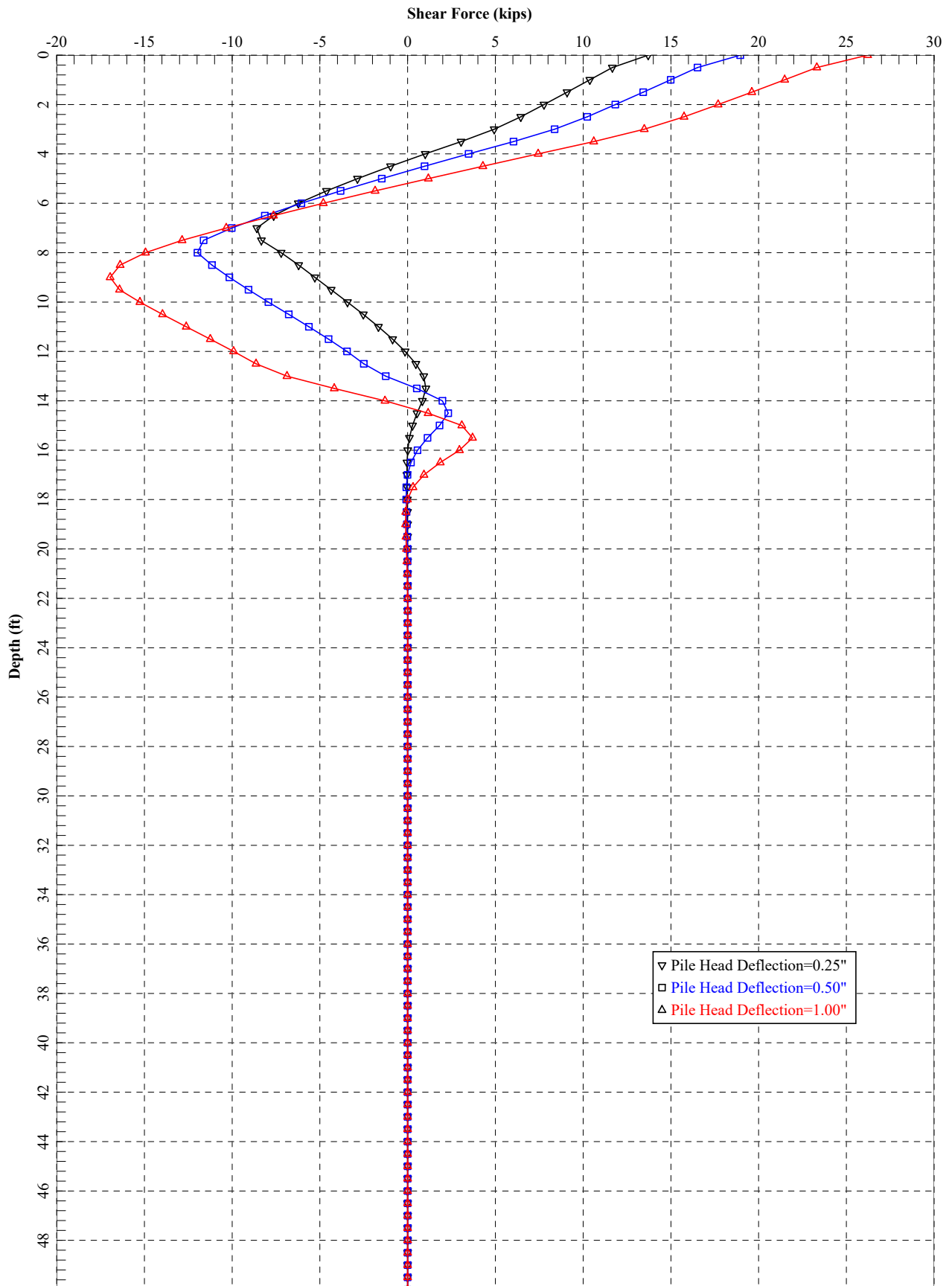
SUPPORT: ABUTMENT 1R

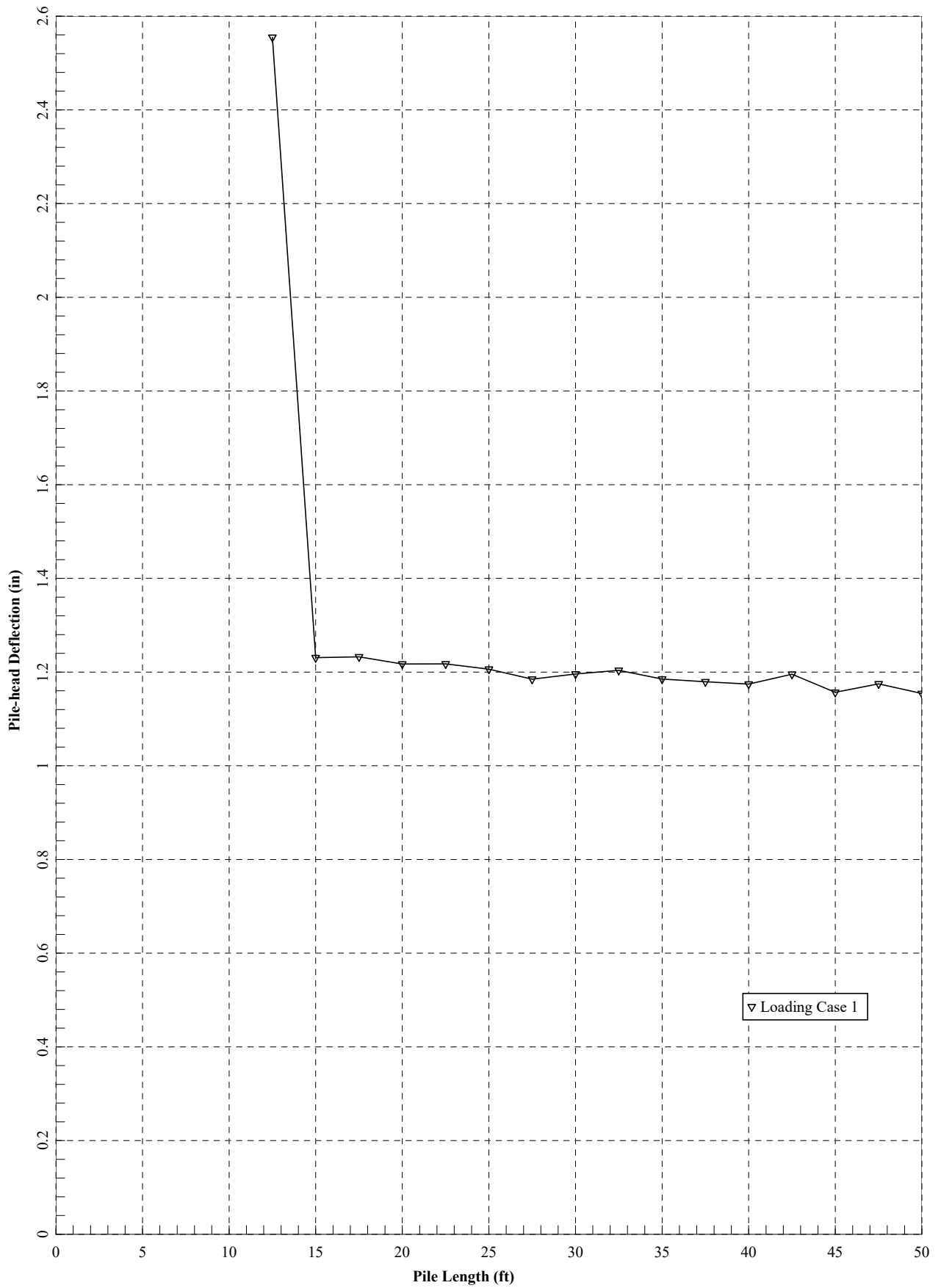
LOAD DIRECTION: TRANSVERSE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE









Abut 1R_transv_Critical Length.lp9o

LPIle for Windows, Version 2016-09.010

Analysis of Individual Piles and Drilled Shafts
Subjected to Lateral Loading Using the p-y Method
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Files Used for Analysis

Path to file locations:
\\Projects_LA\L1100\LA1143 PTG - 101 & Palo Comado Cyn\Irvine Foundation Report\Calculations\Lateral Pile Capacity\Updated 08-24-17\

Name of input data file:
Abut 1R_transv_Critical Length.lp9d

Name of output report file:
Abut 1R_transv_Critical Length.lp9o

Name of plot output file:
Abut 1R_transv_Critical Length.lp9p

Name of runtime message file:
Abut 1R_transv_Critical Length.lp9r

Date and Time of Analysis

Date: August 24, 2017 Time: 11:13:12

Problem Title

Project Name: Palo Comado OC Bridge Widen

Job Number: LA-1143

Client: Parson Transportation

Abut 1R_transv_Critical Length.lp9o

Engineer: Mario DiNicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options and Settings

Computational Options:

- Use unfactored loads in computations (conventional analysis)
- Engineering Units Used for Data Input and Computations:
 - US Customary System Units (pounds, feet, inches)

Analysis Control Options:

- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in
- Number of pile increments = 100

Loading Type and Number of Cycles of Loading:

- Static loading specified

- Analysis uses p-y modification factors for p-y curves
- No distributed lateral loads are entered
- Loading by lateral soil movements acting on pile not selected
- Input of shear resistance at the pile tip not selected
- Computation of pile-head foundation stiffness matrix not selected
- Push-over analysis of pile not selected
- Buckling analysis of pile not selected

Output Options:

- Output files use decimal points to denote decimal symbols.
- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1
- No p-y curves to be computed and reported for user-specified depths
- Print using wide report formats

Pile Structural Properties and Geometry

Number of pile sections defined = 1
Total length of pile = 50.000 ft
Depth of ground surface below top of pile = -2.0000 ft

Pile diameters used for p-y curve computations are defined using 2 points.

p-y curves are computed using pile diameter values interpolated with depth over the length of the pile. A summary of values of pile diameter vs. depth follows.

Point No.	Depth Below Pile Head feet	Pile Diameter inches
1	0.000	16.0000
2	50.000	16.0000

Input Structural Properties for Pile Sections:

Pile Section No. 1:

Section 1 is an elastic pile
 Cross-sectional Shape = Circular Pile
 Length of section = 50.000000 ft
 Width of top of section = 16.000000 in
 Width of bottom of section = 16.000000 in
 Top Area = 201.061930 sq. in
 Bottom Area = 201.061930 sq. in
 Moment of Inertia at Top = 1608. in^4
 Moment of Inertia at Bottom = 1608. in^4
 Elastic Modulus = 3605000. psi

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 8 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.000000 ft
 Distance from top of pile to bottom of layer = 0.100000 ft
 Effective unit weight at top of layer = 120.000000 pcf
 Effective unit weight at bottom of layer = 120.000000 pcf
 Undrained cohesion at top of layer = 3500. psf
 Undrained cohesion at bottom of layer = 3500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.100000 ft
 Distance from top of pile to bottom of layer = 3.000000 ft
 Effective unit weight at top of layer = 120.000000 pcf
 Effective unit weight at bottom of layer = 120.000000 pcf
 Undrained cohesion at top of layer = 1500. psf
 Undrained cohesion at bottom of layer = 1500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 3.000000 ft
 Distance from top of pile to bottom of layer = 8.000000 ft
 Effective unit weight at top of layer = 120.000000 pcf
 Effective unit weight at bottom of layer = 120.000000 pcf
 Undrained cohesion at top of layer = 2500. psf
 Undrained cohesion at bottom of layer = 2500. psf
 Epsilon-50 at top of layer = 0.007000

Epsilon-50 at bottom of layer = 0.007000

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 8.000000 ft
 Distance from top of pile to bottom of layer = 13.000000 ft
 Effective unit weight at top of layer = 120.000000 pcf
 Effective unit weight at bottom of layer = 120.000000 pcf
 Undrained cohesion at top of layer = 1500. psf
 Undrained cohesion at bottom of layer = 1500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 13.000000 ft
 Distance from top of pile to bottom of layer = 18.000000 ft
 Effective unit weight at top of layer = 125.000000 pcf
 Effective unit weight at bottom of layer = 125.000000 pcf
 Undrained cohesion at top of layer = 4500. psf
 Undrained cohesion at bottom of layer = 4500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 6 is stiff clay without free water

Distance from top of pile to top of layer = 18.000000 ft
 Distance from top of pile to bottom of layer = 23.000000 ft
 Effective unit weight at top of layer = 125.000000 pcf
 Effective unit weight at bottom of layer = 125.000000 pcf
 Undrained cohesion at top of layer = 2500. psf
 Undrained cohesion at bottom of layer = 2500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 7 is stiff clay without free water

Distance from top of pile to top of layer = 23.000000 ft
 Distance from top of pile to bottom of layer = 28.000000 ft
 Effective unit weight at top of layer = 125.000000 pcf
 Effective unit weight at bottom of layer = 125.000000 pcf
 Undrained cohesion at top of layer = 3500. psf
 Undrained cohesion at bottom of layer = 3500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 8 is stiff clay without free water

Distance from top of pile to top of layer = 28.000000 ft
 Distance from top of pile to bottom of layer = 80.000000 ft
 Effective unit weight at top of layer = 125.000000 pcf
 Effective unit weight at bottom of layer = 125.000000 pcf
 Undrained cohesion at top of layer = 4500. psf
 Undrained cohesion at bottom of layer = 4500. psf
 Epsilon-50 at top of layer = 0.005000
 Epsilon-50 at bottom of layer = 0.005000

(Depth of the lowest soil layer extends 30.000 ft below the pile tip)

Abut 1R_transv_Critical Length.lp9o
Summary of Input Soil Properties

Layer Num.	Soil Type Name (p-y Curve Type)	Layer Depth ft	Effective Unit Wt. pcf	Undrained Cohesion psf	E50 or krm
1	Stiff Clay	-2.0000	120.0000	3500.	0.00700
	w/o Free Water	0.10000	120.0000	3500.	0.00700
2	Stiff Clay	0.10000	120.0000	1500.	0.00700
	w/o Free Water	3.00000	120.0000	1500.	0.00700
3	Stiff Clay	3.00000	120.0000	2500.	0.00700
	w/o Free Water	8.00000	120.0000	2500.	0.00700
4	Stiff Clay	8.00000	120.0000	1500.	0.00700
	w/o Free Water	13.00000	120.0000	1500.	0.00700
5	Stiff Clay	13.00000	125.0000	4500.	0.00700
	w/o Free Water	18.00000	125.0000	4500.	0.00700
6	Stiff Clay	18.00000	125.0000	2500.	0.00700
	w/o Free Water	23.00000	125.0000	2500.	0.00700
7	Stiff Clay	23.00000	125.0000	3500.	0.00700
	w/o Free Water	28.00000	125.0000	3500.	0.00500
8	Stiff Clay	28.00000	125.0000	4500.	0.00500
	w/o Free Water	80.00000	125.0000	4500.	0.00500

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.6500	1.0000
2	50.000	0.6500	1.0000

Static Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	1	V = 28000. lbs	M = 0.0000 in-lbs	154000.	Yes

V = shear force applied normal to pile axis
M = bending moment applied to pile head
y = lateral deflection normal to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Values of top y vs. pile lengths can be computed only for load types with specified shear loading (Load Types 1, 2, and 3).
Thrust force is assumed to be acting axially for all pile batter angles.

Abut 1R_transv_Critical Length.lp9o

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Layering Correction Equivalent Depths of Soil & Rock Layers

Layer No.	Top of Layer Below Pile Head ft	Equivalent Top Depth Below Grnd Surf ft	Same Layer Type As Layer Above	Layer is Rock or is Below Rock Layer	F0 Integral for Layer lbs	F1 Integral for Layer lbs
1	-2.0000	0.00	N.A.	No	0.00	1790.
2	0.1000	2.1000	Yes	No	1790.	25921.
3	3.0000	5.0000	Yes	No	27711.	101146.
4	8.0000	10.0000	Yes	No	128856.	84678.
5	13.0000	15.0000	Yes	No	213535.	269497.
6	18.0000	20.0000	Yes	No	483031.	150300.
7	23.0000	25.0000	Yes	No	633331.	210000.
8	28.0000	30.0000	Yes	No	843331.	N.A.

Notes: The F0 integral of Layer n+1 equals the sum of the F0 and F1 integrals for Layer n. Layering correction equivalent depths are computed only for soil types with both shallow-depth and deep-depth expressions for peak lateral load transfer. These soil types are soft and stiff clays, non-liquefied sands, and cemented c-phi soil.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head = 28000.0 lbs
Applied moment at pile head = 0.0 in-lbs
Axial thrust load on pile head = 154000.0 lbs

Depth X feet	Deflect. y inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness in-lb*2	Soil Res. p lb/inch	Soil Spr. Es*h lb/inch	Distrib. Lat. Load lb/inch
0.00	1.1543	5.01E-07	28000.	-0.01706	765.9332	5.80E+09	-687.7017	1787.	0.00
0.5000	1.0519	171385.	25001.	-0.01697	1618.	5.80E+09	-312.0168	1780.	0.00
1.0000	0.9506	331374.	23102.	-0.01671	2414.	5.80E+09	-320.9448	2026.	0.00
1.5000	0.8514	479493.	21154.	-0.01629	3151.	5.80E+09	-328.4915	2315.	0.00
2.0000	0.7551	615327.	19164.	-0.01573	3826.	5.80E+09	-334.5756	2659.	0.00
2.5000	0.6627	738528.	17143.	-0.01503	4439.	5.80E+09	-339.1131	3070.	0.00
3.0000	0.5748	848814.	14784.	-0.01420	4988.	5.80E+09	-447.3773	4670.	0.00
3.5000	0.4922	942184.	11781.	-0.01328	5452.	5.80E+09	-553.6993	6750.	0.00
4.0000	0.4155	1014720.	8464.	-0.01227	5813.	5.80E+09	-551.8007	7969.	0.00

			Abut 1R_transv_Critical Length.lp9o
20.00000	1.21727646	1147967.	28000.
17.50000	1.23258829	1155301.	28000.
15.00000	1.23068707	1155212.	28000.
12.50000	2.55492662	1124242.	28000.

Summary of Pile-head Responses for Conventional Analyses

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, V, lbs, and Load 2 = Moment, M, in-lbs
Load Type 2: Load 1 = Shear, V, lbs, and Load 2 = Slope, S, radians
Load Type 3: Load 1 = Shear, V, lbs, and Load 2 = Rot. Stiffness, R, in-lbs/rad.
Load Type 4: Load 1 = Top Deflection, y, inches, and Load 2 = Moment, M, in-lbs
Load Type 5: Load 1 = Top Deflection, y, inches, and Load 2 = Slope, S, radians

Load Case	Load Type	Load 1	Load 2	Axial Loading	Pile-head Deflection	Pile-head Rotation	Max Shear	Max Moment	
No.		Load 1	Load 2	lbs	inches	radians	lbs	in-lbs	
1	V, lb	28000.	M, in-lb	0.00	154000.	1.1543	-0.01706	28000.	1107964.

Maximum pile-head deflection = 1.1542764728 inches
Maximum pile-head rotation = -0.0170606763 radians = -0.977505 deg.

The analysis ended normally.

Abut 1R_transv_Ave P.lp9o

LPIle for Windows, Version 2016-09.010

Analysis of Individual Piles and Drilled Shafts
Subjected to Lateral Loading Using the p-y Method
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Files Used for Analysis

Path to file locations:
\\Projects_LA\L1100\LA1143 PTG - 101 & Palo Comado Cyn\Irvine Foundation Report\Calculations\Lateral Pile Capacity\Updated 08-24-17\

Name of input data file:
Abut 1R_transv_Ave P.lp9d

Name of output report file:
Abut 1R_transv_Ave P.lp9o

Name of plot output file:
Abut 1R_transv_Ave P.lp9p

Name of runtime message file:
Abut 1R_transv_Ave P.lp9r

Date and Time of Analysis

Date: August 24, 2017 Time: 11:10:15

Problem Title

Project Name: Palo Comado OC Bridge Widen

Job Number: LA-1143

Client: Parson Transportation

Abut 1R_transv_Ave P.lp9o

Engineer: Mario DiNicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options and Settings

Computational Options:

- Use unfactored loads in computations (conventional analysis)
- Engineering Units Used for Data Input and Computations:
 - US Customary System Units (pounds, feet, inches)

Analysis Control Options:

- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in
- Number of pile increments = 100

Loading Type and Number of Cycles of Loading:

- Static loading specified

- Analysis uses p-y modification factors for p-y curves
- No distributed lateral loads are entered
- Loading by lateral soil movements acting on pile not selected
- Input of shear resistance at the pile tip not selected
- Computation of pile-head foundation stiffness matrix not selected
- Push-over analysis of pile not selected
- Buckling analysis of pile not selected

Output Options:

- Output files use decimal points to denote decimal symbols.
- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1
- No p-y curves to be computed and reported for user-specified depths
- Print using wide report formats

Pile Structural Properties and Geometry

Number of pile sections defined = 1
Total length of pile = 50.000 ft
Depth of ground surface below top of pile = -2.0000 ft

Pile diameters used for p-y curve computations are defined using 2 points.

p-y curves are computed using pile diameter values interpolated with depth over the length of the pile. A summary of values of pile diameter vs. depth follows.

Point No.	Depth Below Pile Head feet	Pile Diameter inches
1	0.000	16.0000
2	50.000	16.0000

Input Structural Properties for Pile Sections:

Abut 1R_transv_Ave P.lp9o

Pile Section No. 1:

Section 1 is an elastic pile
Cross-sectional Shape = Circular Pile
Length of section = 50.000000 ft
Width of top of section = 16.000000 in
Width of bottom of section = 16.000000 in
Top Area = 201.061930 sq. in
Bottom Area = 201.061930 sq. in
Moment of Inertia at Top = 1608. in^4
Moment of Inertia at Bottom = 1608. in^4
Elastic Modulus = 3605000. psi

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
= 0.000 radians
Pile Batter Angle = 0.000 degrees
= 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 8 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.000000 ft
Distance from top of pile to bottom of layer = 0.100000 ft
Effective unit weight at top of layer = 120.000000 pcf
Effective unit weight at bottom of layer = 120.000000 pcf
Undrained cohesion at top of layer = 3500. psf
Undrained cohesion at bottom of layer = 3500. psf
Epsilon-50 at top of layer = 0.007000
Epsilon-50 at bottom of layer = 0.007000

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.100000 ft
Distance from top of pile to bottom of layer = 3.000000 ft
Effective unit weight at top of layer = 120.000000 pcf
Effective unit weight at bottom of layer = 120.000000 pcf
Undrained cohesion at top of layer = 1500. psf
Undrained cohesion at bottom of layer = 1500. psf
Epsilon-50 at top of layer = 0.007000
Epsilon-50 at bottom of layer = 0.007000

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 3.000000 ft
Distance from top of pile to bottom of layer = 8.000000 ft
Effective unit weight at top of layer = 120.000000 pcf
Effective unit weight at bottom of layer = 120.000000 pcf
Undrained cohesion at top of layer = 2500. psf
Undrained cohesion at bottom of layer = 2500. psf
Epsilon-50 at top of layer = 0.007000

Abut 1R_transv_Ave P.lp9o

Epsilon-50 at bottom of layer = 0.007000

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 8.000000 ft
Distance from top of pile to bottom of layer = 13.000000 ft
Effective unit weight at top of layer = 120.000000 pcf
Effective unit weight at bottom of layer = 120.000000 pcf
Undrained cohesion at top of layer = 1500. psf
Undrained cohesion at bottom of layer = 1500. psf
Epsilon-50 at top of layer = 0.007000
Epsilon-50 at bottom of layer = 0.007000

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 13.000000 ft
Distance from top of pile to bottom of layer = 18.000000 ft
Effective unit weight at top of layer = 125.000000 pcf
Effective unit weight at bottom of layer = 125.000000 pcf
Undrained cohesion at top of layer = 4500. psf
Undrained cohesion at bottom of layer = 4500. psf
Epsilon-50 at top of layer = 0.007000
Epsilon-50 at bottom of layer = 0.007000

Layer 6 is stiff clay without free water

Distance from top of pile to top of layer = 18.000000 ft
Distance from top of pile to bottom of layer = 23.000000 ft
Effective unit weight at top of layer = 125.000000 pcf
Effective unit weight at bottom of layer = 125.000000 pcf
Undrained cohesion at top of layer = 2500. psf
Undrained cohesion at bottom of layer = 2500. psf
Epsilon-50 at top of layer = 0.007000
Epsilon-50 at bottom of layer = 0.007000

Layer 7 is stiff clay without free water

Distance from top of pile to top of layer = 23.000000 ft
Distance from top of pile to bottom of layer = 28.000000 ft
Effective unit weight at top of layer = 125.000000 pcf
Effective unit weight at bottom of layer = 125.000000 pcf
Undrained cohesion at top of layer = 3500. psf
Undrained cohesion at bottom of layer = 3500. psf
Epsilon-50 at top of layer = 0.007000
Epsilon-50 at bottom of layer = 0.007000

Layer 8 is stiff clay without free water

Distance from top of pile to top of layer = 28.000000 ft
Distance from top of pile to bottom of layer = 80.000000 ft
Effective unit weight at top of layer = 125.000000 pcf
Effective unit weight at bottom of layer = 125.000000 pcf
Undrained cohesion at top of layer = 4500. psf
Undrained cohesion at bottom of layer = 4500. psf
Epsilon-50 at top of layer = 0.005000
Epsilon-50 at bottom of layer = 0.005000

(Depth of the lowest soil layer extends 30.000 ft below the pile tip)

Abut 1R_transv_Ave P.lp90
Summary of Input Soil Properties

Layer Layer Num.	Soil Type Name (p-y Curve Type)	Layer Depth ft	Effective Unit Wt. pcf	Undrained Cohesion psf	E50 or krm
1	Stiff Clay	-2.0000	120.0000	3500.	0.00700
	w/o Free Water	0.10000	120.0000	3500.	0.00700
2	Stiff Clay	0.10000	120.0000	1500.	0.00700
	w/o Free Water	3.0000	120.0000	1500.	0.00700
3	Stiff Clay	3.0000	120.0000	2500.	0.00700
	w/o Free Water	8.0000	120.0000	2500.	0.00700
4	Stiff Clay	8.0000	120.0000	1500.	0.00700
	w/o Free Water	13.0000	120.0000	1500.	0.00700
5	Stiff Clay	13.0000	125.0000	4500.	0.00700
	w/o Free Water	18.0000	125.0000	4500.	0.00700
6	Stiff Clay	18.0000	125.0000	2500.	0.00700
	w/o Free Water	23.0000	125.0000	2500.	0.00700
7	Stiff Clay	23.0000	125.0000	3500.	0.00700
	w/o Free Water	28.0000	125.0000	3500.	0.00700
8	Stiff Clay	28.0000	125.0000	4500.	0.00500
	w/o Free Water	80.0000	125.0000	4500.	0.00500

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.6500	1.0000
2	50.000	0.6500	1.0000

Static Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4	y = 0.250000 in	M = 0.0000 in-lbs	154000.	N.A.
2	4	y = 0.500000 in	M = 0.0000 in-lbs	154000.	N.A.
3	4	y = 1.000000 in	M = 0.0000 in-lbs	154000.	N.A.

V = shear force applied normal to pile axis
M = bending moment applied to pile head
y = lateral deflection normal to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Values of top y vs. pile lengths can be computed only for load types with specified shear loading (Load Types 1, 2, and 3).

Abut 1R_transv_Ave P.lp90

Thrust force is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Layering Correction Equivalent Depths of Soil & Rock Layers

Layer No.	Top of Layer Below Pile Head ft	Equivalent Top Depth Below Grnd Surf ft	Same Layer Type As Layer Above	Layer is Rock or is Below Rock Layer	F0 Integral for Layer lbs	F1 Integral for Layer lbs
1	-2.0000	0.00	N.A.	No	0.00	1790.
2	0.1000	2.1000	Yes	No	1790.	25921.
3	3.0000	5.0000	Yes	No	27711.	101146.
4	8.0000	10.0000	Yes	No	128856.	84678.
5	13.0000	15.0000	Yes	No	213535.	269497.
6	18.0000	20.0000	Yes	No	483031.	150300.
7	23.0000	25.0000	Yes	No	633331.	210000.
8	28.0000	30.0000	Yes	No	843331.	N.A.

Notes: The F0 integral of Layer n+1 equals the sum of the F0 and F1 integrals for Layer n. Layering correction equivalent depths are computed only for soil types with both shallow-depth and deep-depth expressions for peak lateral load transfer. These soil types are soft and stiff clays, non-liquefied sands, and cemented c-phi soil.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.250000 inches
Moment at pile head = 0.0 in-lbs
Axial load at pile head = 154000.0 lbs

Depth X feet	Deflect. y inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness in-lb^2	Soil Res. p lb/inch	Soil Spr. Es*h lb/inch	Distrib. Lat. Load lb/inch
0.00	0.2500	0.00	13707.	-0.00474	765.9332	5.80E+09	-469.1431	5630.	0.00
0.5000	0.2215	78179.	11665.	-0.00470	1155.	5.80E+09	-211.3709	5725.	0.00
1.0000	0.1936	148674.	10384.	-0.00459	1505.	5.80E+09	-215.5942	6683.	0.00
1.5000	0.1665	211266.	9082.	-0.00440	1817.	5.80E+09	-218.4539	7872.	0.00
2.0000	0.1408	265791.	7767.	-0.00415	2088.	5.80E+09	-219.8509	9370.	0.00
2.5000	0.1167	312147.	6449.	-0.00385	2318.	5.80E+09	-219.6763	11296.	0.00
3.0000	0.09453	350297.	4935.	-0.00351	2508.	5.80E+09	-284.9063	18083.	0.00
3.5000	0.07455	377855.	3044.	-0.00313	2645.	5.80E+09	-345.4401	27801.	0.00

Abut 1R_transv_Ave P.lp90 table with columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load

Abut 1R_transv_Ave P.lp90 table with columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load

* The above values of total stress are combined axial and bending stresses.

Output Summary for Load Case No. 1: Pile-head deflection = 0.2500000 inches, Computed slope at pile head = -0.00474337 radians, Maximum bending moment = 394915. inch-lbs, Maximum shear force = 13707. lbs, Depth of maximum bending moment = 4.5000000 feet below pile head, Depth of maximum shear force = 0.0000000 feet below pile head, Number of iterations = 11, Number of zero deflection points = 12

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4) Displacement of pile head = 0.5000000 inches, Moment at pile head = 0.0 in-lbs, Axial load at pile head = 154000.0 lbs

Table with columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load

Table with columns for Case No., Load, Abut 1R_transv_Ave P.lp90, and various stress/strain values. Includes a 'Page 11' label at the bottom.

Table with columns for Case No., Load, Abut 1R_transv_Ave P.lp90, and various stress/strain values. Includes a 'Page 12' label at the bottom.

* The above values of total stress are combined axial and bending stresses.

Output Summary for Load Case No. 3:

Summary table showing metrics: Pile-head deflection, Computed slope at pile head, Maximum bending moment, Maximum shear force, Depth of maximum bending moment, Depth of maximum shear force, Number of iterations, and Number of zero deflection points.

Summary of Pile-head Responses for Conventional Analyses

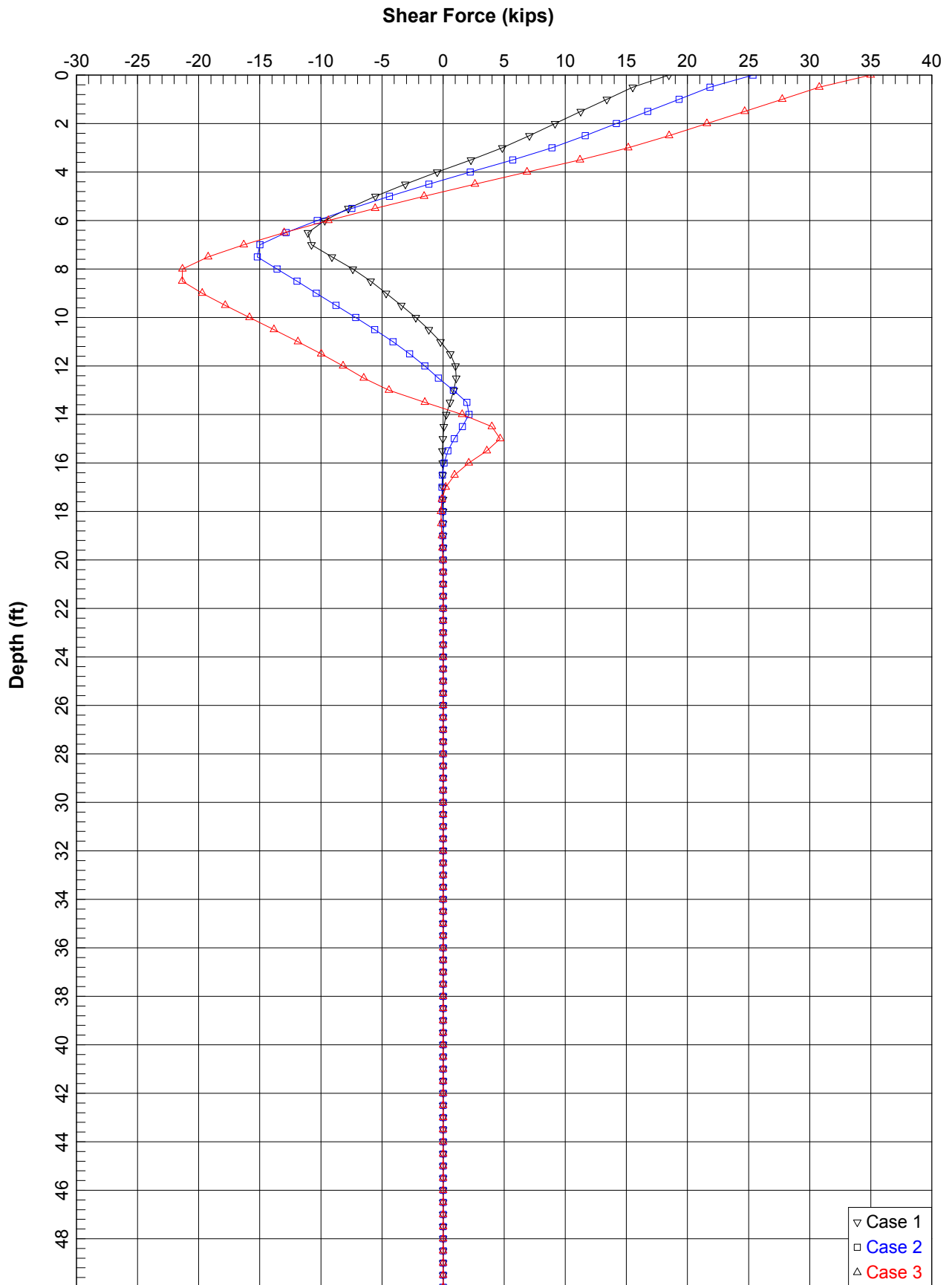
Definitions of Pile-head Loading Conditions:

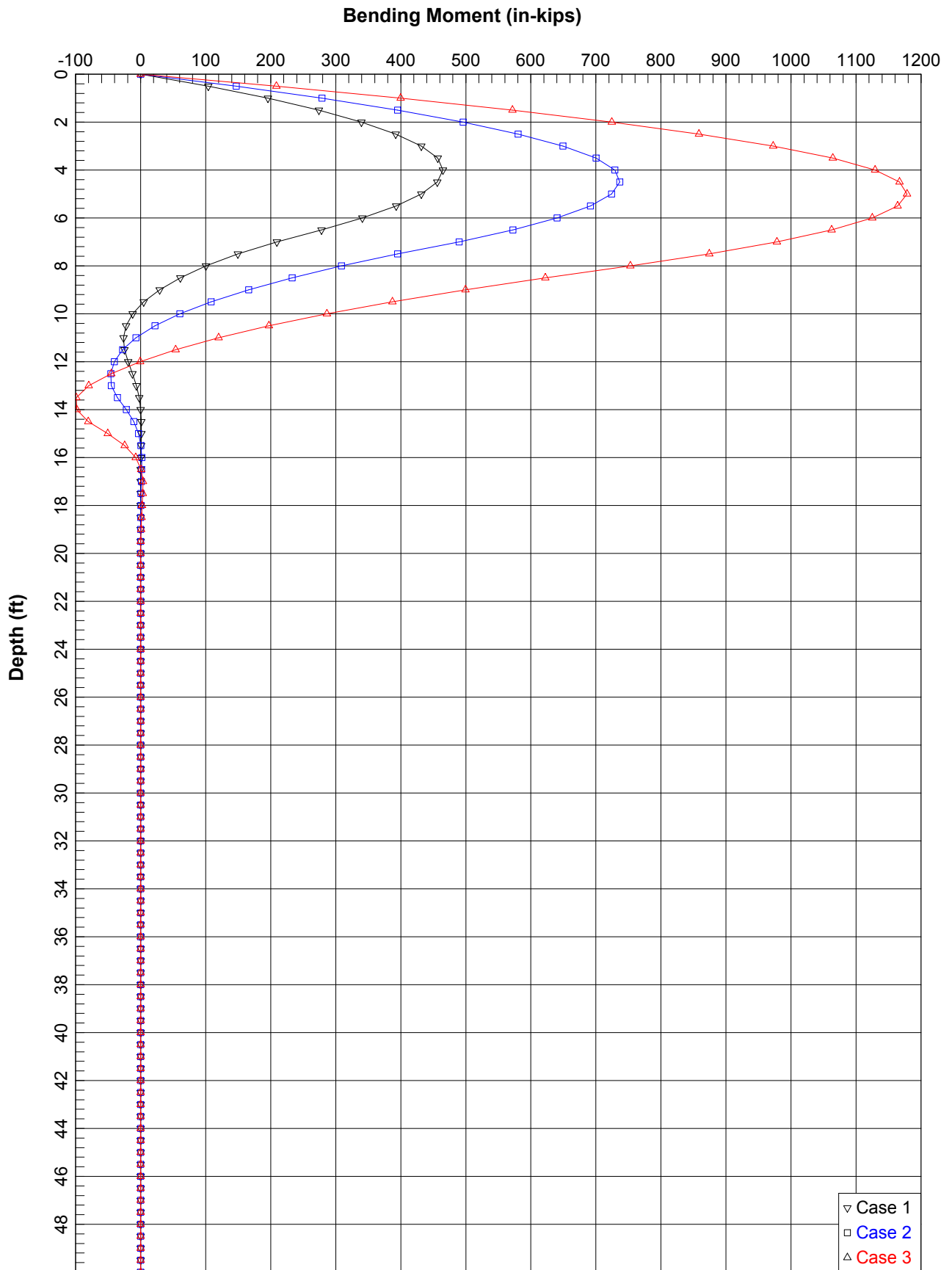
Load Type 1: Load 1 = Shear, V, lbs, and Load 2 = Moment, M, in-lbs
Load Type 2: Load 1 = Shear, V, lbs, and Load 2 = Slope, S, radians
Load Type 3: Load 1 = Shear, V, lbs, and Load 2 = Rot. Stiffness, R, in-lbs/rad.
Load Type 4: Load 1 = Top Deflection, y, inches, and Load 2 = Moment, M, in-lbs
Load Type 5: Load 1 = Top Deflection, y, inches, and Load 2 = Slope, S, radians

Table with columns: Load Case No., Pile-head Load 1, Load 2, Axial Loading lbs, Pile-head Deflection inches, Pile-head Rotation radians, Max Shear in lbs, and Max Moment in lbs.

Maximum pile-head deflection = 1.000000000 inches
Maximum pile-head rotation = -0.0151455973 radians = -0.867779 deg.

The analysis ended normally.





Abut 1R_transv_Max P

Pile Plus For Windows, Version 2012-06.031
Analysis of Individual Piles and Drilled Shafts
Subjected to Lateral Loading Using the p-y Method
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Serial Number of Security Device: 161633771
Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 1\
Name of input data file: Abut 1R_transv_Max P.lpd
Name of output report file: Abut 1R_transv_Max P.lpp
Name of plot output file: Abut 1R_transv_Max P.lpp
Name of runtime message file: Abut 1R_transv_Max P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 9:25:27

Problem Title

Project Name: Palo Comado OC Bridge Widen

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Page 1

Abut 1R_transv_Max P

Total Number of Sections = 1
Total Pile Length = 50.00 ft
Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:

Section Type = Elastic Pile
Cross-sectional Shape = Circular
Section Length = 50.0000000 ft
Top Width = 16.0000000 in
Bottom Width = 16.0000000 in
Top Area = 201.06192983 in
Bottom Area = 201.06192983 in
Moment of Inertia at Top = 1608.49543864 in
Moment of Inertia at Bottom = 1608.49543864 in
Elastic Modulus = 365000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
= 0.000 radians
Pile Batter Angle = 0.000 degrees
= 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 8 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
Distance from top of pile to bottom of layer = 0.10000 ft
Effective unit weight at top of layer = 120.00000 pcf
Effective unit weight at bottom of layer = 120.00000 pcf
Undrained cohesion at top of layer = 3500.00000 psi
Undrained cohesion at bottom of layer = 3500.00000 psi
Epsilon-50 at top of layer = 0.00700
Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
Distance from top of pile to bottom of layer = 3.00000 ft
Effective unit weight at top of layer = 120.00000 pcf
Effective unit weight at bottom of layer = 120.00000 pcf
Undrained cohesion at top of layer = 1500.00000 psi
Undrained cohesion at bottom of layer = 1500.00000 psi
Epsilon-50 at top of layer = 0.00700
Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 3.00000 ft
Distance from top of pile to bottom of layer = 8.00000 ft
Effective unit weight at top of layer = 120.00000 pcf
Effective unit weight at bottom of layer = 120.00000 pcf
Undrained cohesion at top of layer = 2500.00000 psi
Undrained cohesion at bottom of layer = 2500.00000 psi

Page 2

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water
 Distance from top of pile to top of layer = 8.00000 ft
 Distance from top of pile to bottom of layer = 13.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water
 Distance from top of pile to top of layer = 13.00000 ft
 Distance from top of pile to bottom of layer = 18.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 6 is stiff clay without free water
 Distance from top of pile to top of layer = 18.00000 ft
 Distance from top of pile to bottom of layer = 23.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 2500.00000 psi
 Undrained cohesion at bottom of layer = 2500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 7 is stiff clay without free water
 Distance from top of pile to top of layer = 23.00000 ft
 Distance from top of pile to bottom of layer = 28.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 8 is stiff clay without free water
 Distance from top of pile to top of layer = 28.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type	Rock Mass Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Uniaxial Elastic Mod.	ROD %
Num.	Epsilon 50	(p-y Curve Criteria) Factor	Rock Emass	pcf	psf	deg.	psi	or GSI
			ft	pcf	Type	Property	psi	
1	0.00700	Stiff Clay w/o Free Water	-2.000	120.000	3500.000	--	--	--
	0.00700	--	0.10000	120.000	3500.000	--	--	--
2	0.00700	Stiff Clay w/o Free Water	0.10000	120.000	1500.000	--	--	--
	0.00700	--	3.000	120.000	1500.000	--	--	--
3	0.00700	Stiff Clay w/o Free Water	3.000	120.000	2500.000	--	--	--
	0.00700	--	8.000	120.000	2500.000	--	--	--

			Abut 1R_transv_Max P				
4	0.00700	Stiff Clay w/o Free Water	8.000	120.000	1500.000	--	--
	0.00700	--	13.000	120.000	1500.000	--	--
5	0.00700	Stiff Clay w/o Free Water	13.000	125.000	4500.000	--	--
	0.00700	--	18.000	125.000	4500.000	--	--
6	0.00700	Stiff Clay w/o Free Water	18.000	125.000	2500.000	--	--
	0.00700	--	23.000	125.000	2500.000	--	--
7	0.00700	Stiff Clay w/o Free Water	23.000	125.000	3500.000	--	--
	0.00700	--	28.000	125.000	3500.000	--	--
8	0.00500	Stiff Clay w/o Free Water	28.000	125.000	4500.000	--	--
	0.00500	--	80.000	125.000	4500.000	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.8800	1.0000
2	50.000	0.8800	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4	y = 0.25000 in	M = 0.0000 in-lbs	154000.	False
2	4	y = 0.50000 in	M = 0.0000 in-lbs	154000.	False
3	4	y = 1.00000 in	M = 0.0000 in-lbs	154000.	False

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Abut 1R_transv_Max P									
516.000	0.000	1.587E-08	2.092E-09	0.000	765.9332	5.799E+09	-5.390E-10	7425000.	0.000
522.000	0.000	1.876E-08	-1.670E-10	0.000	765.9332	5.799E+09	-2.140E-10	7425000.	0.000
528.000	0.000	1.393E-08	-9.084E-10	0.000	765.9332	5.799E+09	-3.314E-11	7425000.	0.000
534.000	0.000	7.888E-09	-8.857E-10	0.000	765.9332	5.799E+09	4.072E-11	7425000.	0.000
540.000	0.000	3.309E-09	-6.016E-10	0.000	765.9332	5.799E+09	5.397E-11	7425000.	0.000
546.000	0.000	6.690E-10	-3.143E-10	0.000	765.9332	5.799E+09	4.180E-11	7425000.	0.000
552.000	0.000	-4.665E-10	-1.154E-10	0.000	765.9332	5.799E+09	2.450E-11	7425000.	0.000
558.000	0.000	-7.196E-10	-9.567E-12	0.000	765.9332	5.799E+09	1.078E-11	7425000.	0.000
564.000	0.000	-5.841E-10	3.052E-11	0.000	765.9332	5.799E+09	2.584E-12	7425000.	0.000
570.000	0.000	-3.549E-10	3.490E-11	0.000	765.9332	5.799E+09	-1.122E-12	7425000.	0.000
576.000	0.000	-1.658E-10	2.524E-11	0.000	765.9332	5.799E+09	-2.101E-12	7425000.	0.000
582.000	0.000	-5.217E-11	1.352E-11	0.000	765.9332	5.799E+09	-1.806E-12	7425000.	0.000
588.000	0.000	-3.495E-12	4.769E-12	0.000	765.9332	5.799E+09	-1.110E-12	7425000.	0.000
594.000	0.000	5.227E-12	0.000	0.000	765.9332	5.799E+09	0.000	7425000.	0.000
600.000	0.000	0.000	0.000	0.000	765.9332	5.799E+09	0.000	3712500.	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

Pile-head deflection = 1.0000000 inches
 Computed slope at pile head = -0.0164760 radians
 Maximum bending moment = 1178281. inch-lbs
 Maximum shear force = 34979. lbs
 Depth of maximum bending moment = 60.0000000 inches below pile head
 Depth of maximum shear force = 0.0000000 inches below pile head
 Number of iterations = 24
 Number of zero deflection points = 13

 Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.		Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 M = in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y =	0.2500	M = 0.000	154000.	0.25000000	464759.	18474.	-0.00516364
2	4	sy =	0.5000	M = 0.000	154000.	0.50000000	736801.	25365.	-0.00920138
3	4	y =	1.0000	M = 0.000	154000.	1.00000000	1178281.	34979.	-0.01647604

The analysis ended normally.

SUPPORT: ABUTMENT 1L

LOAD DIRECTION: LONGITUDE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE

Layer 1, Depth -2.00 to 0.10 ft = Stiff Clay without Free Water

Layer 2, Depth 0.10 to 3.00 ft = Stiff Clay without Free Water

Layer 3, Depth 3.00 to 8.00 ft = Stiff Clay without Free Water

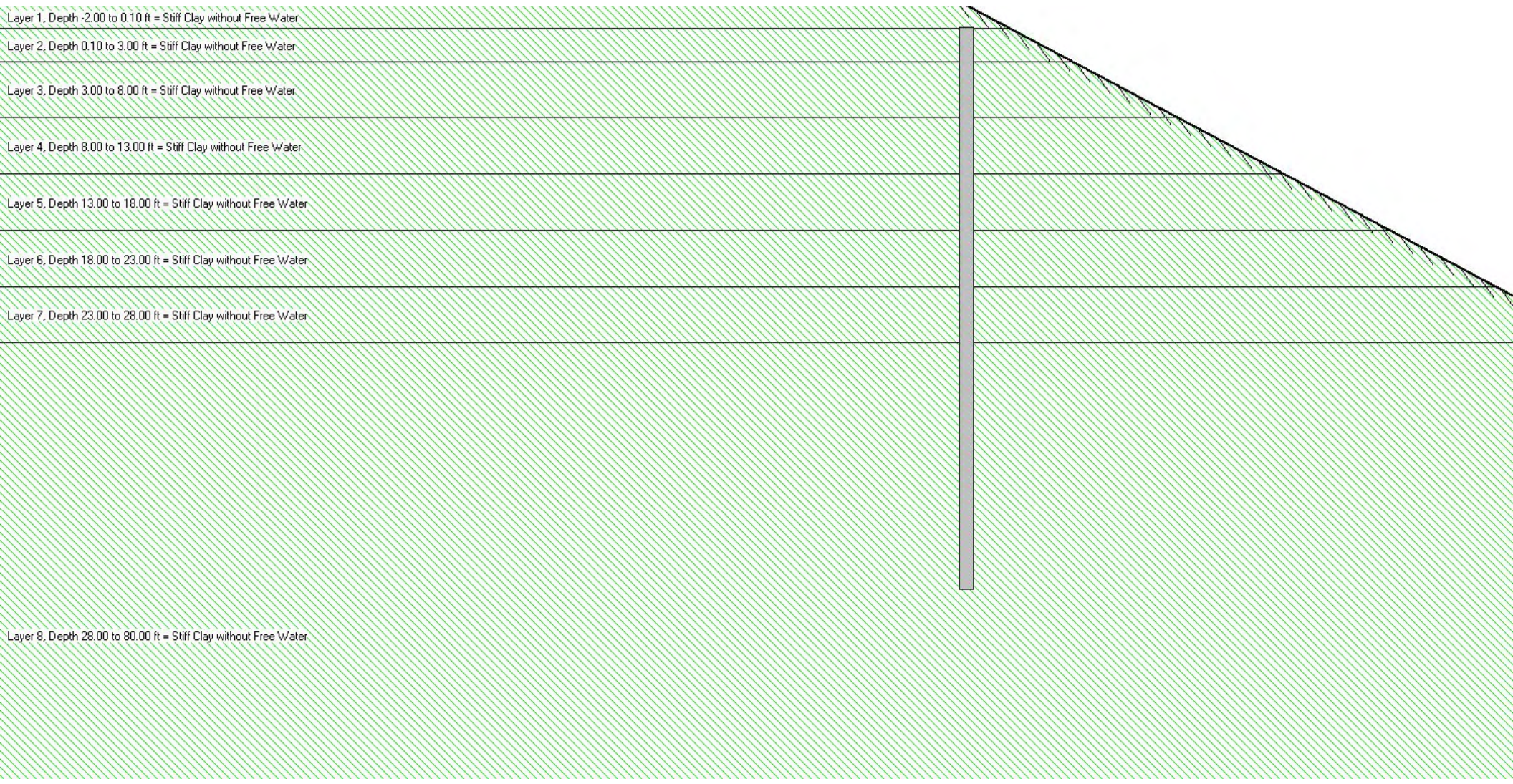
Layer 4, Depth 8.00 to 13.00 ft = Stiff Clay without Free Water

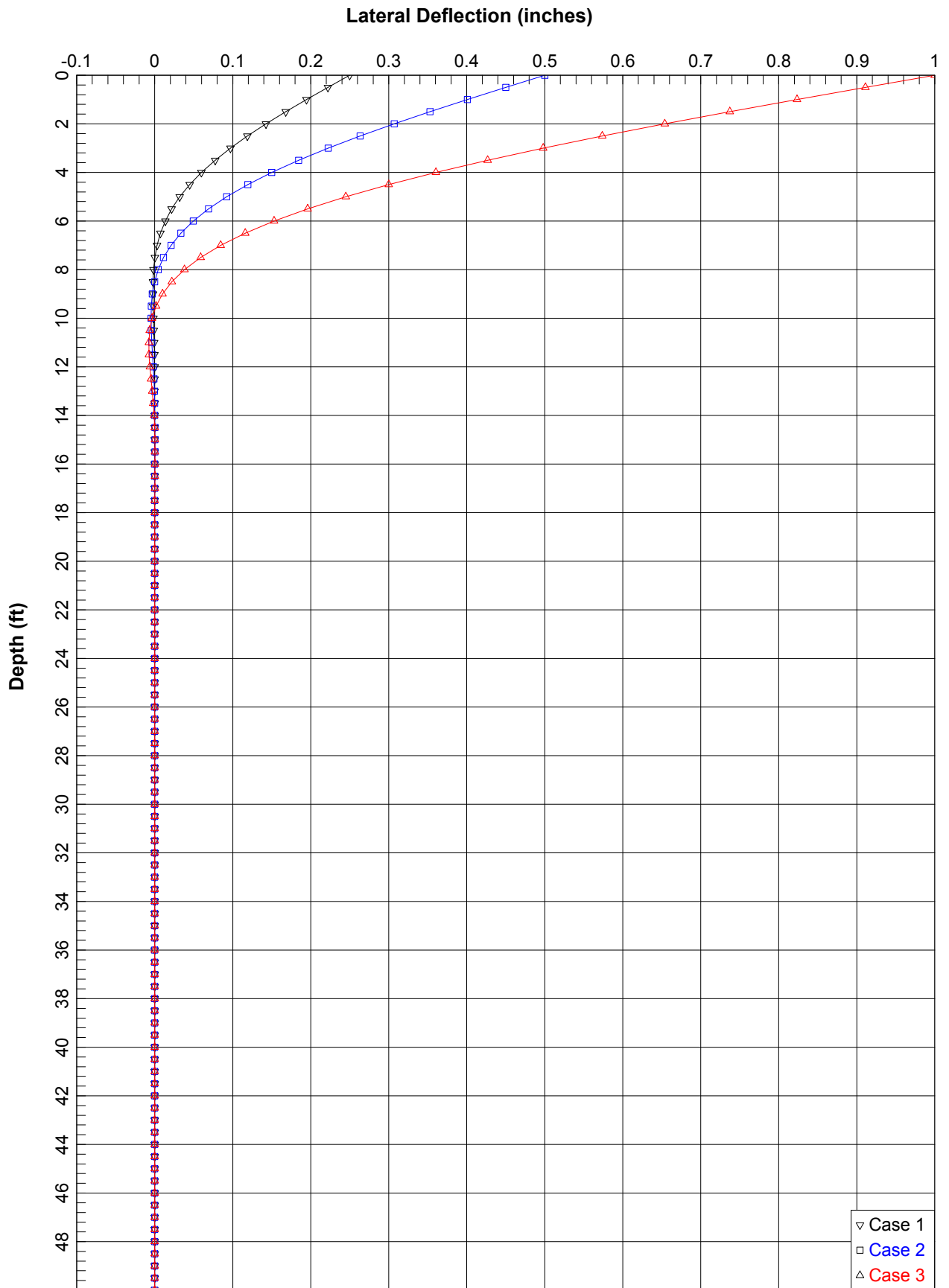
Layer 5, Depth 13.00 to 18.00 ft = Stiff Clay without Free Water

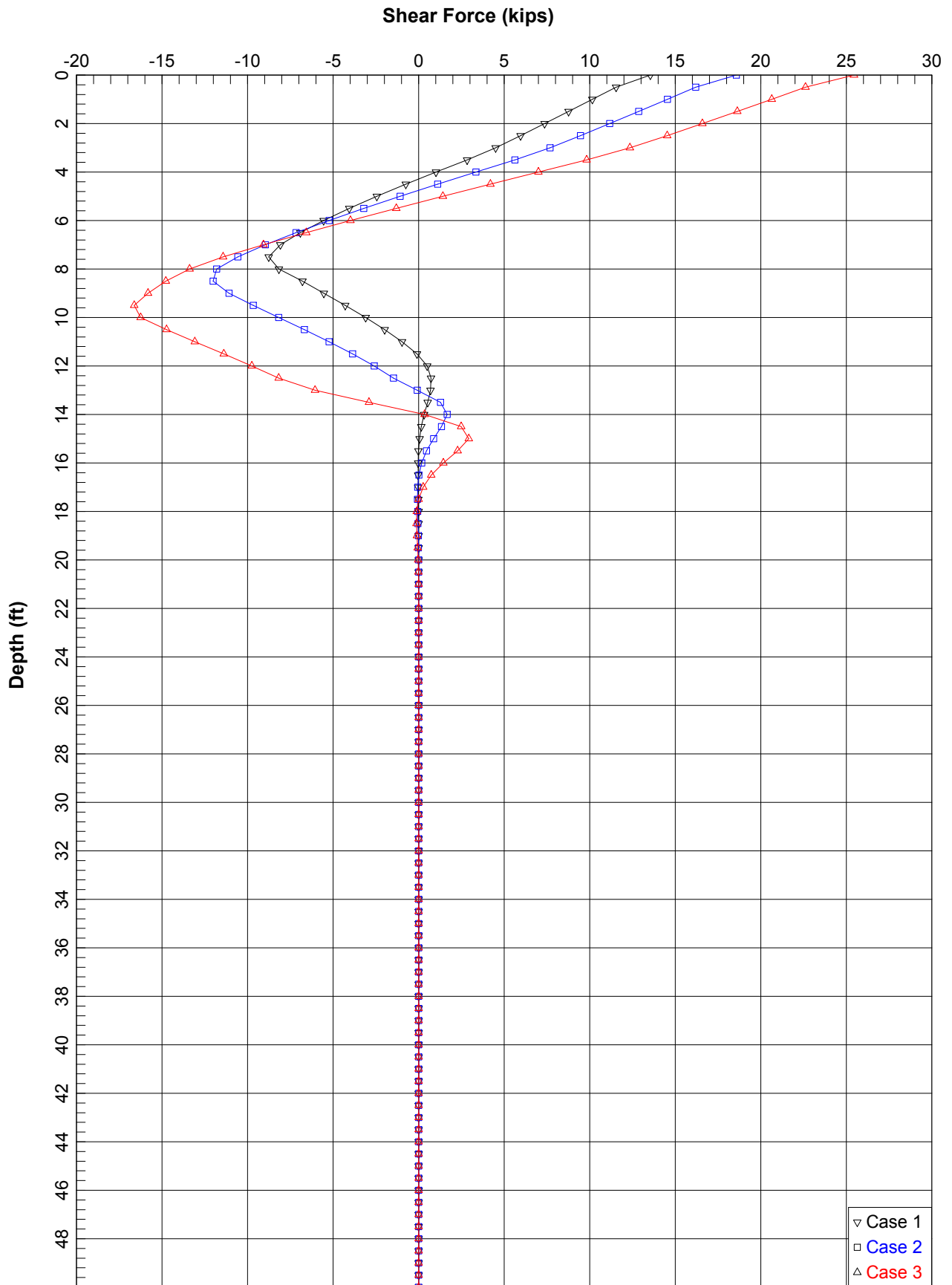
Layer 6, Depth 18.00 to 23.00 ft = Stiff Clay without Free Water

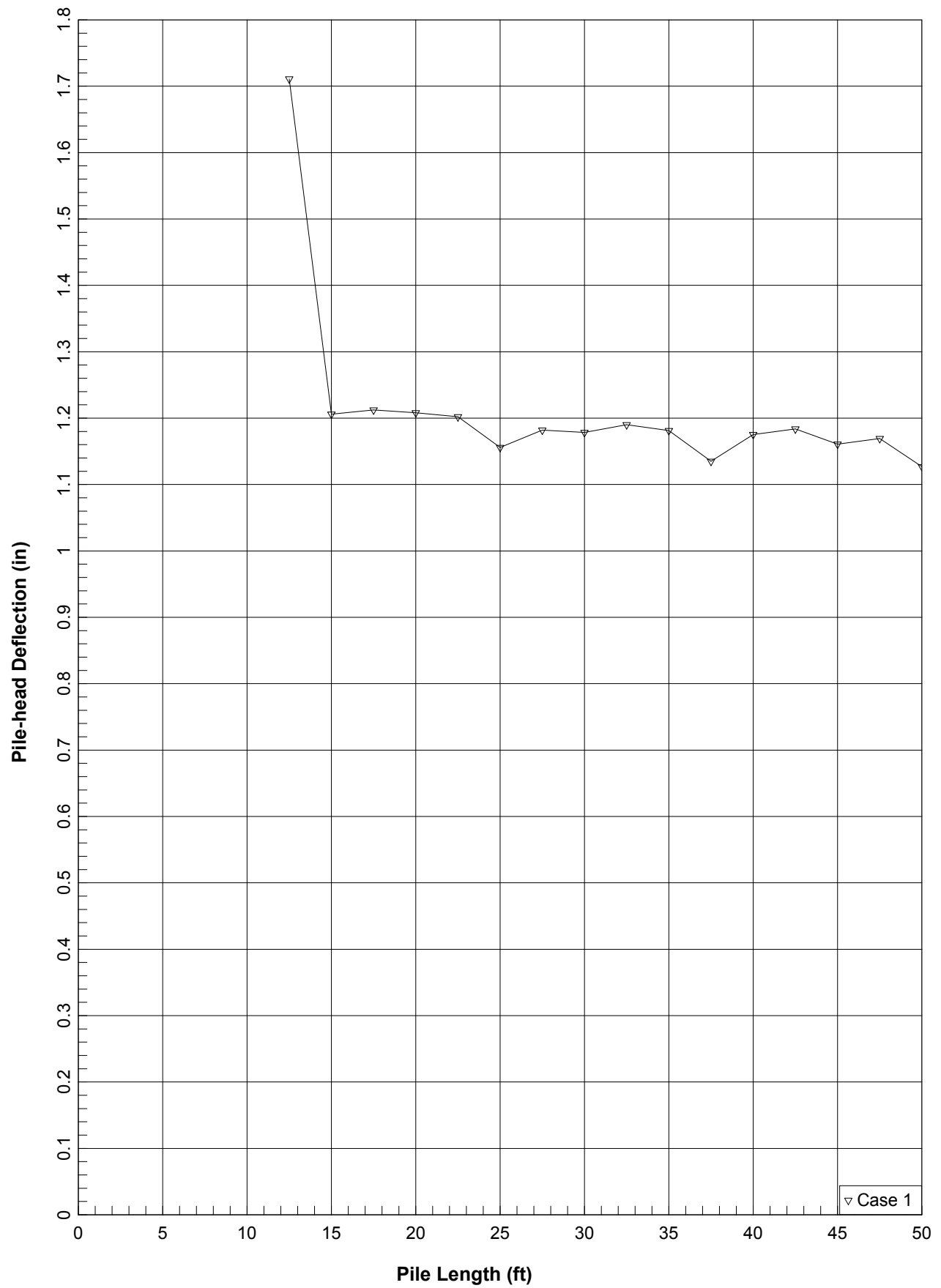
Layer 7, Depth 23.00 to 28.00 ft = Stiff Clay without Free Water

Layer 8, Depth 28.00 to 80.00 ft = Stiff Clay without Free Water









 Abut 1L_long_Critical Length

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 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

 Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 1\
 Name of input data file: Abut 1L_long_Critical Length.lp6d
 Name of output report file: Abut 1L_long_Critical Length.lp6o
 Name of plot output file: Abut 1L_long_Critical Length.lp6p
 Name of runtime message file: Abut 1L_long_Critical Length.lp6r

 Date and Time of Analysis

Date: September 13, 2014 Time: 10:47:49

 Problem Title

Project Name: Palo Comado OC Bridge Widen

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

 Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

 Pile Structural Properties and Geometry

Page 1

 Abut 1L_long_Critical Length

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

 Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.00000000 ft
 Top Width = 16.00000000 in
 Bottom Width = 16.00000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 365000. lbs/in²

 Ground Slope and Pile Batter Angles

Ground Slope Angle = 33.700 degrees
 = 0.588 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

 Soil and Rock Layering Information

The soil profile is modelled using 8 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer	=	-2.00000 ft
Distance from top of pile to bottom of layer	=	0.10000 ft
Effective unit weight at top of layer	=	120.00000 pcf
Effective unit weight at bottom of layer	=	120.00000 pcf
Undrained cohesion at top of layer	=	3500.00000 psi
Undrained cohesion at bottom of layer	=	3500.00000 psi
Epsilon-50 at top of layer	=	0.00700
Epsilon-50 at bottom of layer	=	0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer	=	0.10000 ft
Distance from top of pile to bottom of layer	=	3.00000 ft
Effective unit weight at top of layer	=	120.00000 pcf
Effective unit weight at bottom of layer	=	120.00000 pcf
Undrained cohesion at top of layer	=	1500.00000 psi
Undrained cohesion at bottom of layer	=	1500.00000 psi
Epsilon-50 at top of layer	=	0.00700
Epsilon-50 at bottom of layer	=	0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer	=	3.00000 ft
Distance from top of pile to bottom of layer	=	8.00000 ft
Effective unit weight at top of layer	=	120.00000 pcf
Effective unit weight at bottom of layer	=	120.00000 pcf
Undrained cohesion at top of layer	=	2500.00000 psi
Undrained cohesion at bottom of layer	=	2500.00000 psi

Page 2

Abut 1L_long_Critical Length
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water
 Distance from top of pile to top of layer = 8.00000 ft
 Distance from top of pile to bottom of layer = 13.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water
 Distance from top of pile to top of layer = 13.00000 ft
 Distance from top of pile to bottom of layer = 18.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 6 is stiff clay without free water
 Distance from top of pile to top of layer = 18.00000 ft
 Distance from top of pile to bottom of layer = 23.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 2500.00000 psi
 Undrained cohesion at bottom of layer = 2500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 7 is stiff clay without free water
 Distance from top of pile to top of layer = 23.00000 ft
 Distance from top of pile to bottom of layer = 28.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 8 is stiff clay without free water
 Distance from top of pile to top of layer = 28.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type	Rock Mass Depth	Effective Unit Wt.	Undrained In-situ Cohesion Test	Angle of In-situ Friction Test	Uniaxial Elastic Subgrade Mod.	RQD %
Num.	Epsilon on 50	(p-y Curve Criteria) Factor	Rock Mass Depth	pcf	psf	deg.	psi	or GSI
			ft	krm	Type	Property	psi	
1	0.00700	Stiff Clay w/o Free Water	-2.000	120.000	3500.000	--	--	--
	0.00700	--	0.10000	120.000	3500.000	--	--	--
2	0.00700	Stiff Clay w/o Free Water	0.10000	120.000	1500.000	--	--	--
	0.00700	--	3.000	120.000	1500.000	--	--	--
3	0.00700	Stiff Clay w/o Free Water	3.000	120.000	2500.000	--	--	--
	0.00700	--	8.000	120.000	2500.000	--	--	--

		Abut 1L_long_Critical Length			
4	0.00700	Stiff Clay w/o Free Water	8.000	120.000	1500.000
	0.00700	--	13.000	120.000	1500.000
5	0.00700	Stiff Clay w/o Free Water	13.000	125.000	4500.000
	0.00700	--	18.000	125.000	4500.000
6	0.00700	Stiff Clay w/o Free Water	18.000	125.000	2500.000
	0.00700	--	23.000	125.000	2500.000
7	0.00700	Stiff Clay w/o Free Water	23.000	125.000	3500.000
	0.00700	--	28.000	125.000	3500.000
8	0.00500	Stiff Clay w/o Free Water	28.000	125.000	4500.000
	0.00500	--	80.000	125.000	4500.000

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.9300	1.0000
2	50.000	0.9300	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	1	V = 25000. lbs	M = 0.0000 in-lbs	154000.	True

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head	=	25000.000 lbs
Applied moment at pile head	=	0.000 in-lbs
Axial thrust load on pile head	=	154000.000 lbs

Abut 1L_long_Critical Length

Abut 1L_long_Ave P

Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 1\
 Name of input data file: Abut 1L_long_Ave P.lpd
 Name of output report file: Abut 1L_long_Ave P.lpo
 Name of plot output file: Abut 1L_long_Ave P.lpp
 Name of runtime message file: Abut 1L_long_Ave P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 10:44:57

Problem Title

Project Name: Palo Comado OC Bridge Widen

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Abut 1L_long_Ave P

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.00000000 ft
 Top Width = 16.00000000 in
 Bottom Width = 16.00000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 28.000 degrees
 = 0.489 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 8 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 3.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 3.00000 ft
 Distance from top of pile to bottom of layer = 8.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2500.00000 psi
 Undrained cohesion at bottom of layer = 2500.00000 psi

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 8.00000 ft
 Distance from top of pile to bottom of layer = 13.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 13.00000 ft
 Distance from top of pile to bottom of layer = 18.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 6 is stiff clay without free water

Distance from top of pile to top of layer = 18.00000 ft
 Distance from top of pile to bottom of layer = 23.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 2500.00000 psi
 Undrained cohesion at bottom of layer = 2500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 7 is stiff clay without free water

Distance from top of pile to top of layer = 23.00000 ft
 Distance from top of pile to bottom of layer = 28.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 8 is stiff clay without free water

Distance from top of pile to top of layer = 28.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 125.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type	Rock Mass Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Uniaxial Elastic Modulus	ROD %
Num.	Epsilon 50	(p-y Curve Criteria)	ft	pcf	psf	deg.	psi	GSI
		Factor	psi		Type	Property	Mod. pci	
1	0.00700	Stiff Clay w/o Free Water	-2.000	120.000	3500.000	--	--	--
	0.00700	--	0.10000	120.000	3500.000	--	--	--
2	0.00700	Stiff Clay w/o Free Water	0.10000	120.000	1500.000	--	--	--
	0.00700	--	3.000	120.000	1500.000	--	--	--
3	0.00700	Stiff Clay w/o Free Water	3.000	120.000	2500.000	--	--	--
	0.00700	--	8.000	120.000	2500.000	--	--	--

		Abut 1L_long_Ave P						
4	0.00700	Stiff Clay w/o Free Water	8.000	120.000	1500.000	--	--	--
	0.00700	--	13.000	120.000	1500.000	--	--	--
5	0.00700	Stiff Clay w/o Free Water	13.000	125.000	4500.000	--	--	--
	0.00700	--	18.000	125.000	4500.000	--	--	--
6	0.00700	Stiff Clay w/o Free Water	18.000	125.000	2500.000	--	--	--
	0.00700	--	23.000	125.000	2500.000	--	--	--
7	0.00700	Stiff Clay w/o Free Water	23.000	125.000	3500.000	--	--	--
	0.00700	--	28.000	125.000	3500.000	--	--	--
8	0.00500	Stiff Clay w/o Free Water	28.000	125.000	4500.000	--	--	--
	0.00500	--	80.000	125.000	125.000	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.9300	1.0000
2	50.000	0.9300	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4 y =	0.25000 in	M = 0.0000 in-lbs	154000.	False
2	4 y =	0.50000 in	M = 0.0000 in-lbs	154000.	False
3	4 y =	1.00000 in	M = 0.0000 in-lbs	154000.	False

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Page 4

				Abut	1L_Long_Ave P				
516.000	0.000	-2.455E-08	7.196E-09	0.000	765.9332	5.799E+09	-8.122E-10	5646229	0.000
522.000	0.000	4.051E-09	3.178E-09	0.000	765.9332	5.799E+09	-5.270E-10	5572874	0.000
528.000	0.000	1.368E-08	7.810E-10	0.000	765.9332	5.799E+09	-2.721E-10	5499519	0.000
534.000	0.000	1.349E-08	-3.369E-10	0.000	765.9332	5.799E+09	-1.005E-10	5426164	0.000
540.000	0.000	9.678E-09	-6.634E-10	0.000	765.9332	5.799E+09	-8.286E-12	5352809	0.000
546.000	0.000	5.554E-09	-6.024E-10	0.000	765.9332	5.799E+09	2.862E-11	5279455	0.000
552.000	0.000	2.456E-09	-4.129E-10	0.000	765.9332	5.799E+09	3.458E-11	5206100	0.000
558.000	0.000	5.999E-10	-2.272E-10	0.000	765.9332	5.799E+09	2.732E-11	5132745	0.000
564.000	0.000	-2.732E-10	-9.391E-11	0.000	765.9332	5.799E+09	1.711E-11	5059390	0.000
570.000	0.000	-5.303E-10	-1.682E-11	0.000	765.9332	5.799E+09	8.591E-12	4986035	0.000
576.000	0.000	-4.776E-10	1.800E-11	0.000	765.9332	5.799E+09	3.016E-12	4912680	0.000
582.000	0.000	-3.159E-10	2.703E-11	0.000	765.9332	5.799E+09	0.000	4839325	0.000
588.000	0.000	-1.541E-10	2.288E-11	0.000	765.9332	5.799E+09	-1.379E-12	4765971	0.000
594.000	0.000	-4.177E-11	1.286E-11	0.000	765.9332	5.799E+09	-1.961E-12	4692616	0.000
600.000	0.000	0.000	0.000	0.000	765.9332	5.799E+09	-2.325E-12	2309630	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

Pile-head deflection = 1.0000000 inches
 Computed slope at pile head = -0.0148086 radians
 Maximum bending moment = 961341. inch-lbs
 Maximum shear force = 25448. lbs
 Depth of maximum bending moment = 66.0000000 inches below pile head
 Depth of maximum shear force = 0.0000000 inches below pile head
 Number of iterations = 24
 Number of zero deflection points = 12

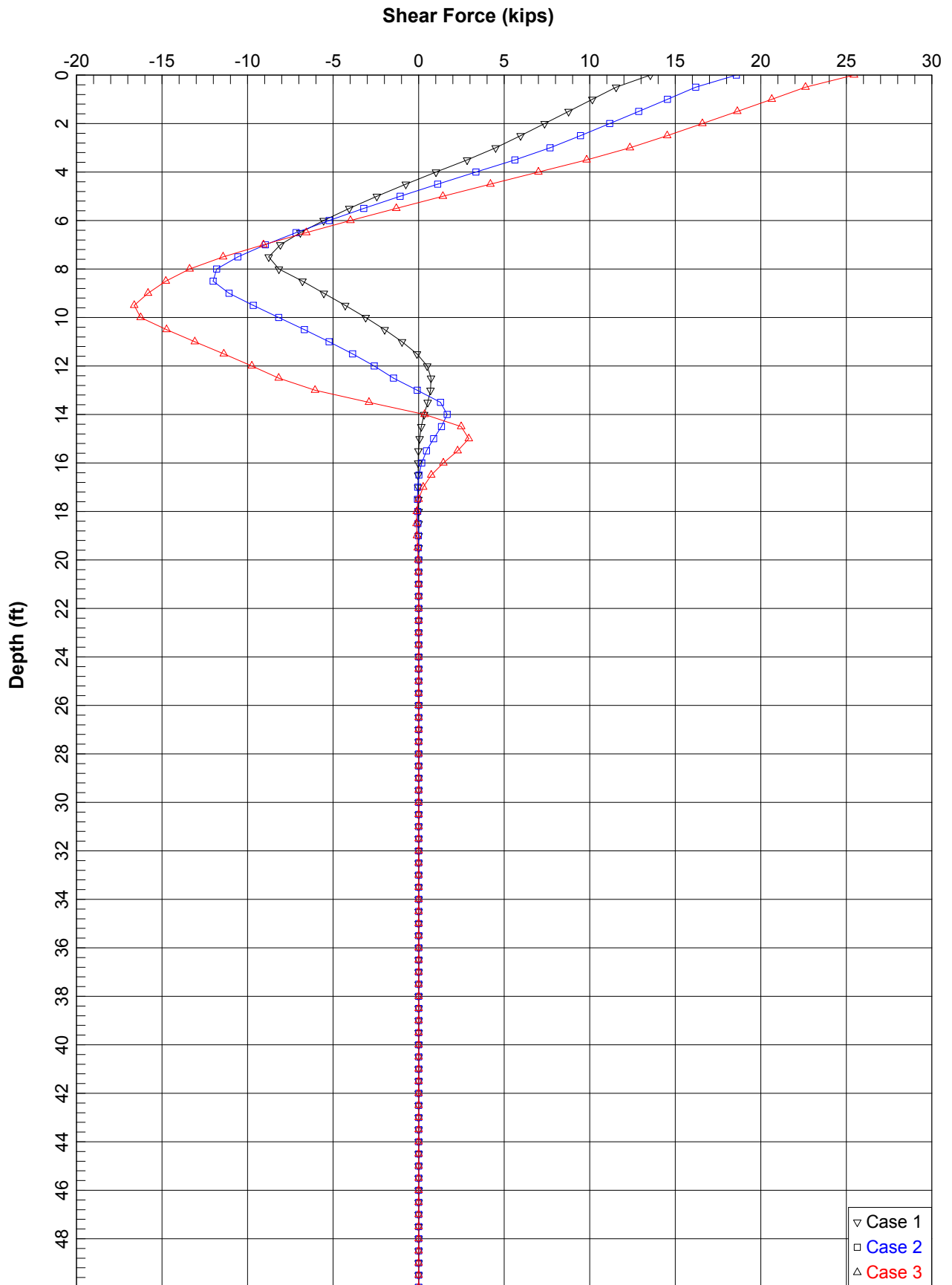
 Summary of Pile Response(s)

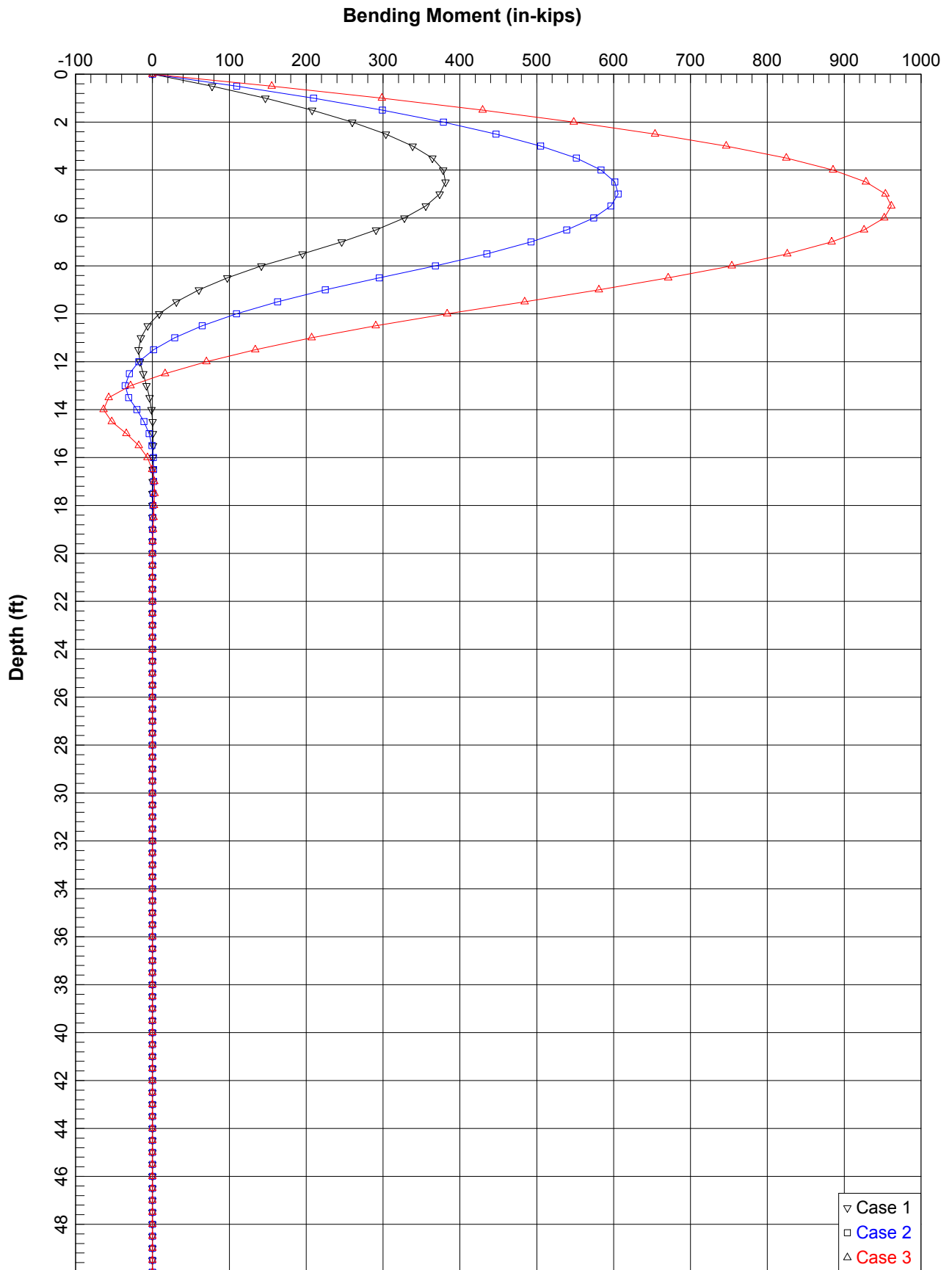
Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 M = in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	154000.	0.25000000	381279.	13537.	-0.00466505
2	4	y = 0.5000	M = 0.000	154000.	0.50000000	605801.	18573.	-0.00831653
3	4	y = 1.0000	M = 0.000	154000.	1.00000000	961341.	25448.	-0.01480856

The analysis ended normally.





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Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 1\
 Name of input data file: Abut 1L_long_Ave P.lpd
 Name of output report file: Abut 1L_long_Ave P.lpo
 Name of plot output file: Abut 1L_long_Ave P.lpp
 Name of runtime message file: Abut 1L_long_Ave P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 10:44:57

Problem Title

Project Name: Palo Comado OC Bridge Widen

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Abut 1L_long_Ave P

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.00000000 ft
 Top Width = 16.00000000 in
 Bottom Width = 16.00000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 365000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 28.000 degrees
 = 0.489 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 8 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 3.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 3.00000 ft
 Distance from top of pile to bottom of layer = 8.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2500.00000 psi
 Undrained cohesion at bottom of layer = 2500.00000 psi

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 8.00000 ft
 Distance from top of pile to bottom of layer = 13.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 13.00000 ft
 Distance from top of pile to bottom of layer = 18.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 6 is stiff clay without free water

Distance from top of pile to top of layer = 18.00000 ft
 Distance from top of pile to bottom of layer = 23.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 2500.00000 psi
 Undrained cohesion at bottom of layer = 2500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 7 is stiff clay without free water

Distance from top of pile to top of layer = 23.00000 ft
 Distance from top of pile to bottom of layer = 28.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 8 is stiff clay without free water

Distance from top of pile to top of layer = 28.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 125.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type	Rock Mass Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Elastic Mod.	Uniaxial Subgrade	ROD %
1	0.00700	Stiff Clay w/o Free Water	-2.000	120.000	3500.000	--	--	--	--
	0.00700	--	0.10000	120.000	3500.000	--	--	--	--
2	0.00700	Stiff Clay w/o Free Water	0.10000	120.000	1500.000	--	--	--	--
	0.00700	--	3.000	120.000	1500.000	--	--	--	--
3	0.00700	Stiff Clay w/o Free Water	3.000	120.000	2500.000	--	--	--	--
	0.00700	--	8.000	120.000	2500.000	--	--	--	--

		Abut 1L_long_Ave P					
4	0.00700	Stiff Clay w/o Free Water	8.000	120.000	1500.000	--	--
	0.00700	--	13.000	120.000	1500.000	--	--
5	0.00700	Stiff Clay w/o Free Water	13.000	125.000	4500.000	--	--
	0.00700	--	18.000	125.000	4500.000	--	--
6	0.00700	Stiff Clay w/o Free Water	18.000	125.000	2500.000	--	--
	0.00700	--	23.000	125.000	2500.000	--	--
7	0.00700	Stiff Clay w/o Free Water	23.000	125.000	3500.000	--	--
	0.00700	--	28.000	125.000	3500.000	--	--
8	0.00500	Stiff Clay w/o Free Water	28.000	125.000	4500.000	--	--
	0.00500	--	80.000	125.000	125.000	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.9300	1.0000
2	50.000	0.9300	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4 y =	0.25000 in	M = 0.0000 in-lbs	154000.	False
2	4 y =	0.50000 in	M = 0.0000 in-lbs	154000.	False
3	4 y =	1.00000 in	M = 0.0000 in-lbs	154000.	False

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Page 4

				Abut 1L_Long_Ave P					
516.000	0.000	-2.455E-08	7.196E-09	0.000	765.9332	5.799E+09	-8.122E-10	5646229	0.000
522.000	0.000	4.051E-09	3.178E-09	0.000	765.9332	5.799E+09	-5.270E-10	5572874	0.000
528.000	0.000	1.368E-08	7.810E-10	0.000	765.9332	5.799E+09	-2.721E-10	5499519	0.000
534.000	0.000	1.349E-08	-3.369E-10	0.000	765.9332	5.799E+09	-1.005E-10	5426164	0.000
540.000	0.000	9.678E-09	-6.634E-10	0.000	765.9332	5.799E+09	-8.286E-12	5352809	0.000
546.000	0.000	5.554E-09	-6.024E-10	0.000	765.9332	5.799E+09	2.862E-11	5279455	0.000
552.000	0.000	2.456E-09	-4.129E-10	0.000	765.9332	5.799E+09	3.458E-11	5206100	0.000
558.000	0.000	5.999E-10	-2.272E-10	0.000	765.9332	5.799E+09	2.732E-11	5132745	0.000
564.000	0.000	-2.732E-10	-9.391E-11	0.000	765.9332	5.799E+09	1.711E-11	5059390	0.000
570.000	0.000	-5.303E-10	-1.682E-11	0.000	765.9332	5.799E+09	8.591E-12	4986035	0.000
576.000	0.000	-4.776E-10	1.800E-11	0.000	765.9332	5.799E+09	3.016E-12	4912680	0.000
582.000	0.000	-3.159E-10	2.703E-11	0.000	765.9332	5.799E+09	0.000	4839325	0.000
588.000	0.000	-1.541E-10	2.288E-11	0.000	765.9332	5.799E+09	-1.379E-12	4765971	0.000
594.000	0.000	-4.177E-11	1.286E-11	0.000	765.9332	5.799E+09	-1.961E-12	4692616	0.000
600.000	0.000	0.000	0.000	0.000	765.9332	5.799E+09	-2.325E-12	2309630	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

Pile-head deflection = 1.0000000 inches
 Computed slope at pile head = -0.0148086 radians
 Maximum bending moment = 961341. inch-lbs
 Maximum shear force = 25448. lbs
 Depth of maximum bending moment = 66.0000000 inches below pile head
 Depth of maximum shear force = 0.0000000 inches below pile head
 Number of iterations = 24
 Number of zero deflection points = 12

 Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

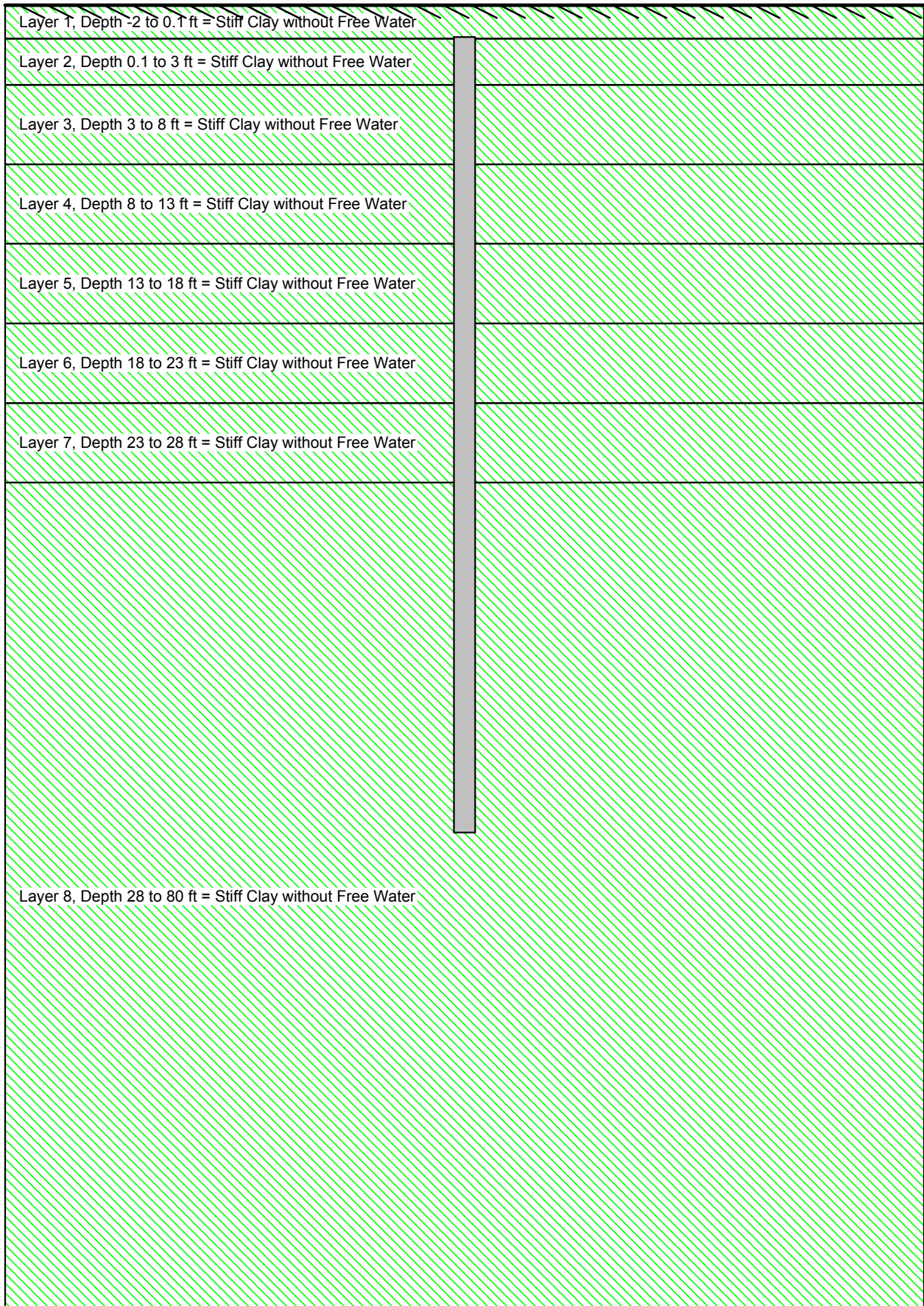
Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 M = in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	154000.	0.25000000	381279.	13537.	-0.00466505
2	4	y = 0.5000	M = 0.000	154000.	0.50000000	605801.	18573.	-0.00831653
3	4	y = 1.0000	M = 0.000	154000.	1.00000000	961341.	25448.	-0.01480856

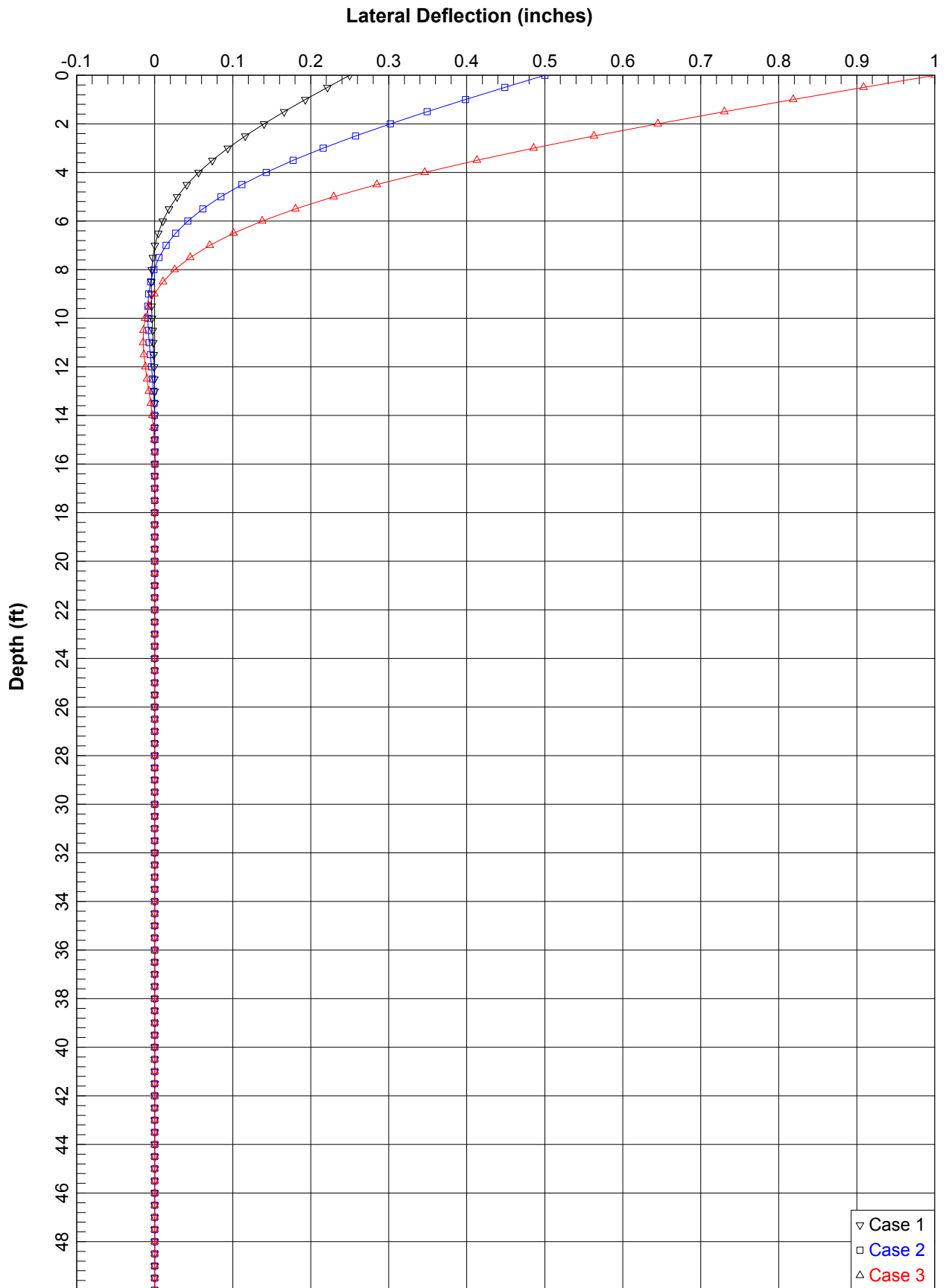
The analysis ended normally.

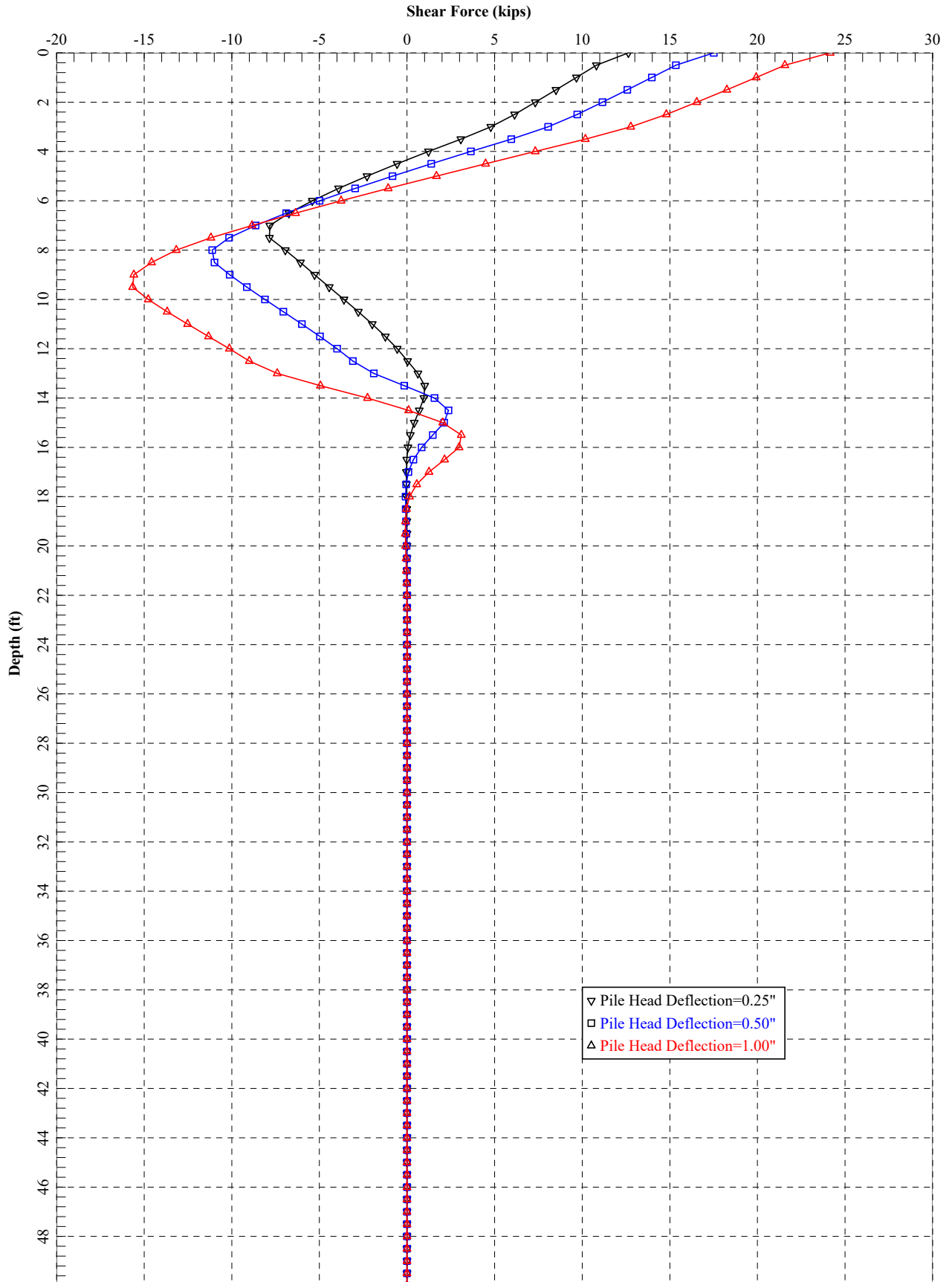
SUPPORT: ABUTMENT 1L

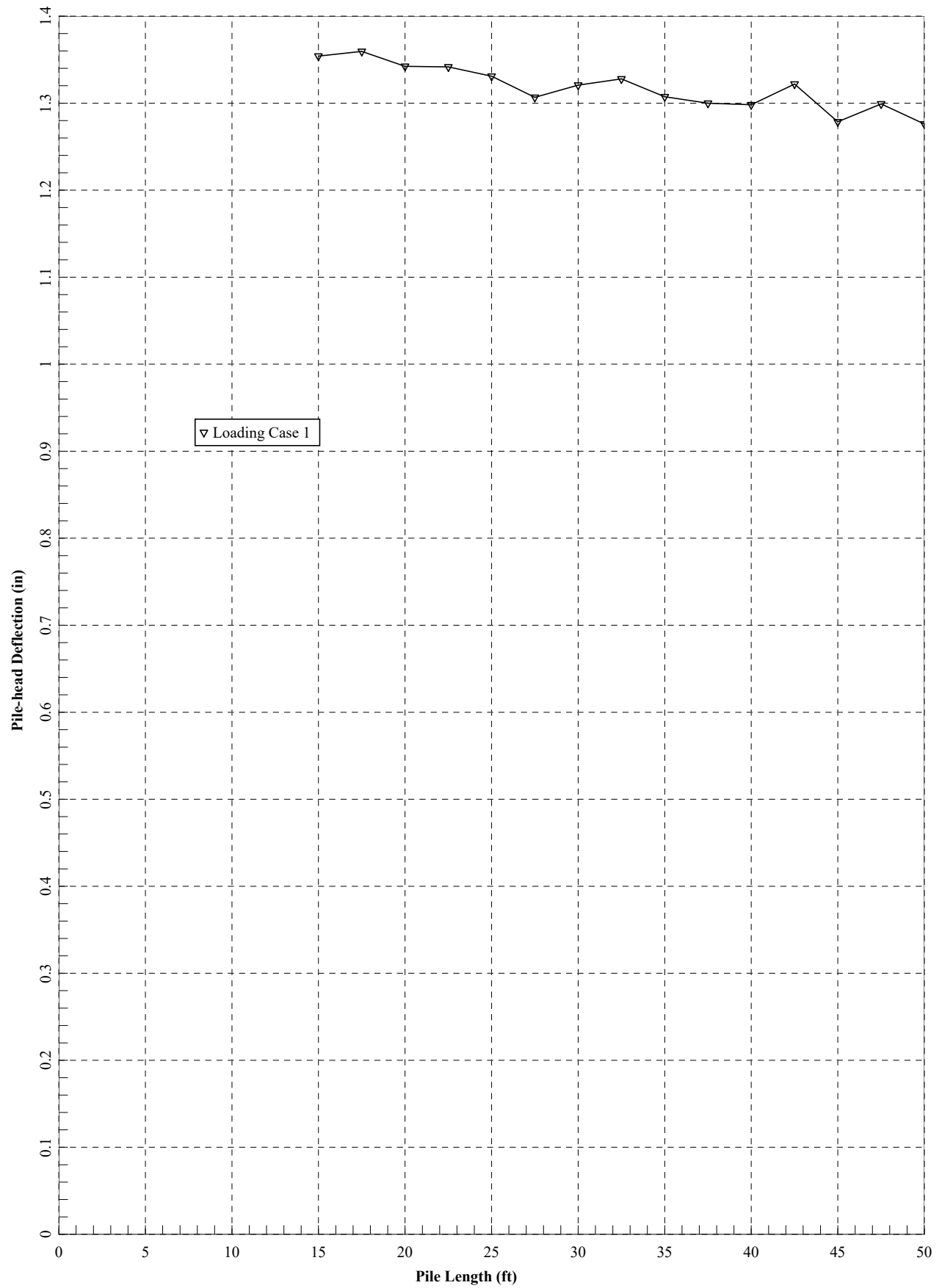
LOAD DIRECTION: TRANSVERSE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE









Abut 1L_transv_Critical Length.lp9o

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Analysis of Individual Piles and Drilled Shafts
Subjected to Lateral Loading Using the p-y Method
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Files Used for Analysis

Path to file locations:
\\Projects_LA\L1100\LA1143 PTG - 101 & Palo Comado Cyn\Irvine Foundation Report\Calculations\Lateral Pile Capacity\Updated 08-24-17\

Name of input data file:
Abut 1L_transv_Critical Length.lp9d

Name of output report file:
Abut 1L_transv_Critical Length.lp9o

Name of plot output file:
Abut 1L_transv_Critical Length.lp9p

Name of runtime message file:
Abut 1L_transv_Critical Length.lp9r

Date and Time of Analysis

Date: August 24, 2017 Time: 10:43:53

Problem Title

Project Name: Palo Comado OC Bridge Widen

Job Number: LA-1143

Client: Parson Transportation

Abut 1L_transv_Critical Length.lp9o

Engineer: Mario DiNicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options and Settings

Computational Options:

- Use unfactored loads in computations (conventional analysis)
- Engineering Units Used for Data Input and Computations:
 - US Customary System Units (pounds, feet, inches)

Analysis Control Options:

- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in
- Number of pile increments = 100

Loading Type and Number of Cycles of Loading:

- Static loading specified

- Analysis uses p-y modification factors for p-y curves
- No distributed lateral loads are entered
- Loading by lateral soil movements acting on pile not selected
- Input of shear resistance at the pile tip not selected
- Computation of pile-head foundation stiffness matrix not selected
- Push-over analysis of pile not selected
- Buckling analysis of pile not selected

Output Options:

- Output files use decimal points to denote decimal symbols.
- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1
- No p-y curves to be computed and reported for user-specified depths
- Print using wide report formats

Pile Structural Properties and Geometry

Number of pile sections defined = 1
Total length of pile = 50.000 ft
Depth of ground surface below top of pile = -2.0000 ft

Pile diameters used for p-y curve computations are defined using 2 points.

p-y curves are computed using pile diameter values interpolated with depth over the length of the pile. A summary of values of pile diameter vs. depth follows.

Point No.	Depth Below Pile Head feet	Pile Diameter inches
1	0.000	16.0000
2	50.000	16.0000

Input Structural Properties for Pile Sections:

Pile Section No. 1:

Section 1 is an elastic pile
 Cross-sectional Shape = Circular Pile
 Length of section = 50.000000 ft
 Width of top of section = 16.000000 in
 Width of bottom of section = 16.000000 in
 Top Area = 201.061930 sq. in
 Bottom Area = 201.061930 sq. in
 Moment of Inertia at Top = 1608. in^4
 Moment of Inertia at Bottom = 1608. in^4
 Elastic Modulus = 3605000. psi

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 8 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.000000 ft
 Distance from top of pile to bottom of layer = 0.100000 ft
 Effective unit weight at top of layer = 120.000000 pcf
 Effective unit weight at bottom of layer = 120.000000 pcf
 Undrained cohesion at top of layer = 3500. psf
 Undrained cohesion at bottom of layer = 3500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.100000 ft
 Distance from top of pile to bottom of layer = 3.000000 ft
 Effective unit weight at top of layer = 120.000000 pcf
 Effective unit weight at bottom of layer = 120.000000 pcf
 Undrained cohesion at top of layer = 1500. psf
 Undrained cohesion at bottom of layer = 1500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 3.000000 ft
 Distance from top of pile to bottom of layer = 8.000000 ft
 Effective unit weight at top of layer = 120.000000 pcf
 Effective unit weight at bottom of layer = 120.000000 pcf
 Undrained cohesion at top of layer = 2500. psf
 Undrained cohesion at bottom of layer = 2500. psf
 Epsilon-50 at top of layer = 0.007000

Epsilon-50 at bottom of layer = 0.007000

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 8.000000 ft
 Distance from top of pile to bottom of layer = 13.000000 ft
 Effective unit weight at top of layer = 120.000000 pcf
 Effective unit weight at bottom of layer = 120.000000 pcf
 Undrained cohesion at top of layer = 1500. psf
 Undrained cohesion at bottom of layer = 1500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 13.000000 ft
 Distance from top of pile to bottom of layer = 18.000000 ft
 Effective unit weight at top of layer = 125.000000 pcf
 Effective unit weight at bottom of layer = 125.000000 pcf
 Undrained cohesion at top of layer = 4500. psf
 Undrained cohesion at bottom of layer = 4500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 6 is stiff clay without free water

Distance from top of pile to top of layer = 18.000000 ft
 Distance from top of pile to bottom of layer = 23.000000 ft
 Effective unit weight at top of layer = 125.000000 pcf
 Effective unit weight at bottom of layer = 125.000000 pcf
 Undrained cohesion at top of layer = 2500. psf
 Undrained cohesion at bottom of layer = 2500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 7 is stiff clay without free water

Distance from top of pile to top of layer = 23.000000 ft
 Distance from top of pile to bottom of layer = 28.000000 ft
 Effective unit weight at top of layer = 125.000000 pcf
 Effective unit weight at bottom of layer = 125.000000 pcf
 Undrained cohesion at top of layer = 3500. psf
 Undrained cohesion at bottom of layer = 3500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 8 is stiff clay without free water

Distance from top of pile to top of layer = 28.000000 ft
 Distance from top of pile to bottom of layer = 80.000000 ft
 Effective unit weight at top of layer = 125.000000 pcf
 Effective unit weight at bottom of layer = 125.000000 pcf
 Undrained cohesion at top of layer = 4500. psf
 Undrained cohesion at bottom of layer = 4500. psf
 Epsilon-50 at top of layer = 0.005000
 Epsilon-50 at bottom of layer = 0.005000

(Depth of the lowest soil layer extends 30.000 ft below the pile tip)

Abut 1L_transv_Critical Length.lp9o
Summary of Input Soil Properties

Layer Layer Num.	Soil Type Name (p-y Curve Type)	Layer Depth ft	Effective Unit Wt. pcf	Undrained Cohesion psf	E50 or krm
1	Stiff Clay	-2.0000	120.0000	3500.	0.00700
	w/o Free Water	0.10000	120.0000	3500.	0.00700
2	Stiff Clay	0.10000	120.0000	1500.	0.00700
	w/o Free Water	3.00000	120.0000	1500.	0.00700
3	Stiff Clay	3.00000	120.0000	2500.	0.00700
	w/o Free Water	8.00000	120.0000	2500.	0.00700
4	Stiff Clay	8.00000	120.0000	1500.	0.00700
	w/o Free Water	13.00000	120.0000	1500.	0.00700
5	Stiff Clay	13.00000	125.0000	4500.	0.00700
	w/o Free Water	18.00000	125.0000	4500.	0.00700
6	Stiff Clay	18.00000	125.0000	2500.	0.00700
	w/o Free Water	23.00000	125.0000	2500.	0.00700
7	Stiff Clay	23.00000	125.0000	3500.	0.00700
	w/o Free Water	28.00000	125.0000	3500.	0.00500
8	Stiff Clay	28.00000	125.0000	4500.	0.00500
	w/o Free Water	80.00000	125.0000	4500.	0.00500

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.5800	1.0000
2	50.000	0.5800	1.0000

Static Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	1	V = 27000. lbs	M = 0.0000 in-lbs	154000.	Yes

V = shear force applied normal to pile axis
M = bending moment applied to pile head
y = lateral deflection normal to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Values of top y vs. pile lengths can be computed only for load types with specified shear loading (Load Types 1, 2, and 3).
Thrust force is assumed to be acting axially for all pile batter angles.

Abut 1L_transv_Critical Length.lp9o

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Layering Correction Equivalent Depths of Soil & Rock Layers

Layer No.	Top of Layer Below Pile Head ft	Equivalent Top Depth Below Grnd Surf ft	Same Layer Type As Layer Above	Layer is Rock or is Below Rock Layer	F0 Integral for Layer lbs	F1 Integral for Layer lbs
1	-2.0000	0.00	N.A.	No	0.00	1790.
2	0.1000	2.1000	Yes	No	1790.	25921.
3	3.0000	5.0000	Yes	No	27711.	101146.
4	8.0000	10.0000	Yes	No	128856.	84678.
5	13.0000	15.0000	Yes	No	213535.	269497.
6	18.0000	20.0000	Yes	No	483031.	150300.
7	23.0000	25.0000	Yes	No	633331.	210000.
8	28.0000	30.0000	Yes	No	843331.	N.A.

Notes: The F0 integral of Layer n+1 equals the sum of the F0 and F1 integrals for Layer n. Layering correction equivalent depths are computed only for soil types with both shallow-depth and deep-depth expressions for peak lateral load transfer. These soil types are soft and stiff clays, non-liquefied sands, and cemented c-phi soil.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head = 27000.0 lbs
Applied moment at pile head = 0.0 in-lbs
Axial thrust load on pile head = 154000.0 lbs

Depth X feet	Deflect. y inches	Bending Moment in-lb	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness in-lb*2	Soil Res. p lb/inch	Soil Spr. Es*h lb/inch	Distrib. Lat. Load lb/inch
0.00	1.2760	7.15E-08	27000.	-0.01806	765.9332	5.80E+09	-629.2200	1479.	0.00
0.5000	1.1676	167365.	24255.	-0.01798	1598.	5.80E+09	-285.7758	1468.	0.00
1.0000	1.0603	324283.	22515.	-0.01772	2379.	5.80E+09	-294.3075	1665.	0.00
1.5000	0.9550	470295.	20727.	-0.01731	3105.	5.80E+09	-301.6521	1895.	0.00
2.0000	0.8526	604998.	18899.	-0.01676	3775.	5.80E+09	-307.7428	2166.	0.00
2.5000	0.7539	728044.	17038.	-0.01607	4387.	5.80E+09	-312.5109	2487.	0.00
3.0000	0.6598	839143.	14861.	-0.01526	4939.	5.80E+09	-413.1967	3758.	0.00
3.5000	0.5708	934565.	12883.	-0.01434	5414.	5.80E+09	-512.7193	5389.	0.00
4.0000	0.4877	1010636.	9007.	-0.01333	5792.	5.80E+09	-512.5120	6305.	0.00

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20.00000	1.34232153	1163216.	27000.
17.50000	1.35947377	1170485.	27000.
15.00000	1.35411979	1170411.	27000.

 Summary of Pile-head Responses for Conventional Analyses

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, V, lbs, and Load 2 = Moment, M, in-lbs
 Load Type 2: Load 1 = Shear, V, lbs, and Load 2 = Slope, S, radians
 Load Type 3: Load 1 = Shear, V, lbs, and Load 2 = Rot. Stiffness, R, in-lbs/rad.
 Load Type 4: Load 1 = Top Deflection, y, inches, and Load 2 = Moment, M, in-lbs
 Load Type 5: Load 1 = Top Deflection, y, inches, and Load 2 = Slope, S, radians

Case No.	Load Type	Pile-head Load 1	Load Type	Pile-head Load 2	Axial Loading lbs	Pile-head Deflection inches	Pile-head Rotation radians	Max Shear in Pile lbs	Max Moment in Pile in-lbs
1	V, lb	27000.	M, in-lb	0.00	154000.	1.2760	-0.01806	27000.	1122642.

Maximum pile-head deflection = 1.2760276469 inches
 Maximum pile-head rotation = -0.0180640519 radians = -1.034994 deg.

The analysis ended normally.

Abut 1L_transv_Ave P.lp9o

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Analysis of Individual Piles and Drilled Shafts
Subjected to Lateral Loading Using the p-y Method
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Files Used for Analysis

Path to file locations:
\\Projects_LA\L1100\LA1143 PTG - 101 & Palo Comado Cyn\Irvine Foundation Report\Calculations\Lateral Pile
Capacity\Updated 08-24-17\

Name of input data file:
Abut 1L_transv_Ave P.lp9d

Name of output report file:
Abut 1L_transv_Ave P.lp9o

Name of plot output file:
Abut 1L_transv_Ave P.lp9p

Name of runtime message file:
Abut 1L_transv_Ave P.lp9r

Date and Time of Analysis

Date: August 24, 2017 Time: 10:14:14

Problem Title

Project Name: Palo Comado OC Bridge Widen

Job Number: LA-1143

Client: Parson Transportation

Abut 1L_transv_Ave P.lp9o

Engineer: Mario DiNicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options and Settings

Computational Options:

- Use unfactored loads in computations (conventional analysis)
- Engineering Units Used for Data Input and Computations:
 - US Customary System Units (pounds, feet, inches)

Analysis Control Options:

- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in
- Number of pile increments = 100

Loading Type and Number of Cycles of Loading:

- Static loading specified

- Analysis uses p-y modification factors for p-y curves
- No distributed lateral loads are entered
- Loading by lateral soil movements acting on pile not selected
- Input of shear resistance at the pile tip not selected
- Computation of pile-head foundation stiffness matrix not selected
- Push-over analysis of pile not selected
- Buckling analysis of pile not selected

Output Options:

- Output files use decimal points to denote decimal symbols.
- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1
- No p-y curves to be computed and reported for user-specified depths
- Print using wide report formats

Pile Structural Properties and Geometry

Number of pile sections defined = 1
Total length of pile = 50.000 ft
Depth of ground surface below top of pile = -2.0000 ft

Pile diameters used for p-y curve computations are defined using 2 points.

p-y curves are computed using pile diameter values interpolated with depth over the length of the pile. A summary of values of pile diameter vs. depth follows.

Point No.	Depth Below Pile Head feet	Pile Diameter inches
1	0.000	16.0000
2	50.000	16.0000

Input Structural Properties for Pile Sections:

Pile Section No. 1:

Section 1 is an elastic pile
 Cross-sectional Shape = Circular Pile
 Length of section = 50.000000 ft
 Width of top of section = 16.000000 in
 Width of bottom of section = 16.000000 in
 Top Area = 201.061930 sq. in
 Bottom Area = 201.061930 sq. in
 Moment of Inertia at Top = 1608. in^4
 Moment of Inertia at Bottom = 1608. in^4
 Elastic Modulus = 3605000. psi

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 8 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.000000 ft
 Distance from top of pile to bottom of layer = 0.100000 ft
 Effective unit weight at top of layer = 120.000000 pcf
 Effective unit weight at bottom of layer = 120.000000 pcf
 Undrained cohesion at top of layer = 3500. psf
 Undrained cohesion at bottom of layer = 3500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.100000 ft
 Distance from top of pile to bottom of layer = 3.000000 ft
 Effective unit weight at top of layer = 120.000000 pcf
 Effective unit weight at bottom of layer = 120.000000 pcf
 Undrained cohesion at top of layer = 1500. psf
 Undrained cohesion at bottom of layer = 1500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 3.000000 ft
 Distance from top of pile to bottom of layer = 8.000000 ft
 Effective unit weight at top of layer = 120.000000 pcf
 Effective unit weight at bottom of layer = 120.000000 pcf
 Undrained cohesion at top of layer = 2500. psf
 Undrained cohesion at bottom of layer = 2500. psf
 Epsilon-50 at top of layer = 0.007000

Epsilon-50 at bottom of layer = 0.007000

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 8.000000 ft
 Distance from top of pile to bottom of layer = 13.000000 ft
 Effective unit weight at top of layer = 120.000000 pcf
 Effective unit weight at bottom of layer = 120.000000 pcf
 Undrained cohesion at top of layer = 1500. psf
 Undrained cohesion at bottom of layer = 1500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 13.000000 ft
 Distance from top of pile to bottom of layer = 18.000000 ft
 Effective unit weight at top of layer = 125.000000 pcf
 Effective unit weight at bottom of layer = 125.000000 pcf
 Undrained cohesion at top of layer = 4500. psf
 Undrained cohesion at bottom of layer = 4500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 6 is stiff clay without free water

Distance from top of pile to top of layer = 18.000000 ft
 Distance from top of pile to bottom of layer = 23.000000 ft
 Effective unit weight at top of layer = 125.000000 pcf
 Effective unit weight at bottom of layer = 125.000000 pcf
 Undrained cohesion at top of layer = 2500. psf
 Undrained cohesion at bottom of layer = 2500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 7 is stiff clay without free water

Distance from top of pile to top of layer = 23.000000 ft
 Distance from top of pile to bottom of layer = 28.000000 ft
 Effective unit weight at top of layer = 125.000000 pcf
 Effective unit weight at bottom of layer = 125.000000 pcf
 Undrained cohesion at top of layer = 3500. psf
 Undrained cohesion at bottom of layer = 3500. psf
 Epsilon-50 at top of layer = 0.007000
 Epsilon-50 at bottom of layer = 0.007000

Layer 8 is stiff clay without free water

Distance from top of pile to top of layer = 28.000000 ft
 Distance from top of pile to bottom of layer = 80.000000 ft
 Effective unit weight at top of layer = 125.000000 pcf
 Effective unit weight at bottom of layer = 125.000000 pcf
 Undrained cohesion at top of layer = 4500. psf
 Undrained cohesion at bottom of layer = 4500. psf
 Epsilon-50 at top of layer = 0.005000
 Epsilon-50 at bottom of layer = 0.005000

(Depth of the lowest soil layer extends 30.000 ft below the pile tip)

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Summary of Input Soil Properties

Layer Layer Num.	Soil Type Name (p-y Curve Type)	Layer Depth ft	Effective Unit Wt. pcf	Undrained Cohesion psf	E50 or krm
1	Stiff Clay	-2.0000	120.0000	3500.	0.00700
	w/o Free Water	0.10000	120.0000	3500.	0.00700
2	Stiff Clay	0.10000	120.0000	1500.	0.00700
	w/o Free Water	3.0000	120.0000	1500.	0.00700
3	Stiff Clay	3.0000	120.0000	2500.	0.00700
	w/o Free Water	8.0000	120.0000	2500.	0.00700
4	Stiff Clay	8.0000	120.0000	1500.	0.00700
	w/o Free Water	13.0000	120.0000	1500.	0.00700
5	Stiff Clay	13.0000	125.0000	4500.	0.00700
	w/o Free Water	18.0000	125.0000	4500.	0.00700
6	Stiff Clay	18.0000	125.0000	2500.	0.00700
	w/o Free Water	23.0000	125.0000	2500.	0.00700
7	Stiff Clay	23.0000	125.0000	3500.	0.00700
	w/o Free Water	28.0000	125.0000	3500.	0.00700
8	Stiff Clay	28.0000	125.0000	4500.	0.00500
	w/o Free Water	80.0000	125.0000	4500.	0.00500

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.5800	1.0000
2	50.000	0.5800	1.0000

Static Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4	y = 0.250000 in	M = 0.0000 in-lbs	154000.	N.A.
2	4	y = 0.500000 in	M = 0.0000 in-lbs	154000.	N.A.
3	4	y = 1.000000 in	M = 0.0000 in-lbs	154000.	N.A.

V = shear force applied normal to pile axis
M = bending moment applied to pile head
y = lateral deflection normal to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Values of top y vs. pile lengths can be computed only for load types with specified shear loading (Load Types 1, 2, and 3).

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Thrust force is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Layering Correction Equivalent Depths of Soil & Rock Layers

Layer No.	Top of Layer Below Pile Head ft	Equivalent Top Depth Below Grnd Surf ft	Same Layer Type As Layer Above	Layer is Rock or is Below Rock Layer	F0 Integral for Layer lbs	F1 Integral for Layer lbs
1	-2.0000	0.00	N.A.	No	0.00	1790.
2	0.1000	2.1000	Yes	No	1790.	25921.
3	3.0000	5.0000	Yes	No	27711.	101146.
4	8.0000	10.0000	Yes	No	128856.	84678.
5	13.0000	15.0000	Yes	No	213535.	269497.
6	18.0000	20.0000	Yes	No	483031.	150300.
7	23.0000	25.0000	Yes	No	633331.	210000.
8	28.0000	30.0000	Yes	No	843331.	N.A.

Notes: The F0 integral of Layer n+1 equals the sum of the F0 and F1 integrals for Layer n. Layering correction equivalent depths are computed only for soil types with both shallow-depth and deep-depth expressions for peak lateral load transfer. These soil types are soft and stiff clays, non-liquefied sands, and cemented c-phi soil.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.250000 inches
Moment at pile head = 0.0 in-lbs
Axial load at pile head = 154000.0 lbs

Depth X feet	Deflect. y inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness in-lb^2	Soil Res. p lb/inch	Soil Spr. Es*h lb/inch	Distrib. Lat. Load lb/inch
0.00	0.2500	0.00	12633.	-0.00462	765.9332	5.80E+09	-418.6200	5023.	0.00
0.5000	0.2223	72536.	10811.	-0.00459	1127.	5.80E+09	-188.7602	5096.	0.00
1.0000	0.1950	138207.	9666.	-0.00448	1453.	5.80E+09	-192.7229	5931.	0.00
1.5000	0.1685	196808.	8502.	-0.00430	1745.	5.80E+09	-195.5153	6961.	0.00
2.0000	0.1433	248182.	7324.	-0.00407	2000.	5.80E+09	-197.0546	8250.	0.00
2.5000	0.1196	292226.	6141.	-0.00379	2219.	5.80E+09	-197.2507	9892.	0.00
3.0000	0.09778	328888.	4780.	-0.00347	2402.	5.80E+09	-256.3853	15732.	0.00
3.5000	0.07797	356006.	3076.	-0.00312	2537.	5.80E+09	-311.7128	23989.	0.00


```
Abut 1L_transv_Ave P.lp90
8.0000 0.03468 756486. -13167. -0.00314 4528. 5.80E+09 -281.0620 48623. 0.00
8.5000 0.01817 674969. -14579. -0.00240 4123. 5.80E+09 -189.8170 62664. 0.00
9.0000 0.00586 585974. -15591. -0.00175 3680. 5.80E+09 -147.3191 150908. 0.00
9.5000 -0.00282 491115. -15655. -0.00119 3209. 5.80E+09 125.7796 267408. 0.00
10.0000 -0.00845 400315. -14767. -0.31E-04 2757. 5.80E+09 170.3147 128095. 0.00
10.5000 -0.01160 315263. -13688. -0.61E-04 2334. 5.80E+09 189.3332 97949. 0.00
11.0000 -0.01279 236726. -12523. -0.75E-05 1943. 5.80E+09 199.1032 93433. 0.00
11.5000 -0.01250 165130. -11326. 1.32E-04 1587. 5.80E+09 199.8920 95917. 0.00
12.0000 -0.01120 100572. -10143. 2.70E-04 1266. 5.80E+09 194.4522 104197. 0.00
12.5000 -0.00927 42919. -9003. 3.44E-04 979.3932 5.80E+09 185.4609 120093. 0.00
13.0000 -0.00707 -8099. -7407. 3.62E-04 806.2155 5.80E+09 346.6352 294255. 0.00
13.5000 -0.00492 -46631. -4042. 3.34E-04 997.8545 5.80E+09 474.9179 579101. 0.00
14.0000 -0.00306 -68020. -2252. 2.74E-04 1104. 5.80E+09 421.7902 826343. 0.00
14.5000 -0.00163 -74160. 93.5842 2.01E-04 1135. 5.80E+09 360.0341 1327821. 0.00
15.0000 -6.52E-04 -67269. 2033. 1.28E-04 1100. 5.80E+09 286.3153 2636434. 0.00
15.5000 -9.39E-05 -58005. 3103. 6.71E-05 1015. 5.80E+09 70.4395 4498936. 0.00
16.0000 1.53E-04 -38158. 2969. 2.56E-05 915.9253 5.80E+09 -114.9213 4498936. 0.00
16.5000 2.13E-04 -14419. 2145. 2.54E-06 837.6465 5.80E+09 -159.8927 4498936. 0.00
17.0000 1.84E-04 -4422. 1252. -7.21E-06 787.9278 5.80E+09 -137.7421 4498936. 0.00
17.5000 1.27E-04 619.7771 553.8643 -9.18E-06 769.0157 5.80E+09 -95.0050 4498936. 0.00
18.0000 7.36E-05 2241. 140.1591 -7.70E-06 777.0793 5.80E+09 -42.8968 3499172. 0.00
18.5000 3.43E-05 2316. -31.4206 -5.34E-06 777.4516 5.80E+09 -14.2964 2499409. 0.00
19.0000 9.46E-06 1874. -86.1352 -3.17E-06 775.2531 5.80E+09 -3.9417 2499409. 0.00
19.5000 -3.76E-06 1288. -93.2603 -1.54E-06 772.3399 5.80E+09 1.5667 2499409. 0.00
20.0000 -8.99E-06 757.5988 -77.3292 -4.79E-07 769.7012 5.80E+09 3.7437 2499409. 0.00
20.5000 -9.51E-06 361.0909 -54.2139 9.97E-08 767.7291 5.80E+09 3.9614 2499409. 0.00
21.0000 -7.79E-06 106.8479 -32.5940 3.42E-07 766.4646 5.80E+09 3.2452 2499409. 0.00
21.5000 -5.41E-06 -30.6686 -16.1000 3.81E-07 766.0857 5.80E+09 2.2527 2499409. 0.00
22.0000 -3.22E-06 -87.0570 -5.3231 3.20E-07 766.3661 5.80E+09 1.3396 2499409. 0.00
22.5000 -1.56E-06 -95.1375 0.6503 2.26E-07 766.4063 5.80E+09 0.6515 2499409. 0.00
23.0000 -5.03E-07 -79.6714 3.3593 1.36E-07 766.3294 5.80E+09 0.2515 2999290. 0.00
23.5000 6.33E-08 -55.0759 4.0030 6.59E-08 766.2071 5.80E+09 -0.03692 3499172. 0.00
24.0000 2.88E-07 -31.7569 3.3888 2.10E-08 766.0911 5.80E+09 -0.1678 3499172. 0.00
24.5000 3.15E-07 -14.4487 2.3342 -2.93E-09 766.0050 5.80E+09 -0.1837 3499172. 0.00
25.0000 2.53E-07 -3.7410 1.3410 -1.23E-08 765.9518 5.80E+09 -0.1473 3499172. 0.00
25.5000 1.67E-07 1.6666 0.6069 -1.34E-08 765.9415 5.80E+09 -0.09738 3499172. 0.00
26.0000 9.17E-08 3.5668 0.1544 -1.07E-08 765.9509 5.80E+09 -0.05347 3499172. 0.00
26.5000 3.85E-08 3.5387 -0.07346 -7.03E-09 765.9508 5.80E+09 -0.02247 3499172. 0.00
27.0000 7.35E-09 2.6983 -0.1537 -3.80E-09 765.9466 5.80E+09 -0.00429 3499172. 0.00
27.5000 -1.700E-09 1.7008 -0.1542 -1.52E-09 765.9416 5.80E+09 0.00413 3499172. 0.00
28.0000 -1.09E-08 0.8592 -0.1191 -2.05E-10 765.9374 5.80E+09 0.00758 4156176. 0.00
28.5000 -9.54E-09 0.2718 -0.07304 3.75E-10 765.9345 5.80E+09 0.00778 4893750. 0.00
29.0000 -6.44E-09 -0.02688 -0.03395 5.02E-10 765.9333 5.80E+09 0.00525 4893750. 0.00
29.5000 -3.51E-09 -0.1365 -0.00960 4.18E-10 765.9338 5.80E+09 0.00286 4893750. 0.00
30.0000 -1.43E-09 -0.1429 0.00248 2.73E-10 765.9339 5.80E+09 0.00116 4893750. 0.00
30.5000 -2.32E-10 -0.1073 0.00654 1.44E-10 765.9337 5.80E+09 1.90E-04 4893750. 0.00
31.0000 2.97E-10 -0.06469 0.00638 5.47E-11 765.9335 5.80E+09 -2.42E-04 4893750. 0.00
31.5000 4.25E-10 -0.03078 0.00462 5.35E-12 765.9333 5.80E+09 -3.46E-04 4893750. 0.00
32.0000 3.61E-10 -0.00931 0.00269 -1.54E-11 765.9332 5.80E+09 -2.95E-04 4893750. 0.00
32.5000 2.40E-10 0.00157 0.00122 -1.94E-11 765.9332 5.80E+09 -1.96E-04 4893750. 0.00
33.0000 1.28E-10 0.00541 3.22E-04 -1.58E-11 765.9332 5.80E+09 -1.05E-04 4893750. 0.00
33.5000 5.06E-11 0.00546 -1.17E-04 -1.02E-11 765.9332 5.80E+09 -4.13E-05 4893750. 0.00
34.0000 6.67E-12 0.00403 -2.57E-04 -5.24E-12 765.9332 5.80E+09 -5.44E-06 4893750. 0.00
34.5000 -1.23E-11 0.00239 -2.43E-04 -1.92E-12 765.9332 5.80E+09 1.00E-05 4893750. 0.00
35.0000 -1.64E-11 0.00111 -1.73E-04 0.00 765.9332 5.80E+09 1.34E-05 4893750. 0.00
35.5000 -1.37E-11 3.15E-04 -9.92E-05 0.00 765.9332 5.80E+09 1.11E-05 4893750. 0.00
36.0000 -8.93E-12 -8.00E-05 -4.39E-05 0.00 765.9332 5.80E+09 7.28E-06 4893750. 0.00
36.5000 -4.70E-12 -2.13E-04 -1.06E-05 0.00 765.9332 5.80E+09 3.83E-06 4893750. 0.00
37.0000 -1.79E-12 -2.08E-04 5.25E-06 0.00 765.9332 5.80E+09 1.46E-06 4893750. 0.00
37.5000 0.00 -1.51E-04 1.01E-05 0.00 765.9332 5.80E+09 1.42E-07 4893750. 0.00
38.0000 0.00 -8.81E-05 9.25E-06 0.00 765.9332 5.80E+09 -4.11E-07 4893750. 0.00
38.5000 0.00 -4.01E-05 6.46E-06 0.00 765.9332 5.80E+09 -5.17E-07 4893750. 0.00
39.0000 0.00 -1.06E-05 3.65E-06 0.00 765.9332 5.80E+09 -4.21E-07 4893750. 0.00
39.5000 0.00 3.78E-06 1.57E-06 0.00 765.9332 5.80E+09 -2.71E-07 4893750. 0.00
40.0000 0.00 8.38E-06 3.43E-07 0.00 765.9332 5.80E+09 -1.40E-07 4893750. 0.00
40.5000 0.00 7.94E-06 -2.30E-07 0.00 765.9332 5.80E+09 -5.13E-08 4893750. 0.00
41.0000 0.00 5.65E-06 -3.92E-07 0.00 765.9332 5.80E+09 -2.98E-09 4893750. 0.00
41.5000 0.00 3.25E-06 -3.51E-07 0.00 765.9332 5.80E+09 1.67E-08 4893750. 0.00
```

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Abut 1L_transv_Ave P.lp90
42.0000 0.00 1.44E-06 -2.41E-07 0.00 765.9332 5.80E+09 1.99E-08 4893750. 0.00
42.5000 0.00 3.49E-07 -1.34E-07 0.00 765.9332 5.80E+09 1.59E-08 4893750. 0.00
43.0000 0.00 -1.70E-07 -5.62E-08 0.00 765.9332 5.80E+09 1.00E-08 4893750. 0.00
43.5000 0.00 -3.28E-07 -1.08E-08 0.00 765.9332 5.80E+09 5.09E-09 4893750. 0.00
44.0000 0.00 -3.02E-07 9.81E-09 0.00 765.9332 5.80E+09 1.79E-09 4893750. 0.00
44.5000 0.00 -2.11E-07 1.53E-08 0.00 765.9332 5.80E+09 2.52E-11 4893750. 0.00
45.0000 0.00 -1.19E-07 1.33E-08 0.00 765.9332 5.80E+09 -6.73E-10 4893750. 0.00
45.5000 0.00 -5.16E-08 9.00E-09 0.00 765.9332 5.80E+09 -7.66E-10 4893750. 0.00
46.0000 0.00 -1.13E-08 4.91E-09 0.00 765.9332 5.80E+09 -5.98E-10 4893750. 0.00
46.5000 0.00 7.44E-09 2.00E-09 0.00 765.9332 5.80E+09 -3.73E-10 4893750. 0.00
47.0000 0.00 1.28E-08 3.26E-10 0.00 765.9332 5.80E+09 -1.85E-11 4893750. 0.00
47.5000 0.00 1.14E-08 -4.18E-10 0.00 765.9332 5.80E+09 -6.25E-11 4893750. 0.00
48.0000 0.00 7.79E-09 -5.97E-10 0.00 765.9332 5.80E+09 2.59E-12 4893750. 0.00
48.5000 0.00 4.26E-09 -5.05E-10 0.00 765.9332 5.80E+09 2.82E-11 4893750. 0.00
49.0000 0.00 1.74E-09 -3.24E-10 0.00 765.9332 5.80E+09 3.22E-11 4893750. 0.00
49.5000 0.00 3.75E-10 -1.45E-10 0.00 765.9332 5.80E+09 2.74E-11 4893750. 0.00
50.0000 0.00 0.00 0.00 0.00 765.9332 5.80E+09 2.08E-11 2446875. 0.00
```

* The above values of total stress are combined axial and bending stresses.

Output Summary for Load Case No. 3:

Pile-head deflection = 1.00000000 inches
Computed slope at pile head = -0.01475780 radians
Maximum bending moment = 957020. inch-lbs
Maximum shear force = 24146. lbs
Depth of maximum bending moment = 5.50000000 feet below pile head
Depth of maximum shear force = 0.000000 feet below pile head
Number of iterations = 21
Number of zero deflection points = 11

Summary of Pile-head Responses for Conventional Analyses

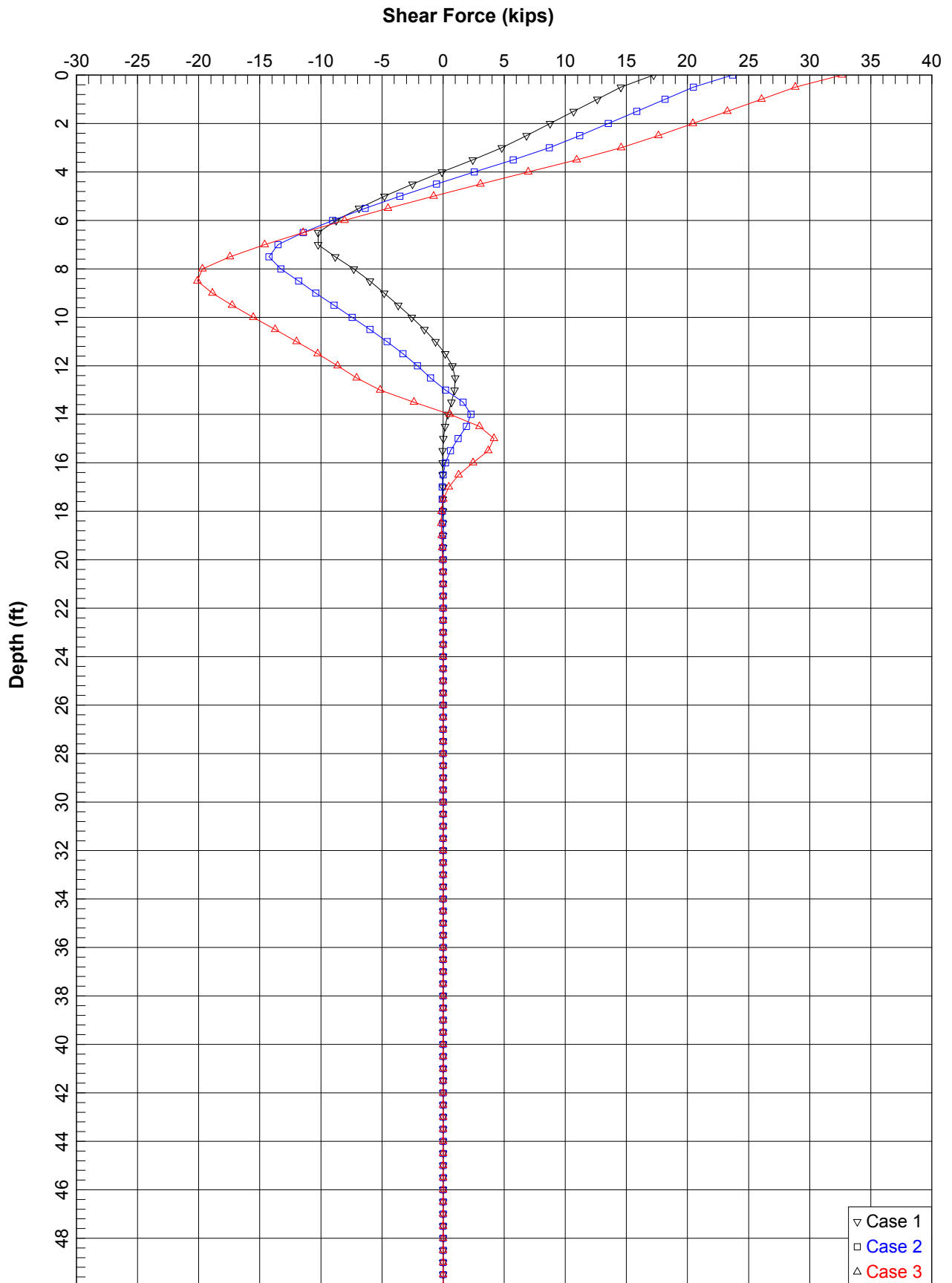
Definitions of Pile-head Loading Conditions:

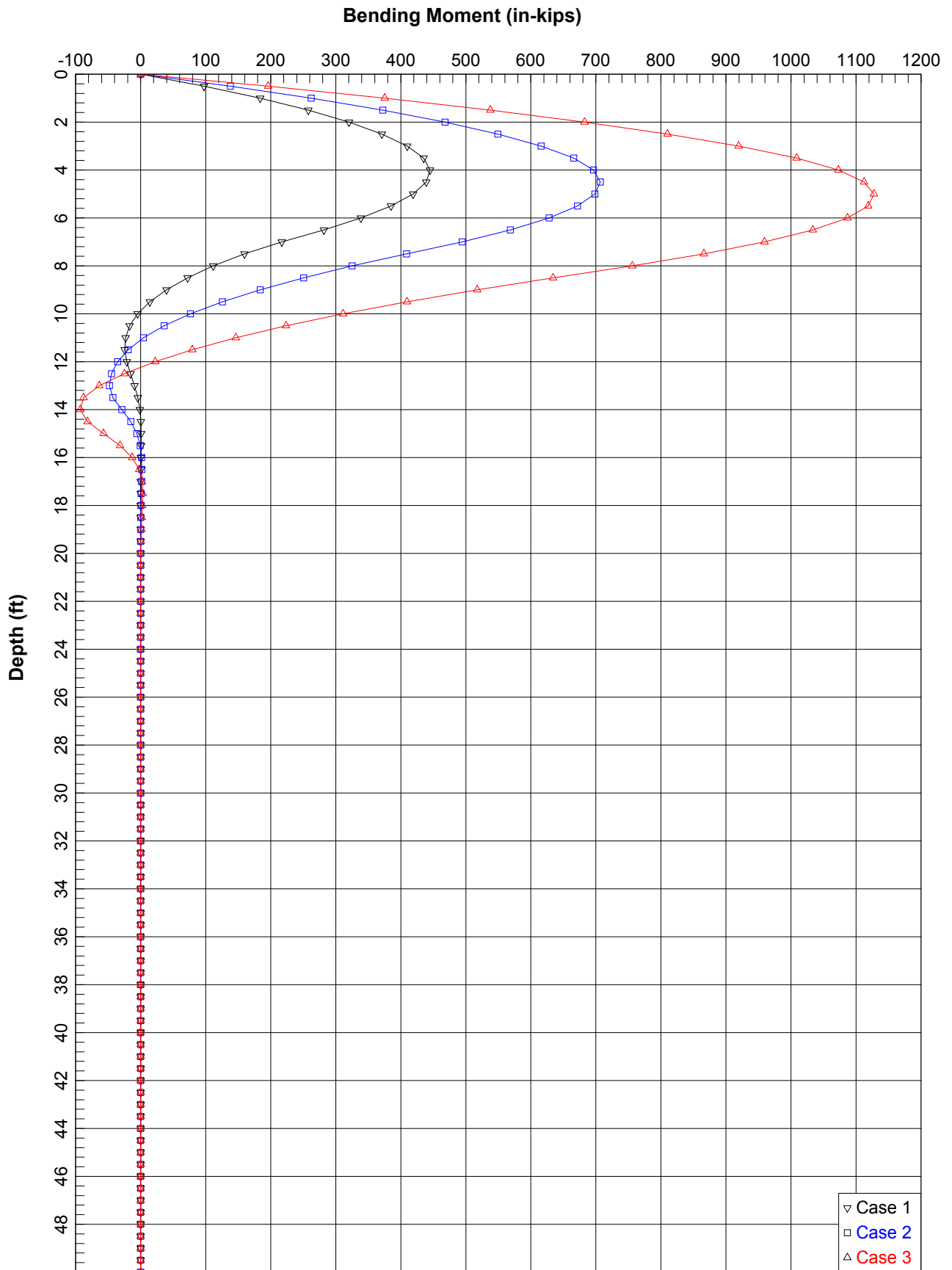
- Load Type 1: Load 1 = Shear, V, lbs, and Load 2 = Moment, M, in-lbs
- Load Type 2: Load 1 = Shear, V, lbs, and Load 2 = Slope, S_y, radians
- Load Type 3: Load 1 = Shear, V, lbs, and Load 2 = Rot. Stiffness, R, in-lbs/rad.
- Load Type 4: Load 1 = Top Deflection, y, inches, and Load 2 = Moment, M, in-lbs
- Load Type 5: Load 1 = Top Deflection, y, inches, and Load 2 = Slope, S_y, radians

Case No.	Load 1	Pile-head Load 1	Load 2	Pile-head Load 2	Axial Loading lbs	Pile-head Deflection inches	Pile-head Rotation radians	Max Shear in lbs	Max Moment in lbs
1	y, in	0.2500	M, in-lb	0.00	154000.	0.2500	-0.00462	12633.	375819.
2	y, in	0.5000	M, in-lb	0.00	154000.	0.5000	-0.00829	17508.	602487.
3	y, in	1.0000	M, in-lb	0.00	154000.	1.0000	-0.01476	24146.	957020.

Maximum pile-head deflection = 1.000000000 inches
Maximum pile-head rotation = -0.014757804 radians = -0.845560 deg.

The analysis ended normally.





Abut 1L_transv_Max P

Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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gdc
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 1\
 Name of input data file: Abut 1L_transv_Max P.lpd
 Name of output report file: Abut 1L_transv_Max P.lpp
 Name of plot output file: Abut 1L_transv_Max P.lpp
 Name of runtime message file: Abut 1L_transv_Max P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 10:55:33

Problem Title

Project Name: Palo Comado OC Bridge Widened

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Abut 1L_transv_Max P

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 16.0000000 in
 Bottom Width = 16.0000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 8 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 3.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 3.00000 ft
 Distance from top of pile to bottom of layer = 8.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2500.00000 psi
 Undrained cohesion at bottom of layer = 2500.00000 psi

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 8.00000 ft
 Distance from top of pile to bottom of layer = 13.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 13.00000 ft
 Distance from top of pile to bottom of layer = 18.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 6 is stiff clay without free water

Distance from top of pile to top of layer = 18.00000 ft
 Distance from top of pile to bottom of layer = 23.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 2500.00000 psi
 Undrained cohesion at bottom of layer = 2500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 7 is stiff clay without free water

Distance from top of pile to top of layer = 23.00000 ft
 Distance from top of pile to bottom of layer = 28.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 8 is stiff clay without free water

Distance from top of pile to top of layer = 28.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type	Rock Mass Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Uniaxial Elastic Mod.	ROD %
Num.	Epsilon 50	(p-y Curve Criteria) Factor	Rock Emass	pcf	psf	deg.	psi	GSI
			ft	pcf	Test Type	Property	psi	
1	0.00700	Stiff Clay w/o Free Water	-2.000	120.000	3500.000	--	--	--
	0.00700	--	0.10000	120.000	3500.000	--	--	--
2	0.00700	Stiff Clay w/o Free Water	0.10000	120.000	1500.000	--	--	--
	0.00700	--	3.000	120.000	1500.000	--	--	--
3	0.00700	Stiff Clay w/o Free Water	3.000	120.000	2500.000	--	--	--
	0.00700	--	8.000	120.000	2500.000	--	--	--

			Abut 1L_transv_Max P				
4	0.00700	Stiff Clay w/o Free Water	8.000	120.000	1500.000	--	--
	0.00700	--	13.000	120.000	1500.000	--	--
5	0.00700	Stiff Clay w/o Free Water	13.000	125.000	4500.000	--	--
	0.00700	--	18.000	125.000	4500.000	--	--
6	0.00700	Stiff Clay w/o Free Water	18.000	125.000	2500.000	--	--
	0.00700	--	23.000	125.000	2500.000	--	--
7	0.00700	Stiff Clay w/o Free Water	23.000	125.000	3500.000	--	--
	0.00700	--	28.000	125.000	3500.000	--	--
8	0.00500	Stiff Clay w/o Free Water	28.000	125.000	4500.000	--	--
	0.00500	--	80.000	125.000	4500.000	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.8000	1.0000
2	50.000	0.8000	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4	y = 0.25000 in	M = 0.0000 in-lbs	154000.	False
2	4	y = 0.50000 in	M = 0.0000 in-lbs	154000.	False
3	4	y = 1.00000 in	M = 0.0000 in-lbs	154000.	False

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Page 4

Table with columns: Depth X inches, Deflect. Y inches, Bending Moment in-lbs, Shear Force lbs, Slope S radians, Total Stress psi, Bending Stiffness lb-in^2, Soil Res. p lb/in, Soil Spr. Es'h lb/inch, Lat. Load lb/inch. Includes displacement and moment at pile head, axial load at pile head, and Abut TL_transv_Max P values.

Table with columns: Depth X inches, Deflect. Y inches, Bending Moment in-lbs, Shear Force lbs, Slope S radians, Total Stress psi, Bending Stiffness lb-in^2, Soil Res. p lb/in, Soil Spr. Es'h lb/inch, Lat. Load lb/inch. Continuation of the main data table.

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Summary table with columns: Item, Value, Unit. Includes: Pile-head deflection, Computed slope at pile head, Maximum bending moment, Maximum shear force, Depth of maximum bending moment, Depth of maximum shear force, Number of iterations, Number of zero deflection points.

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4) = 0.500000 inches, Displacement of pile head = 0.000114 inches, Moment at pile head = 1417.8 lb-in, Axial load at pile head = 154000.000 lbs

Table with columns: Depth X inches, Deflect. Y inches, Bending Moment in-lbs, Shear Force lbs, Slope S radians, Total Stress psi, Bending Stiffness lb-in^2, Soil Res. p lb/in, Soil Spr. Es'h lb/inch, Lat. Load lb/inch. Continuation of the main data table.

Abut TL_transv_Max P									
516.000	0.000	-3.046E-08	9.440E-09	0.000	765.9332	5.799E+09	-1.107E-09	6750000.	0.000
522.000	0.000	6.310E-09	4.001E-09	0.000	765.9332	5.799E+09	-7.059E-10	6750000.	0.000
528.000	0.000	1.766E-08	8.370E-10	0.000	765.9332	5.799E+09	-3.489E-10	6750000.	0.000
534.000	0.000	1.644E-08	-5.553E-10	0.000	765.9332	5.799E+09	-1.152E-10	6750000.	0.000
540.000	0.000	1.105E-08	-8.899E-10	0.000	765.9332	5.799E+09	3.681E-12	6750000.	0.000
546.000	0.000	5.779E-09	-7.426E-10	0.000	765.9332	5.799E+09	4.542E-11	6750000.	0.000
552.000	0.000	2.141E-09	-4.659E-10	0.000	765.9332	5.799E+09	4.679E-11	6750000.	0.000
558.000	0.000	1.862E-10	-2.259E-10	0.000	765.9332	5.799E+09	3.321E-11	6750000.	0.000
564.000	0.000	-5.736E-10	-7.129E-11	0.000	765.9332	5.799E+09	1.833E-11	6750000.	0.000
570.000	0.000	-6.729E-10	6.059E-12	0.000	765.9332	5.799E+09	7.455E-12	6750000.	0.000
576.000	0.000	-5.032E-10	3.226E-11	0.000	765.9332	5.799E+09	1.279E-12	6750000.	0.000
582.000	0.000	-2.870E-10	3.195E-11	0.000	765.9332	5.799E+09	-1.382E-12	6750000.	0.000
588.000	0.000	-1.203E-10	2.169E-11	0.000	765.9332	5.799E+09	-2.038E-12	6750000.	0.000
594.000	0.000	-2.676E-11	1.001E-11	0.000	765.9332	5.799E+09	-1.854E-12	6750000.	0.000
600.000	0.000	0.000	0.000	0.000	765.9332	5.799E+09	-1.484E-12	3375000.	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

Pile-head deflection = 1.0000000 inches
 Computed slope at pile head = -0.0161043 radians
 Maximum bending moment = 1127378. inch-lbs
 Maximum shear force = 32629. lbs
 Depth of maximum bending moment = 60.0000000 inches below pile head
 Depth of maximum shear force = 0.0000000 inches below pile head
 Number of iterations = 24
 Number of zero deflection points = 12

 Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

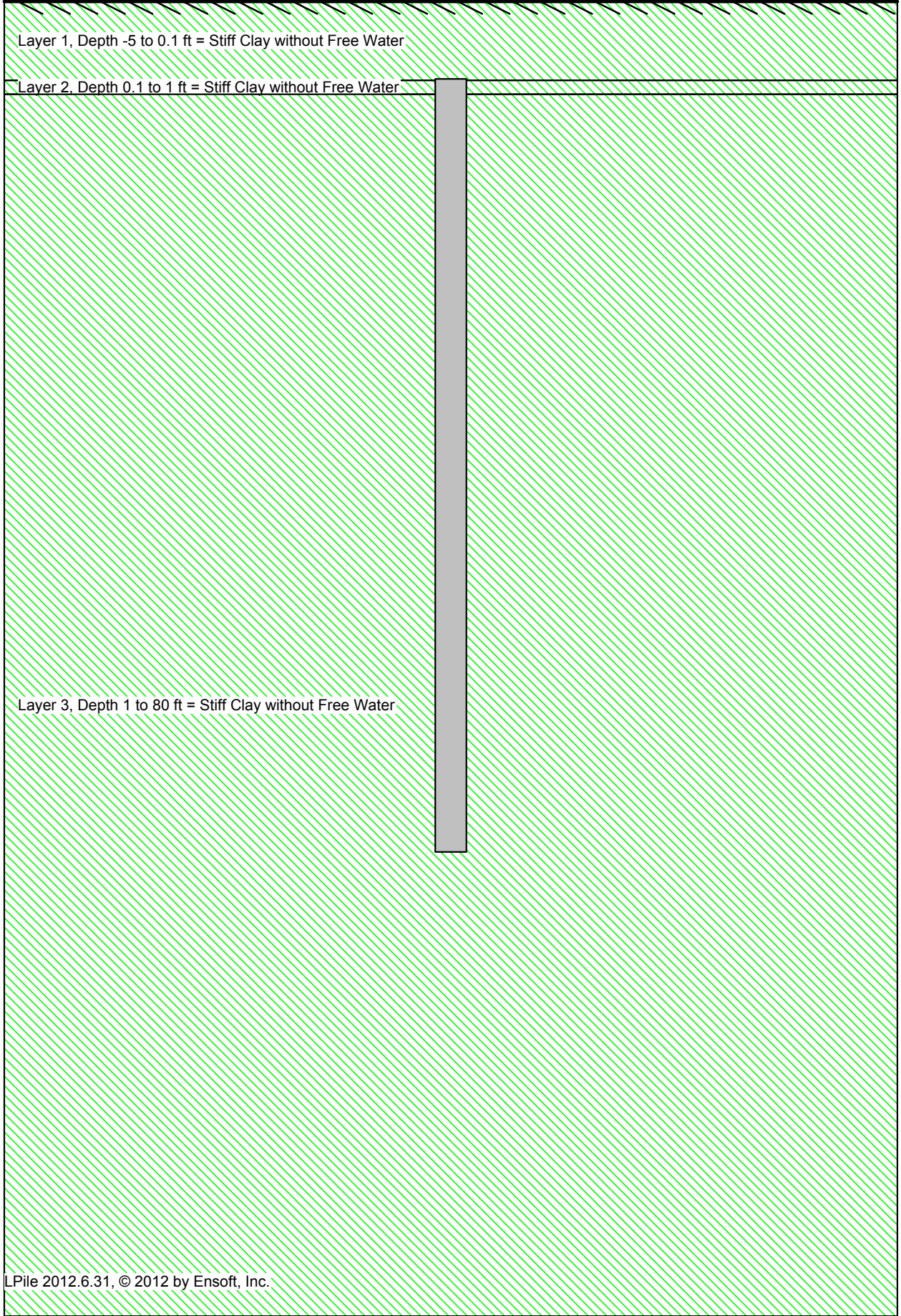
Load Case No.	Load Type No.		Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 M = in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y =	0.2500	M = 0.000	154000.	0.25000000	444819.	17233.	-0.00505059
2	4	y =	0.5000	M = 0.000	154000.	0.50000000	706799.	23685.	-0.00901504
3	4	y =	1.0000	M = 0.000	154000.	1.00000000	1127378.	32629.	-0.01610427

The analysis ended normally.

SUPPORT: BENT 2R

LOAD DIRECTION: LONGITUDE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE

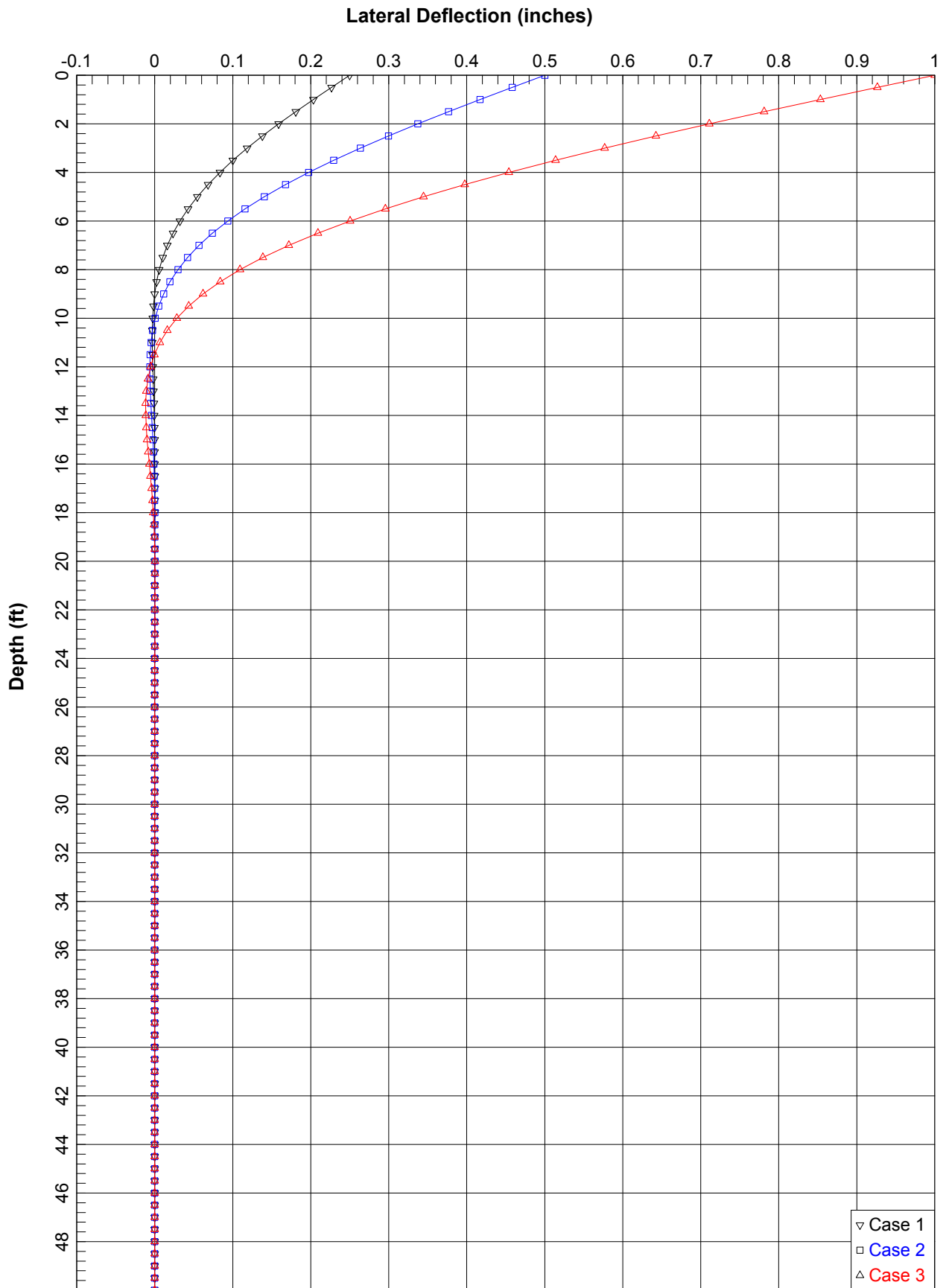


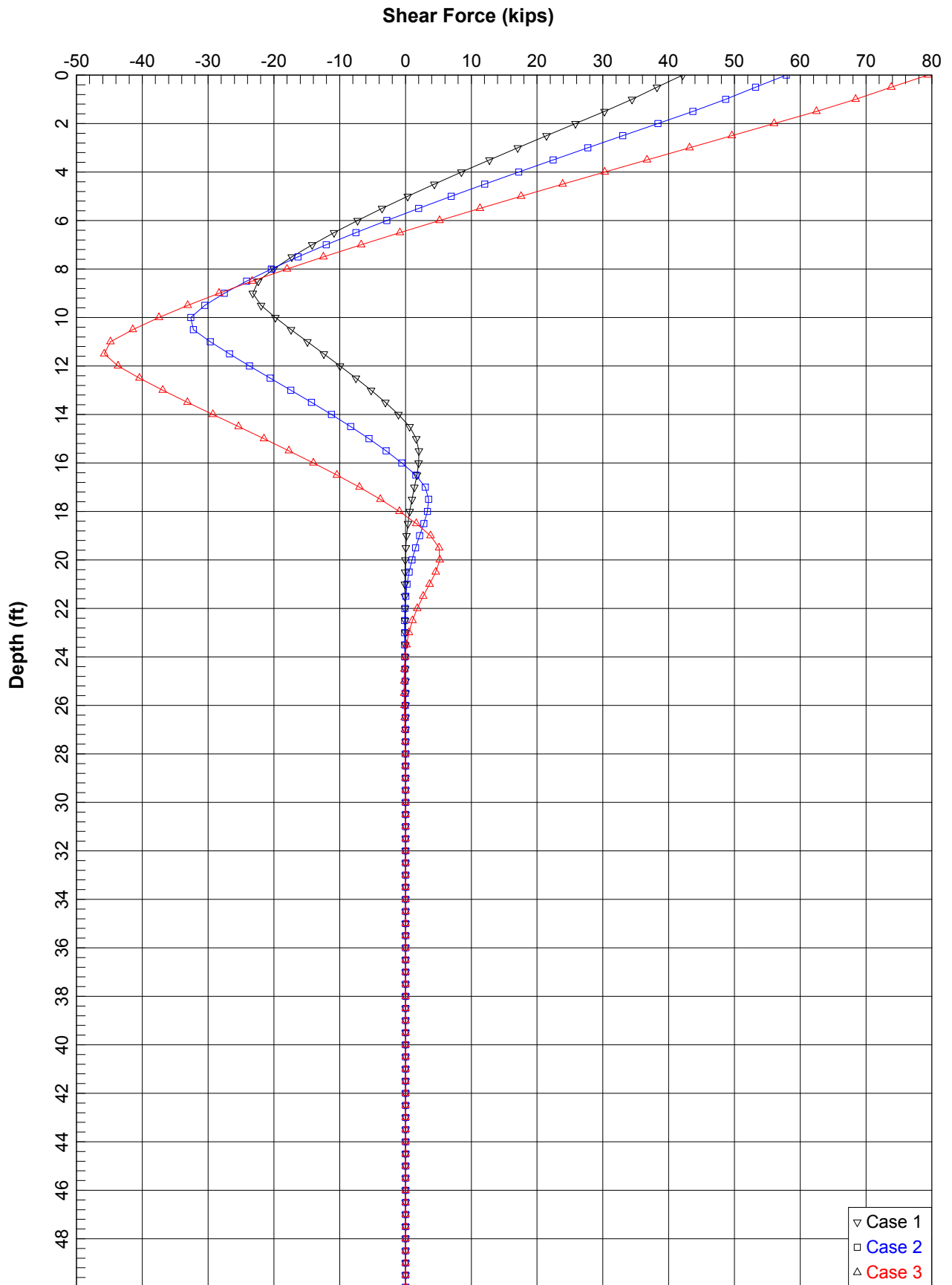
A cross-sectional diagram of a pile foundation. The pile is a vertical grey rectangle extending from the ground surface down into the soil. The soil is divided into three layers, all of which are represented by a green diagonal hatching pattern. The top layer is the shallowest, followed by a slightly thicker middle layer, and the bottom layer is the thickest and extends to a depth of 80 feet. The pile is positioned in the center of the diagram.

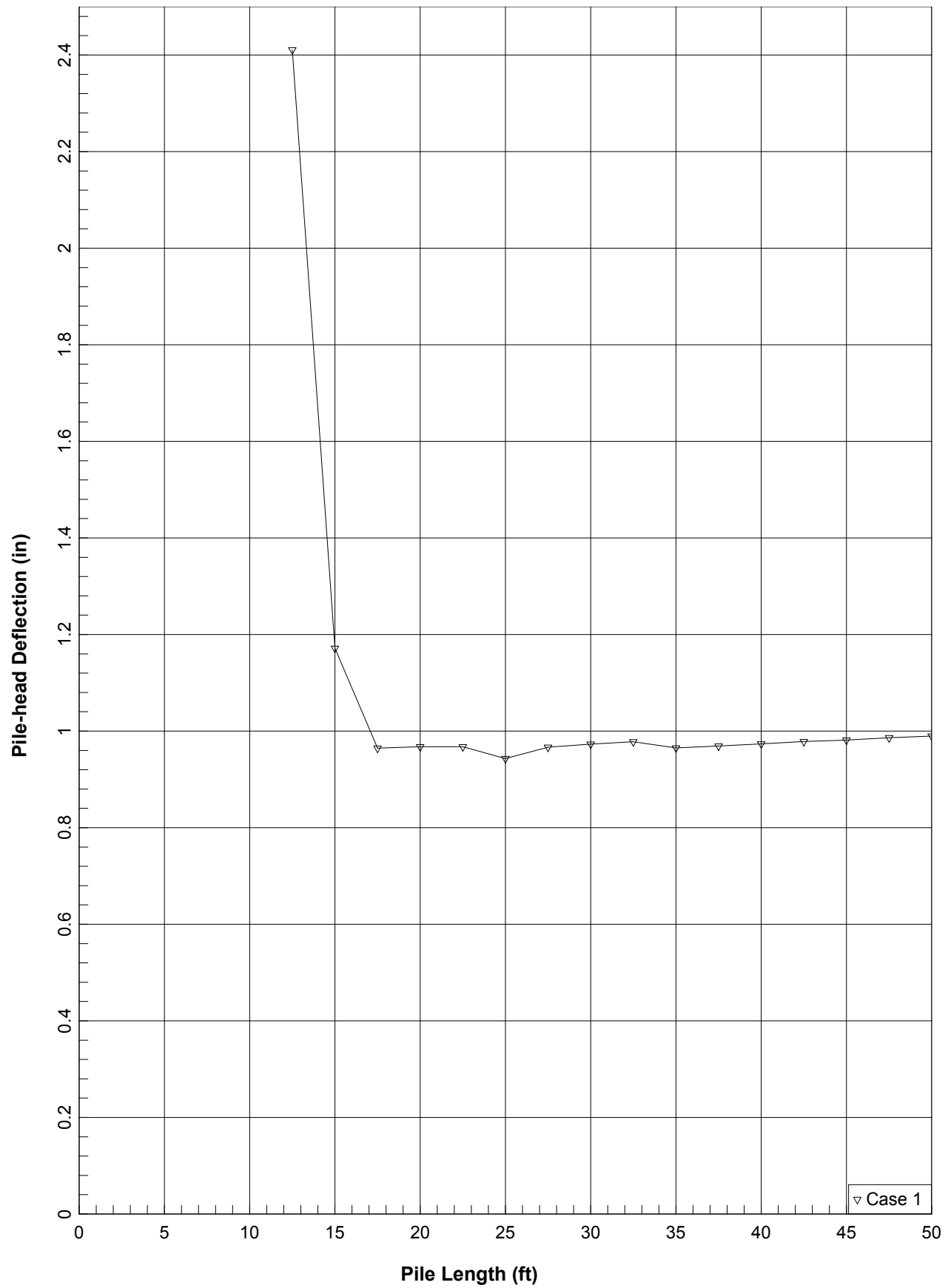
Layer 1, Depth -5 to 0.1 ft = Stiff Clay without Free Water

Layer 2, Depth 0.1 to 1 ft = Stiff Clay without Free Water

Layer 3, Depth 1 to 80 ft = Stiff Clay without Free Water







Bent 2R_long_crit length

File Plus for Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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gdc
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\athant\Desktop\Updated_ET 9-14-14\Bent 2V
 Name of input data file: Bent 2R_long_crit length.lpd
 Name of output report file: Bent 2R_long_crit length.lpd
 Name of plot output file: Bent 2R_long_crit length.lpp
 Name of runtime message file: Bent 2R_long_crit length.lpp

Date and Time of Analysis

Date: September 13, 2014 Time: 20:14:23

Problem Title

Project Name: Palo Comado OC Bridge Widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 241inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Long t.-Avg Pm

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.000000
2	50.00000	24.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 2R_long_crit length

Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. lbf/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modeled using 3 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 1.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass Rock Emass	Layer Depth	Effective Unit Wt	Undrained Cohesion	Angle of Friction	Elastic Mod.	Uniaxial or GSI	ROD %	Epsilon
1	Stiff Clay w/o Free Water		-5.000	125.000	4500.000	--	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--	--
2	Stiff Clay w/o Free Water		0.10000	125.000	3750.000	--	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--	--
3	Stiff Clay w/o Free Water		1.000	125.000	4500.000	--	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.4800	1.0000
2	50.000	0.4800	1.0000

Bent 2R_long_crit length

Table with 2 columns: Loading Type, Condition. Row 1: 1, 79000. lbs. M = 0.000 in-lbs. 185000.

Table with 4 columns: Load Type, Condition, Condition 2, Axial Thrust Force, lbs. Row 1: 1, 79000. lbs, M = 0.000 in-lbs, 185000.

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear Force at pile head = 79000.000 lbs
Applied moment at pile head = 0.000 in-lbs
Axial thrust load on pile head = 185000.000 lbs

Table with 10 columns: Depth y inches, Deflect. y inches, Bending Moment in-lbs, Shear Force lbs, Slope radians, Total Stress psi, Bending Stiffness lb-in^2, Soil Res. lb/in, Soil Spr. lb/in, Distrib. p lb/inch. Rows 0-306.

Table with 10 columns: Depth y inches, Deflect. y inches, Bending Moment in-lbs, Shear Force lbs, Slope radians, Total Stress psi, Bending Stiffness lb-in^2, Soil Res. lb/in, Soil Spr. lb/in, Distrib. p lb/inch. Rows 312-600.

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed Forces and moments are within specified convergence limits.

Table with 2 columns: Item, Value. Rows: Pile-head deflection, Computed slope at pile head, Maxium bending moment, Maxium shear force, Depth of maximum bending moment, Depth of maximum shear force, Number of iterations, Number of zero deflection points.

Pile-head Deflection vs. Pile Length for Load Case 1

Boundary Condition on Type 1, Shear and Moment

Shear = 79000. lbs
Moment = 0.000 in-lbs
Axial Load = 185000. lbs

Table with 4 columns: Pile Length Feet, Pile Head Deflection inches, Maximum Moment in-lbs, Maximum Shear lbs. Rows 47.500-12.500.

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians

Bent 2R_Long_cri_t length

Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lb/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lb
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lb	Maximum Shear lbs	Pile-head Rotation radians
1	1	V = 79000.	M = 0.000	185000.	0.98951526	3229672.	79000.	-0.01217166

The analysis ended normally.

Bent 2R_long_ave P

File Plus for Windows, Version 2012-06-031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\athant\Desktop\Updated_ET 9-14-14\Bent 2\
 Name of input data file: Bent 2R_long_ave P.ipd
 Name of output report file: Bent 2R_long_ave P.ip60
 Name of plot output file: Bent 2R_long_ave P.ip6p
 Name of runtime message file: Bent 2R_long_ave P.ip6r

Date and Time of Analysis

Date: September 13, 2014 Time: 20:12:07

Problem Title

Project Name: Palo Comado OC Bridge Widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 241inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.000000
2	50.00000	24.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 2R_long_ave P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modeled using 3 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 1.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass	Layer Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Elastic Modulus	Uniaxial Compressive Strength	ROD % or GSI	Epsilon
Factor Num. 50	J (p-y Curve Criteria)	Rock Emass	ft	pcf	psi	deg.	psi	psi		
1	Stiff Clay w/o Free Water		-5.000	125.000	4500.000	--	--	--	--	--
0.00700	--	--	--	125.000	4500.000	--	--	--	--	--
0.00700	--	--	0.10000	125.000	3750.000	--	--	--	--	--
0.00700	Stiff Clay w/o Free Water		0.10000	125.000	3750.000	--	--	--	--	--
0.00700	--	--	1.000	125.000	3750.000	--	--	--	--	--
0.00700	--	--	1.000	125.000	4500.000	--	--	--	--	--
0.00500	Stiff Clay w/o Free Water		1.000	125.000	4500.000	--	--	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--	--	--
0.00500	--	--	--	125.000	4500.000	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.4800	1.0000
2	50.000	0.4800	1.0000

Table with columns for coordinates (X, Y, Z) and values for Bent 2R_long_ave P. The table contains multiple rows of numerical data representing structural analysis results for a specific bent.

Table with columns for coordinates (X, Y, Z) and values for Bent 2R_long_ave P. This table continues the structural analysis results, showing a different set of numerical data for the same bent.

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed Forces and moments are within spec'ified convergence limits.

Output Summary For Load Case No. 2: A table listing various structural parameters such as pile-head deflection, computed slope at pile head, maximum bending moment, and maximum shear force.

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 3

Pile-head conditions are Displacement and Moment (Loading Type 4). Displacement of pile head = 1.000000 inches, Moment at pile head = 0.000000 inch-lbs, Axial load at pile head = 185000.00 lbs.

Table with columns: Depth (inches), Deflect. (inches), Bending Moment (in-lbs), Shear Force (lbs), Slope (rad/ans), Total Stress (psi), Bending Moment (lb-in^2), Soil Res. (lb/in), Spr. Es (lb/inch), Distributions (lb/inch). It provides detailed data for different depths along the pile.

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed Forces and moments are within spec'ified convergence limits.

Output Summary For Load Case No. 3: A table listing various structural parameters similar to Load Case No. 2, but for a different load case.

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 3

Pile-head conditions are Displacement and Moment (Loading Type 4). Displacement of pile head = 1.000000 inches, Moment at pile head = 0.000000 inch-lbs, Axial load at pile head = 185000.00 lbs.

Table with columns: Depth (inches), Deflect. (inches), Bending Moment (in-lbs), Shear Force (lbs), Slope (rad/ans), Total Stress (psi), Bending Moment (lb-in^2), Soil Res. (lb/in), Spr. Es (lb/inch), Distributions (lb/inch). It provides detailed data for different depths along the pile.

Bent 2R_long_ave P

Depth of maximum shear force = 0.00000 inches below pile head
 Number of iterations = 19
 Number of zero deflection points = 7

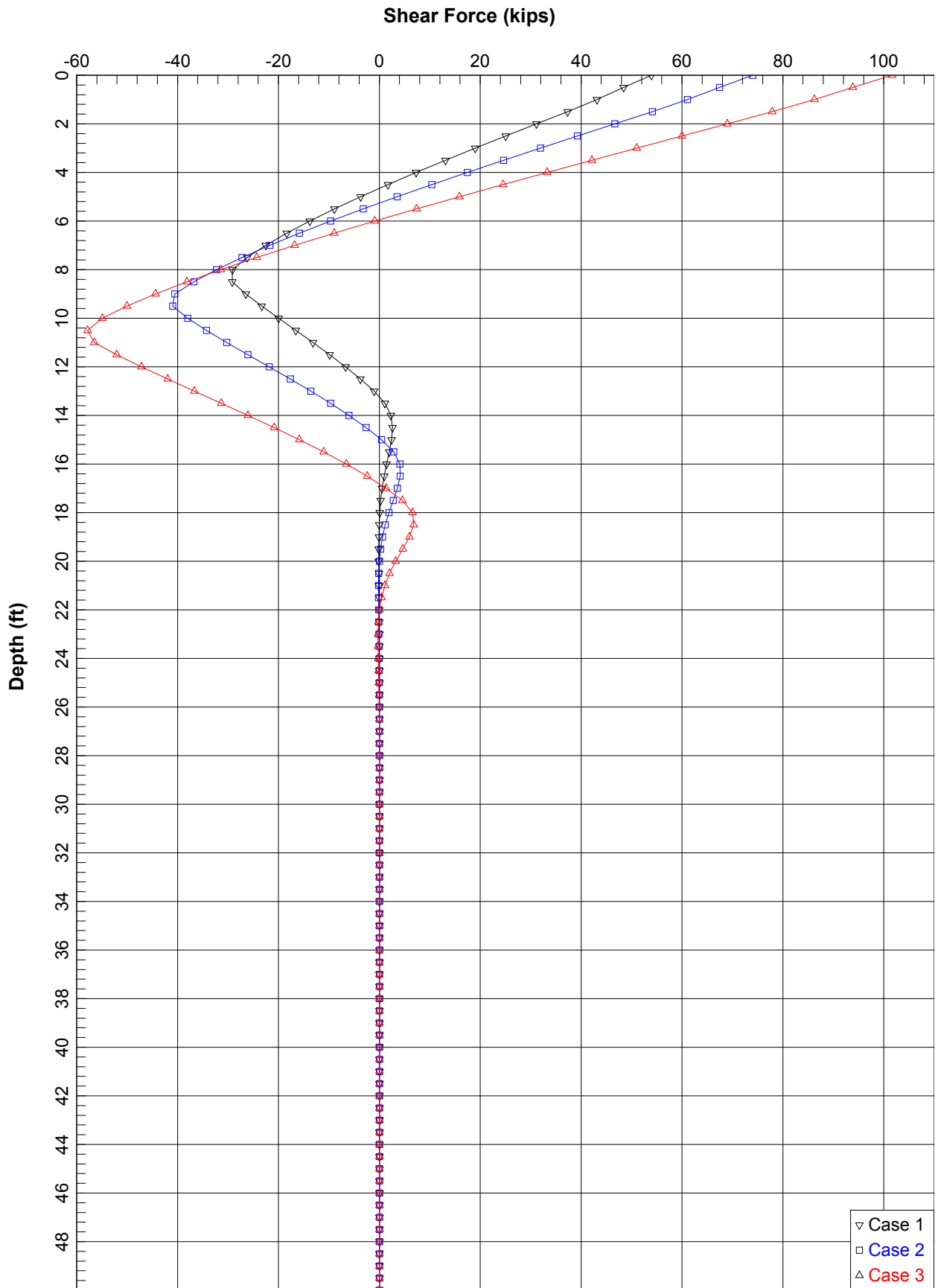
 Summary of Pile Response(s)

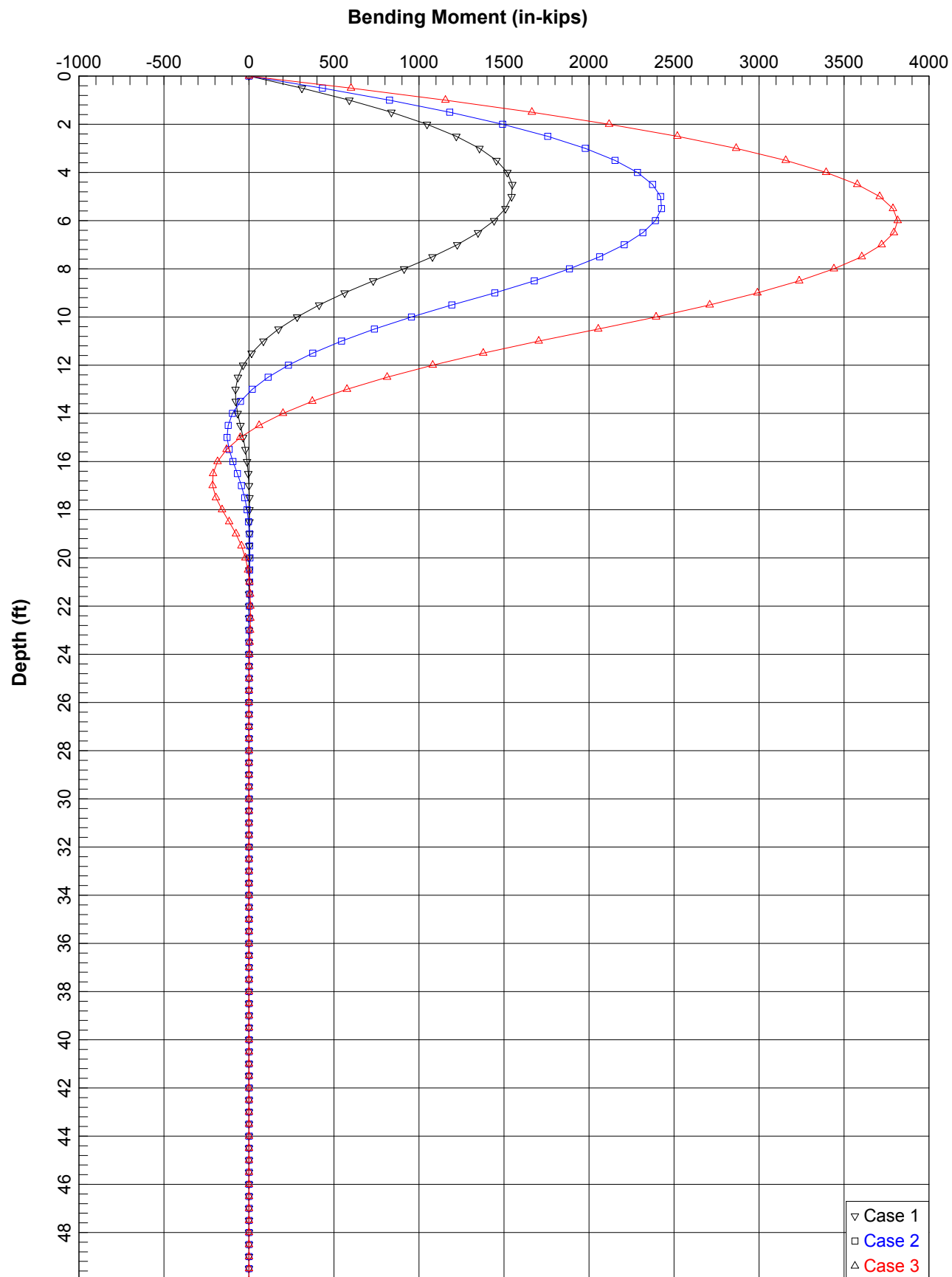
Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	185000.	0.25000000	1320355.	42130.	-0.00391738
2	4	y = 0.5000	M = 0.000	185000.	0.50000000	2071196.	57870.	-0.00694205
3	4	y = 1.0000	M = 0.000	185000.	1.00000000	3252403.	79386.	-0.01227971

The analysis ended normally.





Bent 2R_long_Max P

File Plus for Windows, Version 2012-06-031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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This copy of LPI is licensed to:

gdc
 gdc
 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\athant\Desktop\Updated_ET 9-14-14\Bent 2V
 Name of input data file: Bent 2R_long_Max P.ip6d
 Name of output report file: Bent 2R_long_Max P.ip6o
 Name of plot output file: Bent 2R_long_Max P.ip6p
 Name of runtime message file: Bent 2R_long_Max P.ip6r

Date and Time of Analysis

Date: September 13, 2014 Time: 20:16:14

Problem Title

Project Name: Palo Comado OC Bridge Widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 241inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.000000
2	50.00000	24.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 2R_long_Max P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modeled using 3 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 1.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass	Layer Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Elastic Modulus	Uniaxial Compressive Strength	ROD %	Epsilon
Factor Num.	J (p-y Curve Criteria)	Rock Emass	ft	pcf	psi	deg.	psi	psi	GSI	
50	Factor			Type	Property	Mod.				
1	Stiff Clay w/o Free Water		-5.000	125.000	4500.000	--	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--	--
0.00700	--	--	0.10000	125.000	4500.000	--	--	--	--	--
2	Stiff Clay w/o Free Water		0.10000	125.000	3750.000	--	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--	--
0.00700	--	--	1.000	125.000	3750.000	--	--	--	--	--
3	Stiff Clay w/o Free Water		1.000	125.000	4500.000	--	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.6750	1.0000
2	50.000	0.6750	1.0000

Bent 2R_long_Max P

Load no. Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head loading and pile-head fixity conditions

Number of loads specified = 3

Table with columns: Load No., Load Type, Condition 1, Condition 2, Axial Thrust Force, lbs, Compute Top y vs. Pile Length

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.25000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 185000.000 lbs

Table with columns: Depth X inches, Deflect. Y inches, Bending Moment in-lbs, Shear Force lbs, Slope S radians, Total Stress psi, Bending Stiffness lb-in^2, Soil Res. lb/in, Soil Spr. Es-h lb/inch, Distrib. Lat. Load lb/inch

Bent 2R_long_Max P

Table with columns: Load no. Type, Condition 1, Condition 2, Axial Thrust Force, lbs, Compute Top y vs. Pile Length

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary For Load Case No. 1:

Table with columns: Pile-head deflection, Computed slope at pile head, Maximum bending moment, Maximum shear force, Depth of maximum bending moment, Depth of maximum shear force, Number of iterations, Number of zero deflection points

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.50000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 185000.000 lbs

Table with columns: Depth X inches, Deflect. Y inches, Bending Moment in-lbs, Shear Force lbs, Slope S radians, Total Stress psi, Bending Stiffness lb-in^2, Soil Res. lb/in, Soil Spr. Es-h lb/inch, Distrib. Lat. Load lb/inch

Bent 2R_long_Max P

Depth of maximum shear force = 0.00000 inches below pile head
 Number of iterations = 16
 Number of zero deflection points = 8

 Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

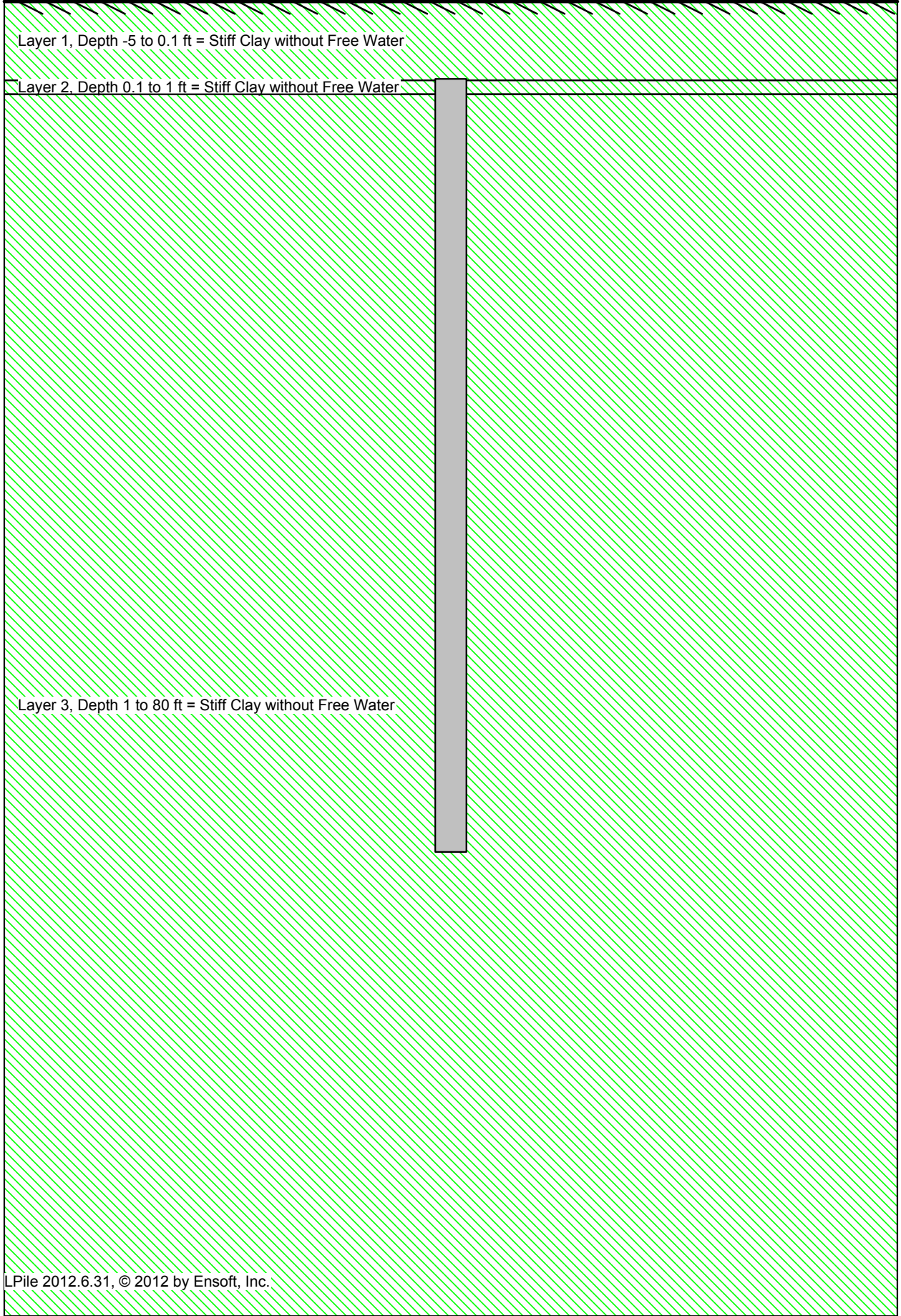
Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	185000.	0.25000000	1548892.	53947.	-0.00424651
2	4	y = 0.5000	M = 0.000	185000.	0.50000000	2425715.	74017.	-0.00750975
3	4	y = 1.0000	M = 0.000	185000.	1.00000000	3815228.	101662.	-0.01331054

The analysis ended normally.

SUPPORT: BENT 2R

LOAD DIRECTION: TRANSVERSE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE

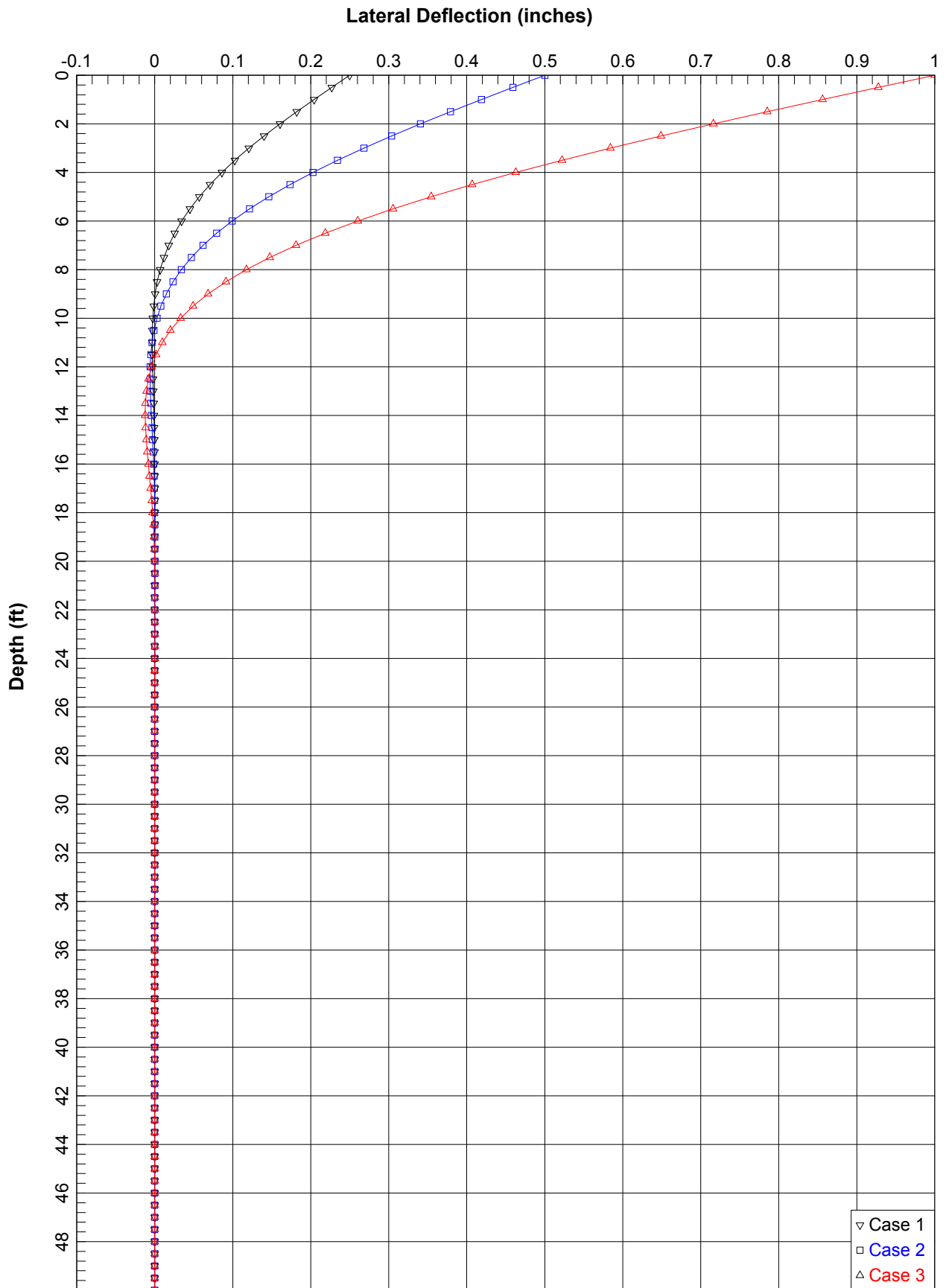


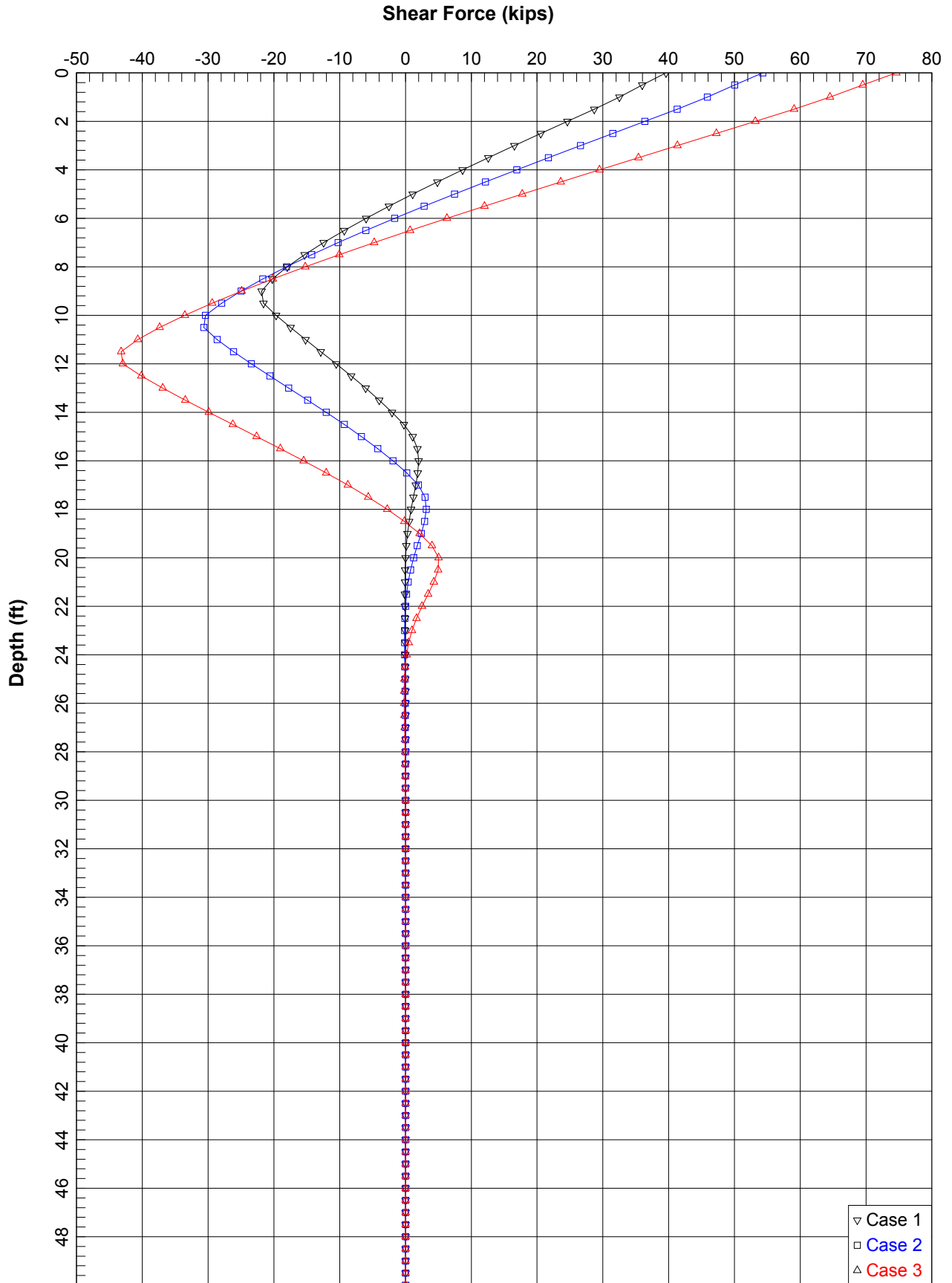
A cross-sectional diagram of a pile foundation. The pile is a vertical grey rectangle extending from the ground surface down to a depth of 80 feet. The soil is divided into three layers, all labeled as 'Stiff Clay without Free Water'. The top layer is from -5 to 0.1 feet depth. The second layer is from 0.1 to 1 foot depth. The third layer is from 1 to 80 feet depth. The entire soil area is filled with a green diagonal hatching pattern. The ground surface is indicated by a horizontal line with a hatched area above it representing the ground above the surface.

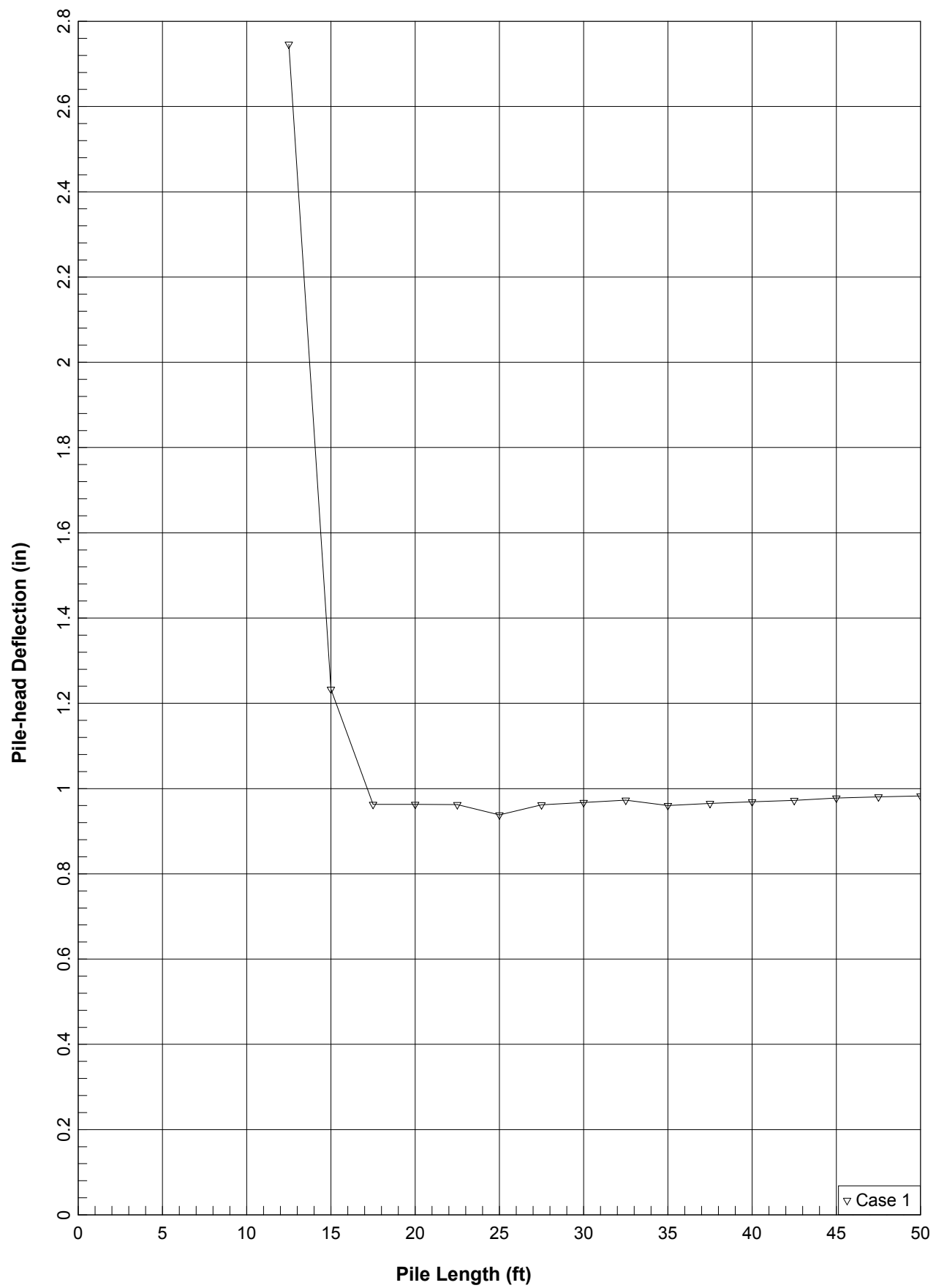
Layer 1, Depth -5 to 0.1 ft = Stiff Clay without Free Water

Layer 2, Depth 0.1 to 1 ft = Stiff Clay without Free Water

Layer 3, Depth 1 to 80 ft = Stiff Clay without Free Water







Bent 2R_transv_crit length

File Plus for Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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This copy of LPI is licensed to:

gdc
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\athant\Desktop\Updated_ET 9-14-14\Bent 2\
 Name of input data file: Bent 2R_transv_crit length.ipd
 Name of output report file: Bent 2R_transv_crit length.ip6
 Name of plot output file: Bent 2R_transv_crit length.ip6p
 Name of runtime message file: Bent 2R_transv_crit length.ip6r

Date and Time of Analysis

Date: September 13, 2014 Time: 20:21:12

Problem Title

Project Name: Palo Comado OC Bridge Widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 241inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.000000
2	50.00000	24.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 2R_transv_crit length
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 3 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 1.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass	Layer Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Elastic Modulus	Uniaxial Compressive Strength	ROD % or GSI	Epsilon
Factor Num. 50	J (p-y Curve Criteria) kpcy pci	Rock Emass psi	ft	pcf	psf	deg.	psi	psi		
1	Stiff Clay w/o Free Water		-5.000	125.000	4500.000	--	--	--	--	--
0.00700	--	--	--	125.000	4500.000	--	--	--	--	--
0.00700	--	--	0.10000	125.000	3750.000	--	--	--	--	--
0.00700	Stiff Clay w/o Free Water		0.10000	125.000	3750.000	--	--	--	--	--
0.00700	--	--	1.000	125.000	3750.000	--	--	--	--	--
0.00700	--	--	1.000	125.000	4500.000	--	--	--	--	--
0.00500	Stiff Clay w/o Free Water		1.000	125.000	4500.000	--	--	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--	--	--
0.00500	--	--	--	125.000	4500.000	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.4400	1.0000
2	50.000	0.4400	1.0000

Bent 2R_transv_crit 1 length

Table with 2 columns: Load Type, Condition 1

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Table with 5 columns: Load No., Load Type, Condition 1, Condition 2, Axial Thrust Force, lbs, Compute Top y vs. Pile Length

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Table with 2 columns: Computed Values of Pile Load and Deflection For Lateral Loading For Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head = 74000.000 lbs
Applied moment at pile head = 0.000 in-lbs
Axial thrust load on pile head = 185000.000 lbs

Table with 11 columns: Depth, y, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Moment, Soil Res., Soil Spr., Distrib. Load

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs

Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians

Bent 2R_transv_crit 1 length

Table with 2 columns: Load Type, Condition 1

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Table with 5 columns: Load No., Load Type, Condition 1, Condition 2, Axial Thrust Force, lbs, Compute Top y vs. Pile Length

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Table with 2 columns: Computed Values of Pile Load and Deflection For Lateral Loading For Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head = 74000.000 lbs
Applied moment at pile head = 0.000 in-lbs
Axial thrust load on pile head = 185000.000 lbs

Table with 11 columns: Depth, y, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Moment, Soil Res., Soil Spr., Distrib. Load

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs

Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary For Load Case No. 1:

Pile-head deflection = 0.9828153 inches
Computed slope at pile head = -0.0118762 radians
Maximum bending moment = 3091864 in-lb
Maximum shear force = 74000 lbs
Depth of maximum bending moment = 78.000000 inches below pile head
Depth of maximum shear force = 0.000000 inches below pile head
Number of iterations = 32
Number of zero deflection points = 7

Pile-head Deflection vs. Pile Length For Load Case 1

Boundary Condition on Type 1, Shear and Moment

Shear = 74000.0 lbs
Moment = 0.0 in-lb
Axial Load = 185000.0 lbs

Table with 4 columns: Pile Length, Pile Head Deflection, Maximum Moment, Maximum Shear

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs

Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians

Bent 2R_transv_crit Length

Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lb/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lb
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lb	Maximum Shear lbs	Pile-head Rotation radians
1	1	V = 74000.	M = 0.000	185000.	0.98281534	3091864.	74000.	-0.01187616

The analysis ended normally.

Bent 2R_transv_ave P

File Plus for Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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Files Used for Analysis

Path to file locations: C:\Users\athant\Desktop\Updated_ET 9-14-14\Bent 2\
 Name of input data file: Bent 2R_transv_ave P.lpd
 Name of output report file: Bent 2R_transv_ave P.lp6
 Name of plot output file: Bent 2R_transv_ave P.lpp
 Name of runtime message file: Bent 2R_transv_ave P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 20:19:13

Problem Title

Project Name: Palo Comado OC Bridge Widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 241inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Long t.-Avg Pm

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.000000
2	50.00000	24.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 2R_transv_ave P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. lbf/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 3 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 1.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass	Layer Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Elastic Modulus	Uniaxial Compressive Strength	ROD % or GSI	Epsilon
Factor Num. 50	J (p-y Curve Criteria)	kpy (psi)	ft	pcf	psi	deg.	psi	psi		
1	Stiff Clay w/o Free Water		-5.000	125.000	4500.000	--	--	--	--	--
0.00700	--	--	--	125.000	4500.000	--	--	--	--	--
0.00700	Stiff Clay w/o Free Water		0.10000	125.000	3750.000	--	--	--	--	--
0.00700	--	--	--	125.000	3750.000	--	--	--	--	--
0.00700	Stiff Clay w/o Free Water		1.000	125.000	4500.000	--	--	--	--	--
0.00500	--	--	--	125.000	4500.000	--	--	--	--	--
0.00500	--	--	--	125.000	4500.000	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.4400	1.0000
2	50.000	0.4400	1.0000

Bent 2R_transv_ave P

Depth of maximum shear force = 0.00000 inches below pile head
 Number of iterations = 21
 Number of zero deflection points = 7

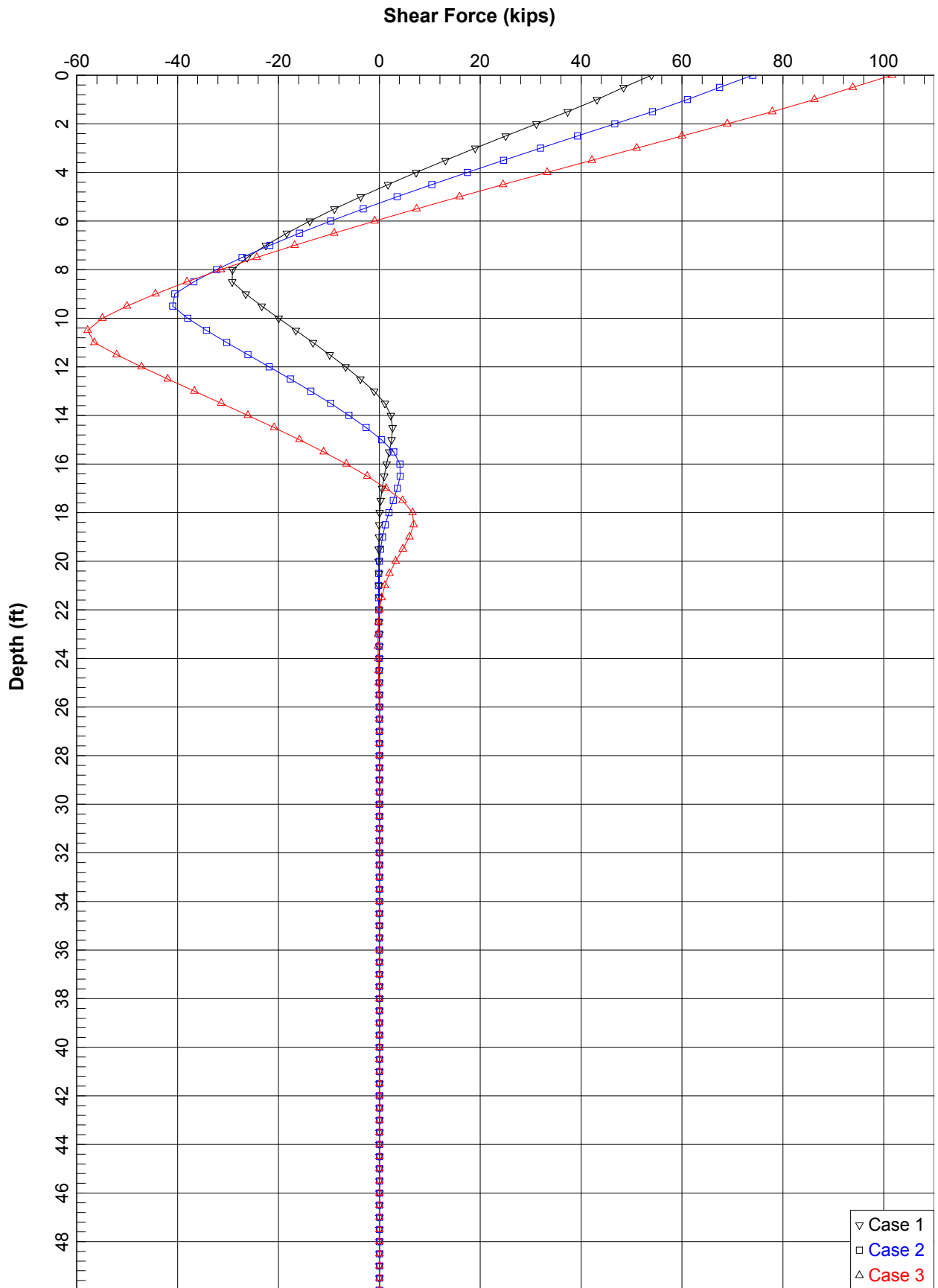
 Summary of Pile Response(s)

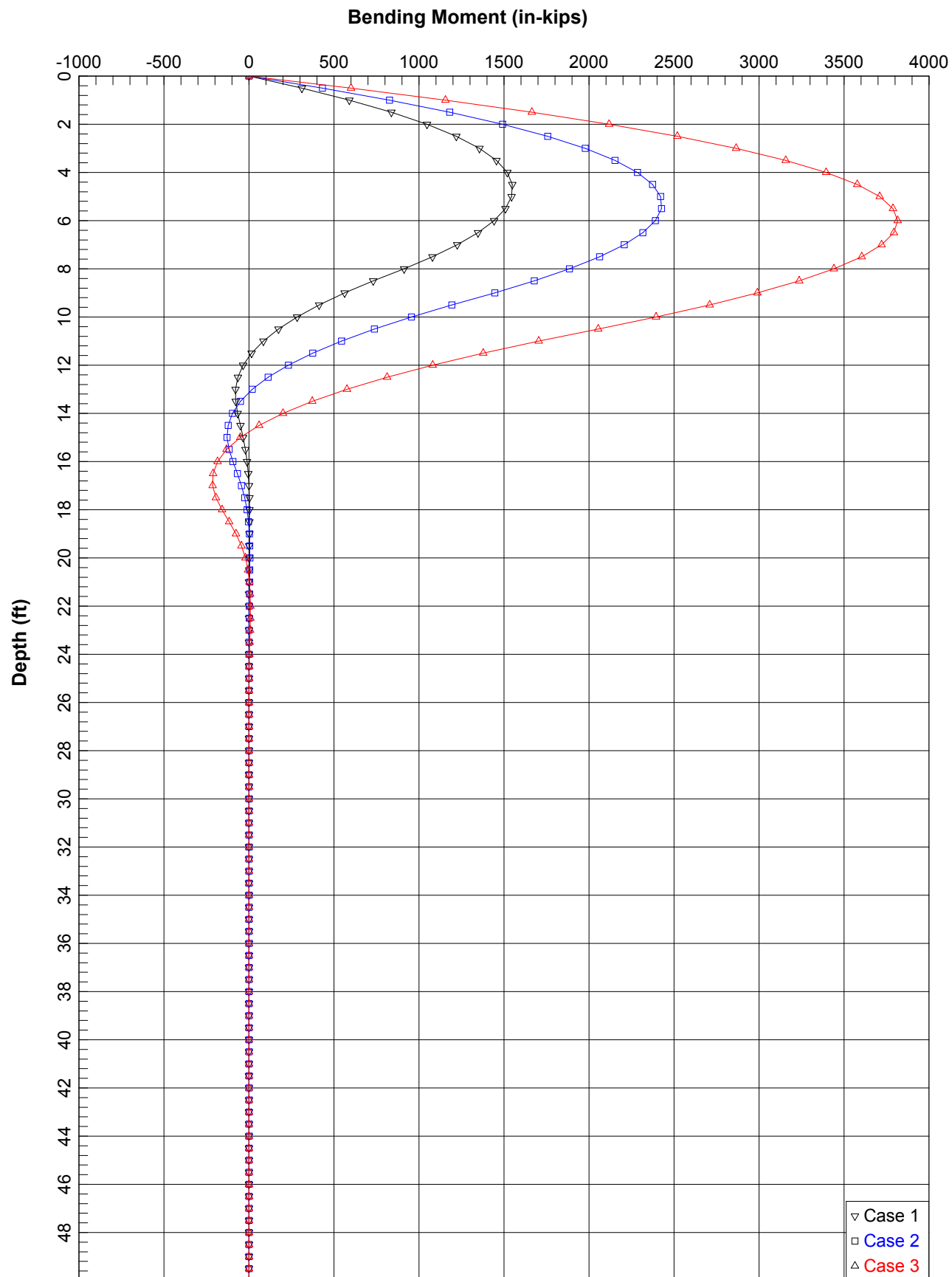
Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	185000.	0.25000000	1267624.	39578.	-0.00384154
2	4	y = 0.5000	M = 0.000	185000.	0.50000000	1988994.	54302.	-0.00679355
3	4	y = 1.0000	M = 0.000	185000.	1.00000000	3126218.	74584.	-0.01204587

The analysis ended normally.





Bent 2R_transv_Max P

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 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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Files Used for Analysis

Path to file locations: C:\Users\athant\Desktop\Updated_ET 9-14-14\Bent 2\
 Name of input data file: Bent 2R_transv_Max P.lpd
 Name of output report file: Bent 2R_transv_Max P.lp6
 Name of plot output file: Bent 2R_transv_Max P.lpp
 Name of runtime message file: Bent 2R_transv_Max P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 20:22:16

Problem Title

Project Name: Palo Comado OC Bridge Widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 241inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Long t.-Avg Pm

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.000000
2	50.00000	24.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 2R_transv_Max P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. lbf/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 3 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 1.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass	Layer Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Elastic Modulus	Uniaxial Compressive Strength	ROD % or GSI	Epsilon
Factor Num. 50	J (p-y Curve Criteria) pci	Rock Emass	ft	pcf	psf	deg.	psi	psi		
1	Stiff Clay w/o Free Water		-5.000	125.000	4500.000	--	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--	--
0.00700	--	--	0.10000	125.000	4500.000	--	--	--	--	--
2	Stiff Clay w/o Free Water		0.10000	125.000	3750.000	--	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--	--
0.00700	--	--	1.000	125.000	3750.000	--	--	--	--	--
3	Stiff Clay w/o Free Water		1.000	125.000	4500.000	--	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.6750	1.0000
2	50.000	0.6750	1.0000

Bent 2R_transv_Max P

Table with 2 columns: Load no, Type. Row 1: 1, y = 0.2500 in. Row 2: 2, y = 0.5000 in. Row 3: 3, y = 1.0000 in.

Static loading criteria were used when computing p-y curves for all analyses.

Number of loads specified = 3

Table with 5 columns: Load No, Load Type, Condition, Condition 2, Axial Thrust Force, lbs. Row 1: 1, 4, y = 0.2500 in, M = 0.0000 in-lbs, 185000, False. Row 2: 2, 4, y = 0.5000 in, M = 0.0000 in-lbs, 185000, False. Row 3: 3, 4, y = 1.0000 in, M = 0.0000 in-lbs, 185000, False.

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = axial thrust stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection For Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.25000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 185000.000 lbs

Main data table for Load Case 1 with columns: Depth, Deflect, Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distri. Lat. Load.

Main data table for Load Case 2 with columns: Depth, Deflect, Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distri. Lat. Load.

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary For Load Case No. 1:

Pile-head deflection = 0.2500000 inches
Computed slope at pile head = -0.002465 radians
Maximum bending moment = 1548892.1 inch-lbs
Maximum shear force = 53947 lbs
Depth of maximum bending moment = 54.000000 inches below pile head
Depth of maximum shear force = 0.000000 inches below pile head
Number of iterations = 18
Number of zero deflection points = 9

Computed Values of Pile Loading and Deflection For Lateral Loading for Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.50000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 185000.000 lbs

Main data table for Load Case 2 with columns: Depth, Deflect, Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distri. Lat. Load.

Bent 2R_transv_Max P

Depth of maximum shear force = 0.00000 inches below pile head
 Number of iterations = 16
 Number of zero deflection points = 8

 Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

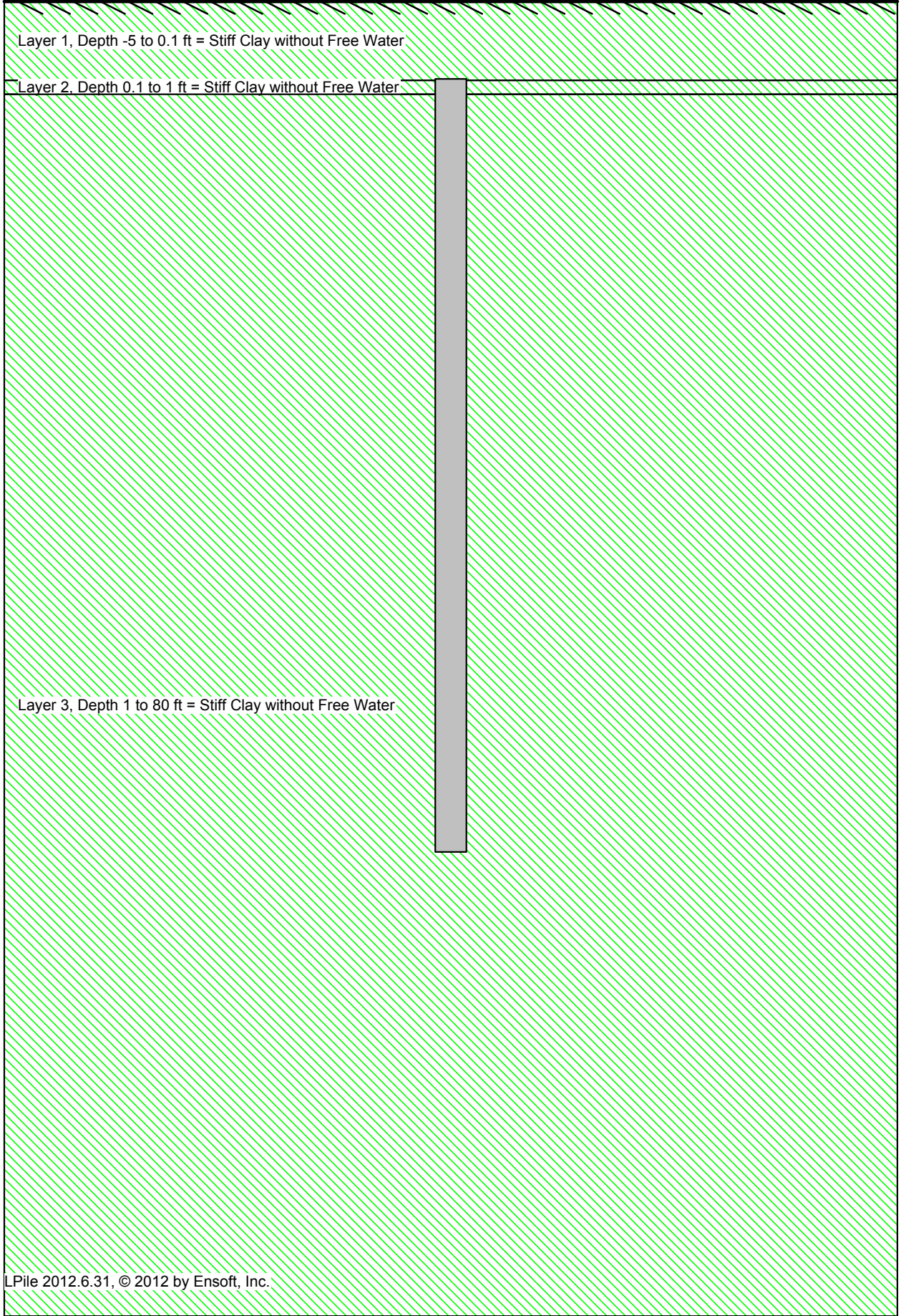
Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	185000.	0.25000000	1548892.	53947.	-0.00424651
2	4	y = 0.5000	M = 0.000	185000.	0.50000000	2425715.	74017.	-0.00750975
3	4	y = 1.0000	M = 0.000	185000.	1.00000000	3815228.	101662.	-0.01331054

The analysis ended normally.

SUPPORT: BENT 2L

LOAD DIRECTION: LONGITUDE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE

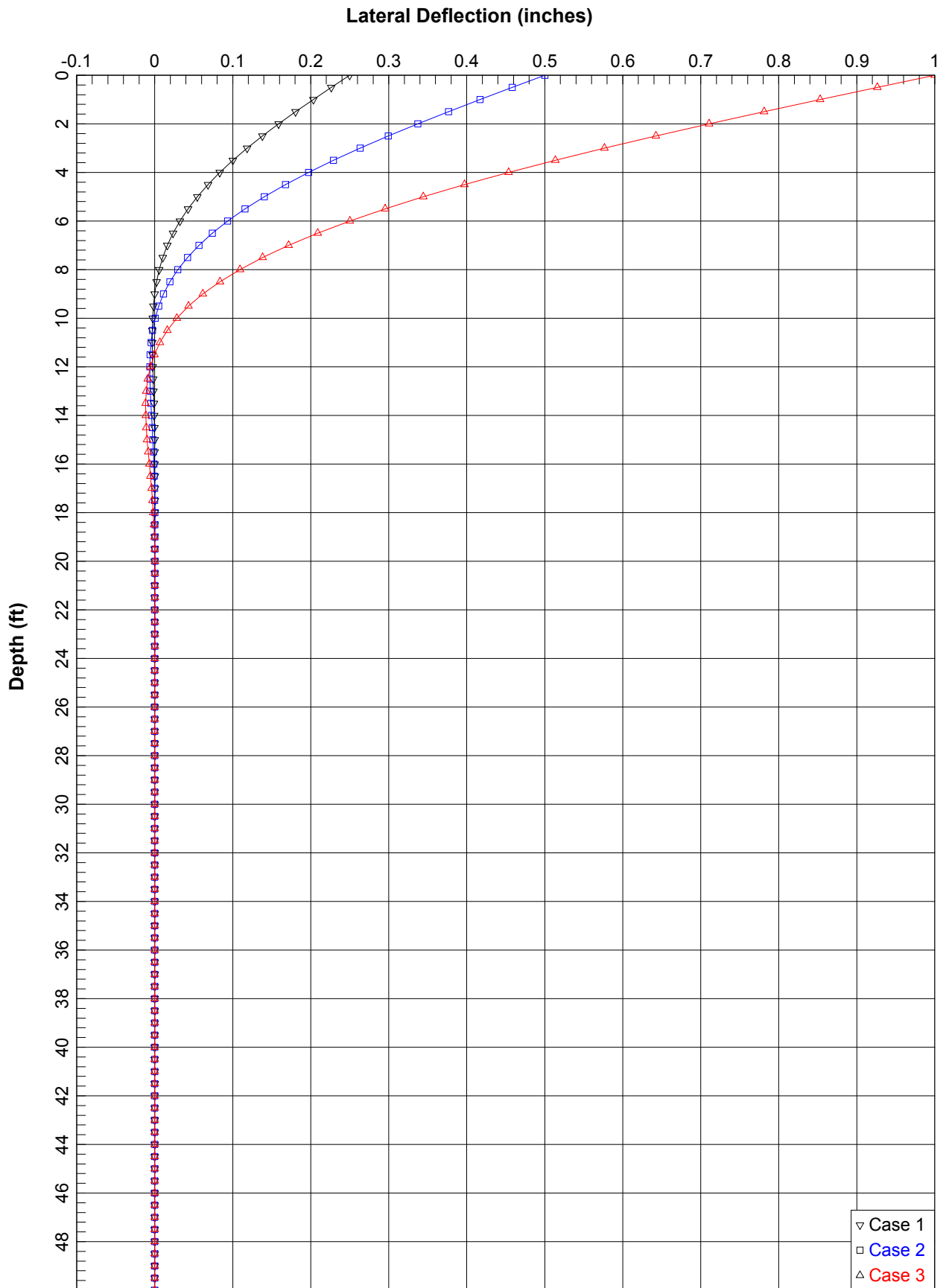


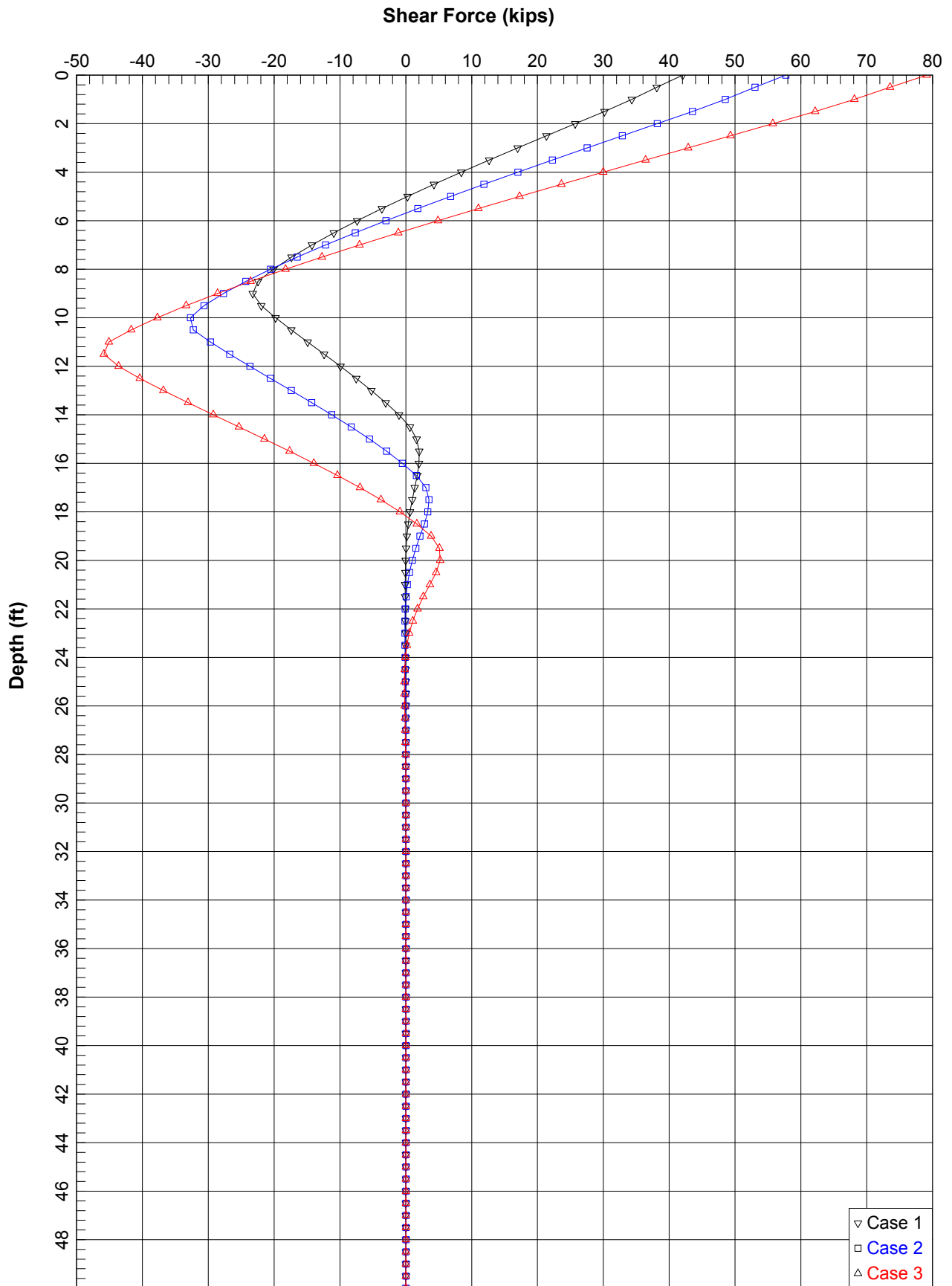
A cross-sectional diagram of a pile foundation. The pile is a vertical grey rectangle extending from the ground surface down to a depth of 80 feet. The soil is divided into three layers, all labeled as 'Stiff Clay without Free Water'. The top layer is from -5 to 0.1 feet depth. The second layer is from 0.1 to 1 foot depth. The third layer is from 1 to 80 feet depth. The entire soil area is filled with a green diagonal hatching pattern. The ground surface is indicated by a horizontal line with a hatched area above it representing the ground above the surface.

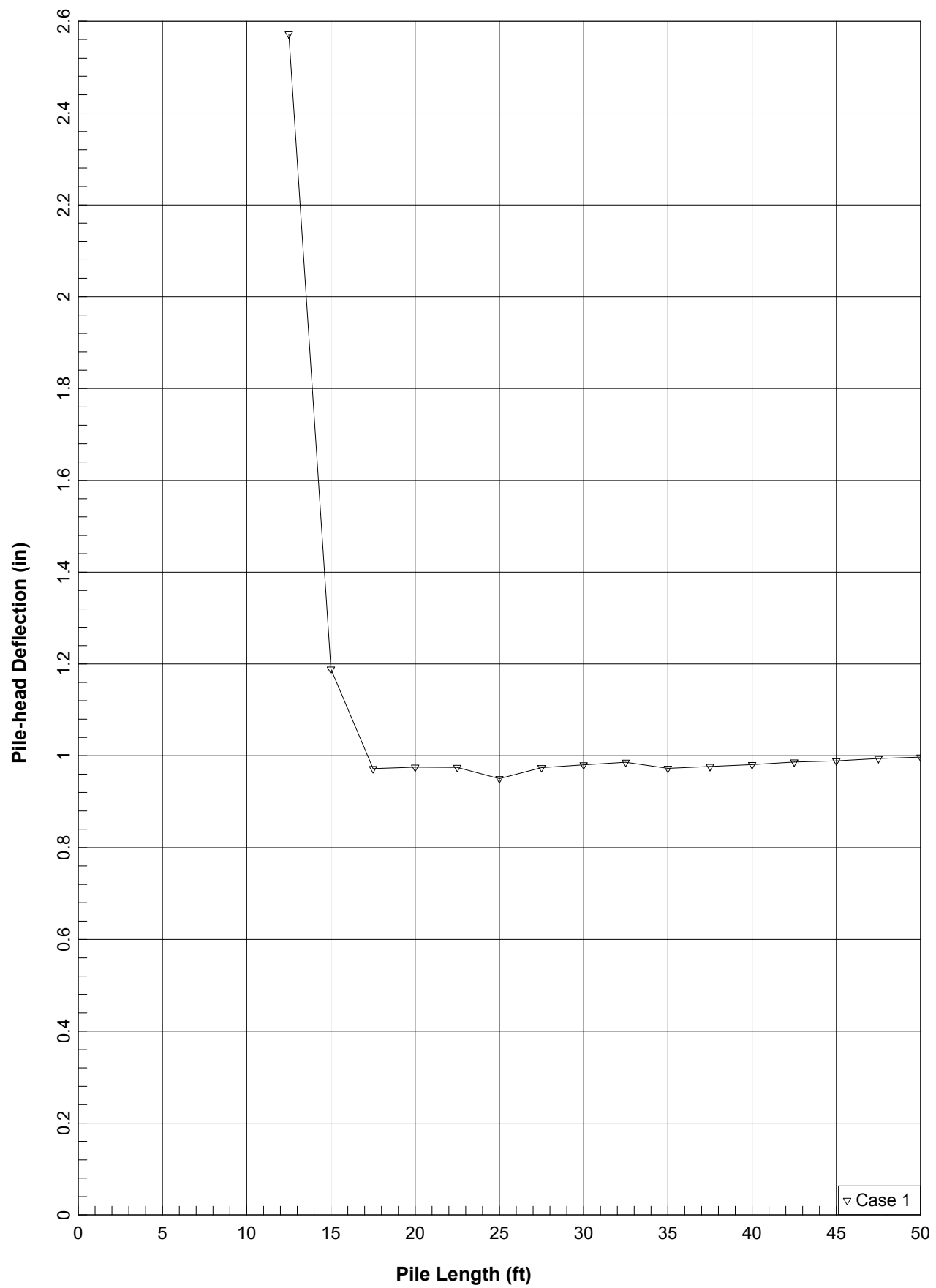
Layer 1, Depth -5 to 0.1 ft = Stiff Clay without Free Water

Layer 2, Depth 0.1 to 1 ft = Stiff Clay without Free Water

Layer 3, Depth 1 to 80 ft = Stiff Clay without Free Water







Bent 2L_long_crit length

File Plus for Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\athant\Desktop\Updated_ET 9-14-14\Bent 2L
 Name of input data file: Bent 2L_long_crit length.lpd
 Name of output report file: Bent 2L_long_crit length.lpr
 Name of plot output file: Bent 2L_long_crit length.lpp
 Name of runtime message file: Bent 2L_long_crit length.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 20:27:17

Problem Title

Project Name: Palo Comado OC Bridge Widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 241inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Long t.-Avg Pm

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.000000
2	50.00000	24.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 2L_long_crit length
 Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modeled using 3 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 1.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass	Layer Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Elastic Modulus	Uniaxial or	ROD %
Factor Num.	J (p-y Curve Criteria)	Rock Emass	ft	pcf	psf	deg.	psi	psi	GSI
50	Factor	psi	ft	Type	Property	Mod.	psi	psi	Epsilon
1	Stiff Clay w/o Free Water	--	-5.000	125.000	4500.000	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--
0.00700	--	--	0.10000	125.000	4500.000	--	--	--	--
2	Stiff Clay w/o Free Water	--	0.10000	125.000	3750.000	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--
0.00700	--	--	1.000	125.000	3750.000	--	--	--	--
3	Stiff Clay w/o Free Water	--	1.000	125.000	4500.000	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.4800	1.0000
2	50.000	0.4800	1.0000

Bent 2L_long_crit length

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Table with 5 columns: Load No., Load Type, Condition 1, Condition 2, Axial Thrust Force, lbs, Compute Top y vs. Pile Length. Row 1: 1, V, 79000. lbs, M = 0.000 in-lbs, 219000., True

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
S = lateral deflection relative to pile axis
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values for Lateral Loading For Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear Force at pile head = 79000.000 lbs
Applied moment at pile head = 0.000 in-lbs
Axial thrust load on pile head = 219000.000 lbs

Table with 10 columns: Depth y inches, Deflect. y inches, Bending Moment in-lbs, Shear Force lbs, Slope radians, Total Stress psi*, Bending Stiffness lb-in^2, Soil Res. lb/in, Soil Spr. lb/inch, Distrib. p lb/inch. Contains 40 rows of data.

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:
Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians

Bent 2L_long_crit length

Table with 10 columns: Depth y inches, Deflect. y inches, Bending Moment in-lbs, Shear Force lbs, Slope radians, Total Stress psi*, Bending Stiffness lb-in^2, Soil Res. lb/in, Soil Spr. lb/inch, Distrib. p lb/inch. Contains 40 rows of data.

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed Forces and moments are within specified convergence limits

Output Summary For Load Case No. 1:

Pile-head deflection = 0.9973184 inches
Computed slope at pile head = -0.0122601 radians
Maxim. bending moment = 3251312 in-lb
Maxim. shear force = 79000 lbs
Depth of maximum bending moment = 78.000000 inches below pile head
Depth of maximum shear force = 0.000000 inches below pile head
Number of iterations = 32
Number of zero deflection points = 7

Pile-head Deflection vs. Pile Length For Load Case 1

Boundary Condition on Type 1, Shear and Moment

Shear = 79000. lbs
Moment = 0 in-lbs
Axial Load = 219000. lbs

Table with 4 columns: Pile Length Feet, Pile Head Deflection Inches, Maximum Moment in-lbs, Maximum Shear lbs. Contains 15 rows of data.

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:
Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians

Bent 2L Long_cri t length

Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lb/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lb
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lb	Maximum Shear lbs	Pile-head Rotation radians
1	1	V = 79000.	M = 0.000	219000.	0.99731839	3251312.	79000.	-0.01226011

The analysis ended normally.

Bent 2L_long_ave P

File Plus for Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\athant\Desktop\Updated_ET 9-14-14\Bent 2L
 Name of input data file: Bent 2L_long_ave P.ipd
 Name of output report file: Bent 2L_long_ave P.ip60
 Name of plot output file: Bent 2L_long_ave P.ip6p
 Name of runtime message file: Bent 2L_long_ave P.ip6r

Date and Time of Analysis

Date: September 13, 2014 Time: 20:24:50

Problem Title

Project Name: Palo Comado OC Bridge Widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 241inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.000000
2	50.00000	24.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 2L_long_ave P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modeled using 3 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 1.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass	Layer Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Elastic Modulus	Uniaxial or	ROD %	Epsilon
Factor Num.	J (p-y Curve Criteria)	Rock Emass	ft	pcf	psi	deg.	psi	psi	GSI	
50	Factor			Type	Property	Mod.				
1	Stiff Clay w/o Free Water		-5.000	125.000	4500.000	--	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--	--
0.00700	--	--	0.10000	125.000	4500.000	--	--	--	--	--
2	Stiff Clay w/o Free Water		0.10000	125.000	3750.000	--	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--	--
0.00700	--	--	1.000	125.000	3750.000	--	--	--	--	--
3	Stiff Clay w/o Free Water		1.000	125.000	4500.000	--	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.4800	1.0000
2	50.000	0.4800	1.0000

Bent 2L_long_ave P

Table with 3 columns: Load no., Load Type, and Condition. It lists three load cases for static loading criteria.

Static loading criteria were used when computing p-y curves for all analyses.

Number of loads specified = 3

Table with 5 columns: Load No., Load Type, Condition, Axial Thrust Force, lbs., and Compute Top y vs. Pile Length. It details the three load cases.

V = perpendicular shear force applied to pile head

M = bending moment applied to pile head

y = lateral deflection relative to pile axis

S = pile slope relative to original pile batter angle

R = rotational stiffness applied to pile head

Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nonlinear Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection

For Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.250000 inches

Moment at pile head = 0.000000 inches-lbs

Axial load at pile head = 219000.000 lbs

Large data table with columns: Depth (inches), Deflect. (inches), Bending Moment (in-lbs), Shear Force (lbs), Slope (rad), Total Stress (psi), Bending Stiffness (lb-in^2), Soil Res. (lb/in), Soil Spt. (lb/inch), Distri. Lat. Load (lb/inch). It lists results for 100 depth intervals.

Bent 2L_long_ave P

Table with 4 columns: Load no., Load Type, Condition, and Compute Top y vs. Pile Length. It lists three load cases for static loading criteria.

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Summary table for Load Case No. 1 with 2 columns: Description and Value. It lists maximum deflection, slope, moment, shear force, bending moment, and iterations.

Computed Values of Pile Loading and Deflection

For Lateral Loading for Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.500000 inches

Moment at pile head = 0.000000 inches-lbs

Axial load at pile head = 219000.000 lbs

Large data table with columns: Depth (inches), Deflect. (inches), Bending Moment (in-lbs), Shear Force (lbs), Slope (rad), Total Stress (psi), Bending Stiffness (lb-in^2), Soil Res. (lb/in), Soil Spt. (lb/inch), Distri. Lat. Load (lb/inch). It lists results for 100 depth intervals.

Bent 2L_long_ave P

Depth of maximum shear force = 0.00000 inches below pile head
 Number of iterations = 21
 Number of zero deflection points = 7

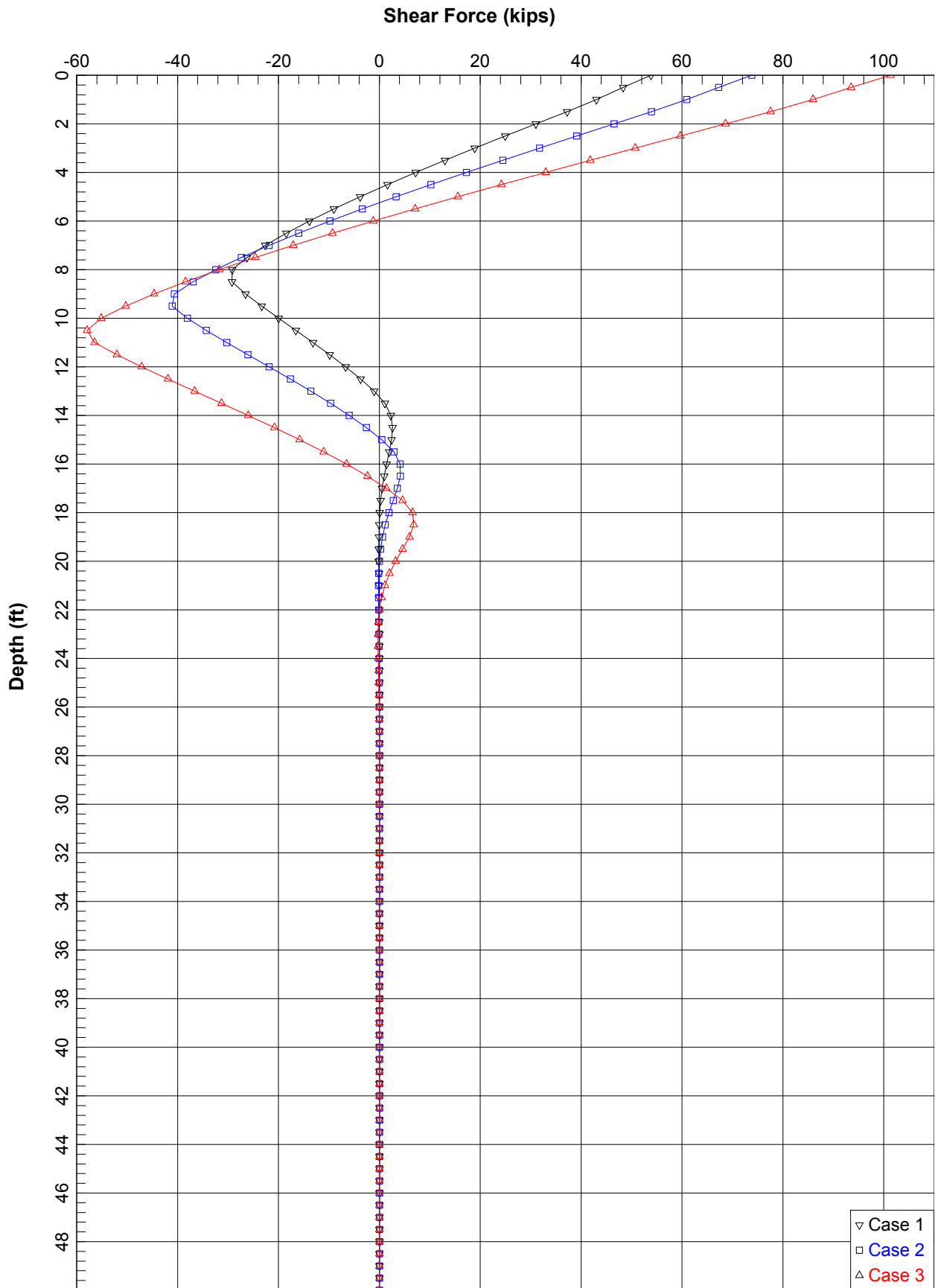
 Summary of Pile Response(s)

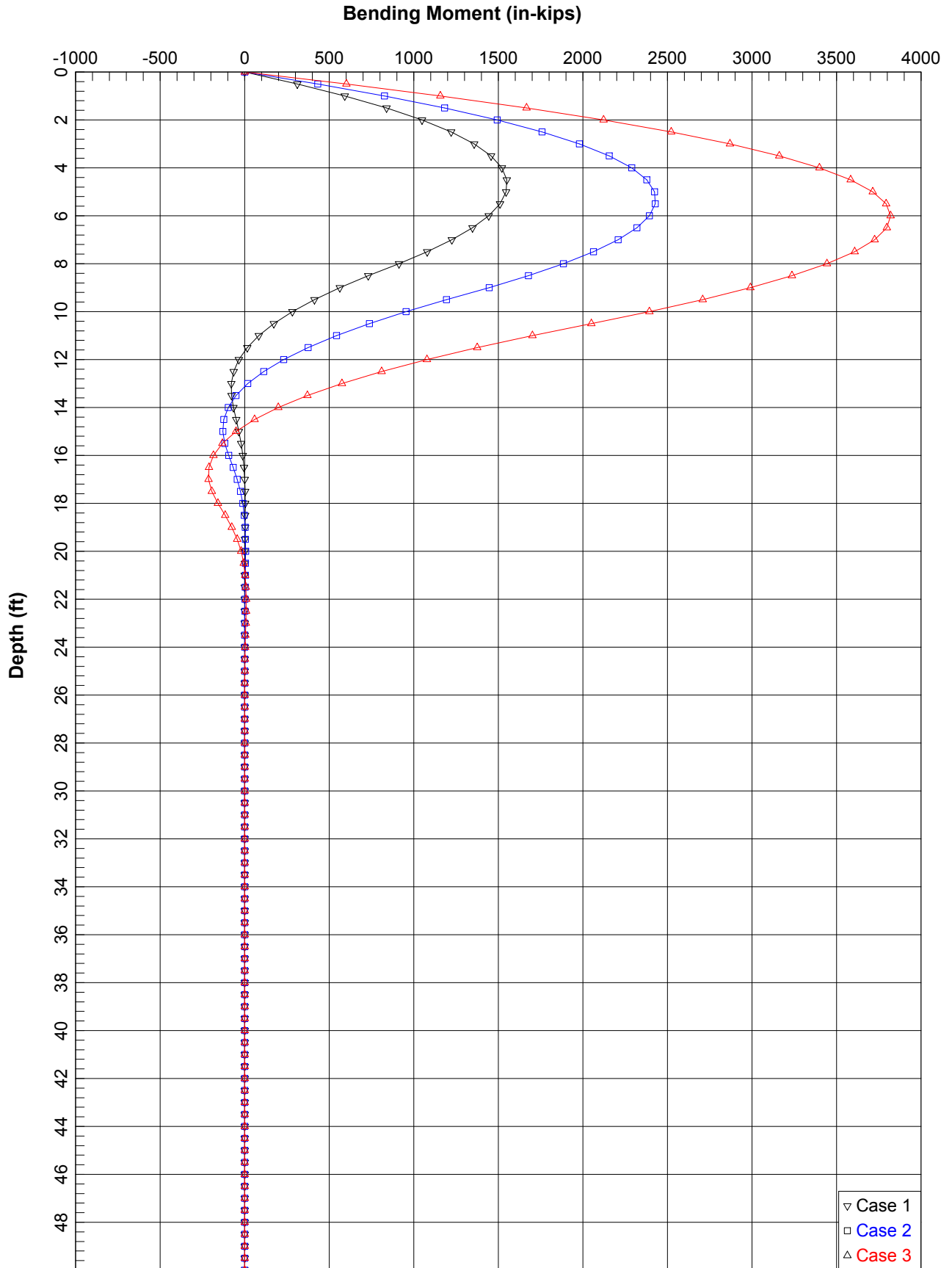
Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	219000.	0.25000000	1321609.	42039.	-0.00391912
2	4	y = 0.5000	M = 0.000	219000.	0.50000000	2073544.	57708.	-0.00694597
3	4	y = 1.0000	M = 0.000	219000.	1.00000000	3257122.	79098.	-0.01228776

The analysis ended normally.





Bent 2L_long_Max P

File Plus for Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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gdc
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\athant\Desktop\Updated_ET 9-14-14\Bent 2L
 Name of input data file: Bent 2L_long_Max P.ip6d
 Name of output report file: Bent 2L_long_Max P.ip6o
 Name of plot output file: Bent 2L_long_Max P.ip6p
 Name of runtime message file: Bent 2L_long_Max P.ip6r

Date and Time of Analysis

Date: September 13, 2014 Time: 20:28:48

Problem Title

Project Name: Palo Comado OC Bridge Widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 241inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Long t.-Avg Pm

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.000000
2	50.00000	24.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 2L_long_Max P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. lbf/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modeled using 3 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 1.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass	Layer Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Elastic Modulus	Uniaxial Compressive Strength	ROD %
Factor Num.	J (p-y Curve Criteria)	Rock Emass	ft	pcf	psi	deg.	psi	psi	GSI
50	Factor	psi	ft	Type	Property	Mod.	psi	psi	Epsilon
1	Stiff Clay w/o Free Water	--	-5.000	125.000	4500.000	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--
0.00700	--	--	0.10000	125.000	4500.000	--	--	--	--
2	Stiff Clay w/o Free Water	--	0.10000	125.000	3750.000	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--
0.00700	--	--	1.000	125.000	3750.000	--	--	--	--
3	Stiff Clay w/o Free Water	--	1.000	125.000	4500.000	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.6750	1.0000
2	50.000	0.6750	1.0000

Bent 2L_long_Max P

Loadng Type

Loadng Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Table with columns: Load No., Load Type, Condition 1, Condition 2, Axial Thrust Force, lbs, Compute Top y vs. Pile Length

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection
For Lateral Loading For Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement at pile head = 0.25000 inches
Moment at pile head = 0.00000 in-lbs
Axial load at pile head = 219000.000 lbs

Table with columns: Depth, Defl ect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distri b. Lat. Load

Bent 2L_long_Max P

Table with columns: Load No., Load Type, Condition 1, Condition 2, Axial Thrust Force, lbs, Compute Top y vs. Pile Length

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed Forces and Moments are within specified convergence limits.

Output Summary For Load Case No. 1:

Table with columns: Pile-head deflection, Computed slope at pile head, Maximum bending moment, Maximum shear force, Depth of maximum bending moment, Depth of maximum shear force, Number of iterations, Number of zero deflection points

Computed Values of Pile Loading and Deflection
For Lateral Loading For Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement at pile head = 0.50000 inches
Moment at pile head = 0.00000 in-lbs
Axial load at pile head = 219000.000 lbs

Table with columns: Depth, Defl ect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distri b. Lat. Load

Bent 2L_long_Max P

Depth of maximum shear force = 0.00000 inches below pile head
 Number of iterations = 17
 Number of zero deflection points = 8

 Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

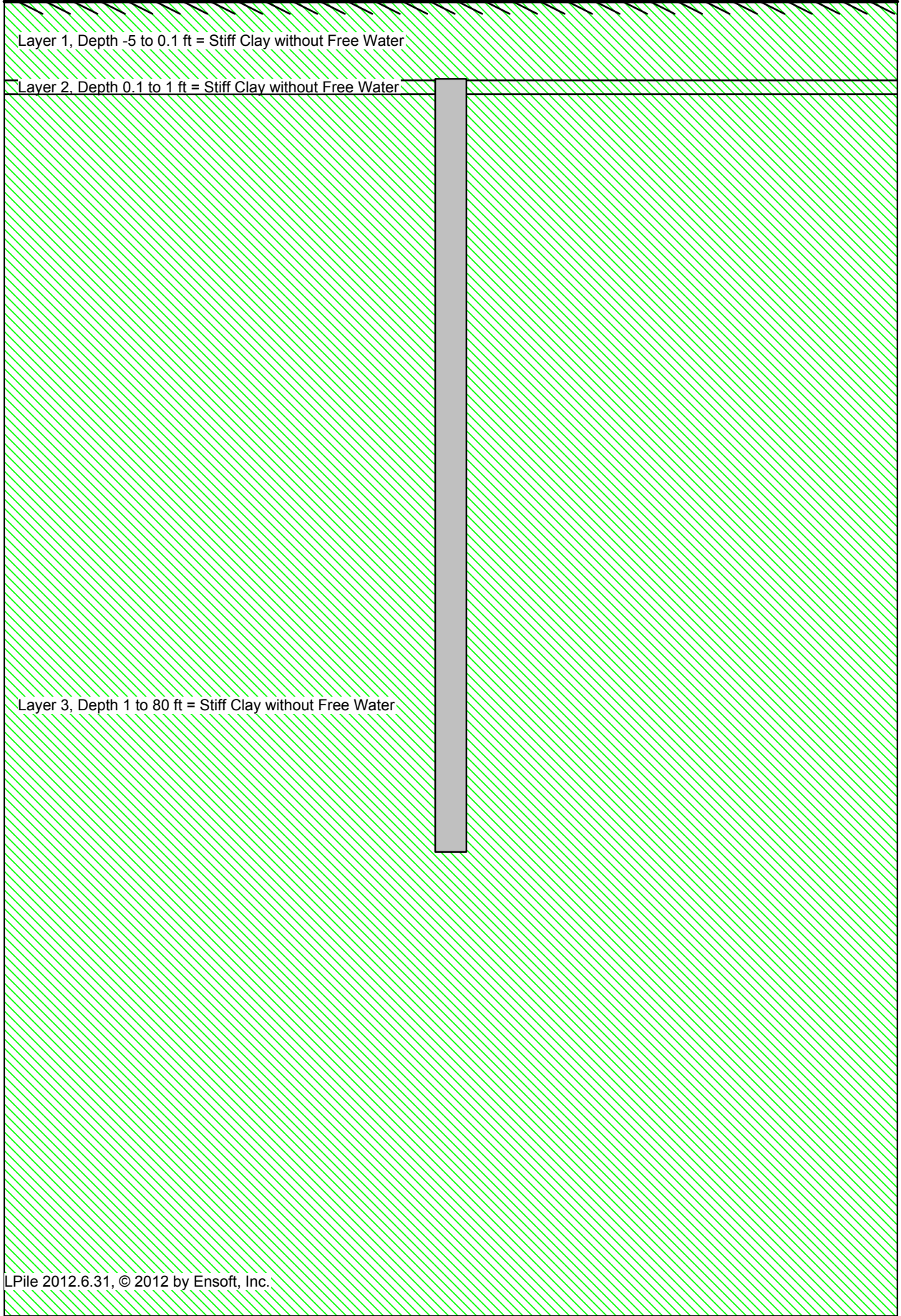
Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	219000.	0.25000000	1550296.	53850.	-0.00424842
2	4	y = 0.5000	M = 0.000	219000.	0.50000000	2428363.	73845.	-0.00751395
3	4	y = 1.0000	M = 0.000	219000.	1.00000000	3819816.	101348.	-0.01331774

The analysis ended normally.

SUPPORT: BENT 2L

LOAD DIRECTION: TRANSVERSE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE

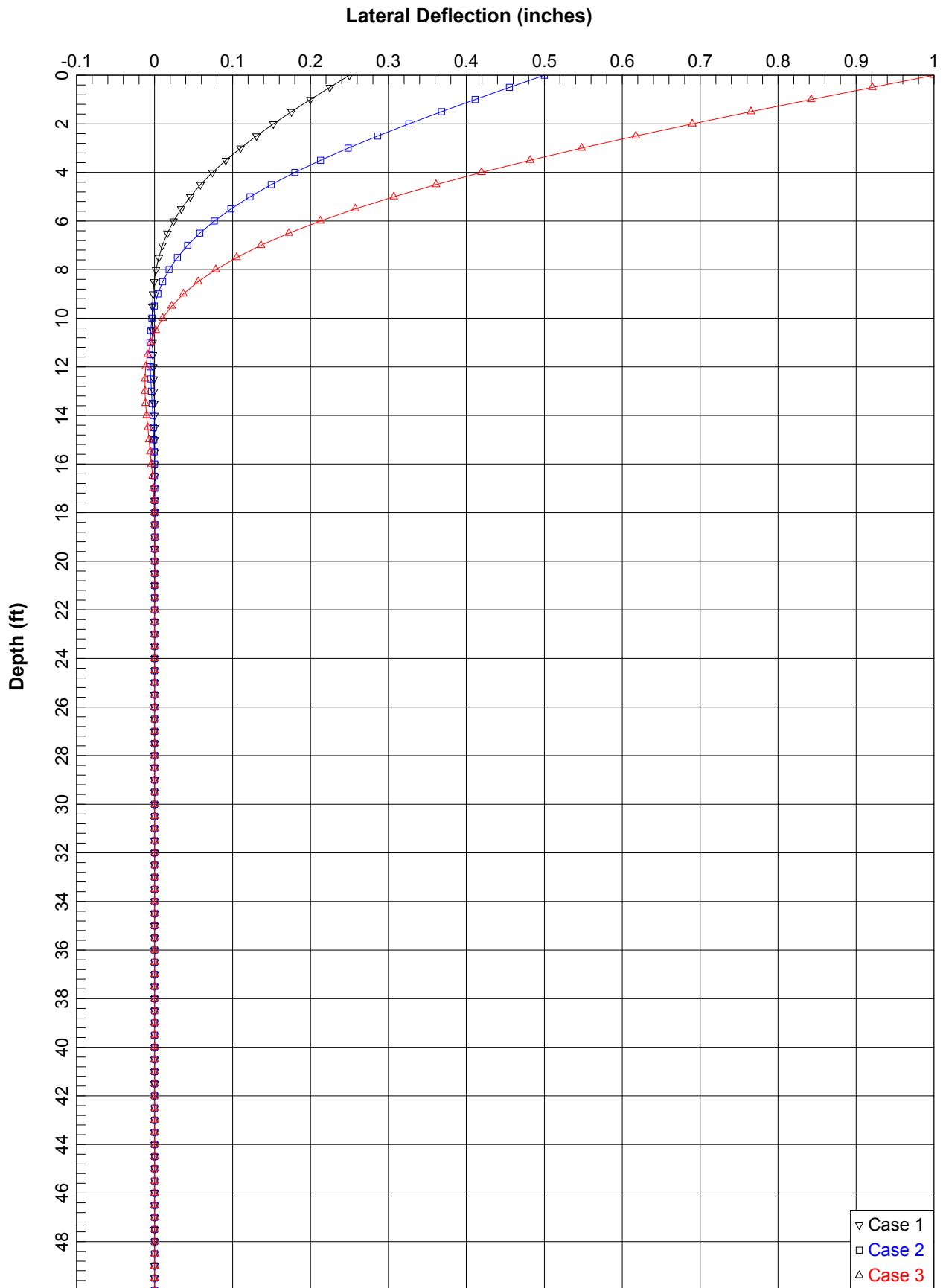


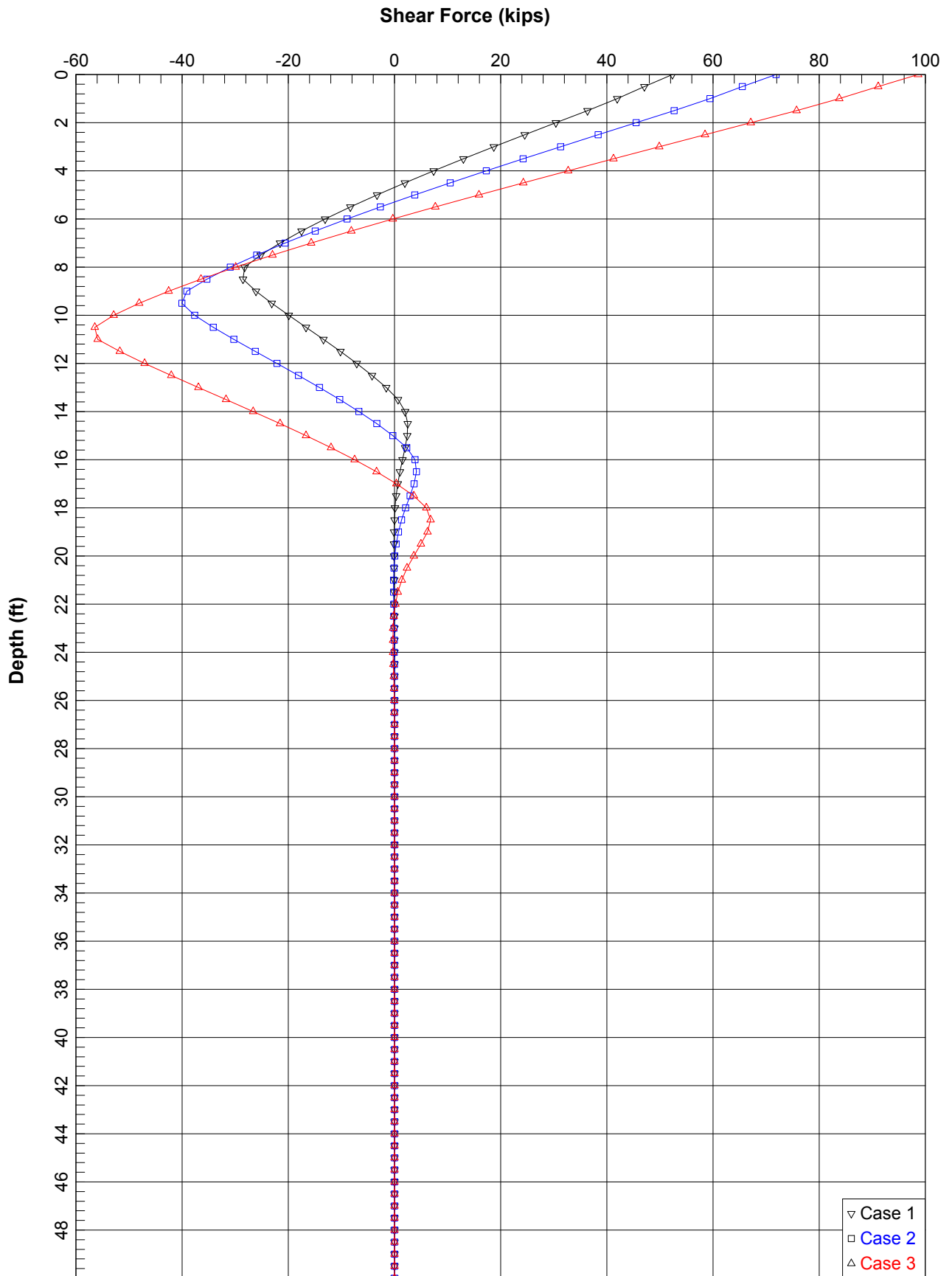
A cross-sectional diagram of a pile foundation. The pile is a vertical grey rectangle extending from the ground surface down to a depth of 80 feet. The soil is divided into three layers, all labeled as 'Stiff Clay without Free Water'. The top layer is from -5 to 0.1 feet depth. The second layer is from 0.1 to 1 foot depth. The third layer is from 1 to 80 feet depth. The entire soil area is filled with a green diagonal hatching pattern. The ground surface is indicated by a horizontal line with a hatched area above it representing the ground above the surface.

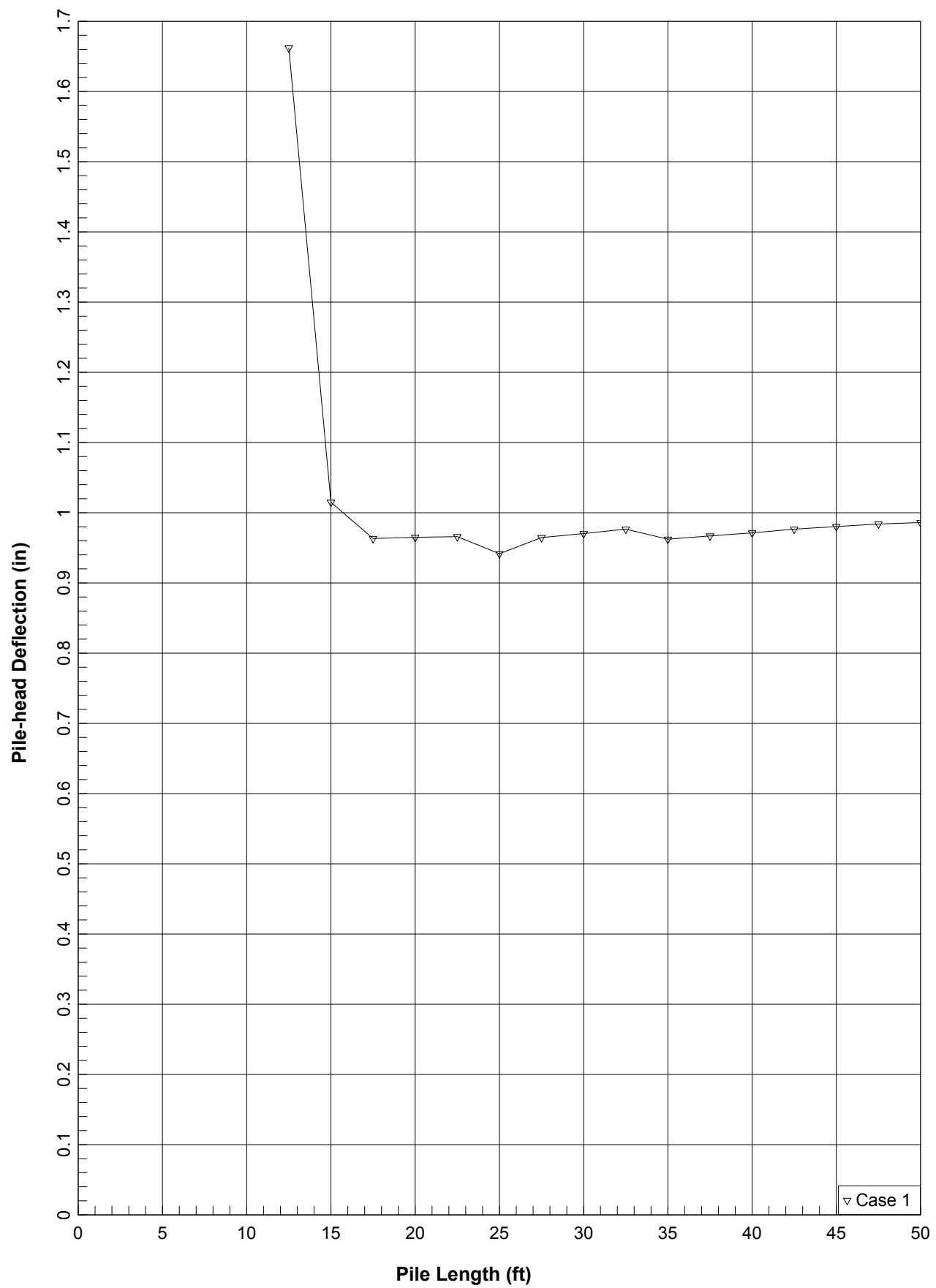
Layer 1, Depth -5 to 0.1 ft = Stiff Clay without Free Water

Layer 2, Depth 0.1 to 1 ft = Stiff Clay without Free Water

Layer 3, Depth 1 to 80 ft = Stiff Clay without Free Water







Bent 2L_transv_crit length

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 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\athant\Desktop\Updated_ET 9-14-14\Bent 2\
 Name of input data file: Bent 2L_transv_crit length.ipd
 Name of output report file: Bent 2L_transv_crit length.ip60
 Name of plot output file: Bent 2L_transv_crit length.ip6p
 Name of runtime message file: Bent 2L_transv_crit length.ip6r

Date and Time of Analysis

Date: September 13, 2014 Time: 20:33:42

Problem Title

Project Name: Palo Comado OC Bridge Widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 241inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.000000
2	50.00000	24.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 2L_transv_crit length
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modeled using 3 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 1.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass	Layer Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Elastic Modulus	Uniaxial Compressive Strength	ROD % or GSI	Epsilon
Factor Num. 50	J (p-y Curve Criteria)	Rock Emass	ft	pcf	psi	deg.	psi	psi		
1	Stiff Clay w/o Free Water		-5.000	125.000	4500.000	--	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--	--
0.00700	--	--	0.10000	125.000	4500.000	--	--	--	--	--
2	Stiff Clay w/o Free Water		0.10000	125.000	3750.000	--	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--	--
0.00700	--	--	1.000	125.000	3750.000	--	--	--	--	--
3	Stiff Clay w/o Free Water		1.000	125.000	4500.000	--	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.6500	1.0000
2	50.000	0.6500	1.0000

Bent 2L_transv_crit 1 length

Table with 2 columns: Load Type, Condition

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Table with 5 columns: Load No., Load Type, Condition, Condition 2, Axial Thrust Force, lbs, Compute Top y vs. Pile Length

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Table with 2 columns: Computed Values, Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Table with 2 columns: Shear Force at pile head, Applied moment at pile head, Axial thrust load on pile head

Main table with columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stress, Soil Res., Soil Spr., Distrib. p, Lat. Load

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs

Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians

Main table with columns: Bent 2L_transv_crit 1 length, Bent 2L_transv_crit 1 length

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed Forces and moments are within specified convergence limits.

Table with 2 columns: Output Summary For Load Case No. 1, Values

Pile-head Deflection vs. Pile Length For Load Case 1

Boundary Condition on Type 1, Shear and Moment

Table with 2 columns: Shear, Moment, Axial Load

Table with 4 columns: Pile Length, Pile Head Deflection, Maximum Moment, Maximum Shear

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs

Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians

Bent 2L_transv_crit Length

Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lb/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lb
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lb	Maximum Shear lbs	Pile-head Rotation radians
1	1	V = 98000.	M = 0.000	219000.	0.98595487	3720564.	98000.	-0.01305263

The analysis ended normally.

Bent 2L_transv_ave P

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 Analysis of Individual Piles and Drilled Shafts
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Files Used for Analysis

Path to file locations: C:\Users\athant\Desktop\Updated_ET 9-14-14\Bent 2\
 Name of input data file: Bent 2L_transv_ave P.lpd
 Name of output report file: Bent 2L_transv_ave P.lp6
 Name of plot output file: Bent 2L_transv_ave P.lpp
 Name of runtime message file: Bent 2L_transv_ave P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 20:32:14

Problem Title

Project Name: Palo Comado OC Bridge Widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 241inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Long t.-Avg Pm

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.000000
2	50.00000	24.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 2L_transv_ave P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. lbf/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 3 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 1.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass	Layer Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Elastic Modulus	Uniaxial Compressive Strength	ROD %
Factor Num. 50	J (p-y Curve Criteria)	Rock Emass	ft	pcf	psi	deg.	psi	psi	GSI
1	Stiff Clay w/o Free Water		-5.000	125.000	4500.000	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--
0.00700	--	--	0.10000	125.000	4500.000	--	--	--	--
0.00700	Stiff Clay w/o Free Water		0.10000	125.000	3750.000	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--
0.00700	--	--	1.000	125.000	3750.000	--	--	--	--
0.00700	Stiff Clay w/o Free Water		1.000	125.000	4500.000	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.6500	1.0000
2	50.000	0.6500	1.0000

Bent 2L_transv_ave P

Table with 2 columns: Loading Type, Condition 1, Condition 2

Static loading criteria was used when computing p-y curves for all analyses.

Number of loads specified = 3

Table with 5 columns: Load No., Load Type, Condition 1, Condition 2, Axial Thrust Force, lbs, Compute Top y vs. Pile Length

V = perpendicular shear force applied to pile head

M = bending moment applied to pile head

y = lateral deflection relative to pile axis

S = pile slope relative to original pile batter angle

R = rotational stiffness applied to pile head

Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement at pile head = 0.250000 inches

Moment at pile head = 0.000000 in-lbs

Axial load at pile head = 219000.000 lbs

Large table with columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distri. Lat. Load

Page 3

Bent 2L_transv_ave P

Table with 5 columns: Load No., Load Type, Condition 1, Condition 2, Axial Thrust Force, lbs, Compute Top y vs. Pile Length

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary For Load Case No. 1:

Table with 2 columns: Parameter, Value

Computed Values of Pile Loading and Deflection

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement at pile head = 0.500000 inches

Moment at pile head = 0.000000 in-lbs

Axial load at pile head = 219000.000 lbs

Large table with columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distri. Lat. Load

Page 4

Table with columns for numerical values and labels, including 'Bent 2L_transv_ave P' and various coordinate pairs.

Table with columns for numerical values and labels, including 'Bent 2L_transv_ave P' and various coordinate pairs.

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within spec'ified convergence limits.

Output Summary For Load Case No. 2: Table with columns for Pile-head deflection, Computed slope at pile head, Maximum bending moment, etc.

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 3

Table with columns for Pile-head conditions are Displacement and Moment (Loading Type 4), Displacement of pile head, Moment at pile head, Axial load at pile head.

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within spec'ified convergence limits.

Output Summary For Load Case No. 3: Table with columns for Pile-head deflection, Computed slope at pile head, Maximum bending moment, etc.

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 3

Table with columns for Pile-head conditions are Displacement and Moment (Loading Type 4), Displacement of pile head, Moment at pile head, Axial load at pile head.

Bent 2L_transv_ave P

Depth of maximum shear force = 0.00000 inches below pile head
 Number of iterations = 21
 Number of zero deflection points = 8

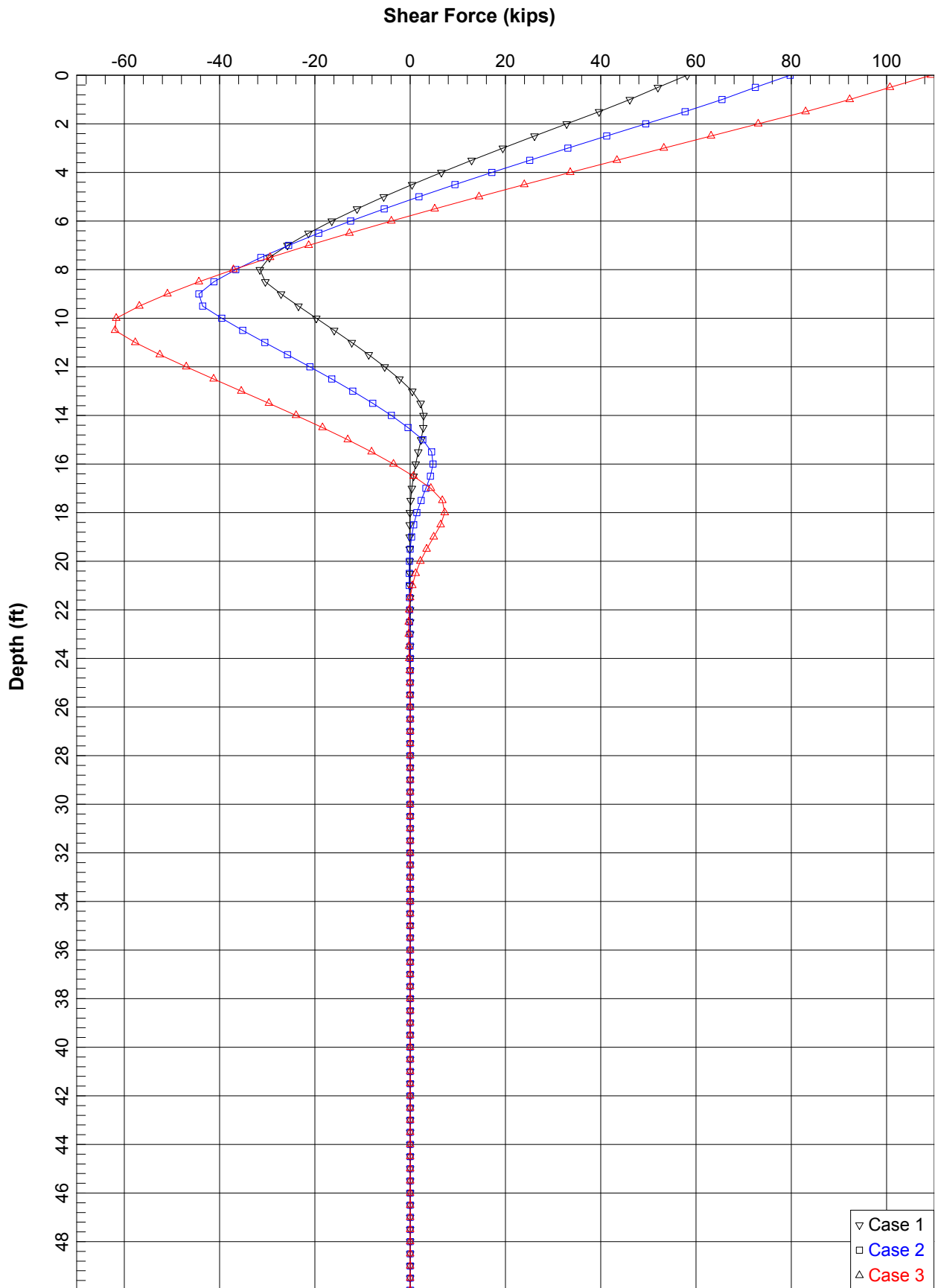
 Summary of Pile Response(s)

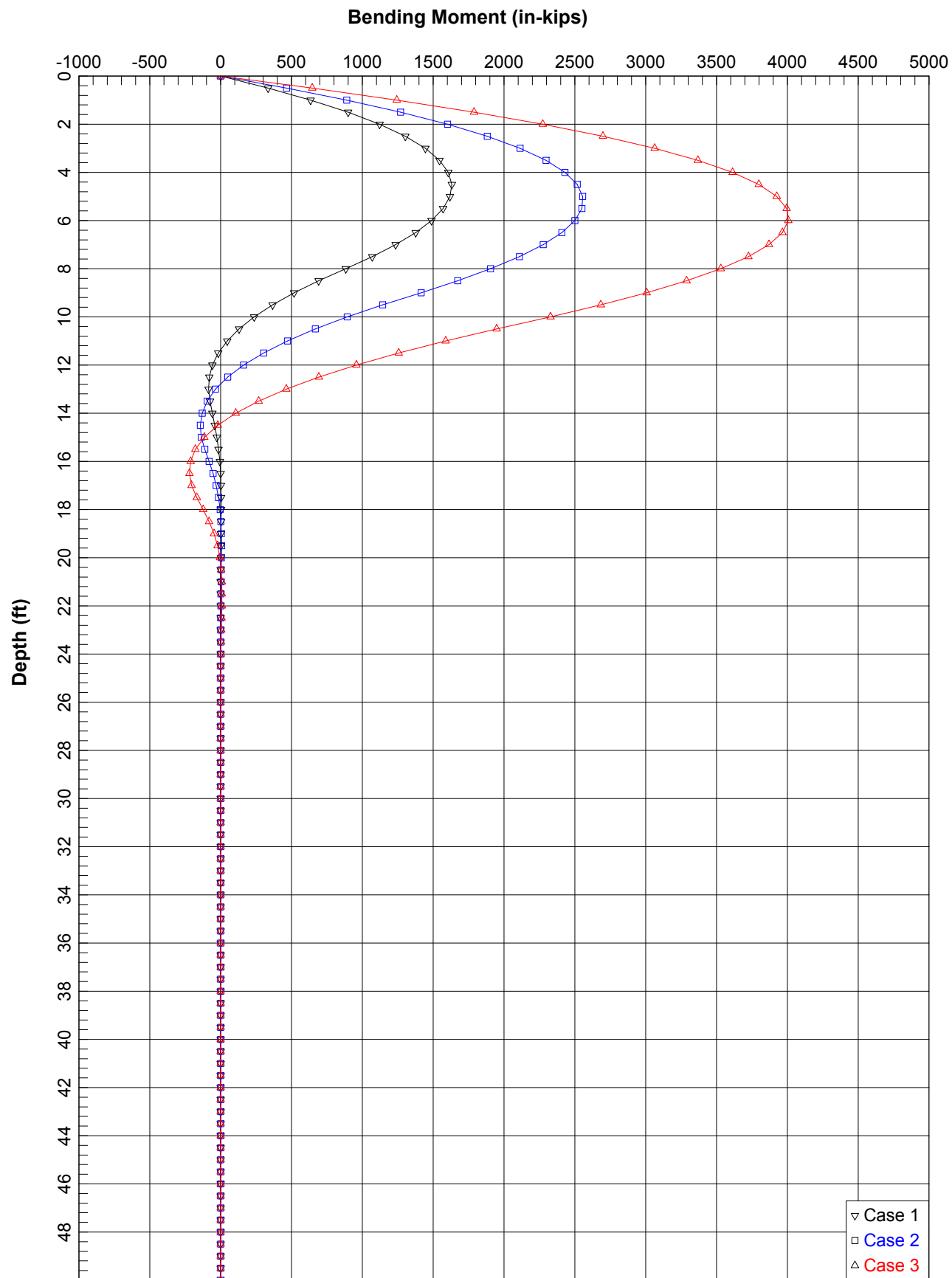
Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	219000.	0.25000000	1520721.	52377.	-0.00420805
2	4	y = 0.5000	M = 0.000	219000.	0.50000000	2386708.	71845.	-0.00744695
3	4	y = 1.0000	M = 0.000	219000.	1.00000000	3754556.	98631.	-0.01320494

The analysis ended normally.





Bent 2L_transv_Max P

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 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\athant\Desktop\Updated_ET 9-14-14\Bent 2L
 Name of input data file: Bent 2L_transv_Max P.lpd
 Name of output report file: Bent 2L_transv_Max P.lp6
 Name of plot output file: Bent 2L_transv_Max P.lpp
 Name of runtime message file: Bent 2L_transv_Max P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 20:35:17

Problem Title

Project Name: Palo Comado OC Bridge Widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 241inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Long t.-Avg Pm

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.000000
2	50.00000	24.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 2L_transv_Max P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. lbf/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 3 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 1.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass	Layer Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Elastic Modulus	Uniaxial Compressive Strength	ROD % or GSI	Epsilon
Factor Num. 50	J (p-y Curve Criteria) kpcy pci	Rock Emass psi	ft	pcf	psf	deg.	psi	psi		
1	Stiff Clay w/o Free Water		-5.000	125.000	4500.000	--	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--	--
0.00700	--	--	0.10000	125.000	4500.000	--	--	--	--	--
2	Stiff Clay w/o Free Water		0.10000	125.000	3750.000	--	--	--	--	--
0.00700	--	--	--	--	--	--	--	--	--	--
0.00700	--	--	1.000	125.000	3750.000	--	--	--	--	--
3	Stiff Clay w/o Free Water		1.000	125.000	4500.000	--	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.7500	1.0000
2	50.000	0.7500	1.0000

Bent 2L_transv_Max P

Table with 3 columns: Load No., Load Type, and Condition. It lists load conditions for static loading criteria.

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head loading and pile-head fixed by conditions. A series of dashes indicating a continuation of data.

Number of loads specified = 3

Table with 5 columns: Load No., Load Type, Condition, Axial Thrust Force, lbs, and Compute Top y vs. Pile Length. It lists load details and computation results.

V = perpendicular shear force applied to pile head

M = bending moment applied to pile head

y = lateral deflection relative to pile axis

S = pile slope relative to original pile batter angle

R = rotation at stiffness apply to pile head

Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness. A series of dashes.

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4). Displacement at pile head = 0.25000 inches, Moment at pile head = 0.000 in-lbs, Axial load at pile head = 219000.000 lbs.

Large table with 12 columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Soil Spr., Distrib. Lat. Load, Distrib. Lat. Load. It contains detailed data for pile loading and deflection.

Bent 2L_transv_Max P

Table with 3 columns: Load No., Load Type, and Condition. It lists load conditions for static loading criteria.

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head loading and pile-head fixed by conditions. A series of dashes indicating a continuation of data.

Number of loads specified = 3

Table with 5 columns: Load No., Load Type, Condition, Axial Thrust Force, lbs, and Compute Top y vs. Pile Length. It lists load details and computation results.

V = perpendicular shear force applied to pile head

M = bending moment applied to pile head

y = lateral deflection relative to pile axis

S = pile slope relative to original pile batter angle

R = rotation at stiffness apply to pile head

Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness. A series of dashes.

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4). Displacement at pile head = 0.25000 inches, Moment at pile head = 0.000 in-lbs, Axial load at pile head = 219000.000 lbs.

Large table with 12 columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Soil Spr., Distrib. Lat. Load, Distrib. Lat. Load. It contains detailed data for pile loading and deflection.

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary For Load Case No. 1:

Table with 2 columns: Parameter and Value. It lists summary statistics for load case no. 1, such as pile-head deflection, computed slope, and maximum bending moment.

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4). Displacement at pile head = 0.50000 inches, Moment at pile head = 0.000 in-lbs, Axial load at pile head = 219000.000 lbs.

Large table with 12 columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Soil Spr., Distrib. Lat. Load, Distrib. Lat. Load. It contains detailed data for pile loading and deflection.

Bent 2L_transv_Max P												
Node	U	V	W	X	Y	Z	U	V	W	X	Y	
156	0.00	-0.003432	-35888	-12040	0	0.000162	720	9411	1260247	0	0.00	
162	0.00	-0.002483	-95360	-7848	3830	0.000149	676	3971	1264264	0	0.00	
168	0.00	-0.001650	-130459	-3956	7026	0.000125	676	3479	1258290	0	0.00	
174	0.00	-0.000717	-143120	-433	8120	9	695	1007	1259966	0	0.00	
180	0.00	-0.000479	-135921	2636	7258	6.900E-05	684	3971	1263E+07	0	0.00	
186	0.00	-0.000149	-117171	4493	6743	4.360E-05	648	7202	1263E+07	0	0.00	
192	0.00	0.000165	-82123	3291	8268	2.380E-05	505	1964	1263E+07	0	0.00	
198	0.00	0.000138	-54138	4237	9229	9.962E-06	563	8765	1262970	0	0.00	
204	0.00	0.000165	-12823	3291	8268	2.380E-05	505	1964	1263E+07	0	0.00	
210	0.00	0.000153	-14639	2290	3320	-3.461E-06	505	6689	1263E+07	0	0.00	
216	0.00	0.000123	-3789	6928	1417	9681	-5.344E-06	489	6810	1263E+07	0	0.00
222	0.00	8.560E-05	2390	8607	748	5128	-5.487E-06	487	6196	1263E+07	0	0.00
228	0.00	5.714E-05	5206	8803	287	3938	-4.711E-06	491	7694	1263E+07	0	0.00
234	0.00	3.207E-05	5851	9652	5	1301	-3.580E-06	492	7201	1263E+07	0	0.00
240	0.00	1.417E-05	5277	8510	-141	1891	-2.443E-06	491	8740	1263E+07	0	0.00
246	0.00	2.753E-06	4164	1169	-194	7500	-1.478E-06	490	2328	1263E+07	0	0.00
252	0.00	3.562E-06	2944	7358	-192	1896	-7.516E-07	488	4358	1263E+07	0	0.00
258	0.00	-6.264E-06	1859	8165	-161	0920	-2.608E-07	486	8370	1263E+07	0	0.00
264	0.00	-6.689E-06	1012	3164	-120	0999	3.292E-08	485	5881	1263E+07	0	0.00
270	0.00	-5.871E-06	418	5310	-80	3579	1.791E-07	484	7131	1263E+07	0	0.00
276	0.00	-4.540E-06	47	5514	-47	4178	2.268E-07	484	1644	1263E+07	0	0.00
282	0.00	-3.150E-06	-151	0790	-23	0884	2.162E-07	484	3189	1263E+07	0	0.00
288	0.00	-1.945E-06	-230	0773	-4	9678	1.772E-07	484	4353	1263E+07	0	0.00
294	0.00	-1.023E-06	-235	1579	2	4230	1.297E-07	484	4428	1263E+07	0	0.00
300	0.00	-3.887E-07	-201	3422	6	8891	8.509E-08	484	3930	1263E+07	0	0.00
306	0.00	-1.631E-07	-152	7125	8	1242	4.891E-08	484	3213	1263E+07	0	0.00
312	0.00	1.982E-07	-103	9798	7	5023	2.268E-08	484	2495	1263E+07	0	0.00
318	0.00	2.705E-07	-62	7446	6	0192	5.461E-09	484	1887	1263E+07	0	0.00
324	0.00	2.659E-07	-31	7638	4	3220	-4.018E-09	484	1431	1263E+07	0	0.00
330	0.00	2.232E-07	-10	8698	2	7774	-8.375E-09	484	1123	1263E+07	0	0.00
336	0.00	1.654E-07	1	5865	1	5507	-9.323E-09	484	0986	1263E+07	0	0.00
342	0.00	1.104E-07	7	7627	0	6780	-8.368E-09	484	1077	1263E+07	0	0.00
348	0.00	6.497E-08	9	7441	0	1230	-6.579E-09	484	1106	1263E+07	0	0.00
354	0.00	3.148E-08	9	2559	0	1822	-4.637E-09	484	1099	1263E+07	0	0.00
360	0.00	9.292E-09	7	5702	0	-3113	-2.918E-09	484	1074	1263E+07	0	0.00
366	0.00	-3.528E-09	5	5281	0	-2880	-6.442E-10	484	1016	1263E+07	0	0.00
372	0.00	-9.619E-09	3	6188	0	-2219	-6.250E-11	484	0993	1263E+07	0	0.00
378	0.00	-1.127E-08	2	6737	0	-152	-2.471E-11	484	0977	1263E+07	0	0.00
384	0.00	-1.395E-08	1	7443	0	-0944	3.685E-10	484	0966	1263E+07	0	0.00
390	0.00	-5.948E-09	0	7179	0	-0493	3.739E-10	484	0965	1263E+07	0	0.00
396	0.00	-3.182E-09	0	7634	0	0184	3.188E-10	484	0968	1263E+07	0	0.00
402	0.00	-2.122E-09	0	8000	0	000342	2.410E-10	484	0969	1263E+07	0	0.00
408	0.00	-9.212E-10	0	8379	0	000971	1.635E-10	484	0968	1263E+07	0	0.00
414	0.00	-4.194E-10	0	8708	0	0134	9.827E-11	484	0967	1263E+07	0	0.00
420	0.00	-2.580E-10	0	9075	0	0131	4.939E-11	484	0966	1263E+07	0	0.00
426	0.00	-4.322E-10	0	9400	0	0109	1.654E-11	484	0965	1263E+07	0	0.00
432	0.00	-4.565E-10	0	9668	0	008076	-2.961E-12	484	0964	1263E+07	0	0.00
438	0.00	-4.977E-10	0	9970	0	005374	-1.256E-11	484	0963	1263E+07	0	0.00
444	0.00	-5.058E-10	0	10029	0	003148	-1.556E-11	484	0963	1263E+07	0	0.00
450	0.00	-5.110E-10	0	10108	0	01018	-0.0001512	484	0963	1263E+07	0	0.00
456	0.00	-5.195E-10	0	10159	0	000435	-1.197E-11	484	0963	1263E+07	0	0.00
462	0.00	-5.270E-10	0	10200	0	000188	-8.714E-12	484	0963	1263E+07	0	0.00
468	0.00	-5.345E-10	0	10241	0	000080	-5.684E-12	484	0963	1263E+07	0	0.00
474	0.00	-5.419E-10	0	10282	0	000056	-3.241E-12	484	0963	1263E+07	0	0.00
480	0.00	-5.493E-10	0	10323	0	000009	-2.00509E-12	484	0963	1263E+07	0	0.00
486	0.00	-5.567E-10	0	10364	0	000000	-1.480E-12	484	0963	1263E+07	0	0.00
492	0.00	-5.641E-10	0	10405	0	000000	0.000000	484	0963	1263E+07	0	0.00
498	0.00	-5.715E-10	0	10446	0	000000	0.000000	484	0963	1263E+07	0	0.00
504	0.00	-5.789E-10	0	10487	0	000000	0.000000	484	0963	1263E+07	0	0.00
510	0.00	-5.863E-10	0	10528	0	000000	0.000000	484	0963	1263E+07	0	0.00
516	0.00	-5.937E-10	0	10569	0	000000	0.000000	484	0963	1263E+07	0	0.00
522	0.00	-6.011E-10	0	10610	0	000000	0.000000	484	0963	1263E+07	0	0.00
528	0.00	-6.085E-10	0	10651	0	000000	0.000000	484	0963	1263E+07	0	0.00
534	0.00	-6.159E-10	0	10692	0	000000	0.000000	484	0963	1263E+07	0	0.00
540	0.00	-6.233E-10	0	10733	0	000000	0.000000	484	0963	1263E+07	0	0.00
546	0.00	-6.307E-10	0	10774	0	000000	0.000000	484	0963	1263E+07	0	0.00
552	0.00	-6.381E-10	0	10815	0	000000	0.000000	484	0963	1263E+07	0	0.00
558	0.00	-6.455E-10	0	10856	0	000000	0.000000	484	0963	1263E+07	0	0.00
564	0.00	-6.529E-10	0	10897	0	000000	0.000000	484	0963	1263E+07	0	0.00
570	0.00	-6.603E-10	0	10938	0	000000	0.000000	484	0963	1263E+07	0	0.00
576	0.00	-6.677E-10	0	10979	0	000000	0.000000	484	0963	1263E+07	0	0.00
582	0.00	-6.751E-10	0	11020	0	000000	0.000000	484	0963	1263E+07	0	0.00
588	0.00	-6.825E-10	0	11061	0	000000	0.000000	484	0963	1263E+07	0	0.00
594	0.00	-6.899E-10	0	11102	0	000000	0.000000	484	0963	1263E+07	0	0.00
600	0.00	-6.973E-10	0	11143	0	000000	0.000000	484	0963	1263E+07	0	0.00

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed Forces and Moments are within spec'ified convergence limits.

Output Summary For Load Case No. 2:

Pile-head deflection	=	0.5000000	inches
Computed slope at pile head	=	-0.0077130	rad/in
Maximum bending moment	=	2554777	in.-lbs
Maximum shear force	=	19796	lbs
Depth of maximum bending moment	=	60.0000000	inches below pile head
Depth of maximum shear force	=	0.0000000	inches below pile head
Number of iterations	=	14	
Number of zero deflection points	=	9	

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 3

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 1.000000 inches
 Moment at pile head = 0.000 in.-lbs
 Axial load at pile head = 219900.000 lbs

Depth	Deflect.	Bending Moment	Shear Force	Slope	Total Stress	Bending Moment	Soil Stress	Res. Soil	Spr. Es*	Distrib. Load
inches	inches	in.-lbs	lbs	rad/in	psi	lb-in ²	lb/in	lb/in	lb/in	lb/in
0.00	1.0000	0.000	19368	-0.0136	484.0963	2.936E+10	-1533.3270	4599.9811	0.000	0.000
6.00	0.9181	646536	100679	-0.0136	1436.8683	2.936E+10	-1363.3003	8909.0166	0.000	0.000
12.00	0.8371	1243819	92262	-0.0134	2317.0592	2.936E+10	-1442.2565	10338.	0.000	0.000

Bent 2L_transv_Max P												
Node	U	V	W	X	Y	Z	U	V	W	X	Y	
18	0.00	0.7576	1788847	82984	-0.0131	3120	2436	936E+10	-1650	5096	13072	
24	0.00	0.6802	2273977	73068	-0.0127	3835	1579	2	936E+10	-1654	6040	
30	0.00	0.6057	2698930	63143	-0.0121	4461	3926	2	936E+10	-1653	8416	
36	0.00	0.5344	3094359	53015	-0.0115	5112	6002	2	936E+10	-1648	10396	
42	0.00	0.4669	3612857	43382	-0.0109	5447	6043	2	936E+10	-1636	12104	
48	0.00	0.4036	3612859	33610	-0.0102	5608	2107	2	936E+10	-1620	14584	
54	0.00	0.3447	3786254	23954	-0.0094	5624	6704	2	936E+10	-1598	17175	
60	0.00	0.2904	3925293	14449	-0.008643	6268	3367	2	936E+10	-1569	19655	
66	0.00	0.2410	3994359	5133	2899	-0.007834	6370	4113	2	936E+10	-1533	36977
72	0.00	0.1964	4007279	-3954	8605	-0.007016	6389	4511	2	936E+10	-14	

Bent 2L_transv_Max P

Depth of maximum shear force = 0.00000 inches below pile head
 Number of iterations = 23
 Number of zero deflection points = 8

 Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

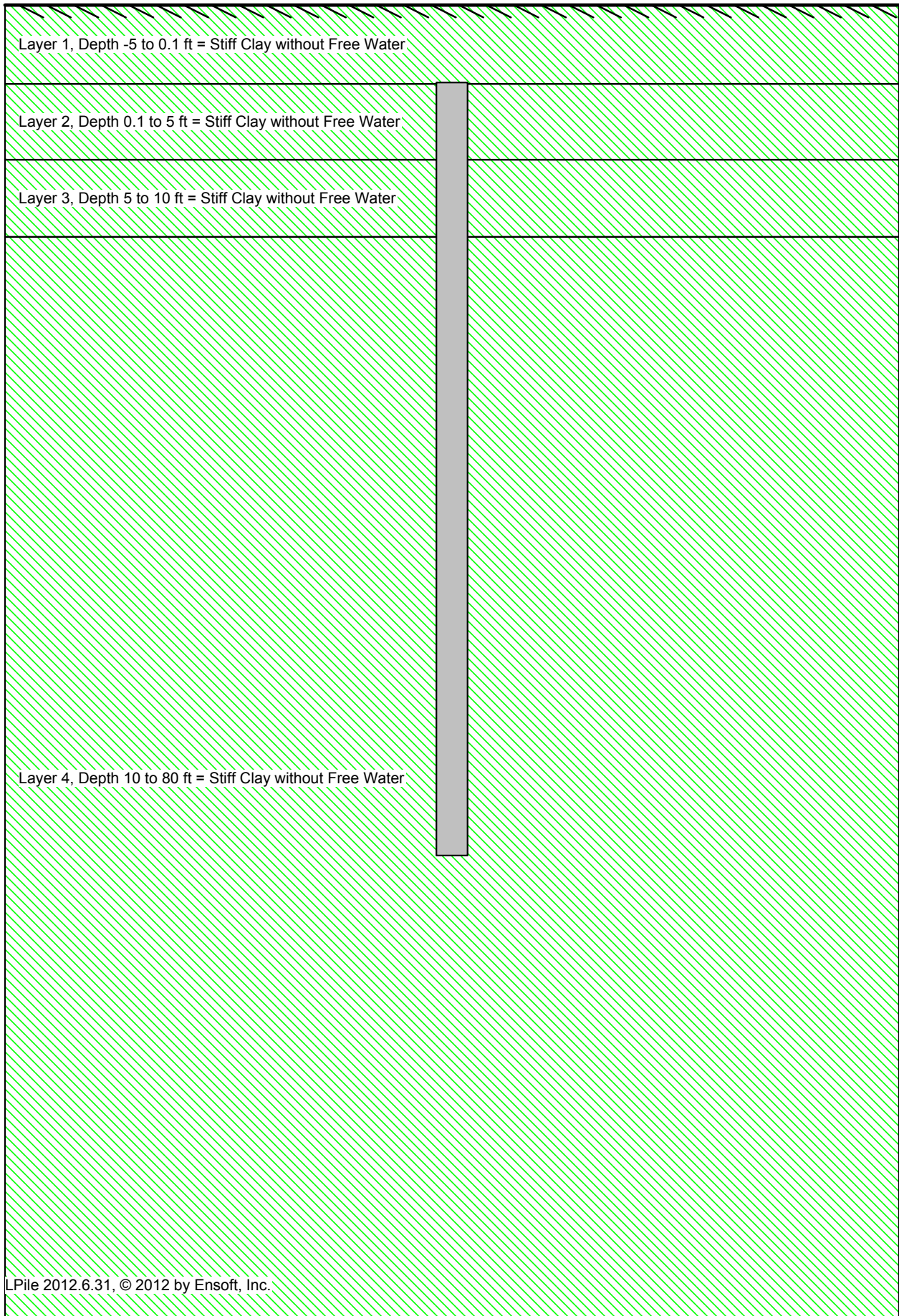
Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	219000.	0.25000000	1631177.	58125.	-0.00435568
2	4	y = 0.5000	M = 0.000	219000.	0.50000000	2555477.	79767.	-0.00771297
3	4	y = 1.0000	M = 0.000	219000.	1.00000000	4007279.	109368.	-0.01364189

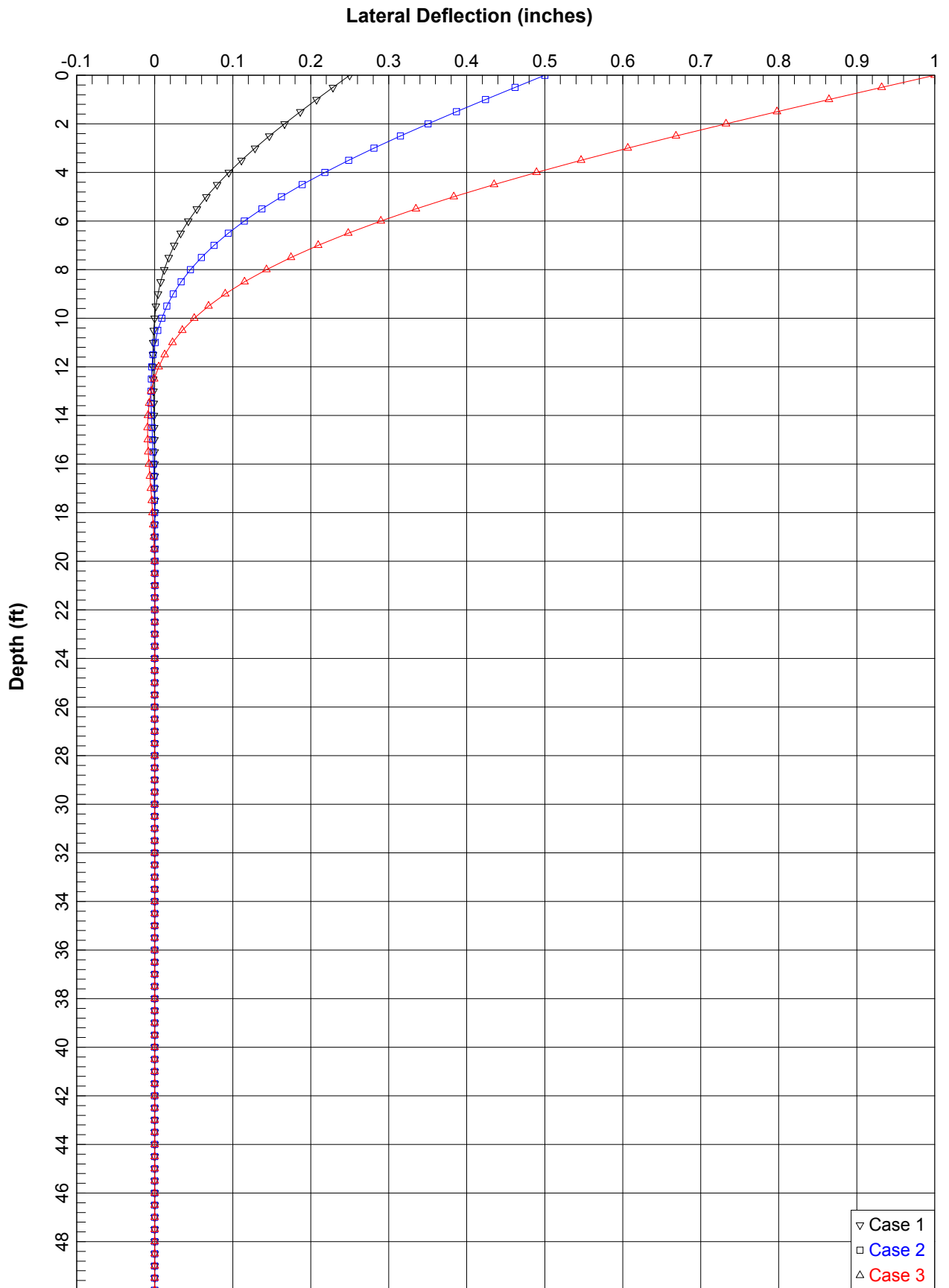
The analysis ended normally.

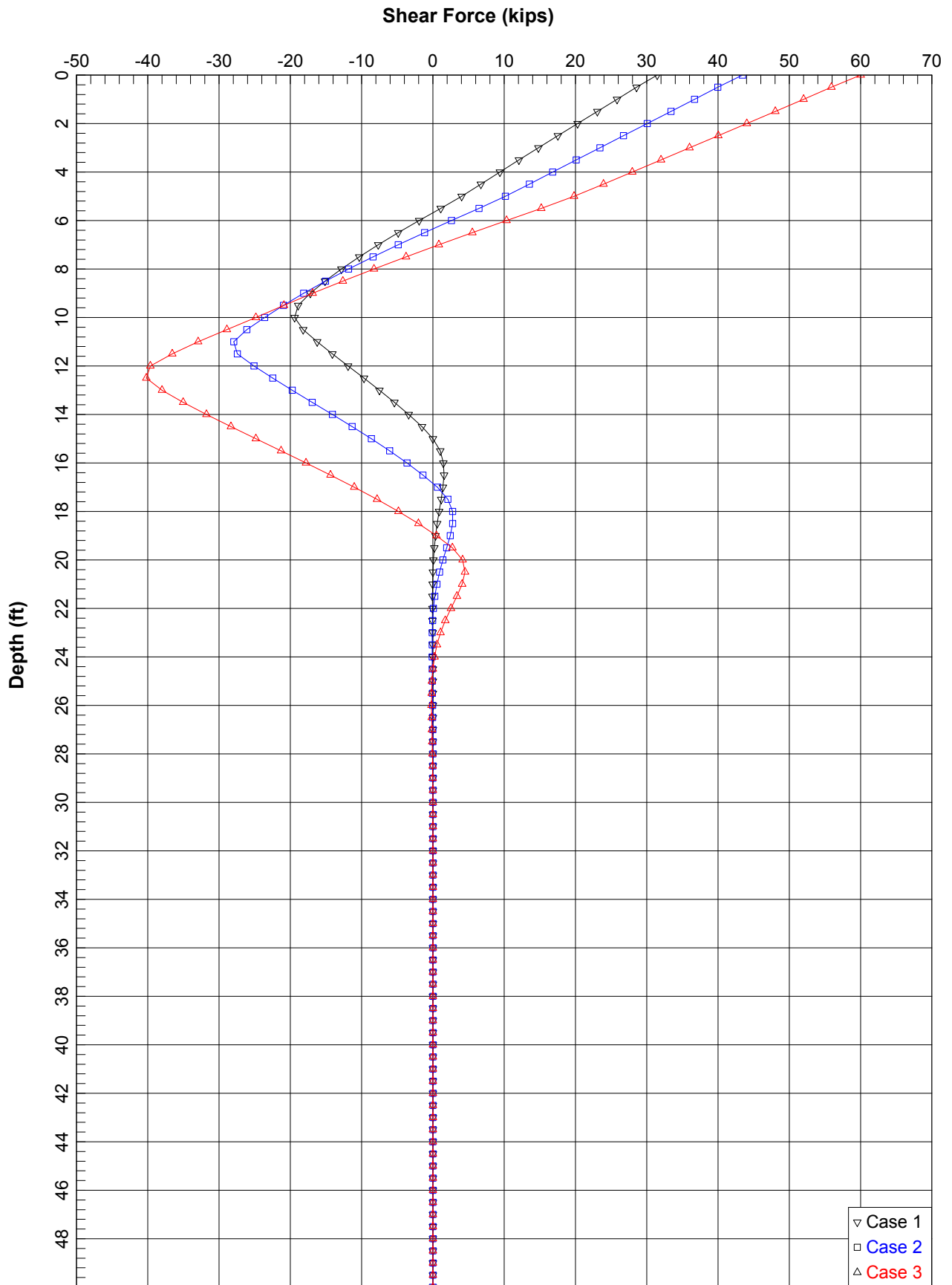
SUPPORT: BENT 3R

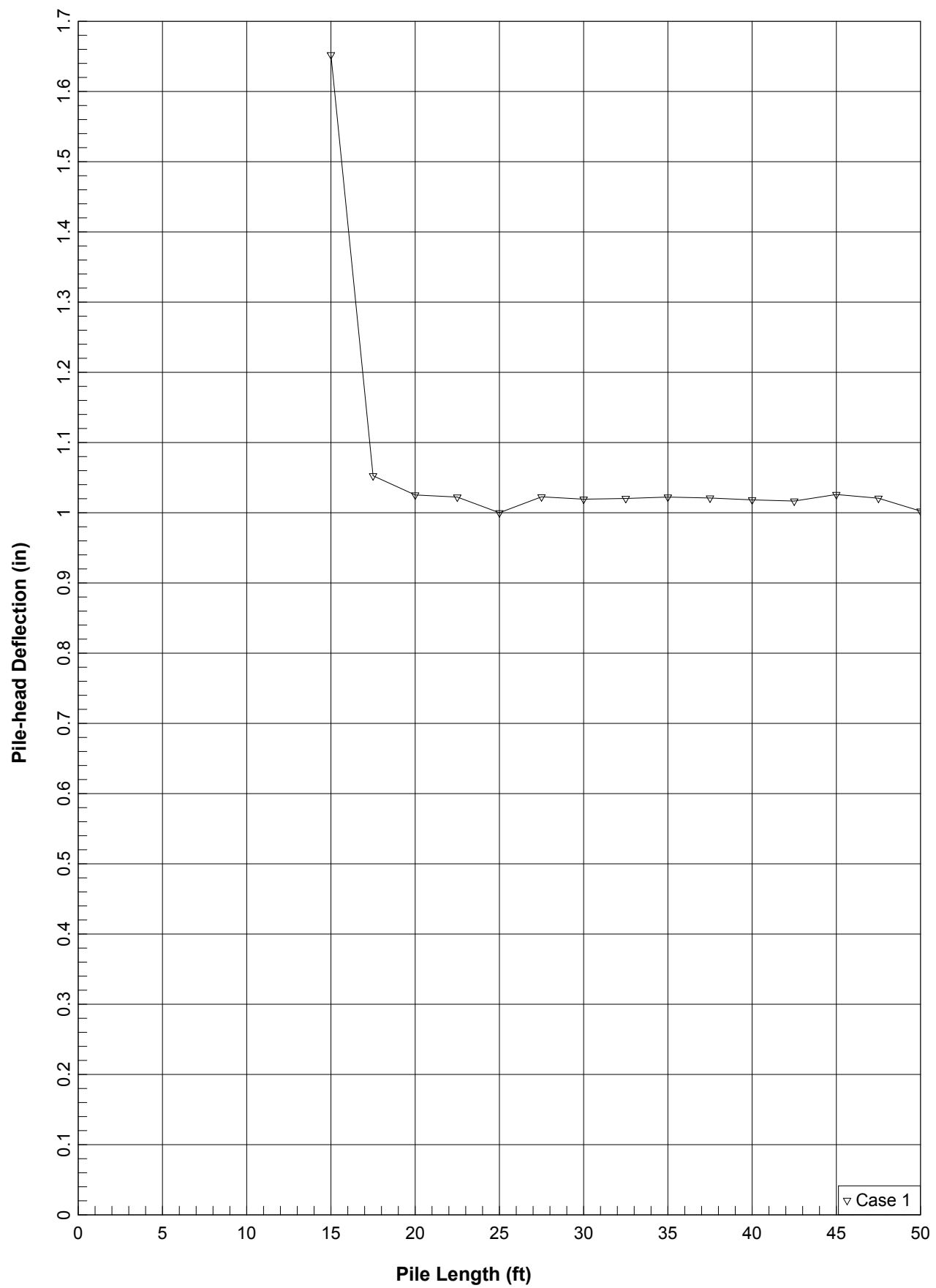
LOAD DIRECTION: LONGITUDE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE









Bent 3R_Long_Crit Length

File Plus for Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\athant\Desktop\Updated_ET 9-14-14\Bent 3V
 Name of input data file: Bent 3R_Long_Crit Length.lpd
 Name of output report file: Bent 3R_Long_Crit Length.lpd
 Name of plot output file: Bent 3R_Long_Crit Length.lpp
 Name of runtime message file: Bent 3R_Long_Crit Length.lpp

Date and Time of Analysis

Date: September 13, 2014 Time: 20:41:06

Problem Title

Project Name: Palo Comado OC Bridge Widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 241inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.000000
2	50.00000	24.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 3R_Long_Crit Length

Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 4 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3250.00000 psi
 Undrained cohesion at bottom of layer = 3250.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2750.00000 psi
 Undrained cohesion at bottom of layer = 2750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 5.00000 ft
 Distance from top of pile to bottom of layer = 10.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 10.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer Factor	Layer Soil Type Num. (p-y Curve Criteria)	Rock Mass Rock Emass psi	Layer Depth ft	Effective Unit Wt. pcf	Undrained Cohesion psi	Angle of Friction deg.	Uniaxial Subgrade Mod. psi	ROD % or GSI	Epsilon
0.00700	1 Stiff Clay w/o Free Water	--	-5.000	120.000	3250.000	--	--	--	--
0.00700	--	--	0.10000	120.000	3250.000	--	--	--	--
0.00700	2 Stiff Clay w/o Free Water	--	0.10000	120.000	2750.000	--	--	--	--
0.00700	--	--	5.000	120.000	2750.000	--	--	--	--
0.00700	3 Stiff Clay w/o Free Water	--	5.000	120.000	3750.000	--	--	--	--
0.00700	--	--	10.000	120.000	3750.000	--	--	--	--
0.00700	--	--	10.000	125.000	4500.000	--	--	--	--
0.00500	4 Stiff Clay w/o Free Water	--	10.000	125.000	4500.000	--	--	--	--
	--	--	80.000	125.000	4500.000	--	--	--	--

0.00500

Bent 3R_long_Crit length

No. Ft

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Table with 4 columns: Point No., Depth X, p-mod, y-mod. Rows 1 to 2.

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Table with 6 columns: Load No., Load Type, Condition V, Condition M, Axial Thrust Force, Compute Top y vs. Pile Length. Row 1.

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head = 60000.000 lbs
Applied moment at pile head = 0.000 in-lbs
Axial thrust load on pile head = 226000.000 lbs

Table with 11 columns: Depth X, Deflect. y, Bending Moment, Shear Force, Slope, Total Stress, Bending p, Soil Res. p, Soil Spr. Es, Distrib. Lat. Load. Rows 0.00 to 210.00.

Main data table with columns: Point No., Depth X, p-mod, y-mod, and various stress/force values. Rows 216.00 to 600.00.

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:
Pile-head deflection = 1.0023641 inches
Computed slope at pile head = -0.0113567 radians
Maximum bending moment = 84.000000 inches below pile head
Number of iterations = 32

Pile-head Deflection vs. Pile Length For Load Case 1

Boundary Condition on Type 1, Shear and Moment

Shear = 60000. lbs
Applied moment = 0.000 in-lbs
Axial Load = 226000. lbs

Table with 4 columns: Pile Length, Pile Head Deflection, Maximum Moment, Maximum Shear. Rows 50 to 22.500.

20.000 1.0254445 2840400. 60000. Bent 3R_long_Cri t length
 17.500 1.0525871 2818443. 60000.
 15.000 1.6523741 2593831. 60000.

 Summary of Pile Response(s)

Defin itions of Pile-head Loading Condi tions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Sti ffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.	Pile-head Condi ti on 1 V(lbs) or y(inches)	Pile-head Condi ti on 2 in-lb, rad, or in-lb/rad.	Axi al Loading lbs	Pile-head Deflecti on inches	Maxi mum Moment in-lbs	Maxi mum Shear lbs	Pile-head Rotati on radi ans
1	1	V = 60000	M = 0.000	226000.	1.00236408	2829048.	60000.	-0.01135673

The analysi s ended normal y.

Bent 3R_Long_Ave P

File Plus for Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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This copy of LPIE is licensed to:

gdc
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\athant\Desktop\Updated_ET 9-14-14\Bent 3R
 Name of input data file: Bent 3R_Long_Ave P.lpd
 Name of output report file: Bent 3R_Long_Ave P.lpr
 Name of plot output file: Bent 3R_Long_Ave P.lpd
 Name of runtime message file: Bent 3R_Long_Ave P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 20:39:25

Problem Title

Project Name: Palo Comado OC Bridge Widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 241inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Transv - Pm,avg -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.000000
2	50.00000	24.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 3R_Long_Ave P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 4 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3250.00000 psi
 Undrained cohesion at bottom of layer = 3250.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2750.00000 psi
 Undrained cohesion at bottom of layer = 2750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 5.00000 ft
 Distance from top of pile to bottom of layer = 10.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 10.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Rock Emass	Layer Depth ft	Effective Unit Weight pcf	Undrained Cohesion psi	Angle of Friction deg	Uniaxial Elastic Modulus psi	ROR GSI	ROD %	Epsilon
1	Stiff Clay w/o Free Water	--	-5.000	125.000	3250.000	--	--	--	--	--
0.00700	--	--	0.10000	125.000	3250.000	--	--	--	--	--
0.00700	Stiff Clay w/o Free Water	--	0.10000	120.000	2750.000	--	--	--	--	--
0.00700	--	--	5.000	120.000	2750.000	--	--	--	--	--
0.00700	Stiff Clay w/o Free Water	--	5.000	120.000	3750.000	--	--	--	--	--
0.00700	--	--	10.000	120.000	3750.000	--	--	--	--	--
0.00700	--	--	10.000	125.000	4500.000	--	--	--	--	--
0.00500	Stiff Clay w/o Free Water	--	10.000	125.000	4500.000	--	--	--	--	--
	--	--	80.000	125.000	4500.000	--	--	--	--	--

0.00500 Bent 3R_long_Ave P

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Table with 4 columns: Point, Depth X, p-mult, y-mult. Rows 1 and 2 showing values for depth 0.000 and 50.000.

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Table with 7 columns: Load No., Load Type, Condition, Condition, Axial Thrust Force, Top y vs. Compute, Pile Length. Rows 1, 2, 3.

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.250000 inches
Moment at pile head = 0.000 inches-lbs
Axial load at pile head = 226000.000 lbs

Large table with 13 columns: Depth X, Deflect. y, Bending Moment, Shear Force, Slope S, Total Stress, Bending Stiffness, Soil Res. p, Soil Spr. Es, Distrib. Lat. Load. Rows 0.00 to 192.00.

Large table with 13 columns: Same as previous table, showing data for multiple pile sections. Rows 198.00 to 600.00.

* The above values of total stress are combined axial and bending stresses.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Pile-head deflection = 0.2500000 inches
Computed slope at pile head = -0.0035728 rad/in
Maximum bending moment = 31460. lbs
Depth of maximum bending moment = 66.000000 inches below pile head

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.500000 inches
Moment at pile head = 226000.000 lbs
Axial load at pile head = 226000.000 lbs

Table with 13 columns: Same as previous table, showing data for multiple pile sections. Rows 0.00 to 54.00.

Table with columns for coordinates (60.000, 66.000, 72.000, etc.), values (1623, 173627, 11448, etc.), and labels (Bent 3R_Long_Ave P). Includes a note: '* The above values of total stress are combined axial and bending stress.'

Computed Values of Pile Loading and Deflection on Bent 3R_Long_Ave P. Includes title 'Computed Values of Pile Loading and Deflection on Bent 3R_Long_Ave P', table headers for pile-head conditions, and a large table with columns: Depth X, Defl. at p, Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res. P, Soil Spr. Es*H, and Distri. Load.

Output Verification: Computed forces and moments are within specified convergence limits.
Output Summary For Load Case No. 2:
Pile-head deflection = 0.500000 inches
Computed slope at pile head = -0.0063648 radian

Bent 3R_long_Ave P
 594.000 -3.365E-11 0.000412 -0.000137 0.000 499.5697 2.936E-10 2.271E-05 4050000. 0.000
 600.000 -3.392E-11 0.000 0.000 0.000 499.5697 2.936E-10 2.290E-05 2025000. 0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

Pile-head deflection = 1.000000 inches
 Computed slope at pile head = -0.0113381 radians
 Maximum bending moment = 2826388 inch-lbs
 Maximum shear force = 60004. lbs
 Depth of maximum bending moment = 84.000000 inches below pile head
 Depth of maximum shear force = 0.000000 inches below pile head
 Number of iterations = 22
 Number of zero deflection points = 7

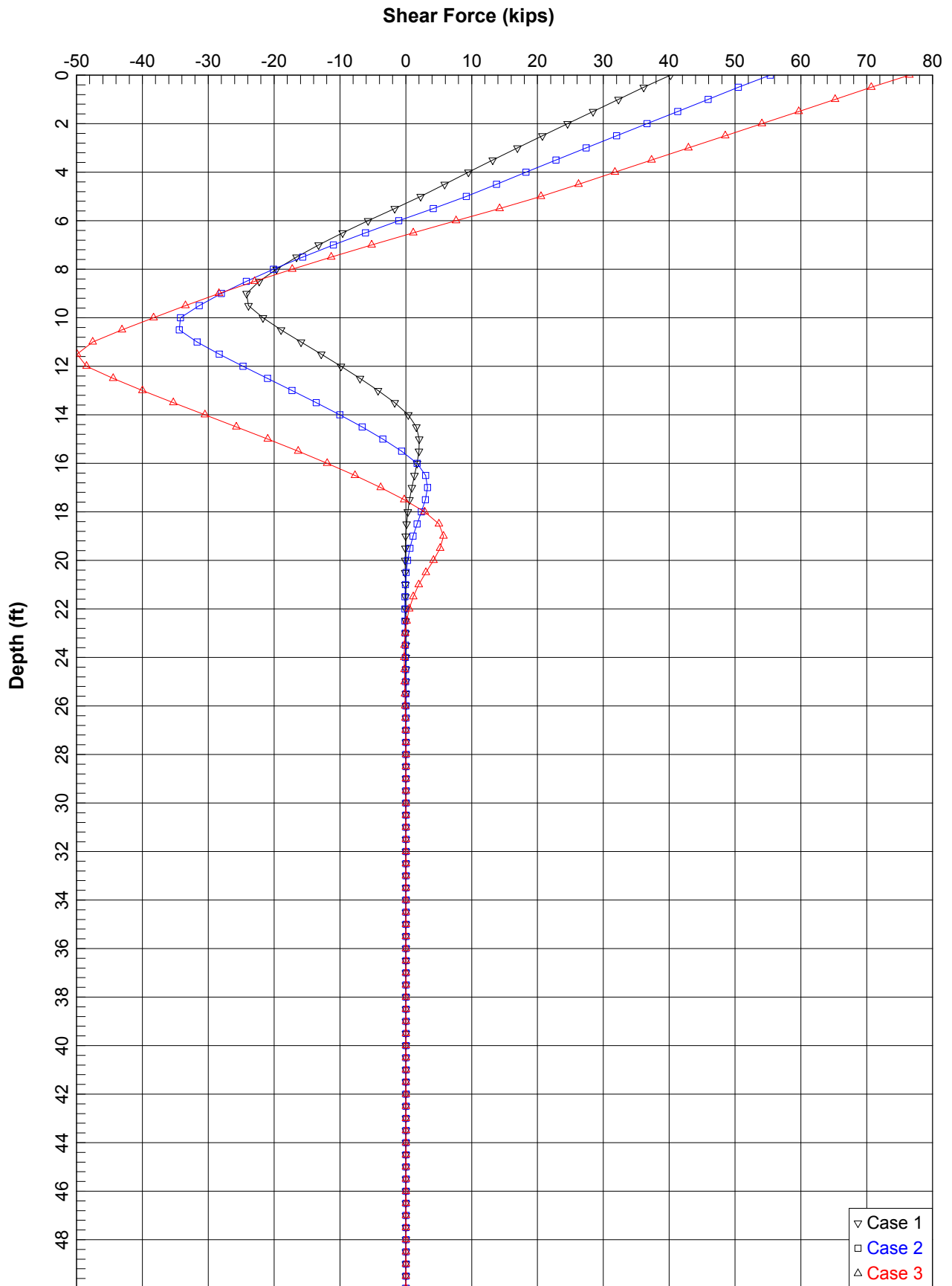
 Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb. rad. or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	226000.	0.25000000	1116166.	31460.	-0.00357284
2	4	y = 0.5000	M = 0.000	226000.	0.50000000	1778692.	43425.	-0.00636475
3	4	y = 1.0000	M = 0.000	226000.	1.00000000	2826388.	60004.	-0.01133813

The analysis ended normally.





Bent 3R_Long_Max P

File Plus for Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\athant\Desktop\Updated_ET 9-14-14\Bent 3R
 Name of input data file: Bent 3R_Long_Max P.lpd
 Name of output report file: Bent 3R_Long_Max P.lpr
 Name of plot output file: Bent 3R_Long_Max P.lpp
 Name of runtime message file: Bent 3R_Long_Max P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 20:42:11

Problem Title

Project Name: Palo Comado OC Bridge Widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 241inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Transv - Pm,avg -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.000000
2	50.00000	24.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 3R_Long_Max P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 4 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3250.00000 psi
 Undrained cohesion at bottom of layer = 3250.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2750.00000 psi
 Undrained cohesion at bottom of layer = 2750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 5.00000 ft
 Distance from top of pile to bottom of layer = 10.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 10.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Rock Emass	Layer Depth ft	Effective Unit Weight pcf	Undrained Cohesion psi	Angle of Friction deg.	Uniaxial Subgrade Mod. psi	ROD % or GSI	Epsilon
1	Stiff Clay w/o Free Water	--	-5.000	125.000	3250.000	--	--	--	--
0.00700	--	--	0.10000	125.000	3250.000	--	--	--	--
0.00700	Stiff Clay w/o Free Water	--	0.10000	120.000	2750.000	--	--	--	--
0.00700	--	--	5.000	120.000	2750.000	--	--	--	--
0.00700	Stiff Clay w/o Free Water	--	5.000	120.000	3750.000	--	--	--	--
0.00700	--	--	10.000	120.000	3750.000	--	--	--	--
0.00700	Stiff Clay w/o Free Water	--	10.000	125.000	4500.000	--	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--	--

0.00500 Bent 3R_long_Max P

p-y Modification Factors for Group Action

Table with columns: Point, Depth X, p=ult, y=ult. Rows 1-2 showing data for depth 0.000 and 50.000.

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Table with columns: Load No., Load Type, Condition, Condition 2, Axial Thrust Force, lbs, Compute Top y vs. Pile Length. Rows 1-3.

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile sltpe relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection
For Lateral Loading For Load Case Number 1

Pile-head conditions are Diplacement and Moment (Loading Type 4)
Diplacement of pile head = 0.250000 inches
Moment at pile head = 0.000 inches-lbs
Axial load at pile head = 226000.000 lbs

Table with columns: Depth X, Deflect. y, Bending Moment, Shear Force, Slope p, Total Stress, Bending Stiffness, Soil Res. p, Soil Spr. Es-h, Distrib. Lat. Load. Rows 0 to 192.

Page 3

Bent 3R_long_Max P

Table with columns: Point, Depth X, p=ult, y=ult. Rows 198 to 600.

* The above values of total stress are combined axial and bending stresses.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary For Load Case No. 1:

Pile-head deflection = 0.2500000 inches
Computed sltpe at pile head = -0.0038639 radian
Maximum shear force = 40200. lbs
Depth of maximum bending moment = 66.000000 inches below pile head
Depth of maximum shear force = 0.000000 inches below pile head
Number of iterations = 13
Number of zero deflection points = 9

Computed Values of Pile Loading and Deflection
For Lateral Loading For Load Case Number 2

Pile-head conditions are Diplacement and Moment (Loading Type 4)
Diplacement of pile head = 0.500000 inches
Moment at pile head = 45117.000 inches-lbs
Axial load at pile head = 226000.000 lbs

Table with columns: Depth X, Deflect. y, Bending Moment, Shear Force, Slope p, Total Stress, Bending Stiffness, Soil Res. p, Soil Spr. Es-h, Distrib. Lat. Load. Rows 0 to 54.

Page 4

Bent 3R_Long_Max P
 594.000 2.570E-12 -6.257E-05 1.779E-05 0.000 499.5697 2.936E-10 -2.439E-06 5695312. 0.000
 600.000 3.677E-12 0.000 0.000 0.000 499.5697 2.936E-10 -3.490E-06 2847656. 0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

Pile-head deflection = 1.0000000 inches
 Computed slope at pile head = -0.0122313 radians
 Maximum bending moment = 3284229 inch-lbs
 Maximum shear force = 76458 lbs
 Depth of maximum bending moment = 78.0000000 inches below pile head
 Depth of maximum shear force = 0.0000000 inches below pile head
 Number of iterations = 15
 Number of zero deflection points = 8

 Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

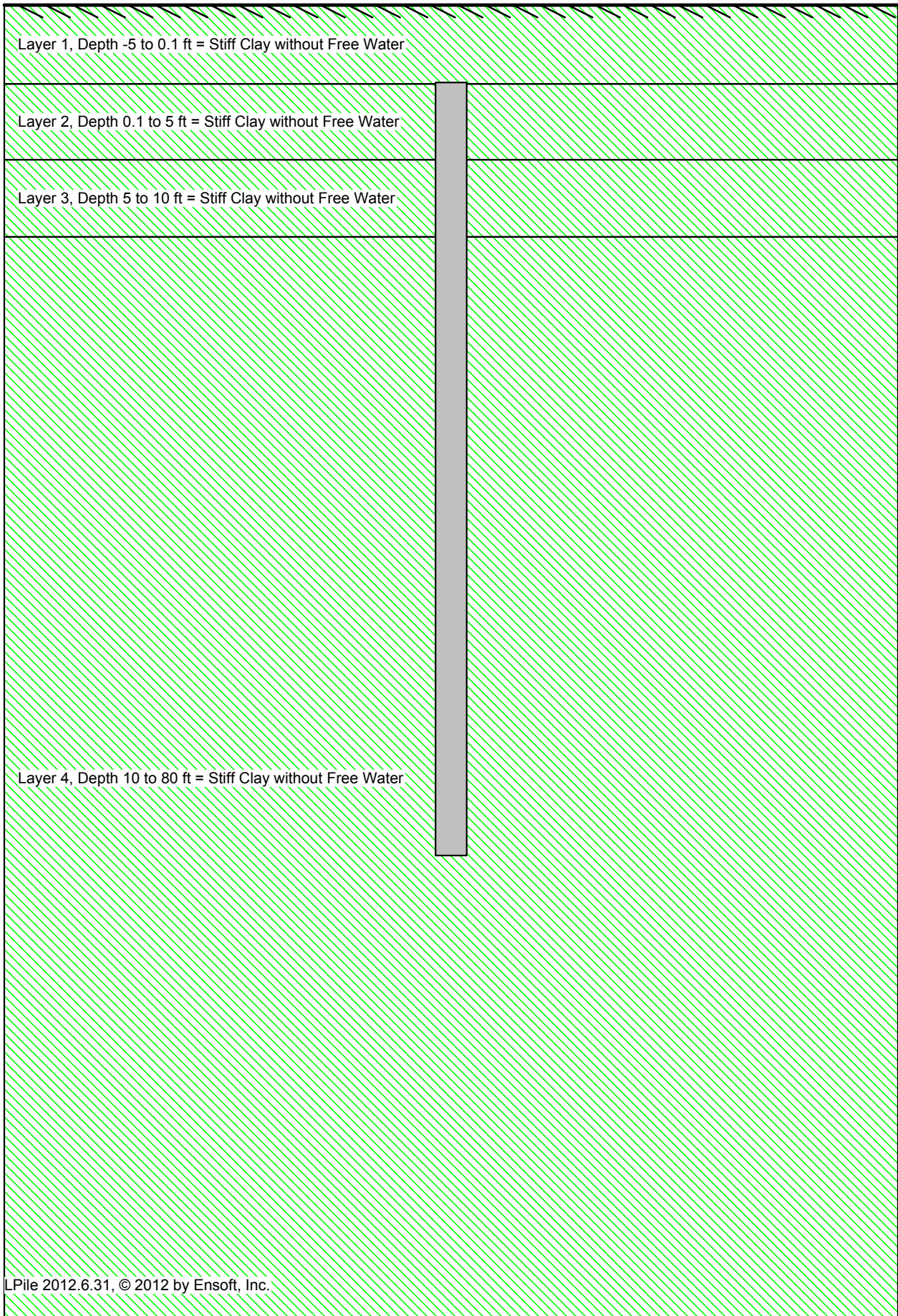
Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	226000.	0.25000000	1301460.	40200.	-0.00386388
2	4	y = 0.5000	M = 0.000	226000.	0.50000000	2065682.	55354.	-0.00686136
3	4	y = 1.0000	M = 0.000	226000.	1.00000000	3284229.	76458.	-0.01223127

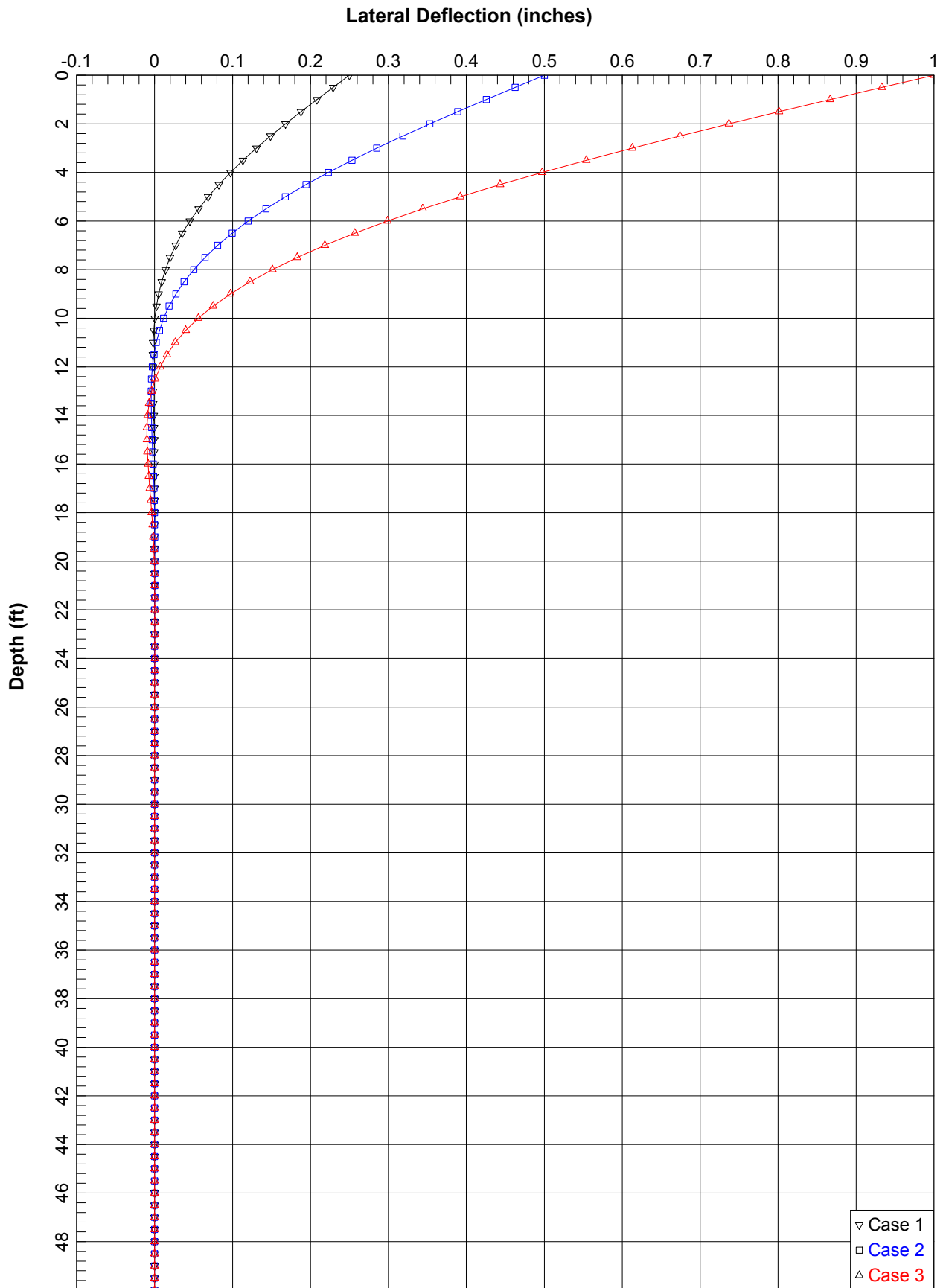
The analysis ended normally.

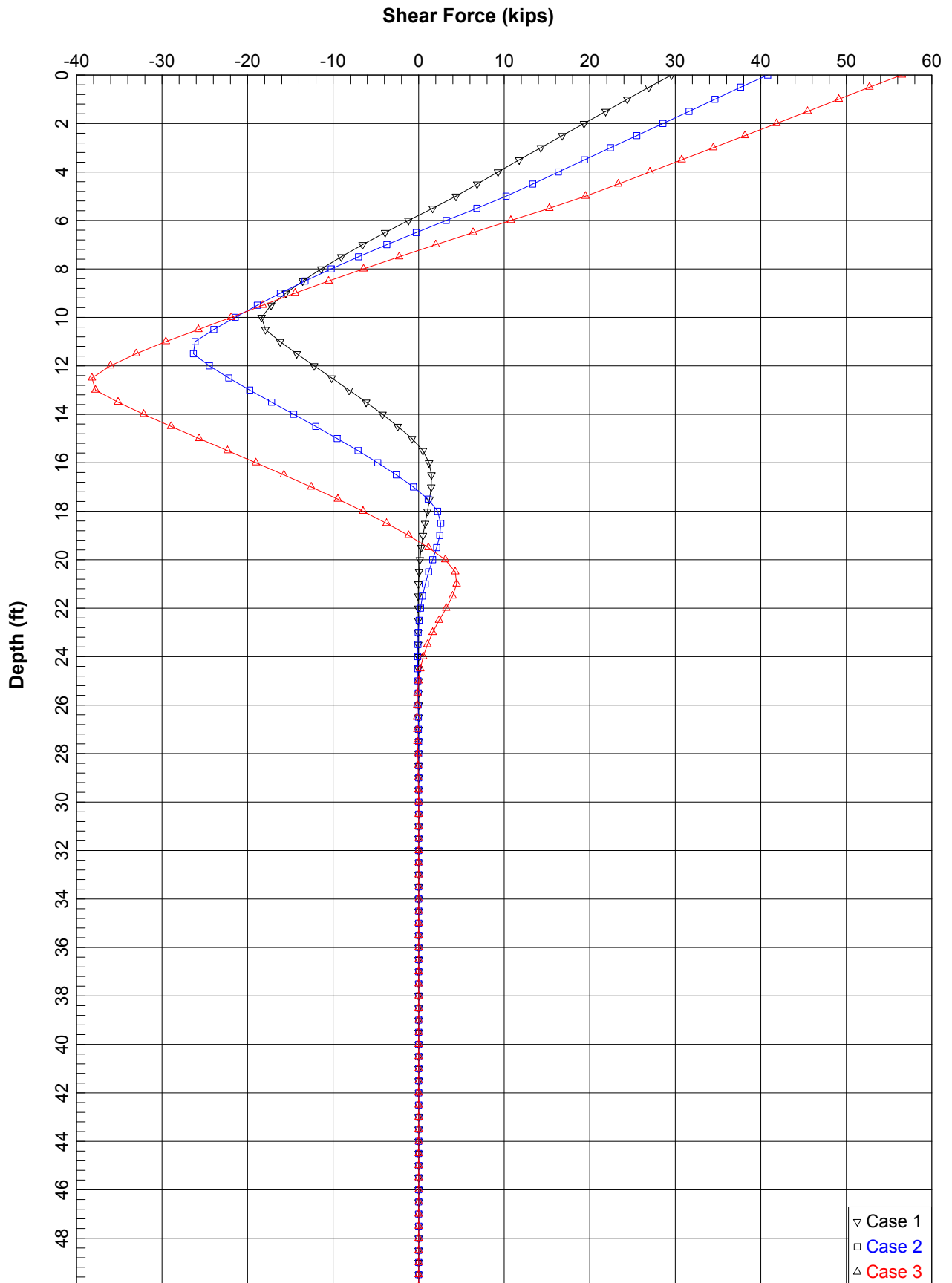
SUPPORT: BENT 3R

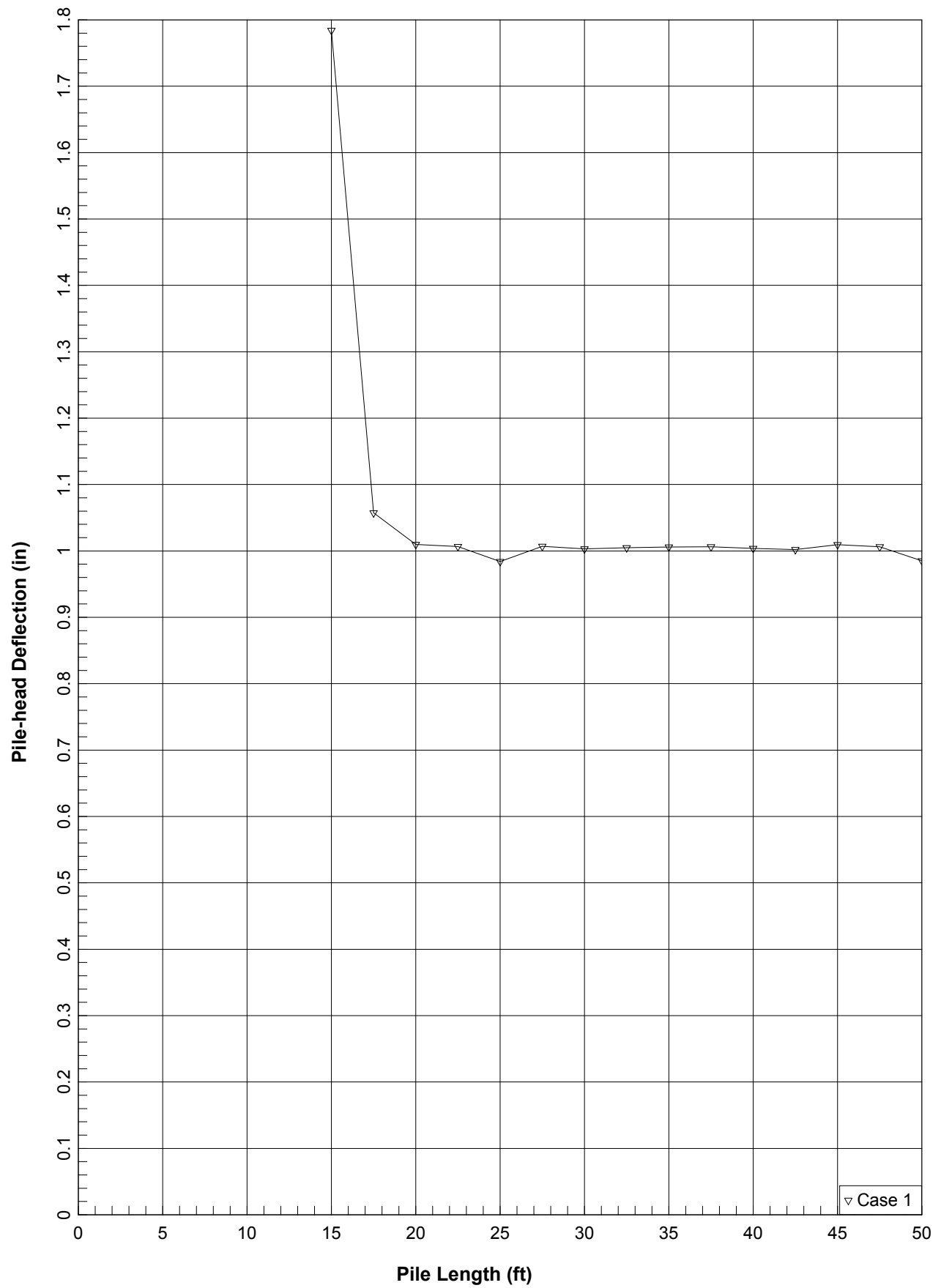
LOAD DIRECTION: TRANSVERSE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE









Bent 3R_transv_Crit length

Pile Plus for windows, version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Bent 3\
 Name of input data file: Bent 3R_transv_Crit length.lpd
 Name of output report file: Bent 3R_transv_Crit length.lpd
 Name of plot output file: Bent 3R_transv_Crit length.lpd
 Name of runtime message file: Bent 3R_transv_Crit length.lpd

Date and Time of Analysis

Date: September 13, 2014 Time: 20:47:13

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24Inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 3R_transv_Crit length
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top width = 24.0000000 in
 Bottom width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 4 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3250.00000 psi
 Undrained cohesion at bottom of layer = 3250.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2750.00000 psi
 Undrained cohesion at bottom of layer = 2750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 5.00000 ft
 Distance from top of pile to bottom of layer = 10.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 10.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass Factor	Layer Depth	Effective Unit wt.	Undrained Cohesion	Angle of Friction	Uniaxial Elastic Modulus	RQD %
Num.	(p-y Curve Criteria)	Rock Emass	ft	pcf	psf	deg.	psi	or GSI
50	Factor	psi	ft	Type	Property	Mod. pcf	psi	Epsilon
1	Stiff Clay w/o Free Water	--	-5.000	120.000	3250.000	--	--	--
0.00700	--	--	0.10000	120.000	3250.000	--	--	--
2	Stiff Clay w/o Free Water	--	0.10000	120.000	2750.000	--	--	--
0.00700	--	--	5.000	120.000	2750.000	--	--	--
3	Stiff Clay w/o Free Water	--	5.000	120.000	3750.000	--	--	--
0.00700	--	--	10.000	120.000	3750.000	--	--	--
4	Stiff Clay w/o Free Water	--	10.000	125.000	4500.000	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--

20.000 1.0097474 2706971. 56000. Bent 3R_transv_Crit Length
 17.500 1.0573063 2673243. 56000.
 15.000 1.7840662 2444493. 56000.

 Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	1	V = 56000.	M = 0.000	226000.	0.98520824	2698865.	56000.	-0.01099589

The analysis ended normally.

Bent 3R_transv_Ave P

File Plus for Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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Files Used for Analysis

Path to file locations: C:\Users\athant\Desktop\Updated_ET 9-14-14\Bent 3V
 Name of input data file: Bent 3R_transv_Ave P.lpd
 Name of output report file: Bent 3R_transv_Ave P.lp6
 Name of plot output file: Bent 3R_transv_Ave P.lpp
 Name of runtime message file: Bent 3R_transv_Ave P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 20:45:13

Problem Title

Project Name: Palo Comado OC Bridge Widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 241inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Transv - Pm,avg -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.000000
2	50.00000	24.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 3R_transv_Ave P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 4 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3250.00000 psi
 Undrained cohesion at bottom of layer = 3250.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2750.00000 psi
 Undrained cohesion at bottom of layer = 2750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 5.00000 ft
 Distance from top of pile to bottom of layer = 10.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 10.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer Factor	Layer Soil Type Num. (p-y Curve Criteria)	Rock Mass Rock Emass	Layer Depth ft	Effective Unit Wt. pcf	Undrained Cohesion psi	Angle of Friction deg.	Uniaxial Subgrade Mod. psi	ROD % or GSI	Epsilon
0.00700	1 Stiff Clay w/o Free Water	--	-5.000	125.000	3250.000	--	--	--	--
0.00700	--	--	0.10000	125.000	3250.000	--	--	--	--
0.00700	2 Stiff Clay w/o Free Water	--	0.10000	120.000	2750.000	--	--	--	--
0.00700	--	--	5.000	120.000	2750.000	--	--	--	--
0.00700	3 Stiff Clay w/o Free Water	--	5.000	120.000	3750.000	--	--	--	--
0.00700	--	--	10.000	120.000	3750.000	--	--	--	--
0.00700	4 Stiff Clay w/o Free Water	--	10.000	125.000	4500.000	--	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--	--

0.00500

Bent 3R_transv_Ave P

p-y Modification Factors For Group Action

Distribution of p-y modifiers with depth defined using 2 points

Table with columns: Point, Depth X, p-mod, y-mod. Rows 1-2 showing values for depth 0.000 and 50.000.

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Table with columns: Load No., Load Type, Condition, Condition, Axial Thrust Force, lbs, Compute Top y vs. Pile Length. Rows 1-3.

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
Y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.250000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 226000.000 lbs

Large table with columns: Depth X, Defl.ect. Y, Bending Moment, Shear Force, Slope S, Total Stress, Bending Stiffness, Soil Res. p, Soil Spr. Es, Distrib. Lat. Load. Rows 0.00 to 192.000.

Bent 3R_transv_Ave P

Large table with columns: 198.000, 204.000, 210.000, 216.000, 222.000, 228.000, 234.000, 240.000, 246.000, 252.000, 258.000, 264.000, 270.000, 276.000, 282.000, 288.000, 294.000, 300.000, 306.000, 312.000, 318.000, 324.000, 330.000, 336.000, 342.000, 348.000, 354.000, 360.000, 366.000, 372.000, 378.000, 384.000, 390.000, 396.000, 402.000, 408.000, 414.000, 420.000, 426.000, 432.000, 438.000, 444.000, 450.000, 456.000, 462.000, 468.000, 474.000, 480.000, 486.000, 492.000, 498.000, 504.000, 510.000, 516.000, 522.000, 528.000, 534.000, 540.000, 546.000, 552.000, 558.000, 564.000, 570.000, 576.000, 582.000, 588.000, 594.000, 600.000.

* The above values of total stress are combined axial and bending stresses.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary For Load Case No. 1:

Pile-head deflection = 0.2500000 inches
Computed slope at pile head = -0.0035048 radians
Maximum bending moment = 1075927.1 inch-lbs
Maximum shear force = 29567.1 lbs
Depth of maximum bending moment = 72.000000 inches below pile head
Depth of maximum shear force = 0.000000 inches below pile head
Number of iterations = 14
Number of zero deflection points = 8

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.500000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 226000.000 lbs

Table with columns: Depth X, Defl.ect. Y, Bending Moment, Shear Force, Slope S, Total Stress, Bending Stiffness, Soil Res. p, Soil Spr. Es, Distrib. Lat. Load. Rows 0.00 to 54.000.

Bent 3R_transv_Ave P
 594.000 -6.852E-11 0.000993 -0.000294 -3.615E-12 499.5697 2.936E+10 4.240E-05 3712500. 0.000
 600.000 -8.961E-11 0.000 0.000 -3.514E-12 499.5697 2.936E+10 5.544E-05 1856250. 0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

Pile-head deflection = 1.000000 inches
 Computed slope at pile head = -0.0111373 radians
 Maximum bending moment = 2727932 inch-lbs
 Maximum shear force = 56459 lbs
 Depth of maximum bending moment = 90.000000 inches below pile head
 Depth of maximum shear force = 0.000000 inches below pile head
 Number of iterations = 19
 Number of zero deflection points = 7

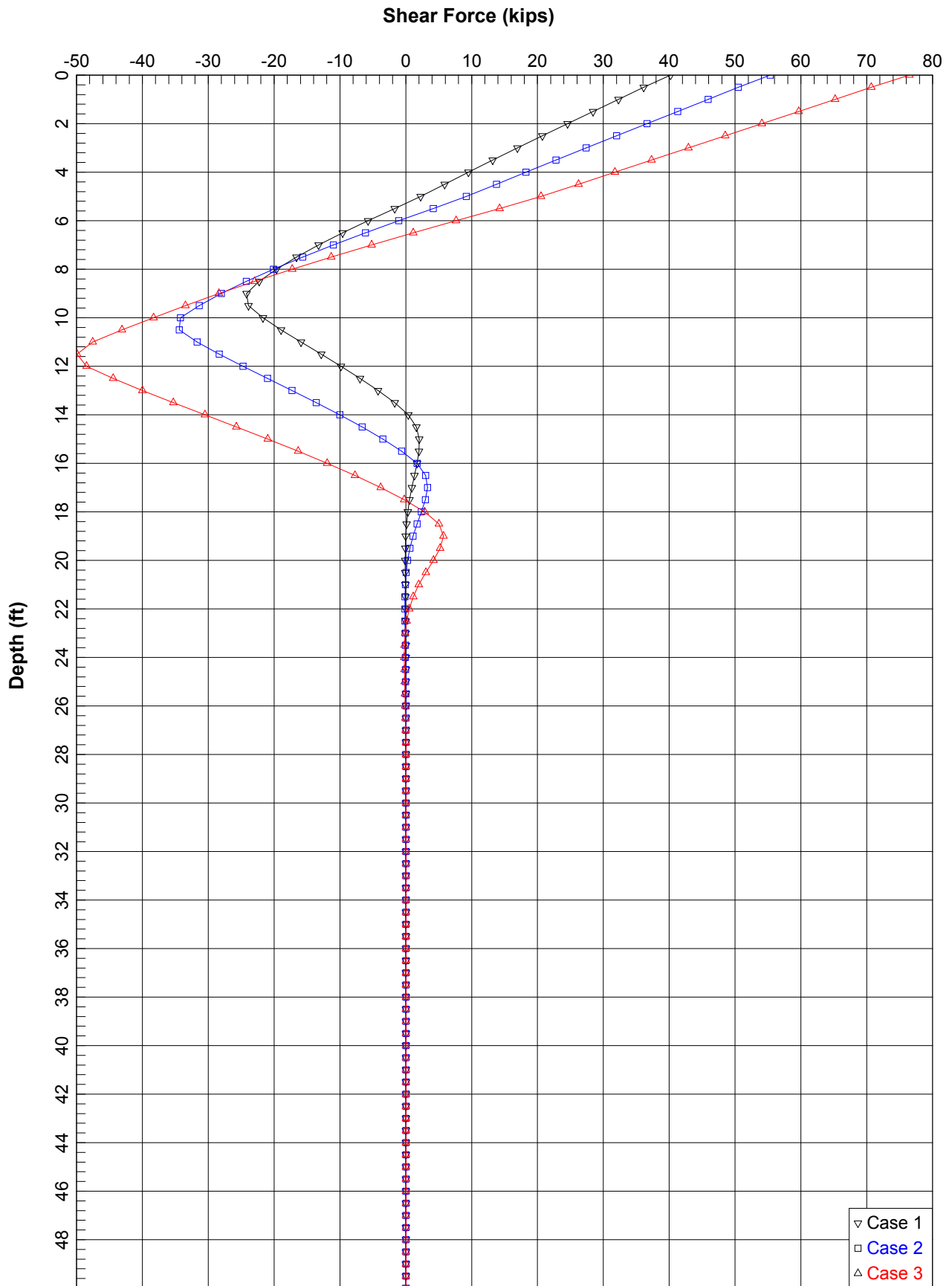
 Summary of Pile Response(s)

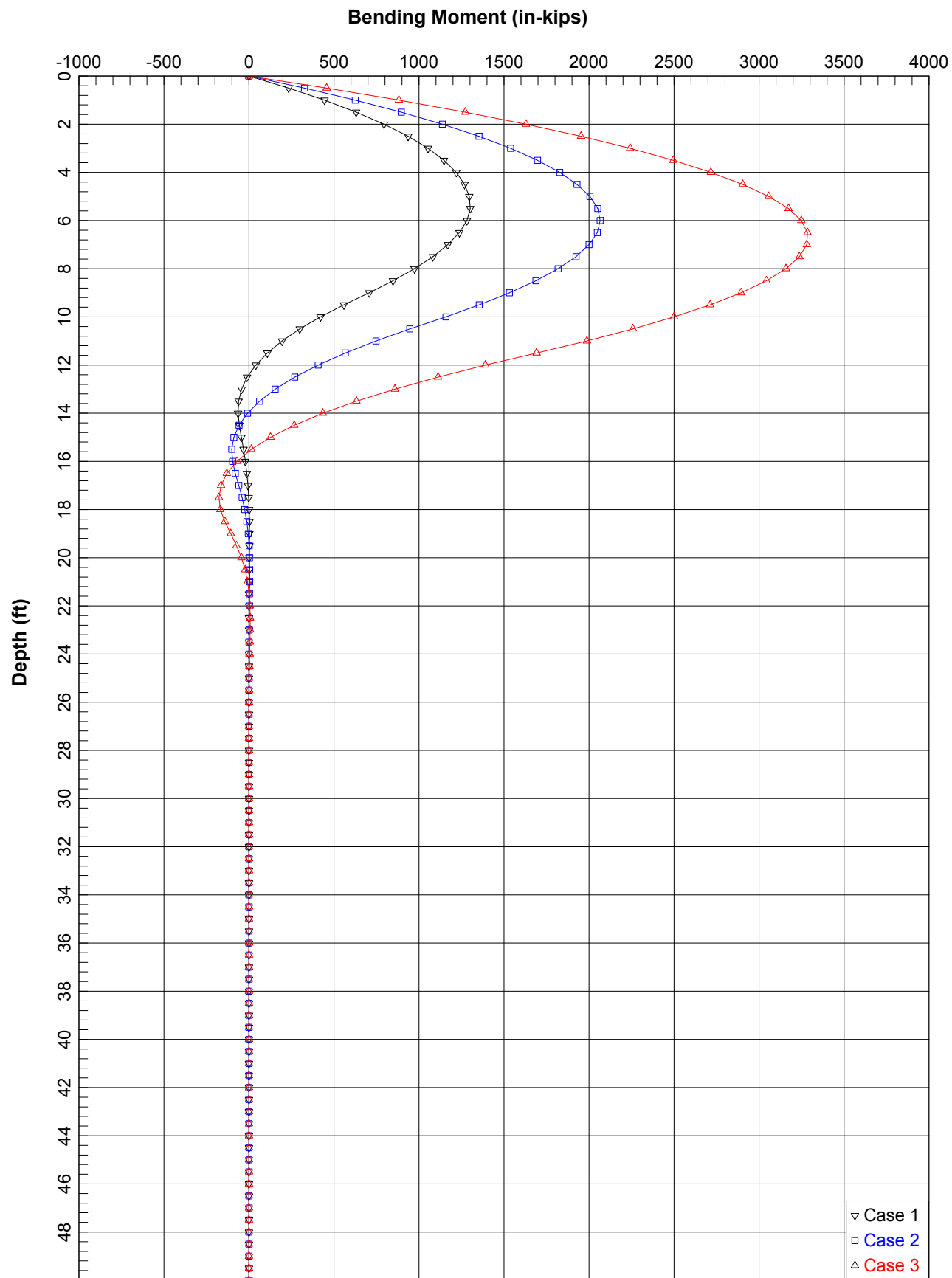
Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	226000.	0.25000000	1075927.	29567.	-0.00350481
2	4	y = 0.5000	M = 0.000	226000.	0.50000000	1710134.	40799.	-0.00623852
3	4	y = 1.0000	M = 0.000	226000.	1.00000000	2727932.	56459.	-0.01113725

The analysis ended normally.





Bent 3R_transv_Max P

Pile Plus for windows, version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Bent 3\
 Name of input data file: Bent 3R_transv_Max P.lp6d
 Name of output report file: Bent 3R_transv_Max P.lp6o
 Name of plot output file: Bent 3R_transv_Max P.lp6p
 Name of runtime message file: Bent 3R_transv_Max P.lp6r

Date and Time of Analysis

Date: September 13, 2014 Time: 20:48:52

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Transv - Pm.avg -

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 3R_transv_Max P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 4 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3250.00000 psi
 Undrained cohesion at bottom of layer = 3250.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2750.00000 psi
 Undrained cohesion at bottom of layer = 2750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 5.00000 ft
 Distance from top of pile to bottom of layer = 10.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 10.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass Factor	Layer Depth	Effective Unit wt.	Undrained Cohesion	Angle of Friction	Uniaxial Elastic Modulus	RQD %
Num.	(p-y Curve Criteria)	Rock Emass	ft	pcf	psf	deg.	psi	or GSI
50	Factor	psi	ft	Type	Property	Mod. pcf	psi	Epsilon
1	Stiff Clay w/o Free Water	--	-5.000	125.000	3250.000	--	--	--
0.00700	--	--	0.10000	125.000	3250.000	--	--	--
2	Stiff Clay w/o Free Water	--	0.10000	120.000	2750.000	--	--	--
0.00700	--	--	5.000	120.000	2750.000	--	--	--
3	Stiff Clay w/o Free Water	--	5.000	120.000	3750.000	--	--	--
0.00700	--	--	10.000	120.000	3750.000	--	--	--
4	Stiff Clay w/o Free Water	--	10.000	125.000	4500.000	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--

0.00500 Bent 3R_transv_Max P

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Table with 4 columns: Point, Depth x, p-mult, y-mult. Rows 1 and 2.

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Table with 7 columns: Load No., Load Type, Condition, Condition, Axial thrust force, Top y vs. Pile Length, Compute. Rows 1, 2, 3.

V = perpendicular shear force applied to pile head
y = bending moment applied to pile head
M = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.250000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 226000.000 lbs

Main data table with 12 columns: Depth x, Deflect. y, Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load. Rows 0.00 to 192.000.

Main data table (continued) with 12 columns: Depth x, Deflect. y, Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load. Rows 198.000 to 600.000.

* The above values of total stress are combined axial and bending stresses.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Summary table with 2 columns: Item, Value. Rows: Pile-head deflection, Computed slope at pile head, Maximum bending moment, Maximum shear force, Depth of maximum bending moment, Depth of maximum shear force, Number of iterations, Number of zero deflection points.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.500000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 226000.000 lbs

Main data table (continued) with 12 columns: Depth x, Deflect. y, Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load. Rows 0.00 to 54.000.


```

          Bent 3R_transv_Max P
594.000 2.570E-12 -6.257E-05 1.779E-05 0.000 499.5697 2.936E+10 -2.439E-06 5695312. 0.000
600.000 3.677E-12 0.000 0.000 0.000 499.5697 2.936E+10 -3.490E-06 2847656. 0.000

```

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

```

Pile-head deflection = 1.0000000 inches
Computed slope at pile head = -0.0122313 radians
Maximum bending moment = 3284229. inch-lbs
Maximum shear force = 76458. lbs
Depth of maximum bending moment = 78.0000000 inches below pile head
Depth of maximum shear force = 0.0000000 inches below pile head
Number of iterations = 15
Number of zero deflection points = 8

```

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

```

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

```

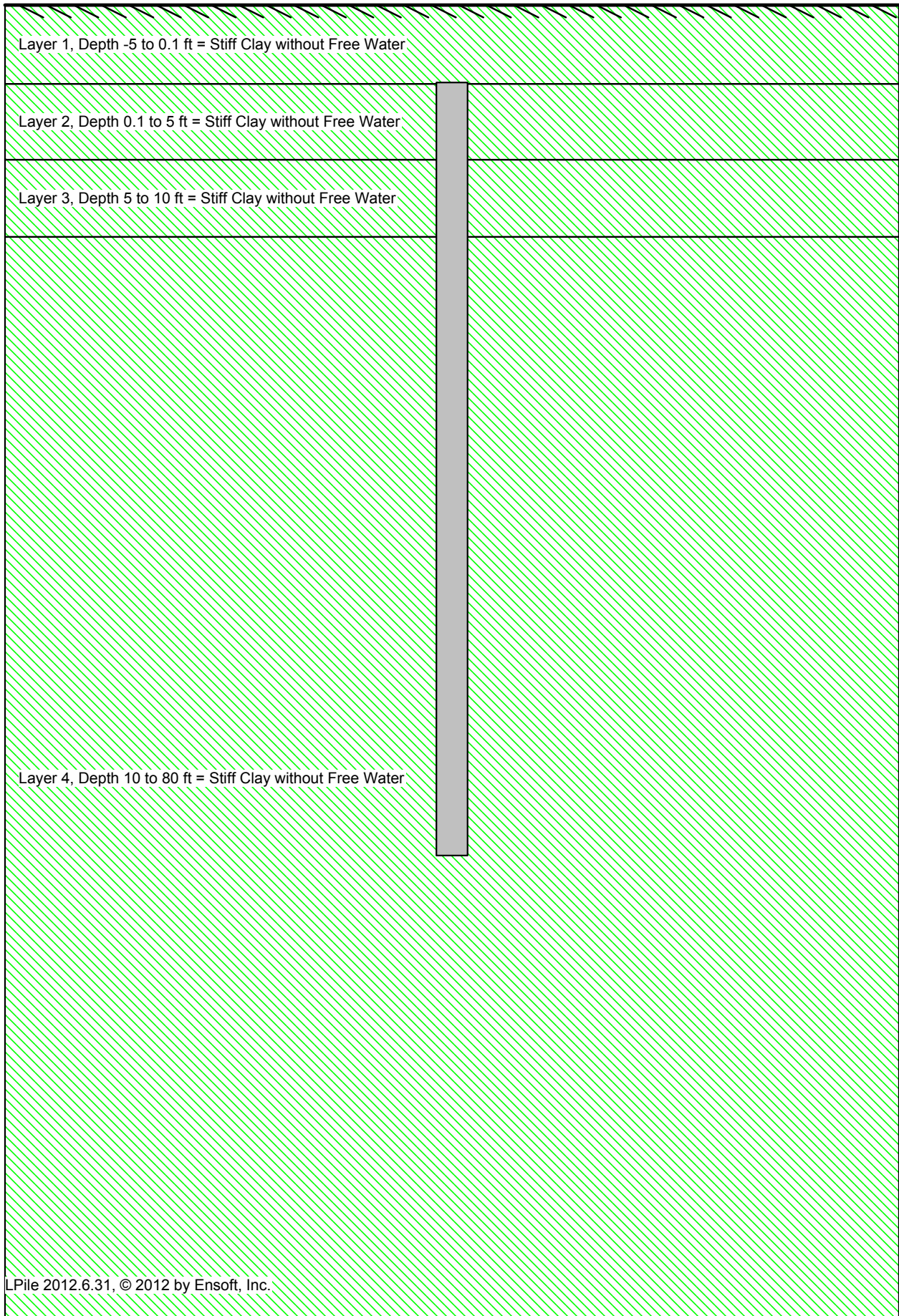
Load Case No.	Load No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 M = 0.000 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	226000.	0.25000000	1301460.	40200.	-0.00386388
2	4	y = 0.5000	M = 0.000	226000.	0.50000000	2065682.	53354.	-0.00686136
3	4	y = 1.0000	M = 0.000	226000.	1.00000000	3284229.	76458.	-0.01223127

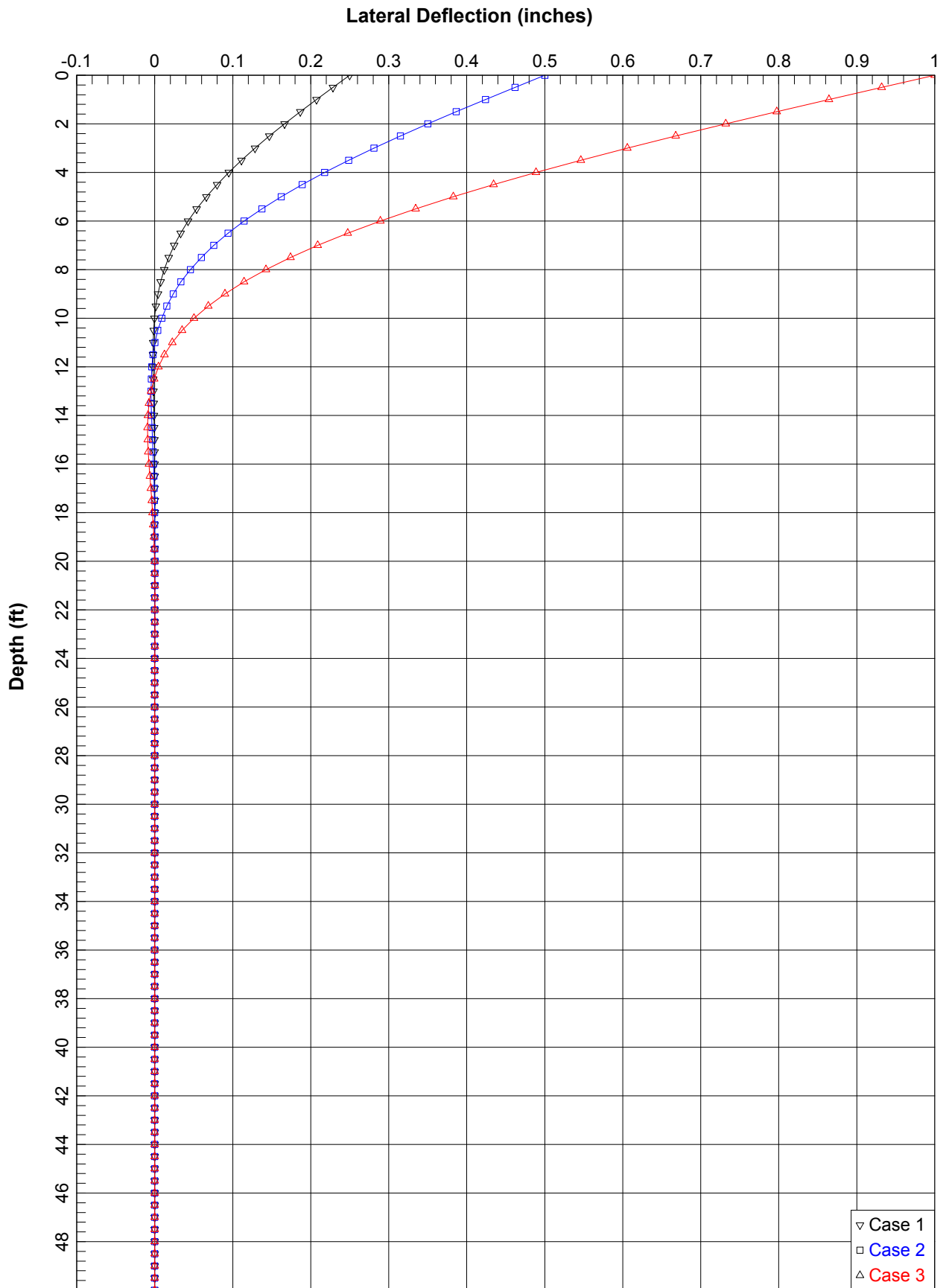
The analysis ended normally.

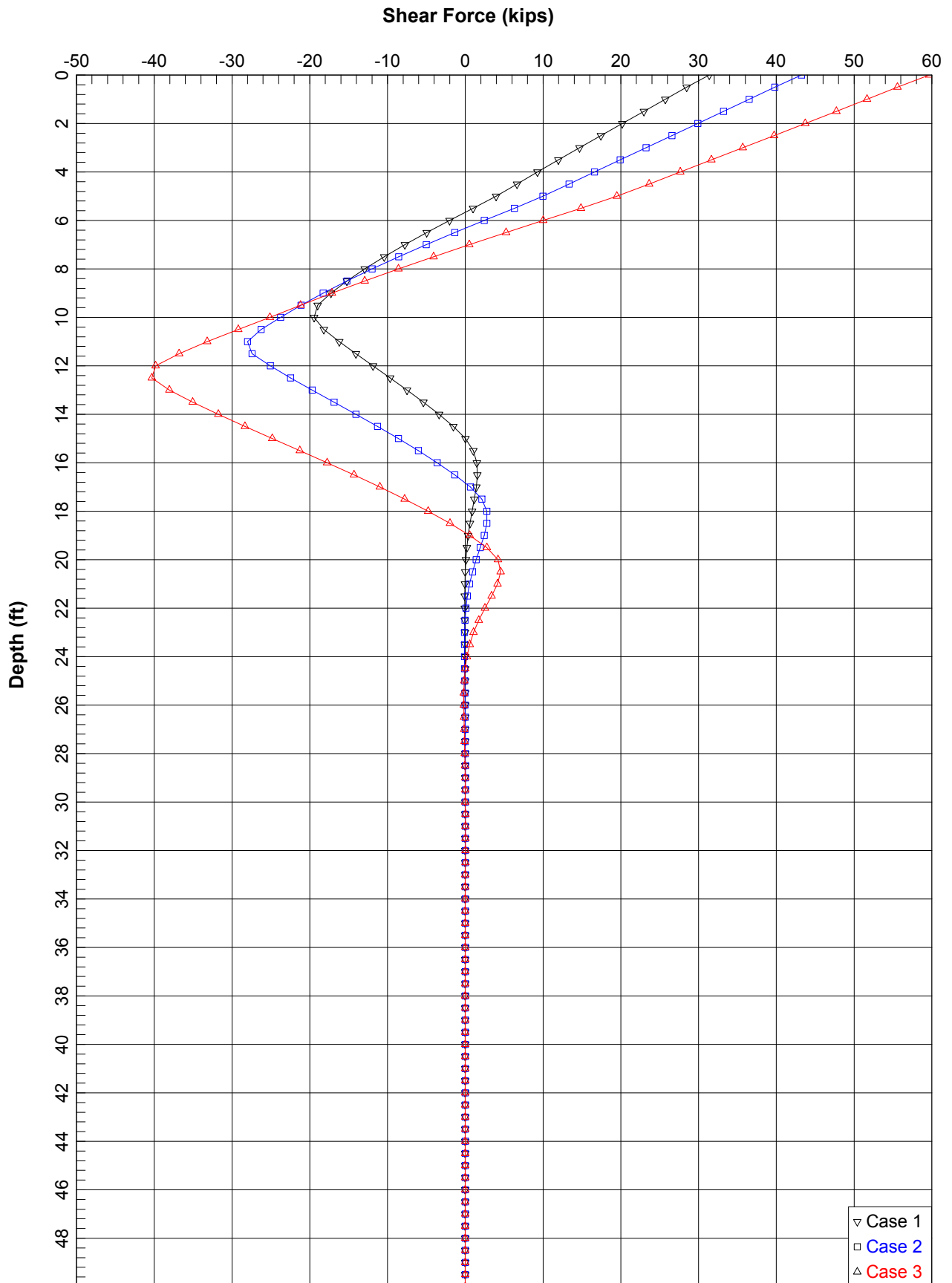
SUPPORT: BENT 3L

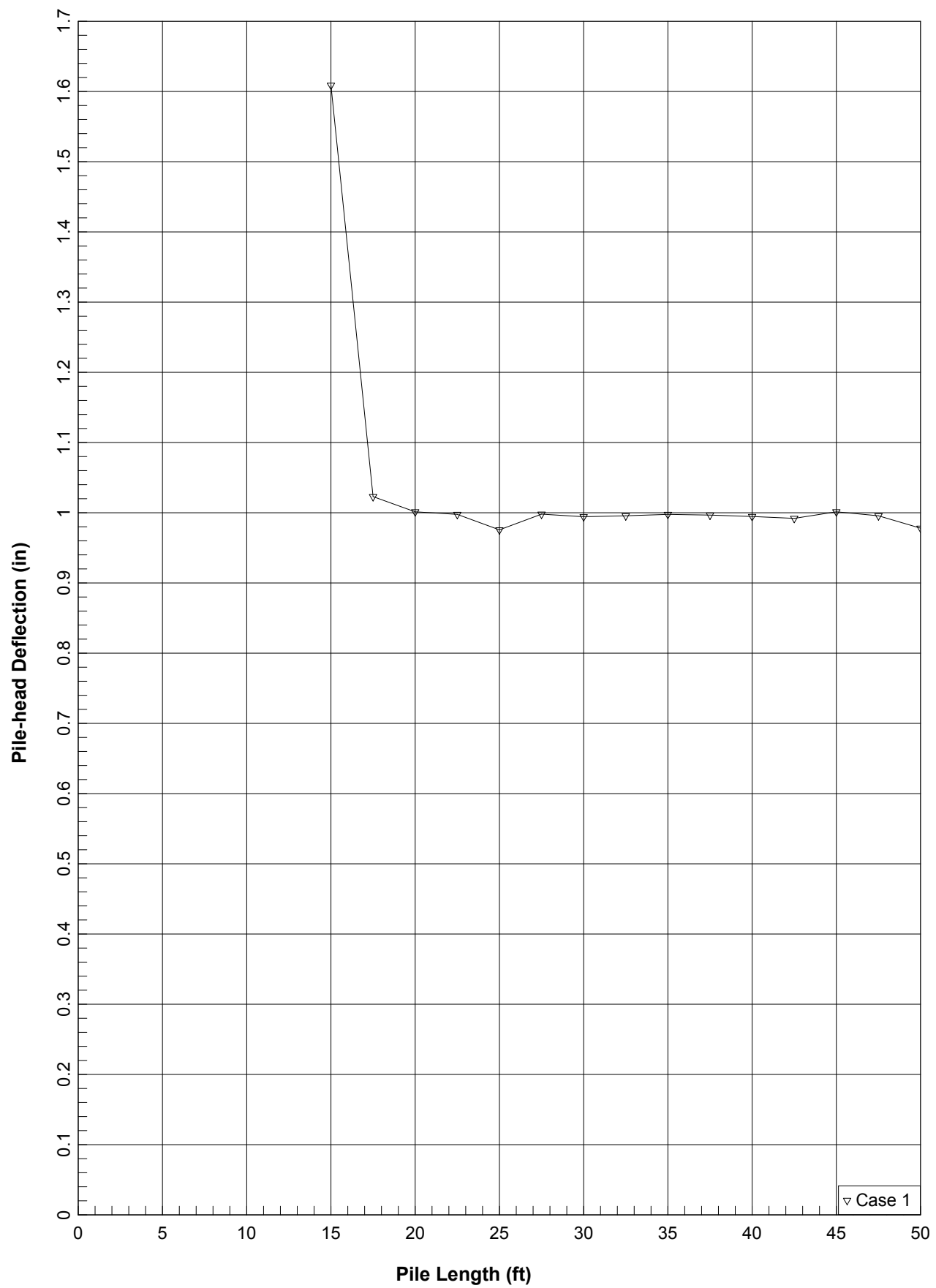
LOAD DIRECTION: LONGITUDE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE









Bent 3L_long_crit length

Pile Plus for windows, version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Bent 3\
 Name of input data file: Bent 3L_long_crit length.lp6d
 Name of output report file: Bent 3L_long_crit length.lp6r
 Name of plot output file: Bent 3L_long_crit length.lp6p
 Name of runtime message file: Bent 3L_long_crit length.lp6r

Date and Time of Analysis

Date: September 13, 2014 Time: 20:53:05

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24Inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 3L_long_crit length
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 4 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3250.00000 psi
 Undrained cohesion at bottom of layer = 3250.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2750.00000 psi
 Undrained cohesion at bottom of layer = 2750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 5.00000 ft
 Distance from top of pile to bottom of layer = 10.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 10.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass Factor	Layer Depth	Effective Unit wt.	Undrained Cohesion	Angle of Friction	Uniaxial Elastic Modulus	RQD %
Num.	(p-y Curve Criteria)	Rock Emass	ft	pcf	psi	deg.	psi	or GSI
50	Factor	psi	ft	Type	Property	Mod. pct		Epsilon
1	Stiff Clay w/o Free Water	--	-5.000	120.000	3250.000	--	--	--
0.00700	--	--	0.10000	120.000	3250.000	--	--	--
2	Stiff Clay w/o Free Water	--	0.10000	120.000	2750.000	--	--	--
0.00700	--	--	5.000	120.000	2750.000	--	--	--
3	Stiff Clay w/o Free Water	--	5.000	120.000	3750.000	--	--	--
0.00700	--	--	10.000	120.000	3750.000	--	--	--
4	Stiff Clay w/o Free Water	--	10.000	125.000	4500.000	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--

0.00500

Bent 3L_long_crit length

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Table with columns: Point, Depth x, p-mult, y-mult. Rows 1, 2.

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Table with columns: Load, Load Type, Condition, Condition, Axial thrust Force, Top y, Compute. Rows 1.

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head = 59000.000 lbs
Applied moment at pile head = 0.000 in-lbs
Axial thrust load on pile head = 268000.000 lbs

Main data table with columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load. Rows 0.00 to 210.00.

Main data table (continued) with columns: 216.000 to 600.000. Rows 216.000 to 600.000.

* The above values of total stress are combined axial and bending stresses.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Pile-head deflection = 0.9780565 inches
Computed slope at pile head = -0.0111399 radians
Maximum bending moment = 84.000000 inches below pile head
Number of iterations = 33
Number of zero deflection points = 7

Pile-head Deflection vs. Pile Length for Load Case 1

Boundary Condition Type 1, Shear and Moment

Shear = 59000. lbs
Moment = 0.000 in-lbs
Axial Load = 268000. lbs

Table with columns: Pile Length, Pile Head Deflection, Maximum Moment, Maximum Shear. Rows 50.00 to 22.500.

20.000 1.0012271 2800609. 59000. Bent 3L_long_crit length
 17.500 1.0231328 2782538. 59000.
 15.000 1.6089180 2573285. 59000.

 Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	1	V = 59000.	M = 0.000	268000.	0.97805652	2790180.	59000.	-0.01113988

The analysis ended normally.

Bent 3L_long_Ave P

Pile Plus for windows, version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\updated_ET 9-14-14\Bent 3\
 Name of input data file: Bent 3L_long_Ave P.lpd
 Name of output report file: Bent 3L_long_Ave P.lpr
 Name of plot output file: Bent 3L_long_Ave P.lpp
 Name of runtime message file: Bent 3L_long_Ave P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 20:51:26

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24Inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Transv - Pm.avg -

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 3L_long_Ave P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top width = 24.0000000 in
 Bottom width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 4 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3250.00000 psi
 Undrained cohesion at bottom of layer = 3250.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2750.00000 psi
 Undrained cohesion at bottom of layer = 2750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 5.00000 ft
 Distance from top of pile to bottom of layer = 10.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 10.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass Factor	Layer Depth	Effective Unit wt.	Undrained Cohesion	Angle of Friction	Uniaxial Elastic Modulus	RQD %
Num.	(p-y Curve Criteria)	Rock Emass	ft	pcf	psf	deg.	psi	or GSI
50	Factor	psi	ft	Type	Property	Mod. pcf	psi	Epsilon
1	Stiff Clay w/o Free Water	--	-5.000	125.000	3250.000	--	--	--
0.00700	--	--	0.10000	125.000	3250.000	--	--	--
2	Stiff Clay w/o Free Water	--	0.10000	120.000	2750.000	--	--	--
0.00700	--	--	5.000	120.000	2750.000	--	--	--
3	Stiff Clay w/o Free Water	--	5.000	120.000	3750.000	--	--	--
0.00700	--	--	10.000	120.000	3750.000	--	--	--
4	Stiff Clay w/o Free Water	--	10.000	125.000	4500.000	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--

0.00500 Bent 3L_Long_Ave P

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Table with 4 columns: Point, Depth x, p-mult, y-mult. Rows 1 and 2 showing modifier values at different depths.

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Table with 7 columns: Load, Load Type, Condition, Condition, Axial Thrust Force, Top y, Compute. Rows 1, 2, 3 detailing load specifications.

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.250000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 268000.000 lbs

Table with 12 columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load. Rows 0.00 to 192.000 showing pile response data.

Table with 12 columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load. Rows 198.000 to 600.000 showing pile response data.

* The above values of total stress are combined axial and bending stress.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Table with 2 columns: Parameter, Value. Rows for Pile-head deflection, Computed slope at pile head, Maximum bending moment, etc.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.500000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 268000.000 lbs

Table with 12 columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load. Rows 0.00 to 54.000 showing pile response data.


```

          Bent 3L_Tong_Ave P
594.000 -3.371E-11 0.000412 -0.000137 0.000 592.4101 2.936E+10 2.276E-05 4050000. 0.000
600.000 -3.388E-11 0.000 0.000 0.000 592.4101 2.936E+10 2.287E-05 2025000. 0.000

```

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

```

Pile-head deflection = 1.0000000 inches
Computed slope at pile head = -0.0113504 radians
Maximum bending moment = 2832694. inch-lbs
Maximum shear force = 59678. lbs
Depth of maximum bending moment = 84.0000000 inches below pile head
Depth of maximum shear force = 0.0000000 inches below pile head
Number of iterations = 22
Number of zero deflection points = 7

```

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

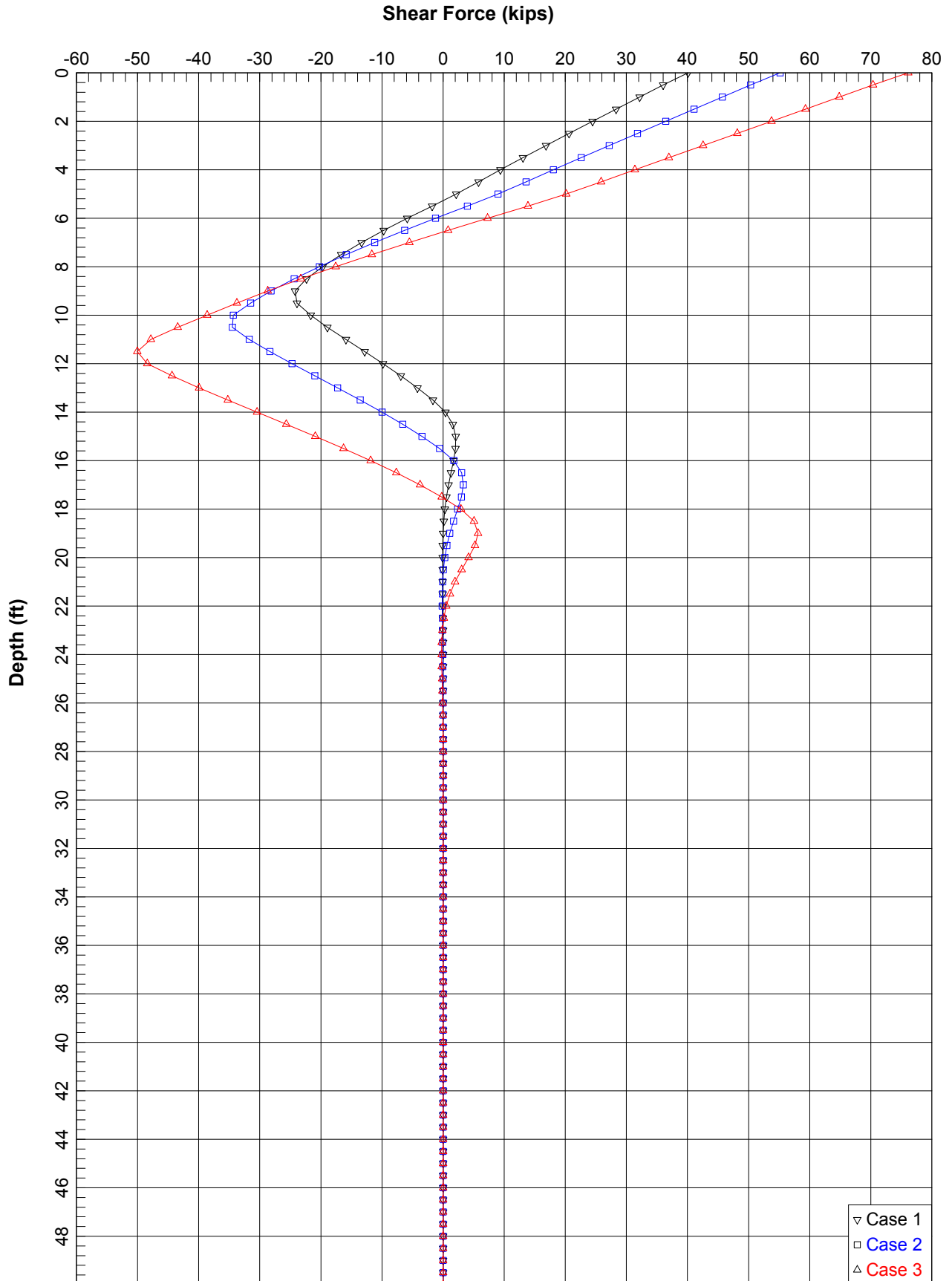
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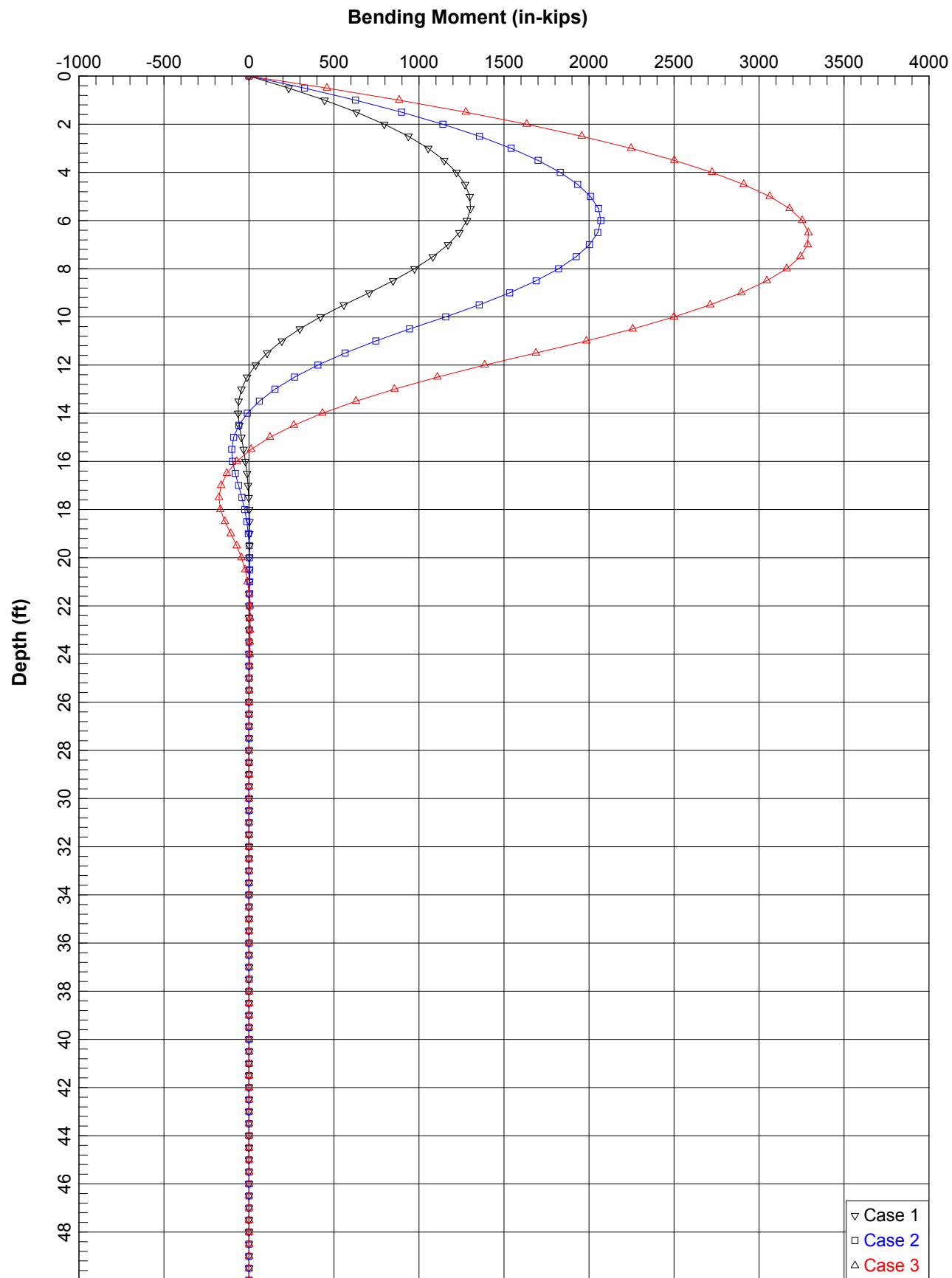
Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

```

Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	268000.	0.25000000	1117720.	31357.	-0.00357516
2	4	y = 0.5000	M = 0.000	268000.	0.50000000	1781471.	43239.	-0.00636952
3	4	y = 1.0000	M = 0.000	268000.	1.00000000	2832694.	59678.	-0.01135036

The analysis ended normally.





Bent 3L_Long_Max P

Pile Plus for windows, version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\updated_ET 9-14-14\Bent 3\
 Name of input data file: Bent 3L_Long_Max P.lpd
 Name of output report file: Bent 3L_Long_Max P.lpr
 Name of plot output file: Bent 3L_Long_Max P.lpp
 Name of runtime message file: Bent 3L_Long_Max P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 20:54:30

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24Inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Transv - Pm.avg -

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 3L_Long_Max P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 4 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3250.00000 psi
 Undrained cohesion at bottom of layer = 3250.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2750.00000 psi
 Undrained cohesion at bottom of layer = 2750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 5.00000 ft
 Distance from top of pile to bottom of layer = 10.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 10.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass Factor	Layer Depth	Effective Unit wt.	Undrained Cohesion	Angle of Friction	Uniaxial Elastic Modulus	RQD %
Num.	(p-y Curve Criteria)	Rock Emass	ft	pcf	psf	deg.	psi	or GSI
50	Factor	psi	ft	Type	Property	Mod. pcf	psi	Epsilon
1	Stiff Clay w/o Free Water	--	-5.000	125.000	3250.000	--	--	--
0.00700	--	--	0.10000	125.000	3250.000	--	--	--
2	Stiff Clay w/o Free Water	--	0.10000	120.000	2750.000	--	--	--
0.00700	--	--	5.000	120.000	2750.000	--	--	--
3	Stiff Clay w/o Free Water	--	5.000	120.000	3750.000	--	--	--
0.00700	--	--	10.000	120.000	3750.000	--	--	--
4	Stiff Clay w/o Free Water	--	10.000	125.000	4500.000	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--

0.00500 Bent 3L_Long_Max P

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Table with 4 columns: Point, Depth x, p-mult, y-mult. Rows 1 and 2 showing modifier values at different depths.

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Table with 7 columns: Load, Load Type, Condition, Condition, Axial thrust force, Top y vs. Pile Length, Compute. Rows 1, 2, 3 detailing load specifications.

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness relative to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection

For Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.250000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 268000.000 lbs

Large table with 12 columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load. Rows 0.00 to 192.000.

Large table with 12 columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load. Rows 198.000 to 54.000.

* The above values of total stress are combined axial and bending stress.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Summary table with 2 columns: Item, Value. Rows for Pile-head deflection, Computed slope, Maximum bending moment, etc.

Computed Values of Pile Loading and Deflection

For Lateral Loading for Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.500000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 268000.000 lbs

Table with 12 columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load. Rows 0.00 to 54.000.


```

          Bent 3L_Tong_Max P
594.000 2.569E-12 -6.237E-05 1.776E-05 0.000 592.4101 2.936E+10 -2.439E-06 5695312. 0.000
600.000 3.667E-12 0.000 0.000 0.000 592.4101 2.936E+10 -3.481E-06 2847656. 0.000

```

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

```

Pile-head deflection = 1.0000000 inches
Computed slope at pile head = -0.0122408 radians
Maximum bending moment = 3289901. inch-lbs
Maximum shear force = 76099. lbs
Depth of maximum bending moment = 78.0000000 inches below pile head
Depth of maximum shear force = 0.0000000 inches below pile head
Number of iterations = 15
Number of zero deflection points = 8

```

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

```

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

```

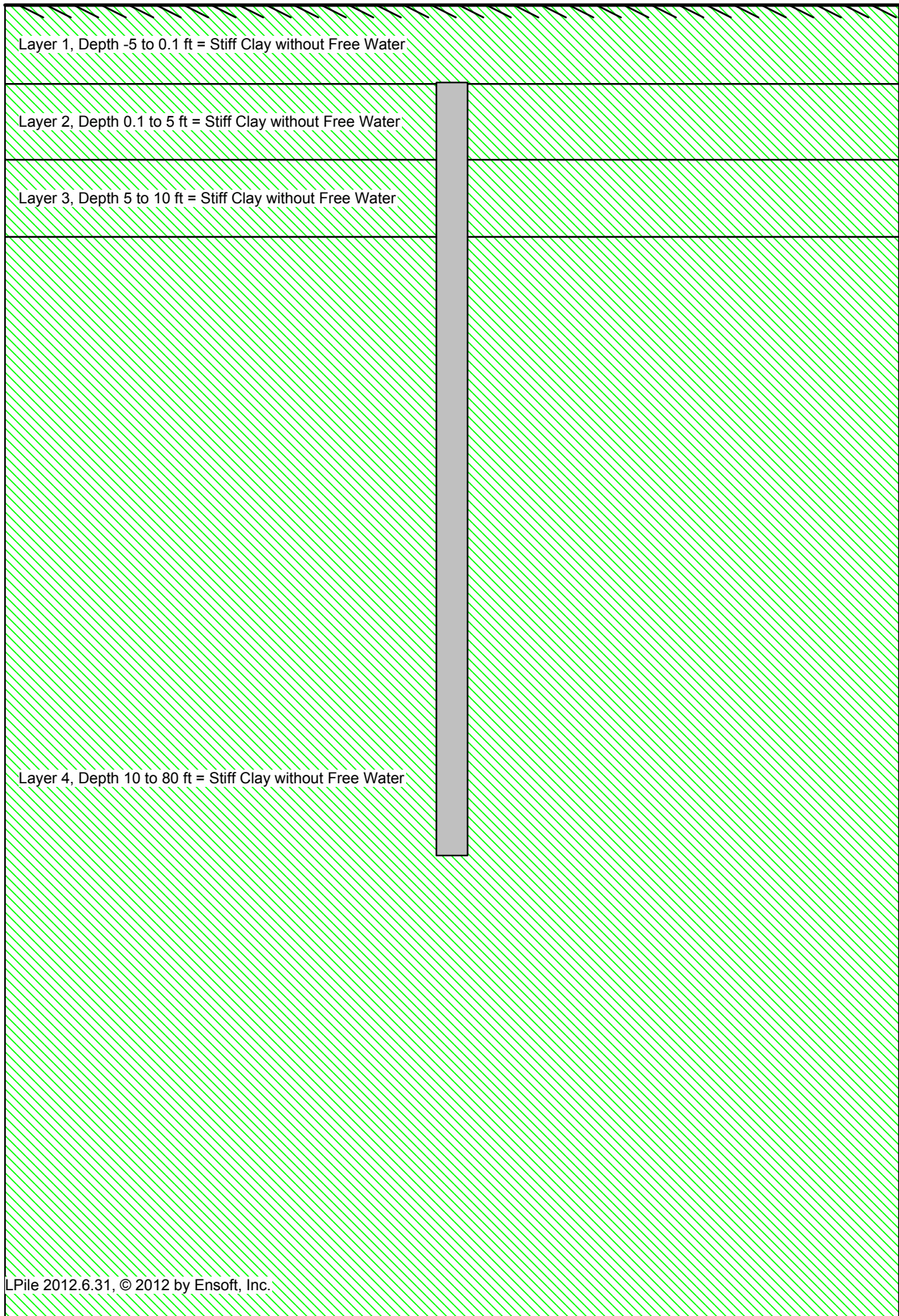
Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 M = 0.000 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	268000.	0.25000000	1302846.	40088.	-0.00386596
2	4	y = 0.5000	M = 0.000	268000.	0.50000000	2068902.	51159.	-0.00686678
3	4	y = 1.0000	M = 0.000	268000.	1.00000000	3289901.	76099.	-0.01224081

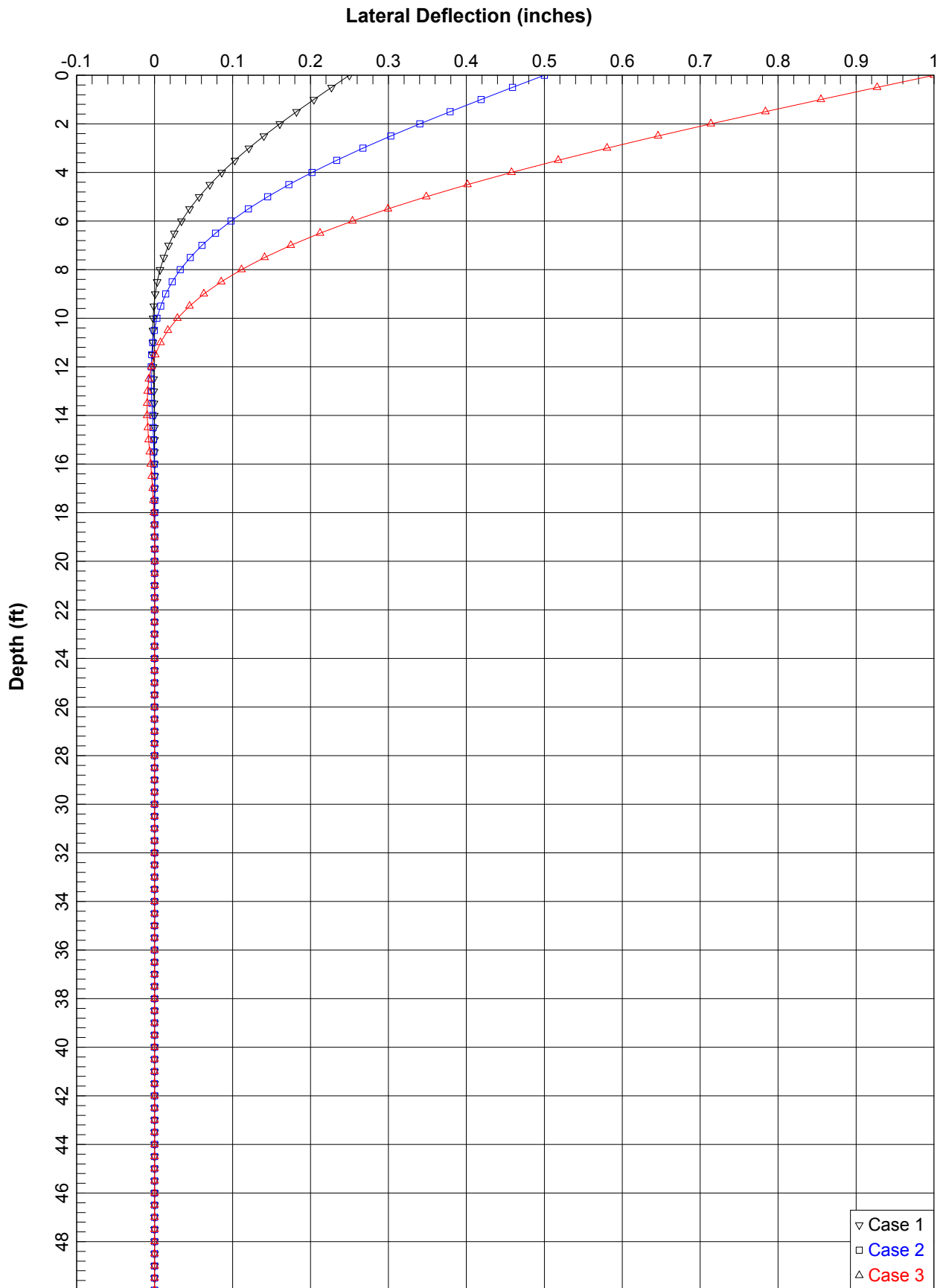
The analysis ended normally.

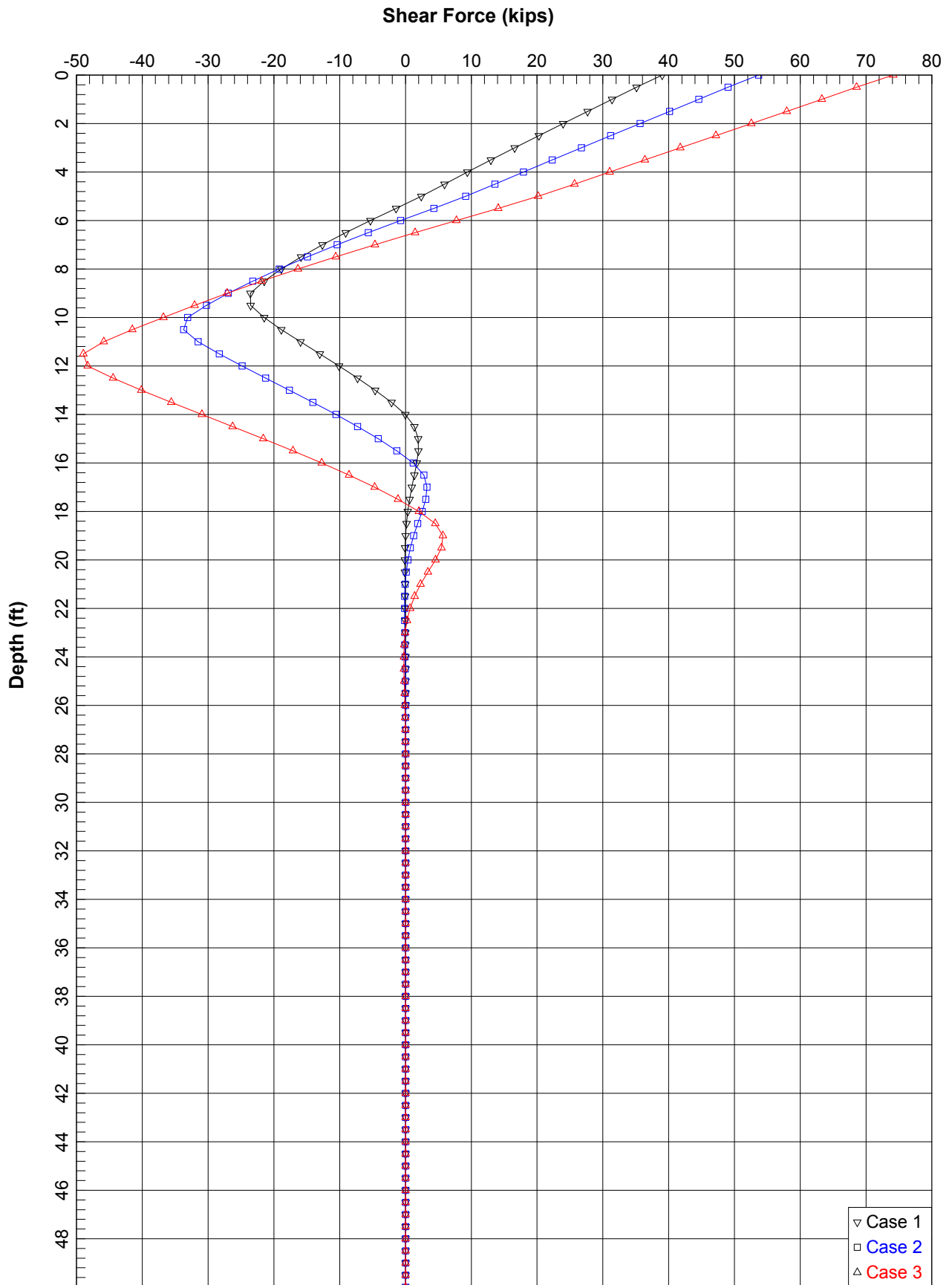
SUPPORT: BENT 3L

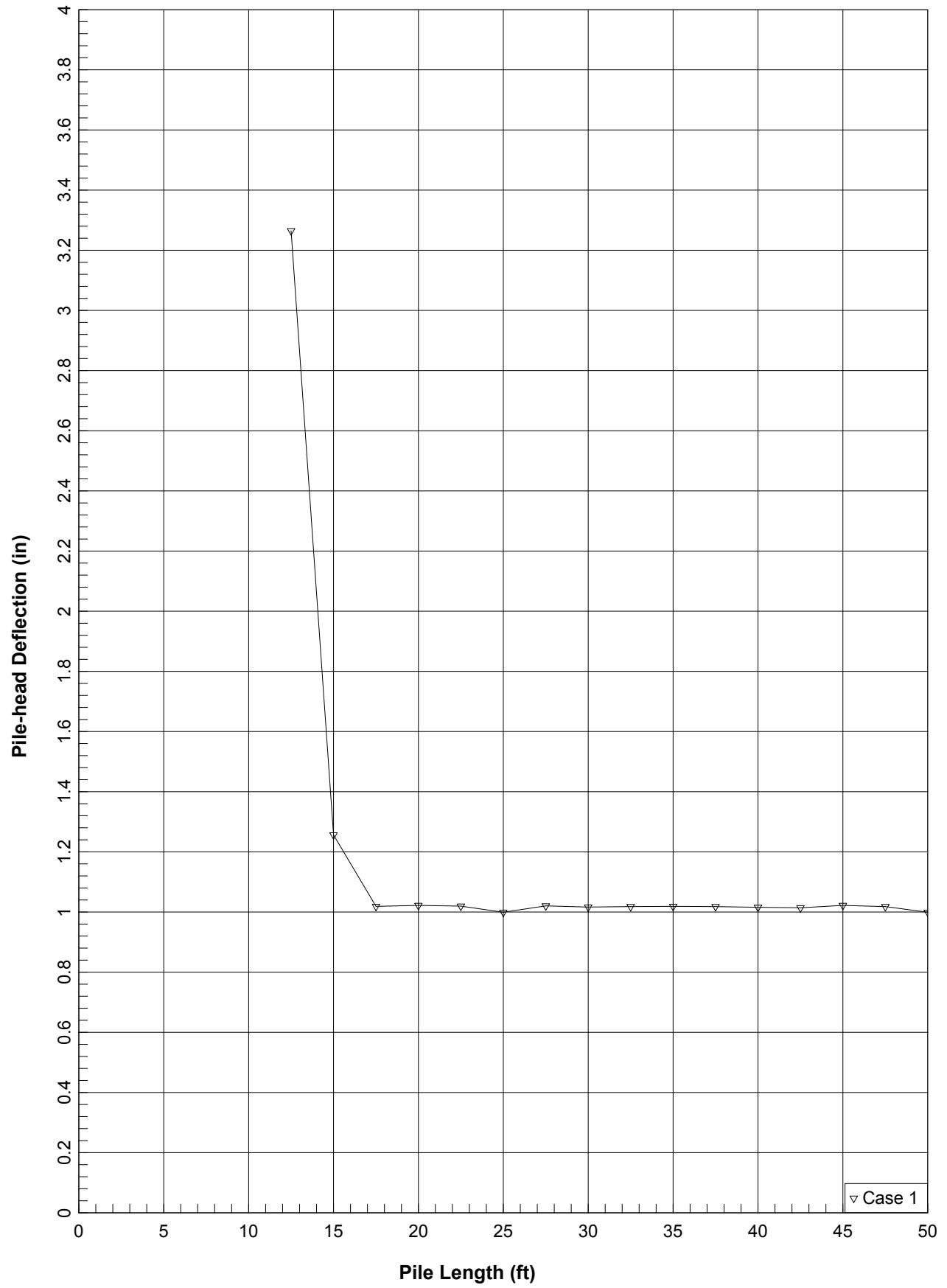
LOAD DIRECTION: TRANSVERSE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE









Bent 3L_transv_Crit Length

Pile Plus for windows, version 2012-06-031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Bent 3\
 Name of input data file: Bent 3L_transv_Crit Length.lpd
 Name of output report file: Bent 3L_transv_Crit Length.lpd
 Name of plot output file: Bent 3L_transv_Crit Length.lpd
 Name of runtime message file: Bent 3L_transv_Crit Length.lpd

Date and Time of Analysis

Date: September 13, 2014 Time: 20:58:36

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24Inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 3L_transv_Crit Length
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 4 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3250.00000 psi
 Undrained cohesion at bottom of layer = 3250.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2750.00000 psi
 Undrained cohesion at bottom of layer = 2750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 5.00000 ft
 Distance from top of pile to bottom of layer = 10.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 10.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass Factor	Layer Depth	Effective Unit wt.	Undrained Cohesion	Angle of Friction	Uniaxial Elastic Modulus	RQD %
Num.	(p-y Curve Criteria)	Rock Emass	ft	pcf	psf	deg.	psi	or GSI
50	Factor	psi	ft	Type	Property	Mod. pcf	psi	Epsilon
1	Stiff Clay w/o Free Water	--	-5.000	120.000	3250.000	--	--	--
0.00700	--	--	0.10000	120.000	3250.000	--	--	--
2	Stiff Clay w/o Free Water	--	0.10000	120.000	2750.000	--	--	--
0.00700	--	--	5.000	120.000	2750.000	--	--	--
3	Stiff Clay w/o Free Water	--	5.000	120.000	3750.000	--	--	--
0.00700	--	--	10.000	120.000	3750.000	--	--	--
4	Stiff Clay w/o Free Water	--	10.000	125.000	4500.000	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--

20.000 1.0221764 3245340. 74000. Bent 3L_transv_Crit length
 17.500 1.0190636 3244163. 74000.
 15.000 1.2561349 3101012. 74000.
 12.500 3.2650818 2787124. 74000.

 Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	1	V = 74000.	M = 0.000	268000.	0.99948576	3233879.	74000.	-0.01213688

The analysis ended normally.

Bent 3L_transv_Ave P

Pile Plus for windows, version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Bent 3\
 Name of input data file: Bent 3L_transv_Ave P.lp6d
 Name of output report file: Bent 3L_transv_Ave P.lp6o
 Name of plot output file: Bent 3L_transv_Ave P.lp6p
 Name of runtime message file: Bent 3L_transv_Ave P.lp6r

Date and Time of Analysis

Date: September 13, 2014 Time: 20:57:12

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24Inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Transv - Pm.avg -

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 3L_transv_Ave P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 4 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3250.00000 psi
 Undrained cohesion at bottom of layer = 3250.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2750.00000 psi
 Undrained cohesion at bottom of layer = 2750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 5.00000 ft
 Distance from top of pile to bottom of layer = 10.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 10.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Rock Emass	Layer Depth krm	Effective unit wt. pcf	Undrained In-situ Cohesion psf	Angle of Friction deg.	Uniaxial Elastic Mod. psi	RQD % or GSI	Epsilon
50	Factor								
1	Stiff Clay w/o Free Water	--	-5.000	125.000	3250.000	--	--	--	--
0.00700	--	--	0.10000	125.000	3250.000	--	--	--	--
2	Stiff Clay w/o Free Water	--	0.10000	120.000	2750.000	--	--	--	--
0.00700	--	--	5.000	120.000	2750.000	--	--	--	--
3	Stiff Clay w/o Free Water	--	5.000	120.000	3750.000	--	--	--	--
0.00700	--	--	10.000	120.000	3750.000	--	--	--	--
4	Stiff Clay w/o Free Water	--	10.000	125.000	4500.000	--	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--	--

0.00500 --- Bent 3l_transv_Ave P ---

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Table with columns: Point, Depth x, p-mult, y-mult. Rows 1-2 showing values for different depths.

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Table with columns: Load No., Load Type, Condition, Condition, Axial thrust Force, Top y vs. Pile Length. Rows 1-3.

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.250000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 268000.000 lbs

Main data table with columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load. Rows 0.00 to 192.000.

Main data table (continued) with columns: 198.000 to 600.000. Rows 198.000 to 600.000.

* The above values of total stress are combined axial and bending stress.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Summary table with columns: Pile-head deflection, Computed slope at pile head, Maximum bending moment, Maximum shear force, Depth of maximum bending moment, Depth of maximum shear force, Number of iterations, Number of zero deflection points.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.500000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 268000.000 lbs

Main data table (continued) with columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load. Rows 0.00 to 54.000.

Table with columns for pile ID, lateral load (k), axial load (k), deflection (in), moment (k-ft), and bending moment (k-ft). Includes a section for Bent 3L transv Ave P.

Table with columns for Depth (ft), Deflect. (in), Bending Moment (k-ft), Shear Force (k), Slope (psi), Total Stress (lb/sq in), Bending Stiffness (lb-in), Soil Res. (lb/in), Soil Spr. (lb/sq ft), and Distrib. Lat. Load (lb/inch). Includes a section for Computed values of Pile Loading and Deflection for Lateral Loading for Load Case Number 3.

* The above values of total stress are combined axial and bending stress.
Output Verification: Computed forces and moments are within specified convergence limits.
Output Summary for Load Case No. 2:

Page 5 Page 6

```

594.000 2.998E-12 -8.016E-05 2.167E-05 0.000 Bent 3L_transV_Ave P 592.4101 2.936E+10 -2.741E-06 5484375. 0.000
600.000 4.903E-12 0.000 0.000 0.000 592.4101 2.936E+10 -4.482E-06 2742187. 0.000

```

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

```

Pile-head deflection = 1.0000000 inches
Computed slope at pile head = -0.0121463 radians
Maximum bending moment = 3236906. inch-lbs
Maximum shear force = 74106. lbs
Depth of maximum bending moment = 84.0000000 inches below pile head
Depth of maximum shear force = 0.0000000 inches below pile head
Number of iterations = 18
Number of zero deflection points = 8

```

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

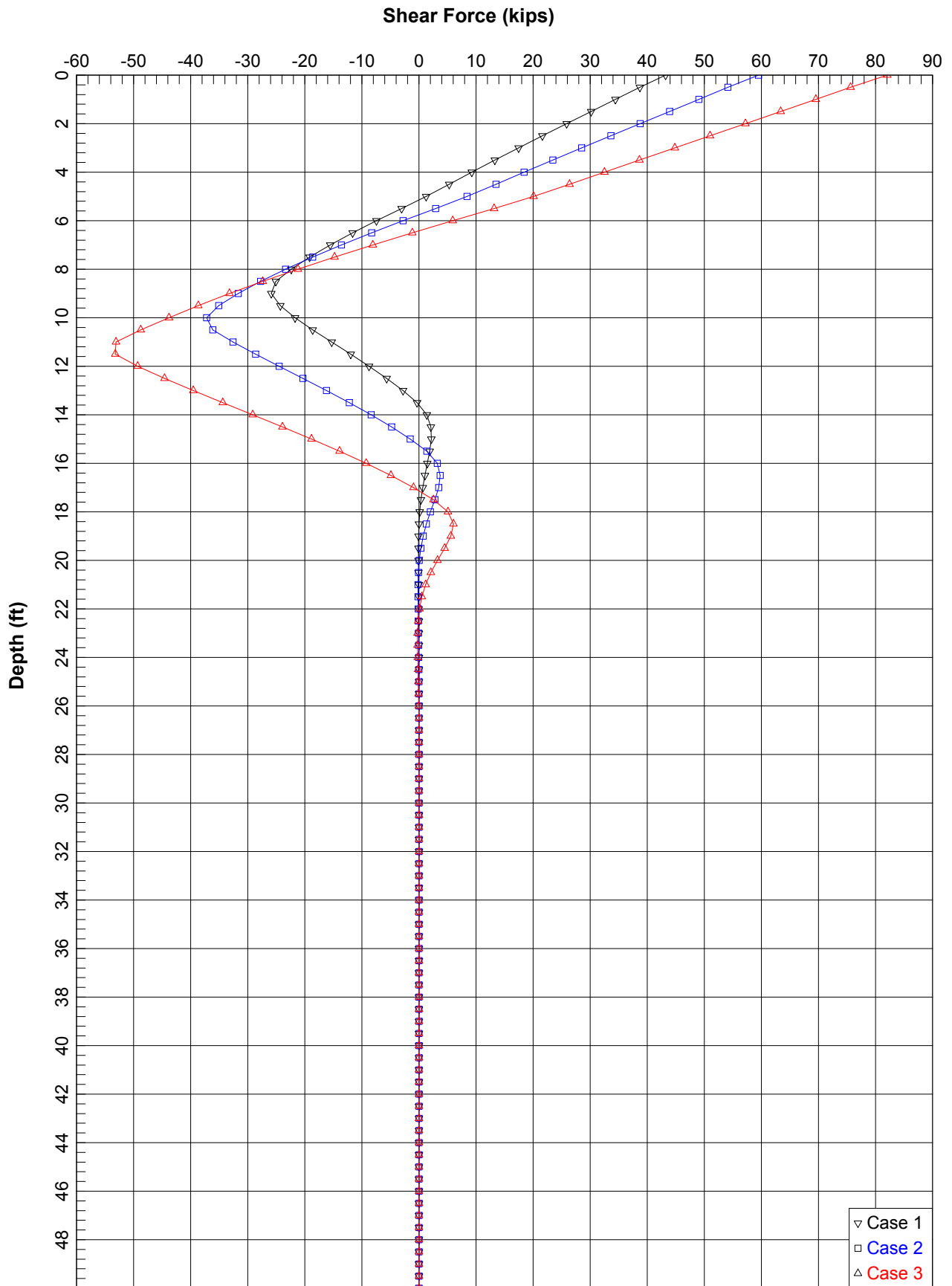
```

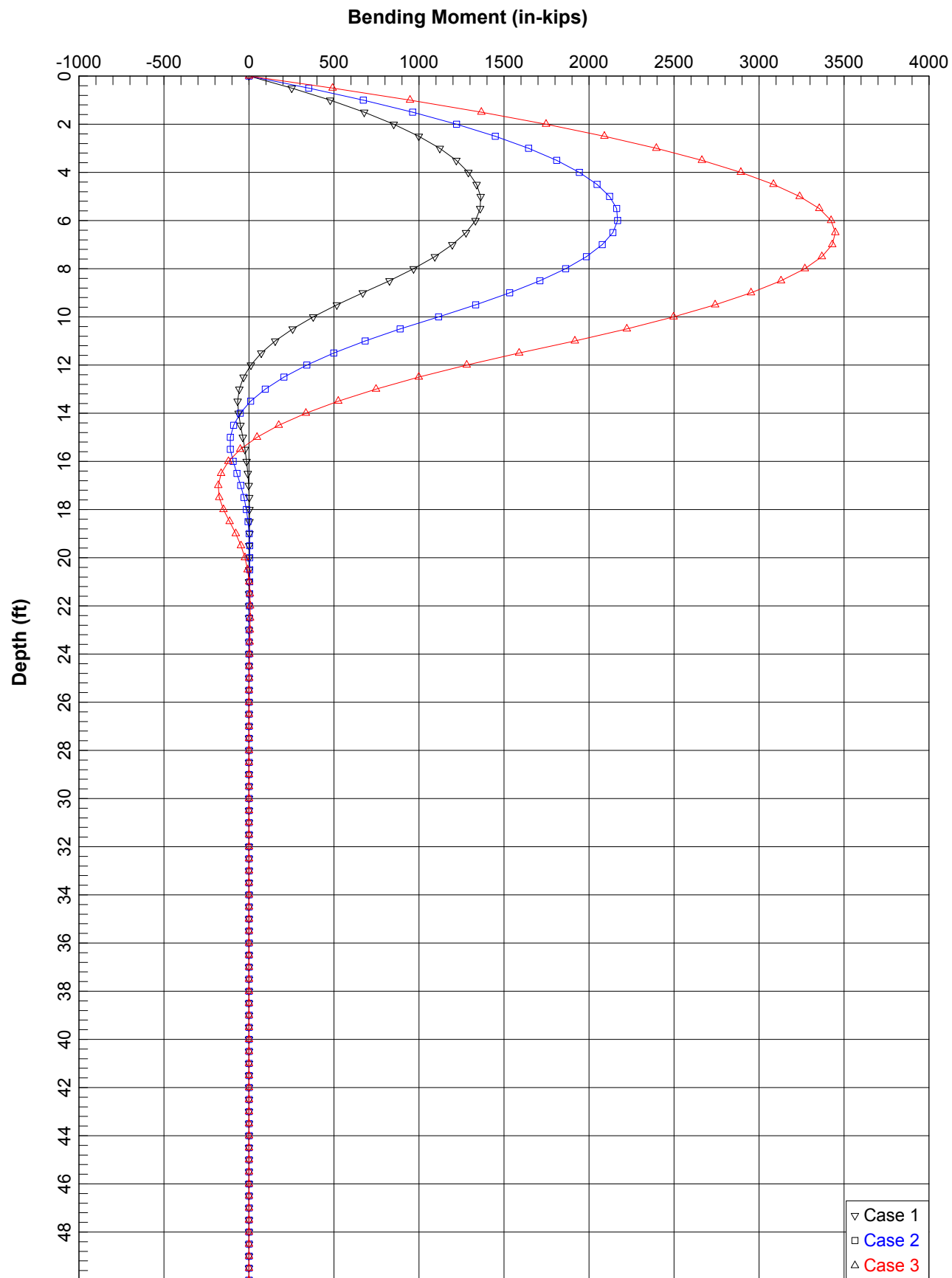
Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

```

Load Case No.	Load No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 M = 0.000 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	268000.	0.25000000	1281545.	39010.	-0.00383198
2	4	y = 0.5000	M = 0.000	268000.	0.50000000	2034209.	53661.	-0.00680806
3	4	y = 1.0000	M = 0.000	268000.	1.00000000	3236906.	74106.	-0.01214626

The analysis ended normally.





Bent 3L_transv_Max P

Pile Plus for windows, version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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 Serial Number of Security Device: 161633771
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Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Bent 3\
 Name of input data file: Bent 3L_transv_Max P.lp6d
 Name of output report file: Bent 3L_transv_Max P.lp6o
 Name of plot output file: Bent 3L_transv_Max P.lp6p
 Name of runtime message file: Bent 3L_transv_Max P.lp6r

Date and Time of Analysis

Date: September 13, 2014 Time: 20:59:44

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24Inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Transv - Pm.avg -

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
 - Maximum number of iterations allowed = 100
 - Deflection tolerance for convergence = 1.0000E-05 in
 - Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 3L_transv_Max P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 4 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3250.00000 psi
 Undrained cohesion at bottom of layer = 3250.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 0.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 2750.00000 psi
 Undrained cohesion at bottom of layer = 2750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 5.00000 ft
 Distance from top of pile to bottom of layer = 10.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3750.00000 psi
 Undrained cohesion at bottom of layer = 3750.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 10.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Soil Type	Rock Mass Factor	Layer Depth	Effective Unit wt.	Undrained Cohesion	Angle of Friction	Uniaxial Elastic Mod.	RQD %
Num.	(p-y Curve Criteria)	Rock Emass	ft	pcf	psf	deg.	psi	or GSI
50	Factor	psi	ft	Type	Property	Mod. pcf	psi	Epsilon
1	Stiff Clay w/o Free Water	--	-5.000	125.000	3250.000	--	--	--
0.00700	--	--	0.10000	125.000	3250.000	--	--	--
2	Stiff Clay w/o Free Water	--	0.10000	120.000	2750.000	--	--	--
0.00700	--	--	5.000	120.000	2750.000	--	--	--
3	Stiff Clay w/o Free Water	--	5.000	120.000	3750.000	--	--	--
0.00700	--	--	10.000	120.000	3750.000	--	--	--
4	Stiff Clay w/o Free Water	--	10.000	125.000	4500.000	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--

0.00500

Bent 3L_transv_Max P

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Table with 4 columns: Point, Depth x, p-mult, y-mult. Rows 1 and 2.

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Table with 7 columns: Load No., Load Type, Condition, Condition, Axial thrust force, Top y vs. Pile Length, Compute. Rows 1, 2, 3.

V = perpendicular shear force applied to pile head

M = bending moment applied to pile head

y = lateral deflection relative to pile axis

S = pile slope relative to original pile batter angle

R = rotational stiffness applied to pile head

Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4) Displacement of pile head = 0.250000 inches Moment at pile head = 0.000 in-lbs Axial load at pile head = 268000.000 lbs

Table with 12 columns: Depth x, Deflect. y, Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load. Rows 0.00 to 192.000.

Table with 12 columns: 198.000 to 600.000, 7.291E-05 to 0.000, -6617.9448 to 0.000, 1032.9582 to 0.000, -1.705E-06 to 0.000, Bent 3L_transv_Max P, -70.8543 to 0.000, 5830514. to 0.000.

* The above values of total stress are combined axial and bending stress.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Table with 2 columns: Item, Value. Rows: Pile-head deflection, Computed slope at pile head, Maximum bending moment, Maximum shear force, Depth of maximum bending moment, Depth of maximum shear force, Number of iterations, Number of zero deflection points.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4) Displacement of pile head = 0.500000 inches Moment at pile head = 0.000 in-lbs Axial load at pile head = 268000.000 lbs

Table with 12 columns: Depth x, Deflect. y, Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load. Rows 0.00 to 54.000.


```

594.000 1.096E-12 -1.972E-05 6.751E-06 0.000 Bent 3L_transv_Max P 592.4101 2.936E+10 -1.155E-06 6328125. 0.000
600.000 1.038E-12 0.000 0.000 0.000 592.4101 2.936E+10 -1.095E-06 3164062. 0.000

```

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

```

Pile-head deflection = 1.0000000 inches
Computed slope at pile head = -0.0125273 radians
Maximum bending moment = 3448188. inch-lbs
Maximum shear force = 82037. lbs
Depth of maximum bending moment = 78.0000000 inches below pile head
Depth of maximum shear force = 0.0000000 inches below pile head
Number of iterations = 22
Number of zero deflection points = 8

```

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

```

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

```

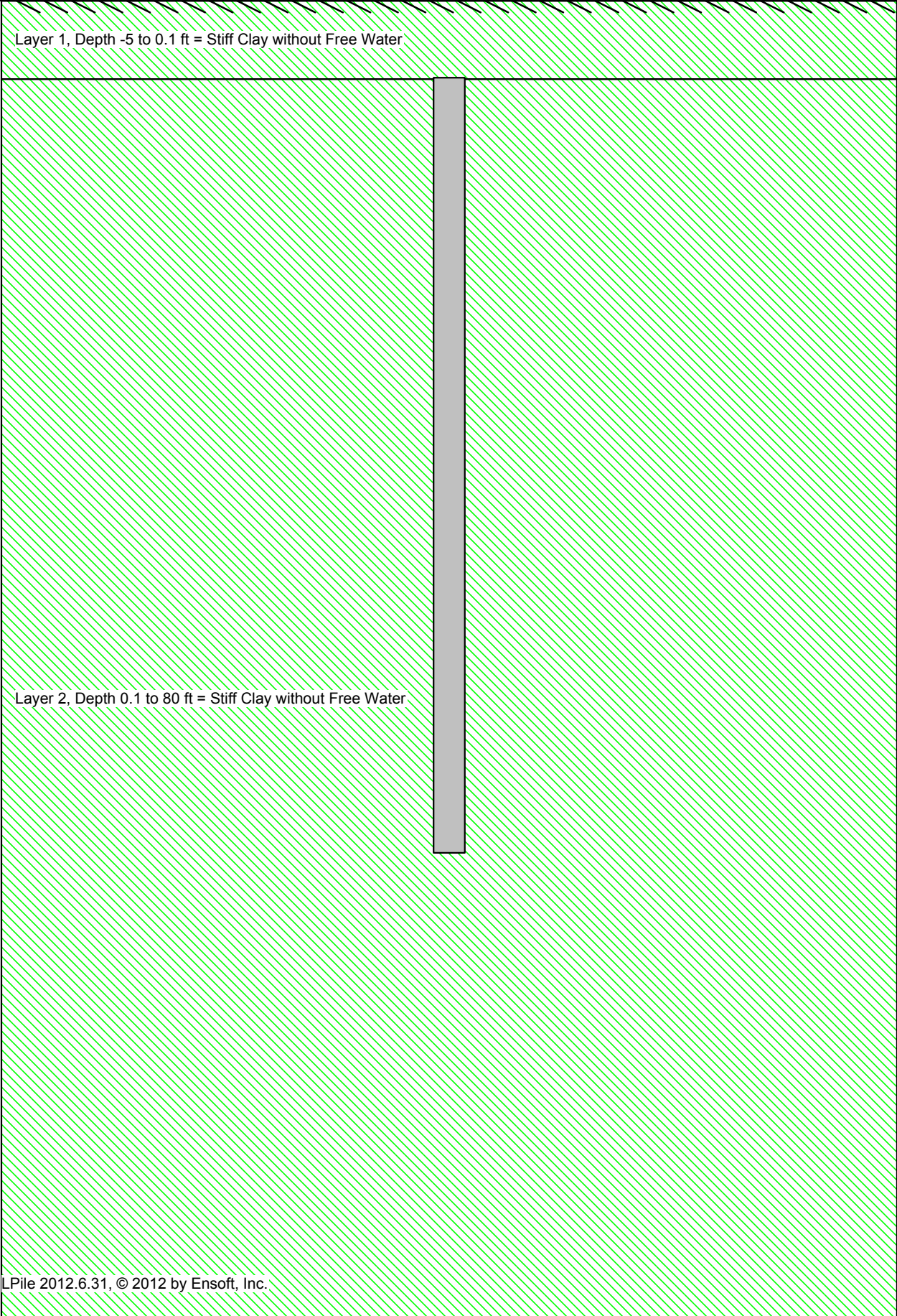
Load Case No.	Load No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 M = 0.000 or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	268000.	0.25000000	1361848.	43226.	-0.00395655
2	4	y = 0.5000	M = 0.000	268000.	0.50000000	2168199.	59514.	-0.00703703
3	4	y = 1.0000	M = 0.000	268000.	1.00000000	3448188.	82037.	-0.01252726

The analysis ended normally.

SUPPORT: BENT 4R

LOAD DIRECTION: LONGITUDE

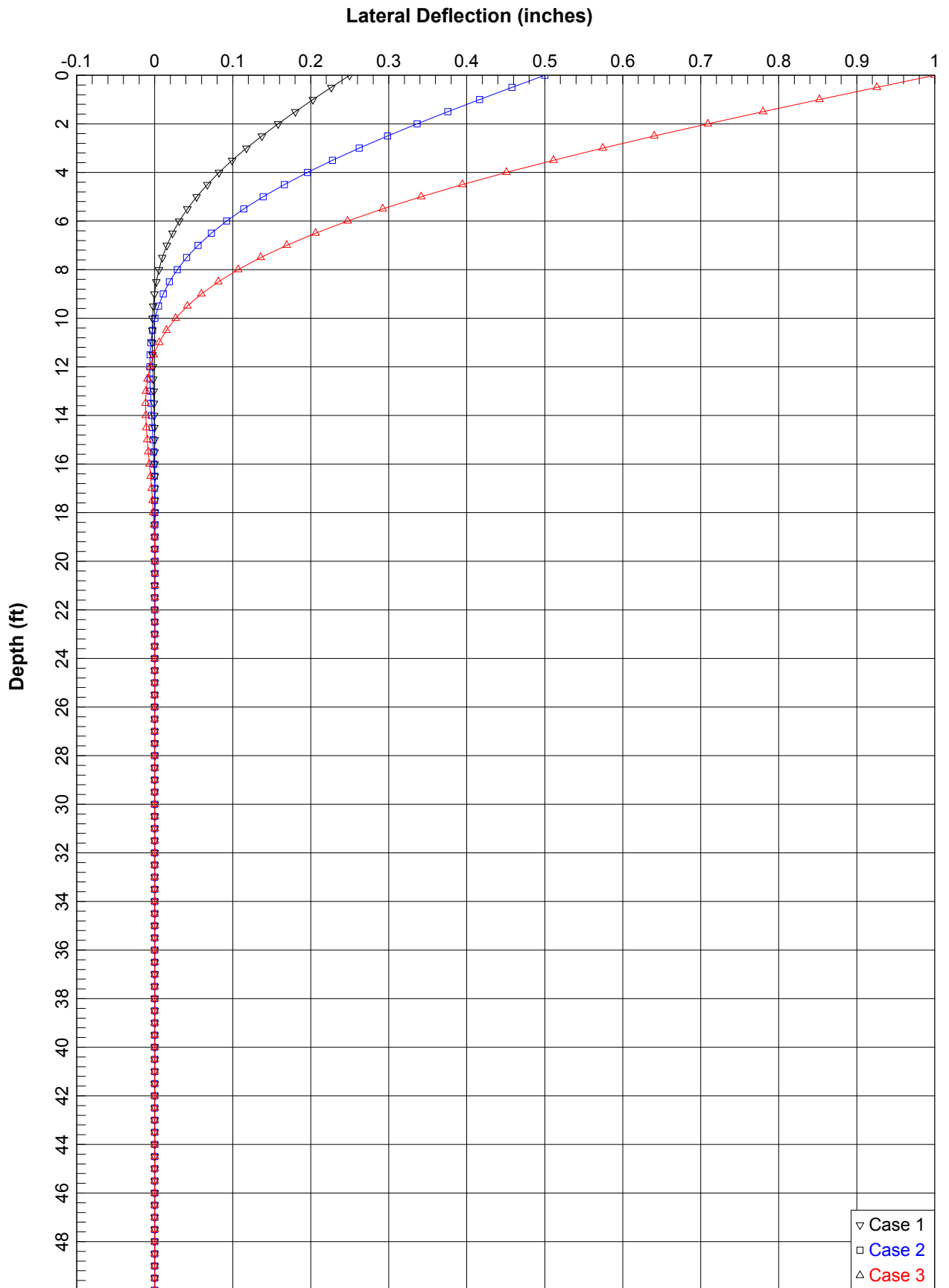
1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE

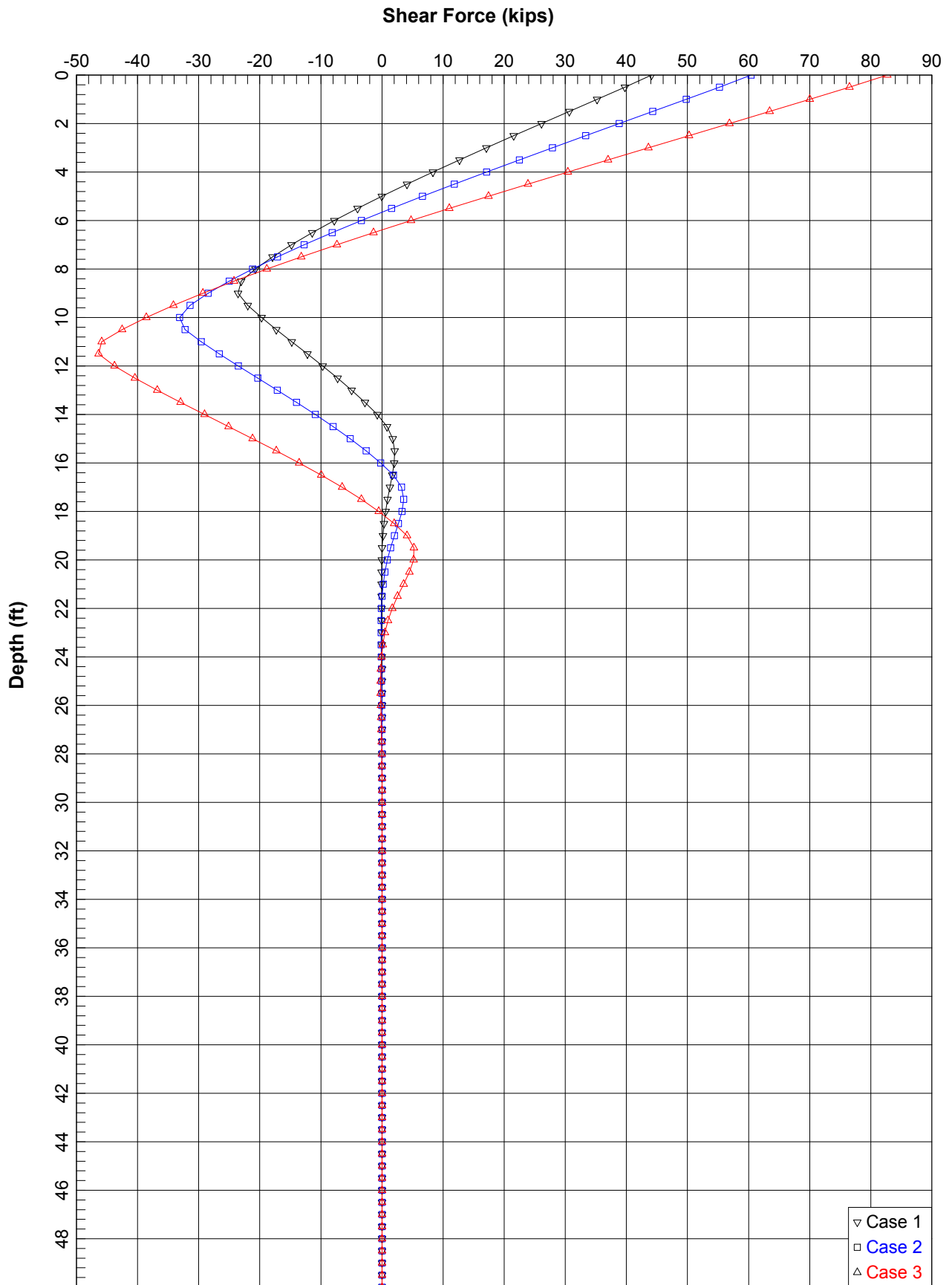


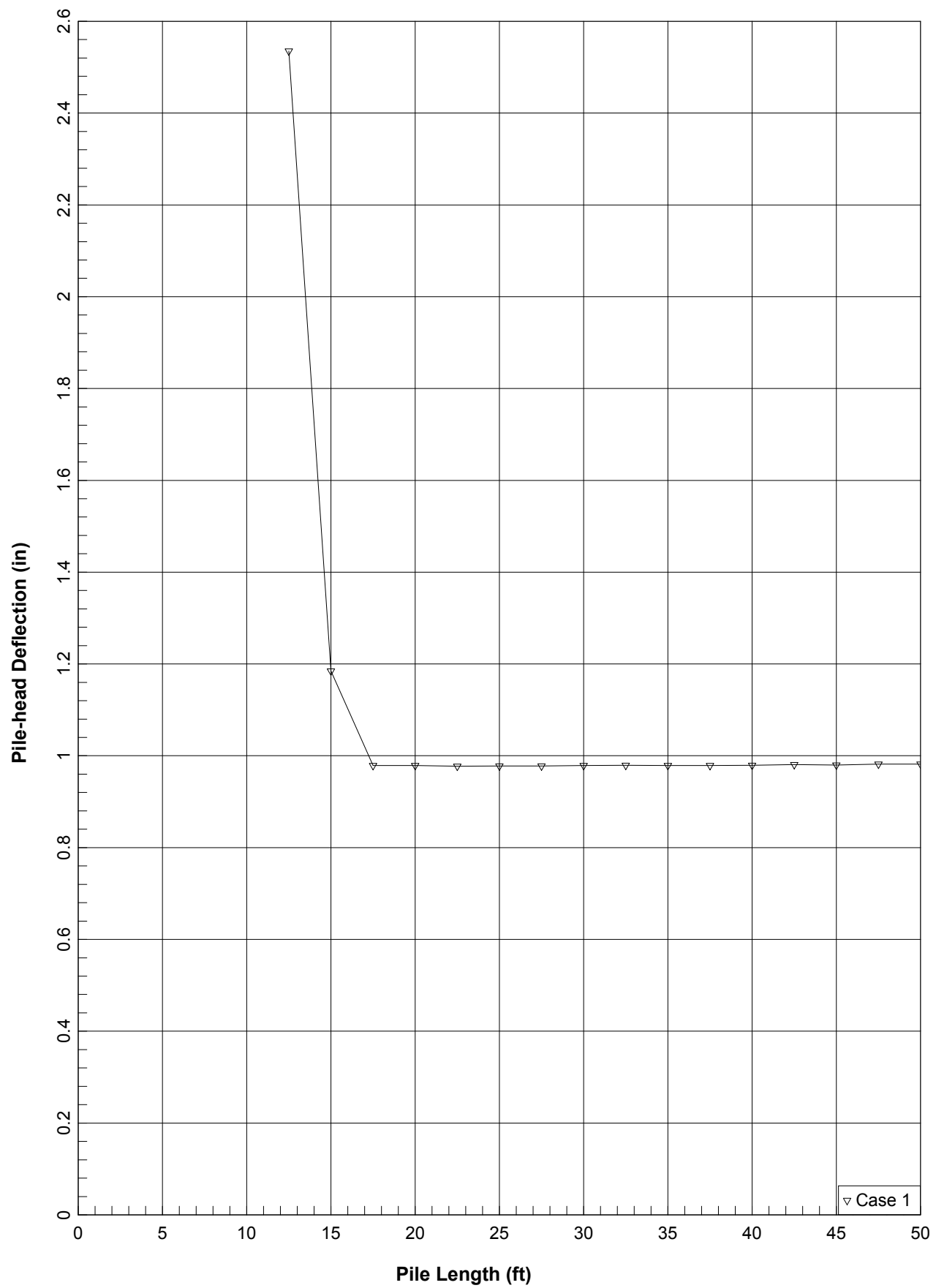
A cross-sectional diagram of a pile foundation. The pile is a vertical grey rectangle extending from the ground surface down into two soil layers. The top layer is labeled 'Layer 1, Depth -5 to 0.1 ft = Stiff Clay without Free Water' and is filled with a light green diagonal hatching pattern. The bottom layer is labeled 'Layer 2, Depth 0.1 to 80 ft = Stiff Clay without Free Water' and is filled with a darker green diagonal hatching pattern. The ground surface is indicated by a horizontal line with diagonal hatching above it.

Layer 1, Depth -5 to 0.1 ft = Stiff Clay without Free Water

Layer 2, Depth 0.1 to 80 ft = Stiff Clay without Free Water







Bent 4R_long_crit length

Pile Plus for windows, version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Bent 4\
 Name of input data file: Bent 4R_long_crit length.lp6d
 Name of output report file: Bent 4R_long_crit length.lp6r
 Name of plot output file: Bent 4R_long_crit length.lp6p
 Name of runtime message file: Bent 4R_long_crit length.lp6r

Date and Time of Analysis

Date: September 13, 2014 Time: 21:05:49

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 4R_long_crit length
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top width = 24.0000000 in
 Bottom width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 2 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer	Rock Mass	Layer	Effective	Undrained	Angle of	Elastic	Uniaxial	RQD %
Factor	Soil Type	Rock Emass	Depth	unit wt.	Cohesion	Friction	Mod.	qu	or
50	(p-y Curve Criteria)	ft	ft	pcf	psf	deg.	psi	psi	GSI
Num.	psi		Type	Test	Property	psi			Epsilon
1	Stiff Clay w/o Free water	--	-5.0000	120.0000	4500.0000	--	--	--	--
0.00700	--	--	0.100000	120.0000	4500.0000	--	--	--	--
2	Stiff Clay w/o Free water	--	0.100000	125.0000	4500.0000	--	--	--	--
0.00500	--	--	80.0000	125.0000	4500.0000	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.0000	0.4800	1.0000
2	50.0000	0.4800	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Bent 4R_long_ave P

Pile Plus for windows, version 2012-06-031
Analysis of Individual Piles and Drilled Shafts
Subjected to Lateral Loading using the p-y Method
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Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\updated_ET 9-14-14\Bent 4
Name of input data file: Bent 4R_long_ave P.lpd
Name of output report file: Bent 4R_long_ave P.lpd
Name of plot output file: Bent 4R_long_ave P.lpd
Name of runtime message file: Bent 4R_long_ave P.lpd

Date and Time of Analysis

Date: September 13, 2014 Time: 21:03:09

Problem Title

Project Name: Palo Comado OC Bridge widen
Job Number: LA-1143
Client: Parson Transportation
Engineer: Mario DiNicola
24inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
Total Pile Length = 50.00 ft
Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
Section Type = Elastic Pile
Page 1

Bent 4R_long_ave P
Cross-sectional Shape = Circular
Section Length = 50.0000000 ft
Top width = 24.0000000 in
Bottom width = 24.0000000 in
Top Area = 452.38934212 in
Bottom Area = 452.38934212 in
Moment of Inertia at Top = 8143.00815810 in
Moment of Inertia at Bottom = 8143.00815810 in
Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
= 0.000 radians
Pile Batter Angle = 0.000 degrees
= 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 2 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
Distance from top of pile to bottom of layer = 0.10000 ft
Effective unit weight at top of layer = 120.00000 pcf
Effective unit weight at bottom of layer = 120.00000 pcf
Undrained cohesion at top of layer = 4500.00000 psi
Undrained cohesion at bottom of layer = 4500.00000 psi
Epsilon-50 at top of layer = 0.00700
Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
Distance from top of pile to bottom of layer = 80.00000 ft
Effective unit weight at top of layer = 125.00000 pcf
Effective unit weight at bottom of layer = 125.00000 pcf
Undrained cohesion at top of layer = 4500.00000 psi
Undrained cohesion at bottom of layer = 4500.00000 psi
Epsilon-50 at top of layer = 0.00500
Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer	Rock Mass	Layer	Effective	Undrained	Angle of	Elastic	Uniaxial	RQD %
Factor	Soil Type	Rock Emass	Depth	unit wt.	Cohesion	Friction	Mod.	qu	or
Num.	(p-y Curve Criteria)	ft	ft	pcf	psf	deg.	psi	psi	GSI
50	Factor	pcf	psi	Type	Property	Mod.	psi	psi	Epsilon
1	Stiff Clay w/o Free water	--	-5.0000	120.000	4500.000	--	--	--	--
0.00700	--	--	0.10000	120.000	4500.000	--	--	--	--
0.00700	--	--	0.10000	125.000	4500.000	--	--	--	--
2	Stiff Clay w/o Free water	--	0.10000	125.000	4500.000	--	--	--	--
0.00500	--	--	80.0000	125.000	4500.000	--	--	--	--
0.00500	--	--	80.0000	125.000	4500.000	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.4800	1.0000
2	50.000	0.4800	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Page 2

Table with columns for various numerical data points, likely representing structural analysis results. Includes headers like 'Bent 48_Long_Ave P' and various numerical values.

* The above values of total stress are combined axial and bending stress.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Summary data for Load Case No. 2: Pile-head deflection, Computed slope at pile head, Maximum bending moment, Depth of maximum bending moment, etc.

Computed values of Pile Loading and Deflection For Lateral Loading for Load Case Number 3

Pile-head conditions are Displacement and Moment (Loading Type 4) Displacement of pile head, Moment at pile head, Axial load at pile head.

Table with columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res. p, Soil Spr. E_s, Distrib. Load, Lat/Load. Lists data for various depths from 0.00 to 108.00.

Table with columns for various numerical data points, likely representing structural analysis results. Includes headers like 'Bent 48_Long_Ave P' and various numerical values.

* The above values of total stress are combined axial and bending stress.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

Summary data for Load Case No. 3: Pile-head deflection, Computed slope at pile head, Maximum bending moment, Maximum shear force, etc.

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

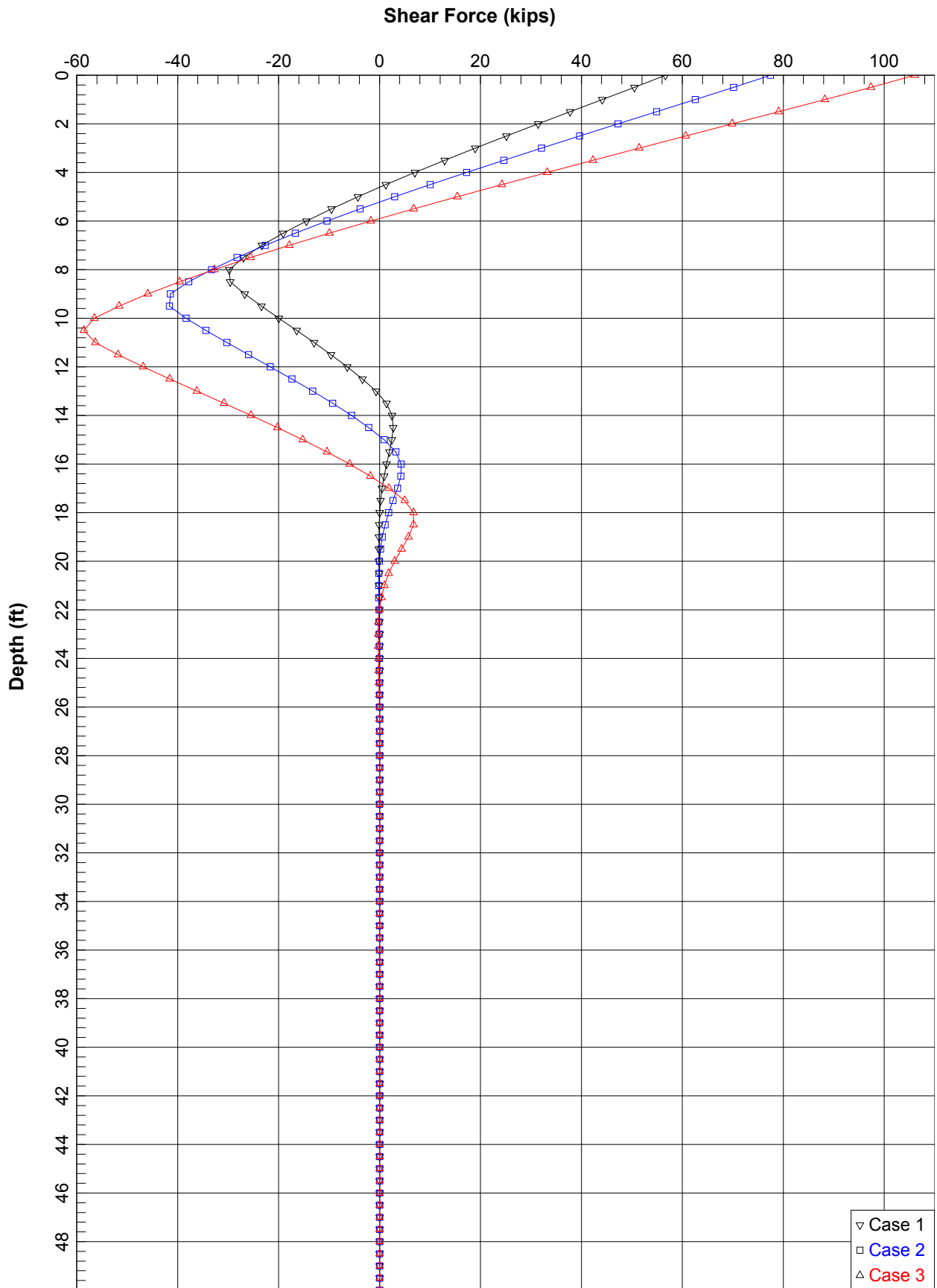
Load Type 1: Load 1 = shear, lbs, and Load 2 = Moment, in-lbs Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radian

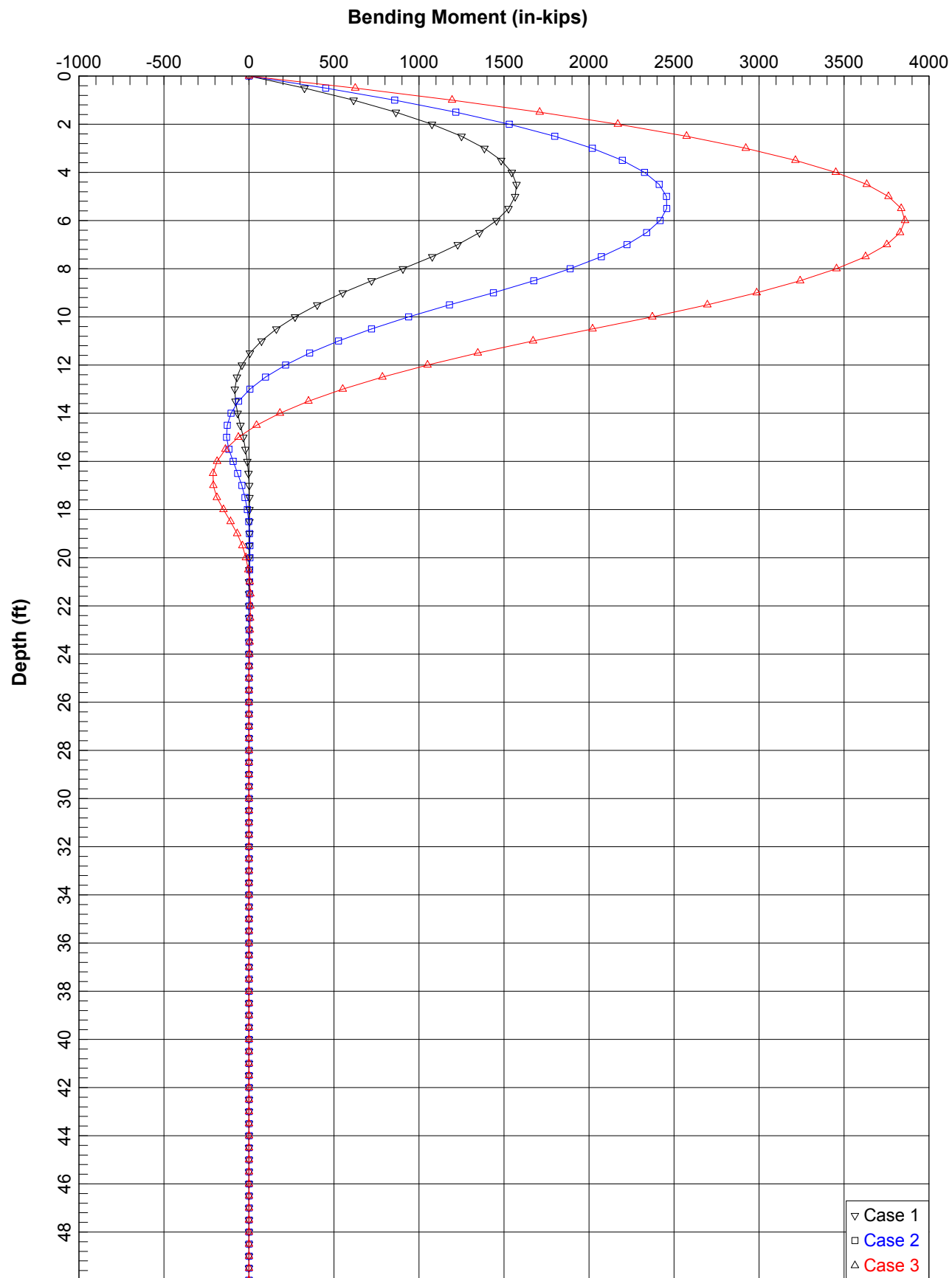
Bent 4R_long_ave P

Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.		Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y =	0.2500	M = 0.000	169000.	0.25000000	1338194.	44114.	-0.00394981
2	4	y =	0.5000	M = 0.000	169000.	0.50000000	2095339.	60407.	-0.00699229
3	4	y =	1.0000	M = 0.000	169000.	1.00000000	3289765.	82677.	-0.01236533

The analysis ended normally.





Pile Plus for windows, version 2012-06-031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\updated_ET 9-14-14\Bent 4\
 Name of input data file: Bent 4R_Long_Max P.lpd
 Name of output report file: Bent 4R_Long_Max P.lpd
 Name of plot output file: Bent 4R_Long_Max P.lpd
 Name of runtime message file: Bent 4R_Long_Max P.lpd

Date and Time of Analysis

Date: September 13, 2014 Time: 21:07:02

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 4R_Long_Max P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top width = 24.0000000 in
 Bottom width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 2 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer	Rock Mass	Layer	Effective	Undrained	Angle of	Elastic	Uniaxial	RQD %
Factor	Soil Type	Rock Emass	Depth	unit wt.	Cohesion	Friction	Subgrade	qu	or
50	(p-y Curve Criteria)	ft	ft	pcf	psf	deg.	psi	GSI	Epsilon
Num.	psi		krm	Test	Test	Mod. pci			
1	Stiff Clay w/o Free water	--	-5.0000	120.0000	4500.0000	--	--	--	--
0.00700	--	--	0.100000	120.0000	4500.0000	--	--	--	--
2	Stiff Clay w/o Free water	--	0.100000	125.0000	4500.0000	--	--	--	--
0.00500	--	--	80.0000	125.0000	4500.0000	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.0000	0.6750	1.0000
2	50.0000	0.6750	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No.	Load Type	Bent 4R_Long_Max P		Compute Top y vs. Pile Length
		Condition 1	Condition 2	
1	4	y = 0.25000 in	M = 0.0000 in-lbs	169000. False
2	4	y = 0.50000 in	M = 0.0000 in-lbs	169000. False
3	4	y = 1.00000 in	M = 0.0000 in-lbs	169000. False

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
e = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Axial thrust force values were determined from pile-head loading conditions
Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed values of Pile Loading and Deflection
For Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.250000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 169000.000 lbs

Depth inches	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil Res. lb/in	Soil Spr. lb/inch	Distrib. Load lb/inch
0.00	0.2500	0.0000	56626.	-0.004288	373.5720	2.936E+10	-974.5682	11695.	0.000
6.000	0.2243	326563.	50513.	-0.004254	854.8139	2.936E+10	-1063.3113	28447.	0.000
0.180	0.1989	614275.	170415.	-0.004158	1279.4364	2.936E+10	-1244.3661	32078.	0.000
18.000	0.1744	864576.	37761.	-0.004007	1647.6606	2.936E+10	-1059.8807	36468.	0.000
24.000	0.1509	1076038.	31426.	-0.003808	1959.2831	2.936E+10	-1051.8045	41830.	0.000
30.000	0.1287	1249414.	23513.	-0.003571	2214.7700	2.936E+10	-1039.2488	48459.	0.000
36.000	0.1080	1385114.	18969.	-0.003302	2414.7555	2.936E+10	-1022.0036	56768.	0.000
42.000	0.0889	1477771.	15204.	-0.003008	2560.0919	2.936E+10	-999.8231	67360.	0.000
48.000	0.0719	1546059.	12865.9475	-0.002699	2651.9329	2.936E+10	-972.4099	81128.	0.000
54.000	0.0567	1573054.	10511.5520	-0.002380	2691.7138	2.936E+10	-939.3886	99455.	0.000
60.000	0.0434	1565995.	8267.3929	-0.002059	2681.1781	2.936E+10	-900.2597	124584.	0.000
66.000	0.0320	1526021.	6131.1120	-0.001743	2622.4039	2.936E+10	-854.3133	160376.	0.000
72.000	0.0224	1455967.	41495.	-0.001439	2517.8409	2.936E+10	-800.4510	214046.	0.000
78.000	0.0147	1354984.	21907.	-0.001151	2370.3682	2.936E+10	-736.7729	300785.	0.000
84.000	0.008621	1228117.	123296.	-0.000887	2181.3947	2.936E+10	-659.4326	413869.	0.000
90.000	0.004049	1077245.	26949.	-0.000652	1961.0621	2.936E+10	-558.2611	572357.	0.000
96.000	0.000798	906651.	29771.	-0.000449	1708.7804	2.936E+10	-382.2321	8272382.	0.000
102.000	-0.001341	720999.	29999.	-0.000283	1435.9439	2.936E+10	439.3404	1965735.	0.000
108.000	-0.002596	531433.	26691.	-0.000153	1186.1950	2.936E+10	530.0255	1224861.	0.000
114.000	-0.003175	400924.	23394.	-5.554E-05	964.3964	2.936E+10	568.9174	1074973.	0.000
120.000	-0.003263	270813.	19935.	1.310E-05	772.6573	2.936E+10	584.2358	1074338.	0.000
126.000	-0.003018	161678.	16430.	5.730E-05	611.8302	2.936E+10	584.1172	1161200.	0.000
132.000	-0.002575	73338.	12961.	8.134E-05	481.9421	2.936E+10	572.0797	1332889.	0.000
138.000	-0.002024	5977.8533	9595.3290	8.947E-05	382.3613	2.936E+10	549.9048	1615723.	0.000
144.000	-0.001502	41797.	6390.0789	8.881E-05	435.1520	2.936E+10	518.5119	2071892.	0.000
150.000	-0.001012	70877.	3399.8365	7.429E-05	478.0206	2.936E+10	478.2356	2834332.	0.000
156.000	-0.000610	82736.	678.9868	5.860E-05	495.4963	2.936E+10	428.7143	4216373.	0.000
162.000	-0.000309	79144.	1402.4799	4.205E-05	490.2028	2.936E+10	265.1079	5143953.	0.000
168.000	-0.000105	65991.	2473.6270	2.722E-05	470.8207	2.936E+10	91.9411	5231844.	0.000
174.000	1.742E-05	49515.	2703.1203	1.542E-05	446.5408	2.936E+10	-15.4433	5197246.	0.000
180.000	7.955E-05	33585.	2441.6927	6.924E-06	423.0651	2.936E+10	-71.6992	5406725.	0.000
186.000	0.000101	20229.	1950.4405	1.424E-06	403.3629	2.936E+10	-92.0515	5495515.	0.000
192.000	6.664E-05	10185.	1404.4900	-1.684E-06	388.5780	2.936E+10	-89.9329	5695312.	0.000
198.000	8.029E-05	3371.9005	907.0062	3.069E-06	378.5410	2.936E+10	-75.8959	5671297.	0.000
204.000	5.981E-05	107.4215	608.2834	-3.341E-06	374.6146	2.936E+10	-56.7750	5695312.	0.000
210.000	4.020E-05	2742.7967	224.1996	-2.989E-06	377.6140	2.936E+10	-38.1562	5695312.	0.000
216.000	2.395E-05	3403.9285	41.5400	-2.361E-06	378.5882	2.936E+10	-22.7303	5695312.	0.000
222.000	1.187E-05	3246.0645	-60.4511	-1.681E-06	378.3556	2.936E+10	-11.2667	5695312.	0.000
228.000	3.773E-06	2681.9249	-104.9968	-1.075E-06	377.5243	2.936E+10	-3.3818	5695312.	0.000
234.000	-1.034E-06	1988.2834	-117.7989	-5.980E-07	376.5021	2.936E+10	0.9811	5695312.	0.000
240.000	-3.002E-06	1329.5931	-100.1668	-3.986E-07	375.5133	2.936E+10	3.7296	5695312.	0.000
246.000	-4.141E-06	786.8068	-78.6870	-4.264E-08	374.7315	2.936E+10	6.9044	5695312.	0.000
252.000	-3.914E-06	385.3933	-55.7502	7.716E-08	374.1400	2.936E+10	3.7152	5695312.	0.000
258.000	-3.216E-06	117.6480	-35.4500	1.286E-07	373.7434	2.936E+10	1.8246	5695312.	0.000
264.000	-2.371E-06	-40.2680	-19.5432	1.365E-07	373.6314	2.936E+10	2.2508	5695312.	0.000
270.000	1.306E-06	117.6480	-1.200E-07	1.700E-07	373.7447	2.936E+10	1.4970	5695312.	0.000
276.000	9.266E-07	-140.1113	-1.1705	9.410E-08	373.7785	2.936E+10	0.8795	5695312.	0.000
282.000	-4.479E-07	-131.3840	2.7435	6.635E-08	373.7636	2.936E+10	0.4252	5695312.	0.000
288.000	1.304E-07	-107.3241	4.3901	4.180E-08	373.5805	2.936E+10	-0.1217	5695312.	0.000
294.000	5.537E-08	-78.7874	4.6031	2.294E-08	373.6881	2.936E+10	-0.1327	5695312.	0.000
300.000	-1.449E-07	-52.1334	4.0323	5.556E-07	373.6488	2.936E+10	-0.1575	5695312.	0.000
306.000	1.702E-07	-30.4193	3.1249	-1.120E-09	373.6168	2.936E+10	-0.1616	5695312.	0.000
312.000	1.583E-07	-14.5166	2.1993	3.472E-09	373.5934	2.936E+10	-0.1503	5695312.	0.000
318.000	-8.366E-08	11.3122	1.3122	7.569E-09	373.5779	2.936E+10	-0.1411	5695312.	0.000
324.000	9.391E-08	2.0819	0.7487	-5.565E-09	373.5751	2.936E+10	-0.0891	5695312.	0.000
330.000	6.180E-08	4.9750	0.3053	-4.844E-09	373.5794	2.936E+10	-0.0587	5695312.	0.000
336.000	3.930E-08	5.6382	0.0724	7.476E-09	373.5805	2.936E+10	0.0349	5695312.	0.000
342.000	1.684E-08	5.3111	-0.1225	-2.616E-09	373.5798	2.936E+10	-0.0160	5695312.	0.000
348.000	4.396E-09	4.2907	-0.1830	-1.635E-09	373.5783	2.936E+10	-0.00473	5695312.	0.000
354.000	2.483E-09	3.1090	-0.1875	-8.777E-07	373.5786	2.936E+10	0.00246	5695312.	0.000
360.000	-6.136E-09	2.0419	-0.1621	-3.503E-10	373.5750	2.936E+10	0.005825	5695312.	0.000
366.000	1.805E-09	1.1510	-0.1249	-1.120E-09	373.5748	2.936E+10	0.004631	5695312.	0.000
372.000	-6.396E-09	0.5446	-0.0867	1.540E-10	373.5728	2.936E+10	0.006071	5695312.	0.000
378.000	-5.138E-09	0.1336	-0.0538	2.233E-10	373.5722	2.936E+10	0.004877	5695312.	0.000
384.000	-3.716E-09	-0.1018	-0.0286	2.266E-10	373.5722	2.936E+10	0.003527	5695312.	0.000

Bent 4R_Long_Max P									
373.5721 2.936E+10 0.002296 5695312. 0.000									
390.000 -2.419E-09 -0.2102 -0.0111 1.947E+10 0.000296 5695312. 0.000									
396.000 -1.370E-09 -0.2359 -0.000326 1.491E+10 0.000130 5695312. 0.000									
402.000 -6.302E-10 -0.2144 0.000398 1.031E+10 0.000598 5695312. 0.000									
408.000 -0.144E-10 -0.1714 0.000001 6.362E+11 0.000000 5695312. 0.000									
414.000 0.1733E-10 -0.1234 0.000763 3.350E+11 0.000000 5695312. 0.000									
420.000 2.587E-10 -0.0799 0.000613 1.275E+11 0.0000246 5695312. 0.000									
426.000 2.861E-10 -0.0452 0.004962 0.000000 5695312. 0.000									
432.000 2.581E-10 -0.0203 0.000342 -6.751E-12 0.000000 5695312. 0.000									
438.000 2.051E-10 -0.004264 0.002093 -9.265E-12 0.000000 5695312. 0.000									
444.000 1.469E-10 0.004801 0.001091 -9.210E-12 0.000000 5695312. 0.000									
450.000 9.458E-11 0.008844 0.000403 7.816E-12 0.000000 5695312. 0.000									
456.000 5.111E-11 0.000655 1.736E-05 -5.926E-12 0.000000 5695312. 0.000									
462.000 2.347E-11 0.008648 -0.000235 -4.055E-12 0.000000 5695312. 0.000									
468.000 4.445E-12 0.006838 -0.000315 -2.472E-12 0.000000 5695312. 0.000									
474.000 -8.136E-12 0.004874 -0.000310 -1.278E-12 0.000000 5695312. 0.000									
480.000 -1.086E-11 0.003121 -0.000261 0.000 0.000000 5695312. 0.000									
486.000 -1.170E-11 0.001739 -0.000187 0.000 0.000000 5695312. 0.000									
492.000 -1.040E-11 0.000756 -0.000134 0.000 0.000000 5695312. 0.000									
498.000 -8.180E-12 0.000128 -8.128E-05 0.000 0.000000 5695312. 0.000									
504.000 -5.802E-12 -0.000221 -4.148E-05 0.000 0.000000 5695312. 0.000									
510.000 -3.693E-12 -0.000371 -1.442E-05 0.000 0.000000 5695312. 0.000									
516.000 -2.040E-12 -0.000394 1.902E-06 0.000 0.000000 5695312. 0.000									
522.000 0.000 -0.001348 1.019E-05 0.000 0.000000 5695312. 0.000									
528.000 0.000 -0.000272 1.302E-05 0.000 0.000000 5695312. 0.000									
534.000 0.000 -0.000182 1.257E-05 0.000 0.000000 5695312. 0.000									
540.000 0.000 -0.000122 1.048E-05 0.000 0.000000 5695312. 0.000									
546.000 0.000 -6.664E-05 7.788E-06 0.000 0.000000 5695312. 0.000									
552.000 0.000 -2.813E-05 5.207E-06 0.000 0.000000 5695312. 0.000									
558.000 0.000 -4.127E-06 3.050E-06 0.000 0.000000 5695312. 0.000									
564.000 0.000 8.503E-06 1.430E-06 0.000 0.000000 5695312. 0.000									
570.000 0.000 2.616E-06 3.916E-07 0.000 0.000000 5695312. 0.000									
576.000 0.000 1.249E-05 -3.236E-07 0.000 0.000000 5695312. 0.000									
582.000 0.000 9.198E-06 -6.208E-07 0.000 0.000000 5695312. 0.000									
588.000 0.000 3.038E-06 -6.372E-07 0.000 0.000000 5695312. 0.000									
594.000 0.000 1.565E-06 -4.226E-07 0.000 0.000000 5695312. 0.000									

		Bent 4R_Long_Max P												
		375.0222	2.936E+10	-1.6196	5695312.	0.000								
252.000	1.706E-06	3698.2845	-176.7033	-1.301E-06	375.0222	2.936E+10	-1.6196	5695312.	0.000					
258.000	-3.832E-06	2609.9472	-170.6507	-6.563E-07	377.4182	2.936E+10	3.6372	5695312.	0.000					
264.000	-6.169E-06	1651.9076	-142.1716	-2.207E-07	376.0064	2.936E+10	5.8558	5695312.	0.000					
270.000	6.483E-06	1511.0179	-106.1884	4.049E-07	375.1510	2.936E+10	2.8712	5695312.	0.000					
276.000	-5.683E-06	378.0329	-71.5109	1.715E-07	374.3291	2.936E+10	5.3946	5695312.	0.000					
282.000	-4.422E-06	485.8565	-42.7346	2.149E-07	373.6396	2.936E+10	4.1975	5695312.	0.000					
288.000	3.105E-06	-215.2180	-21.3006	2.057E-07	373.8938	2.936E+10	2.9471	5695312.	0.000					
294.000	-1.933E-06	-210.1684	-6.8970	1.704E-07	373.8817	2.936E+10	1.8541	5695312.	0.000					
300.000	1.060E-06	-102.9183	6.9134	2.483E-08	373.7237	2.936E+10	1.0057	5695312.	0.000					
306.000	-4.335E-07	-190.2354	5.9342	8.489E-08	373.8524	2.936E+10	0.4115	5695312.	0.000					
312.000	-4.081E-08	-147.2894	7.2849	5.040E-08	373.7891	2.936E+10	0.0387	5695312.	0.000					
318.000	1.713E-07	-102.9183	6.9134	2.483E-08	373.7237	2.936E+10	0.1626	5695312.	0.000					
324.000	2.572E-07	-64.3787	5.6934	7.733E-09	373.6669	2.936E+10	-0.2441	5695312.	0.000					
330.000	2.641E-07	-34.6132	4.2091	-2.383E-09	373.6230	2.936E+10	-0.2507	5695312.	0.000					
336.000	2.786E-07	-15.8645	2.8063	-7.338E-09	373.5925	2.936E+10	-0.2169	5695312.	0.000					
342.000	1.760E-07	-0.9230	1.6542	-8.849E-09	373.5734	2.936E+10	-0.1671	5695312.	0.000					
348.000	1.224E-07	6.0036	0.8045	-8.330E-09	373.5809	2.936E+10	-0.1162	5695312.	0.000					
354.000	7.607E-08	8.7474	0.2394	-6.827E-09	373.5849	2.936E+10	-0.0722	5695312.	0.000					
360.000	4.050E-08	8.8999	-0.0926	-5.020E-09	373.5851	2.936E+10	-0.0384	5695312.	0.000					
366.000	1.584E-08	7.6485	-0.2530	-3.330E-09	373.5833	2.936E+10	-0.0150	5695312.	0.000					
372.000	5.468E-10	5.8603	-0.2997	-1.949E-09	373.5807	2.936E+10	-0.000519	5695312.	0.000					
378.000	-7.536E-09	4.0543	-0.2797	-9.361E-10	373.5780	2.936E+10	-0.007172	5695312.	0.000					
384.000	1.060E-08	2.5056	-0.2278	-2.637E-10	373.5757	2.936E+10	0.0101	5695312.	0.000					
390.000	-1.074E-08	1.3216	-0.1667	1.234E-10	373.5740	2.936E+10	0.0102	5695312.	0.000					
396.000	-9.182E-09	0.5044	-0.1100	3.125E-10	373.5728	2.936E+10	0.008715	5695312.	0.000					
402.000	-7.000E-09	0.000889	-0.0639	3.636E-10	373.5720	2.936E+10	0.006845	5695312.	0.000					
408.000	-4.818E-09	-0.2634	-0.0303	3.368E-10	373.5724	2.936E+10	0.004573	5695312.	0.000					
414.000	-2.959E-09	-0.3630	-0.008124	2.728E-10	373.5726	2.936E+10	0.002808	5695312.	0.000					
420.000	-1.544E-09	-0.3614	0.004699	1.988E-10	373.5726	2.936E+10	0.001466	5695312.	0.000					
426.000	-5.734E-10	-0.3070	0.0107	1.304E-10	373.5725	2.936E+10	0.000544	5695312.	0.000					
432.000	2.176E-10	-0.1161	-0.0236	7.731E-11	373.5723	2.936E+10	-0.000715	5695312.	0.000					
438.000	3.298E-10	-0.1595	0.0113	3.515E-11	373.5723	2.936E+10	-0.000313	5695312.	0.000					
444.000	4.429E-10	-0.0974	0.009103	8.896E-12	373.5722	2.936E+10	-0.000420	5695312.	0.000					
450.000	6.365E-10	0.0503	0.003399	5.063E-11	373.5721	2.936E+10	-0.000144	5695312.	0.000					
456.000	3.685E-10	-0.0182	0.004307	-1.320E-11	373.5720	2.936E+10	-0.000350	5695312.	0.000					
462.000	2.781E-10	0.003388	0.002466	-1.491E-11	373.5720	2.936E+10	-0.000264	5695312.	0.000					
468.000	1.895E-10	0.0114	0.001134	-1.360E-11	373.5720	2.936E+10	-0.000180	5695312.	0.000					
474.000	1.149E-10	0.0150	0.000267	-1.090E-11	373.5720	2.936E+10	-0.000109	5695312.	0.000					
480.000	5.972E-11	0.0147	-0.000227	-7.863E-12	373.5720	2.936E+10	-5.574E-05	5695312.	0.000					
486.000	2.054E-11	0.0123	-0.000453	-5.105E-12	373.5720	2.936E+10	-1.950E-05	5695312.	0.000					
492.000	-2.356E-12	0.009251	-0.000504	-2.901E-12	373.5720	2.936E+10	2.407E-06	5695312.	0.000					
498.000	1.477E-11	0.006572	-0.000616	-1.314E-12	373.5720	2.936E+10	1.534E-05	5695312.	0.000					
504.000	-1.831E-11	0.003779	-0.000363	0.000	373.5720	2.936E+10	1.738E-05	5695312.	0.000					
510.000	-1.771E-11	0.001919	-0.000361	0.000	373.5720	2.936E+10	1.681E-05	5695312.	0.000					
516.000	-1.447E-11	0.000648	-0.000168	0.000	373.5720	2.936E+10	4.407E-05	5695312.	0.000					
522.000	-1.104E-11	-0.000111	-9.490E-05	0.000	373.5720	2.936E+10	1.048E-05	5695312.	0.000					
528.000	-7.444E-12	-0.000492	-4.226E-05	0.000	373.5720	2.936E+10	1.066E-06	5695312.	0.000					
534.000	-4.451E-12	-0.000619	-8.388E-06	0.000	373.5720	2.936E+10	4.225E-06	5695312.	0.000					
540.000	-2.219E-12	-0.000594	1.061E-05	0.000	373.5720	2.936E+10	2.106E-06	5695312.	0.000					
546.000	0.000	0.000493	1.898E-05	0.000	373.5720	2.936E+10	6.777E-07	5695312.	0.000					
552.000	0.000	-0.000367	2.046E-05	0.000	373.5720	2.936E+10	-1.768E-07	5695312.	0.000					
558.000	0.000	-0.000247	1.812E-05	0.000	373.5720	2.936E+10	-0.043E-07	5695312.	0.000					
564.000	1.000	-0.000150	0.000	0.000	373.5720	2.936E+10	-7.437E-07	5695312.	0.000					
570.000	0.000	-7.858E-05	9.713E-06	0.000	373.5720	2.936E+10	-7.090E-07	5695312.	0.000					
576.000	0.000	-3.304E-05	0.000060	0.000	373.5720	2.936E+10	-5.828E-07	5695312.	0.000					
582.000	0.000	-8.473E-06	2.835E-06	0.000	373.5720	2.936E+10	-4.181E-07	5695312.	0.000					
588.000	0.000	1.042E-06	8.498E-07	0.000	373.5720	2.936E+10	-2.436E-07	5695312.	0.000					
594.000	0.000	1.786E-08	-9.132E-08	0.000	373.5720	2.936E+10	7.856E-08	5695312.	0.000					
600.000	0.000	0.000	0.000	0.000	373.5720	2.936E+10	1.009E-07	2847656.	0.000					

* The above values of total stress are combined axial and bending stress.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Pile-head deflection	=	0.5000000 inches
Computed slope at pile head	=	-0.0075752 radians
Maximum bending moment	=	2457428. inch-lbs
Maximum shear force	=	74500 lbs
Depth of maximum bending moment	=	66.000000 inches below pile head
Depth of maximum shear force	=	0.000000 inches below pile head
Number of iterations	=	2
Number of zero deflection points	=	9

Computed values of Pile Loading and Deflection For Lateral Loading for Load Case Number 3

Depth x inches	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil Res. p lb/in	Soil Spr. lb/inch	Distrib. Lat Load lb/inch
0.00	1.0000	0.000	0.000	106014.	-0.0134	373.5720	2.936E+10	-1378.2475	4134.7425
6.00	0.9196	624867.	97340.	-0.0133	1294.4112	2.936E+10	-1513.0834	9872.3163	0.000
12.00	0.8393	1195131.	19277.	-0.0132	2134.7881	2.936E+10	-1574.9176	18091.8577	0.000
18.00	0.7618	1710263.	79056.	-0.0129	2893.9132	2.936E+10	-1532.2698	12069.	0.000
24.00	0.6857	2193877.	69852.	-0.0125	3571.2266	2.936E+10	-1535.7166	13438.	0.000
30.00	0.6123	2572748.	60941.	-0.0120	4186.4049	2.936E+10	-1534.8669	15041.	0.000
36.00	0.5420	2921846.	51447.	-0.0114	4679.3699	2.936E+10	-1529.5597	16932.	0.000
42.00	0.4753	3245268.	42300.	-0.0108	5110.2869	2.936E+10	-1524.9108	19119.	0.000
48.00	0.4126	3451313.	33226.	-0.0101	5459.6239	2.936E+10	-1504.8591	21884.	0.000
54.00	0.3541	3633471.	24257.	-0.009379	5728.0614	2.936E+10	-1485.0612	25164.	0.000
60.00	0.3000	3761411.	15421.	-0.008624	5916.6043	2.936E+10	-1459.3810	29159.880	0.000
66.00	0.2506	3836016.	6753.4274	-0.007847	6026.5439	2.936E+10	-1429.3383	34220.000	0.000
72.00	0.2059	385							

Bent 4R_Long_Max P

Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

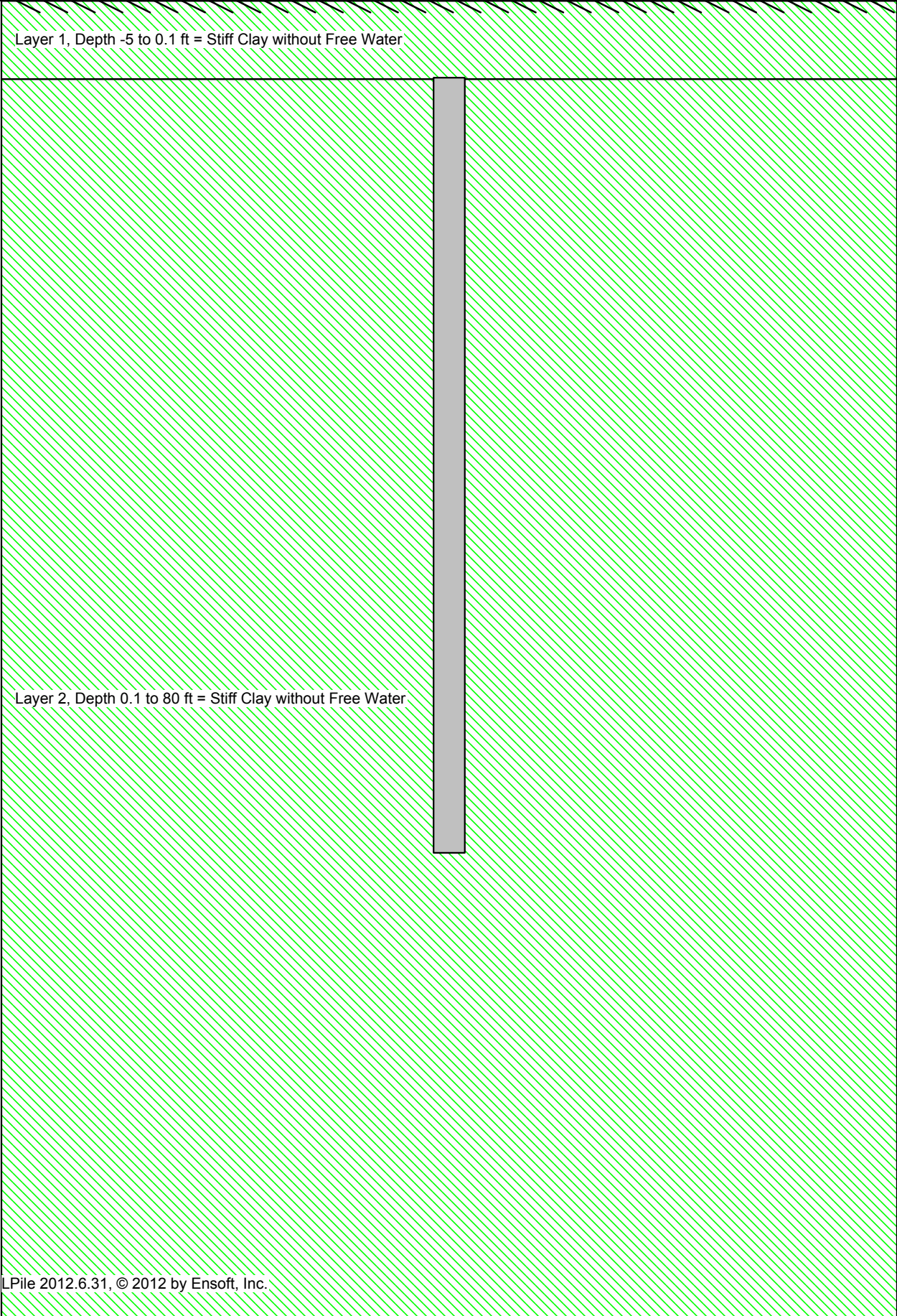
Load Case No.	Load Type No.		Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y =	0.2500	M = 0.000	169000.	0.25000000	1573054.	56626.	-0.00428756
2	4	y =	0.5000	M = 0.000	169000.	0.50000000	2457428.	77450.	-0.00757520
3	4	y =	1.0000	M = 0.000	169000.	1.00000000	3858368.	106014.	-0.01340138

The analysis ended normally.

SUPPORT: BENT 4R

LOAD DIRECTION: TRANSVERSE

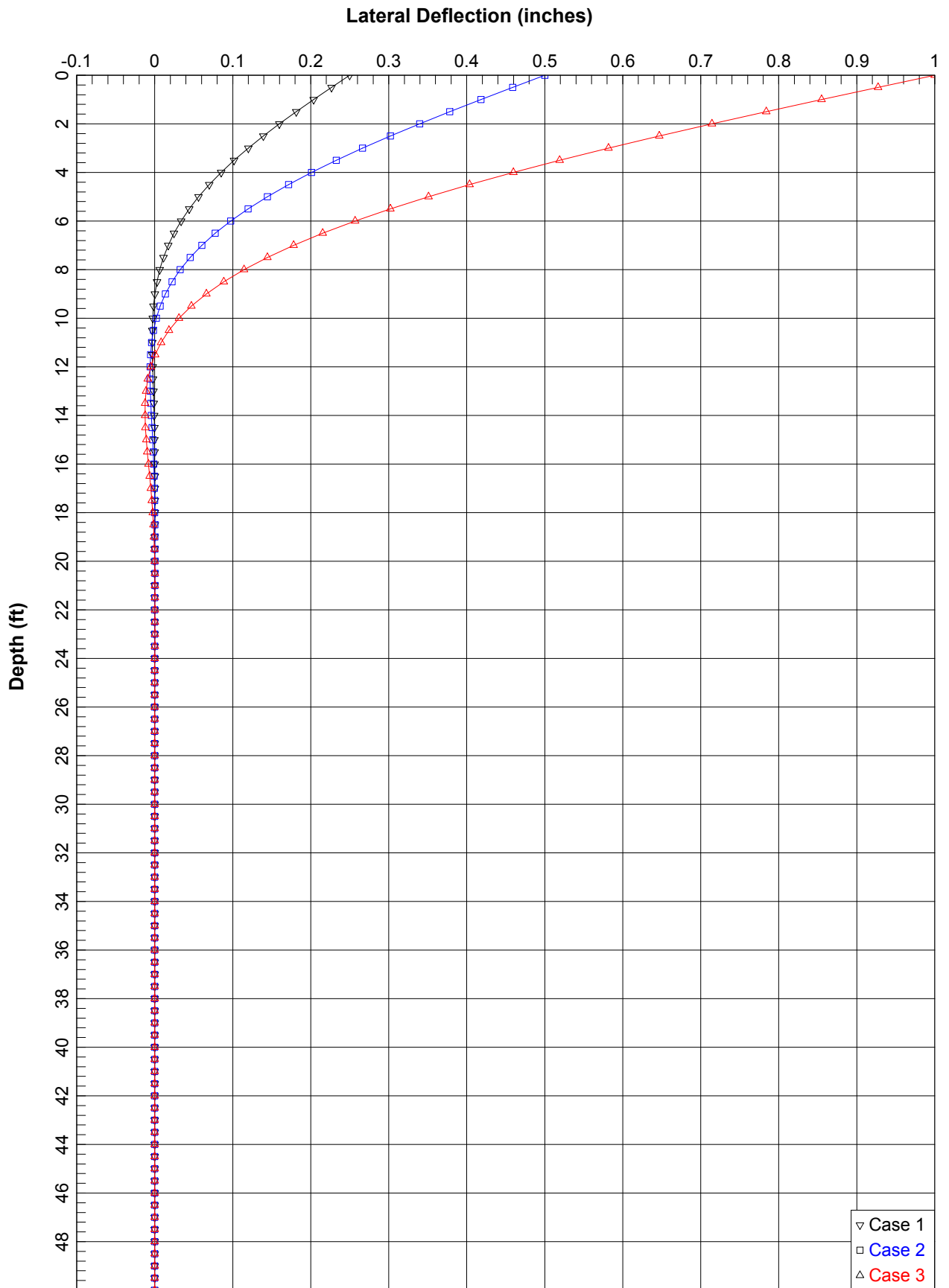
1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE

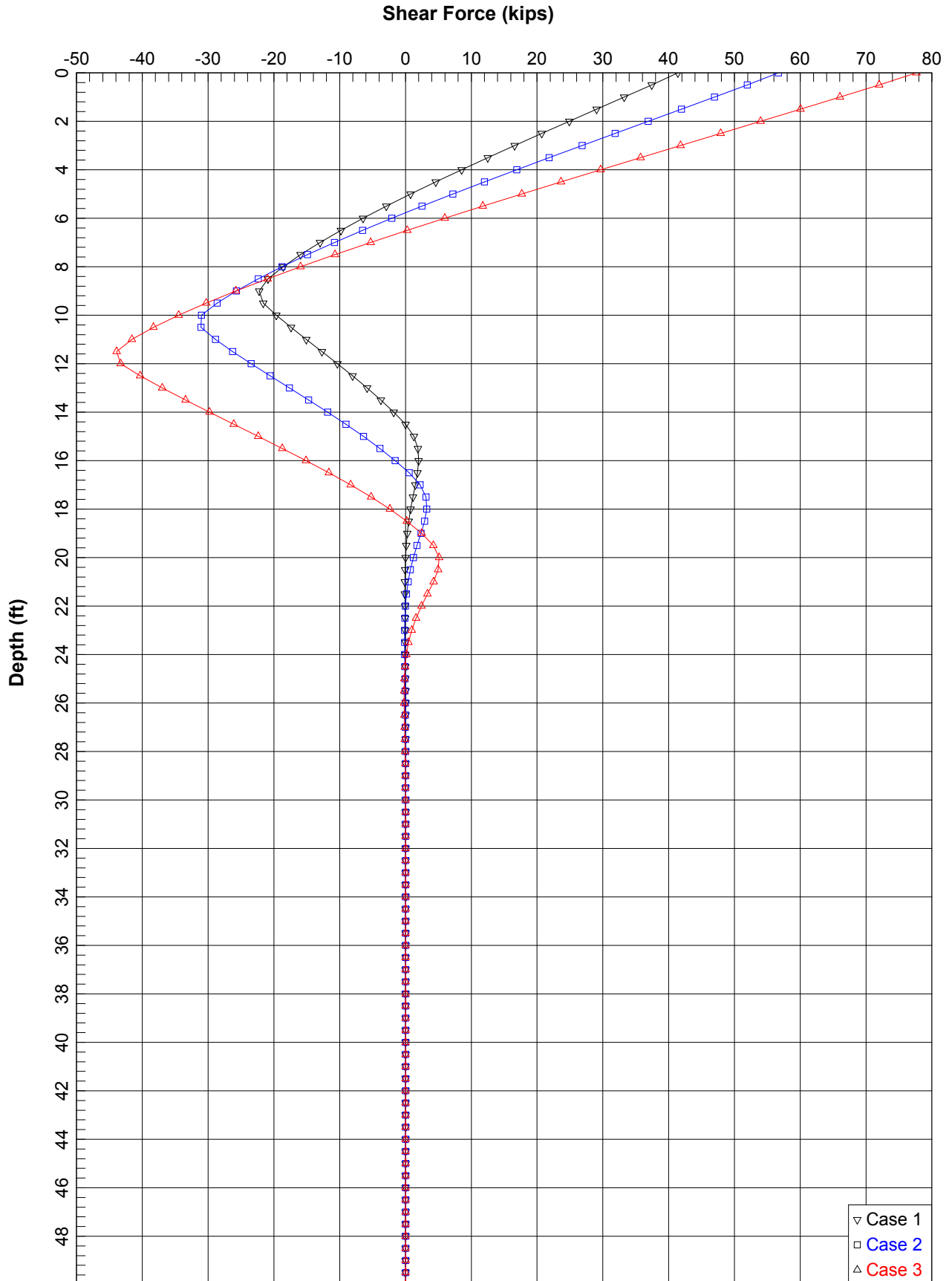


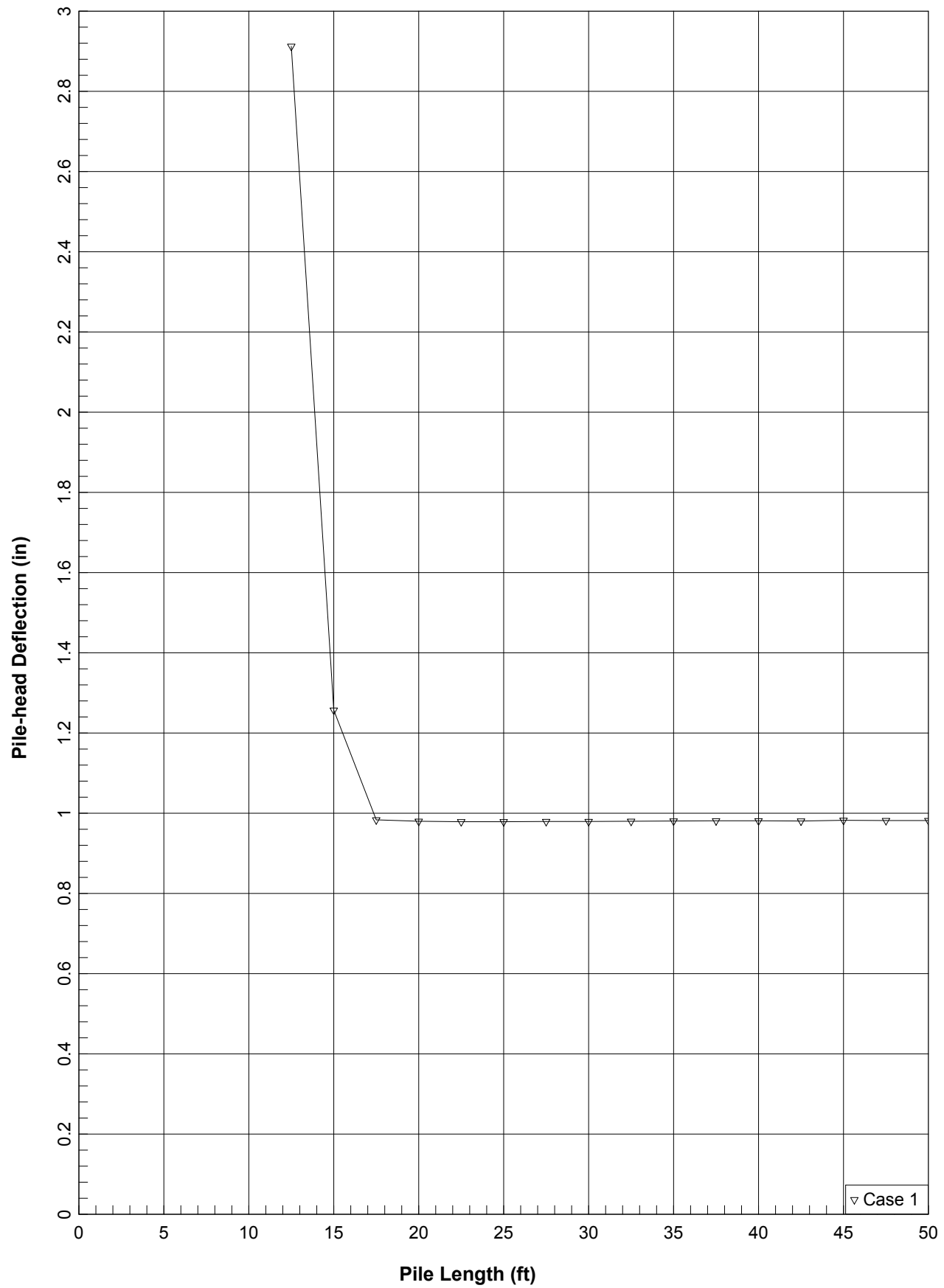
A cross-sectional diagram of a pile foundation. The pile is a vertical grey rectangle extending from the ground surface down into two soil layers. The top layer is labeled 'Layer 1, Depth -5 to 0.1 ft = Stiff Clay without Free Water' and is filled with a light green diagonal hatching pattern. The bottom layer is labeled 'Layer 2, Depth 0.1 to 80 ft = Stiff Clay without Free Water' and is filled with a darker green diagonal hatching pattern. The ground surface is indicated by a horizontal line with diagonal hatching above it.

Layer 1, Depth -5 to 0.1 ft = Stiff Clay without Free Water

Layer 2, Depth 0.1 to 80 ft = Stiff Clay without Free Water







Bent 4R_transv_crit length

Pile Plus for windows, version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Bent 4\
 Name of input data file: Bent 4R_transv_crit length.lpd
 Name of output report file: Bent 4R_transv_crit length.lpd
 Name of plot output file: Bent 4R_transv_crit length.lpd
 Name of runtime message file: Bent 4R_transv_crit length.lpd

Date and Time of Analysis

Date: September 13, 2014 Time: 21:11:21

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 4R_transv_crit length
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top width = 24.0000000 in
 Bottom width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 2 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer	Rock Mass	Layer	Effective	Undrained	Angle of	Elastic	Uniaxial	RQD %
Factor	Soil Type	Rock Emass	Depth	unit wt.	In-situ Cohesion	Friction	Mod.	qu	or
50	(p-y Curve Criteria)	ft	ft	pcf	psf	deg.	psi	psi	GSI
Num.	psi		Type	Test	Property	psi			Epsilon
1	Stiff Clay w/o Free water	--	-5.0000	120.0000	4500.0000	--	--	--	--
0.00700	--	--	0.100000	120.0000	4500.0000	--	--	--	--
2	Stiff Clay w/o Free water	--	0.100000	125.0000	4500.0000	--	--	--	--
0.00500	--	--	80.0000	125.0000	4500.0000	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.0000	0.4400	1.0000
2	50.0000	0.4400	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Load No.	Load Type	Condition 1	Condition 2	Bent 4R_transv_crit length	Compute
1	V	V = 77000. lbs	M = 0.000 in-lbs	169000.	True

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are shear and moment (Loading Type 1)

Shear force at pile head = 77000.000 lbs
 Applied moment at pile head = 0.000 in-lbs
 Axial thrust load on pile head = 169000.000 lbs

Depth inches	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi*	Soil Res. lb/in ²	Soil Spr. lb/in ²	Distrib. Lat. Load lb/inch
0.00	0.9820	1.267E-06	77000.	-0.0119	373.5720	2.936E+10	-894.3440	2732.2499
6.00	0.9103	458016.	71366.	-0.0119	1048.5311	2.936E+10	-983.8108	6484.5131
12.00	0.8392	820521.	65433.	-0.0118	1671.1576	2.936E+10	-993.6411	7104.3790
18.00	0.7691	1267072.	59449.	-0.0115	2240.8008	2.936E+10	-1001.2332	7810.5003
24.00	0.7006	1617316.	53425.	-0.0112	2756.9405	2.936E+10	-1006.4789	8618.9927
30.00	0.6341	2030895.	47378.	-0.0109	3219.1808	2.936E+10	-1009.3270	9549.8803
36.00	0.5700	2207931.	41321.	-0.0105	3627.3051	2.936E+10	-1009.6824	10628.0000
42.00	0.5086	2440065.	35270.	-0.009988	3981.1796	2.936E+10	-1007.4542	11886.0000
48.00	0.4501	2631423.	29240.	-0.009467	4280.8393	2.936E+10	-1002.5452	13363.0000
54.00	0.3950	2818139.	23247.	-0.008908	4526.5426	2.936E+10	-994.8495	15113.0000
60.00	0.3432	2984531.	17310.	-0.008319	4718.5867	2.936E+10	-984.2495	17205.0000
66.00	0.2951	3042732.	11446.	-0.007706	4857.5143	2.936E+10	-970.6129	19322.0000
72.00	0.2508	3101433.	5672.3599	-0.007079	4944.0199	2.936E+10	-953.7867	22820.0000
78.00	0.2102	3123155.	0.006442	4978.9784	2.936E+10	-933.8995	-26648.0000	26648.0000
84.00	0.1735	3114620.	-5519.9364	-0.005805	4963.4539	2.936E+10	-909.7997	31469.0000
90.00	0.1405	3070687.	-10896.	-0.005172	4898.7117	2.936E+10	-882.1353	37658.0000
96.00	0.1114	2994361.	-16093.	-0.004533	4786.2330	2.936E+10	-850.2226	45794.0000
102.00	0.0859	2886806.	-21084.	-0.003952	4627.7341	2.936E+10	-813.5386	56813.0000
108.00	0.0640	2749366.	-25839.	-0.003376	4425.1839	2.936E+10	-771.3028	71234.0000
114.00	0.0454	2583589.	-30319.	-0.002831	4180.8951	2.936E+10	-722.2513	89429.0000
120.00	0.0300	2391275.	-34478.	-0.002322	3897.4906	2.936E+10	-664.0986	123770.0000
126.00	0.0175	2174558.	-38247.	-0.001856	3578.1242	2.936E+10	-591.9651	202444.0000
132.00	0.00745	1936080.	-41498.	-0.001435	3226.6890	2.936E+10	-491.7037	380041.0000
138.00	0.000319	1679499.	-43471.	-0.001066	2848.5768	2.936E+10	-166.0119	3123929.0000
144.00	0.000047	1416593.	-42594.	-0.000750	2461.1444	2.936E+10	458.2862	544799.0000
150.00	0.000876	1169893.	-39616.	-0.000485	2097.5922	2.936E+10	534.2078	369436.0000
156.00	0.00109	942181.	-36288.	-0.000269	1762.0233	2.936E+10	575.1839	317483.0000
162.00	0.00119	748060.	-32767.	-9.801E-05	1456.6931	2.936E+10	598.6891	301635.0000
168.00	0.00120	549181.	-29139.	3.323E-05	1182.8758	2.936E+10	610.6687	304162.0000
174.00	0.00115	385251.	-25465.	0.000129	941.2998	2.936E+10	613.9025	320015.0000
180.00	0.00105	243442.	-21793.	0.000193	732.1747	2.936E+10	609.9034	348464.0000
186.00	0.0009195	123339.	-18165.	0.000230	555.3317	2.936E+10	599.5622	391249.0000
192.00	0.000736	24895.	-14616.	0.000246	410.2387	2.936E+10	583.4157	452475.0000
198.00	0.0006248	-52551.	-11180.	0.000243	451.0147	2.936E+10	561.7690	539509.0000
204.00	0.0004823	-109765.	-7908.7402	0.000226	335.3253	2.936E+10	528.8143	657835.0000
210.00	0.000334	-147915.	-4854.5693	0.000200	591.5478	2.936E+10	489.2430	830780.0000
216.00	0.000245	-168423.	-2050.9016	0.000168	621.7701	2.936E+10	445.3126	1101726.0000
222.00	0.000132	-172865.	-474.3930	0.000133	638.3164	2.936E+10	396.4523	1361462.0000
228.00	0.0000834	-163000.	2686.7219	9.831E-05	613.7774	2.936E+10	340.9907	2454355.0000
234.00	0.0000344	-140824.	4347.6871	6.726E-05	581.0985	2.936E+10	212.6643	3712500.0000
240.00	2.550E-05	-110964.	5034.8730	4.153E-05	537.0944	2.936E+10	16.3976	3712500.0000
246.00	0.000155	-80490.	4797.0565	2.196E-05	492.1865	2.936E+10	-95.6698	3712500.0000
252.00	0.000237	-53444.	4070.0627	8.273E-06	452.3295	2.936E+10	-146.6615	3712500.0000
258.00	0.000234	-31666.	3138.7778	-4.243E-07	316.666	2.936E+10	-157.1001	3712500.0000
264.00	0.000232	-15537.	2256.9455	-5.248E-06	396.4687	2.936E+10	-143.5107	3712500.0000
270.00	0.000191	4571.9367	1472.0189	-7.303E-06	380.3095	2.936E+10	-118.1315	3712500.0000
276.00	0.000191	2141.6895	849.7731	-7.552E-06	376.7181	2.936E+10	-89.2831	3712500.0000
282.00	0.000100	5640.6799	395.7463	-6.756E-06	381.8844	2.936E+10	-62.0598	3712500.0000
288.00	6.222E-05	6904.3471	92.2166	-5.474E-06	383.7467	2.936E+10	-19.1167	3712500.0000
294.00	3.461E-05	6758.3812	-89.3715	-4.078E-06	383.5316	2.936E+10	-21.4126	3712500.0000
300.00	1.428E-05	5840.1600	-180.1197	-2.791E-06	382.1784	2.936E+10	-8.8368	3712500.0000
306.00	1.119E-06	4602.6017	-208.7076	-1.723E-07	380.3347	2.936E+10	0.6592	3712500.0000
312.00	-6.399E-06	3339.1642	-198.9069	-9.118E-07	378.4928	2.936E+10	3.9594	3712500.0000
318.00	-9.002E-06	2217.5704	-168.7963	-3.439E-07	376.8400	2.936E+10	6.0775	3712500.0000
324.00	1.035E-05	1314.3062	-131.0232	-1.703E-08	375.5089	2.936E+10	6.1209	3712500.0000
330.00	-9.618E-06	645.2334	-93.6336	2.173E-07	374.5229	2.936E+10	5.9510	3712500.0000
336.00	-7.918E-06	190.2627	-61.0821	3.027E-07	373.8524	2.936E+10	5.9995	3712500.0000
342.00	-5.986E-06	-88.3654	-35.2727	3.131E-07	373.7022	2.936E+10	3.7036	3712500.0000
348.00	-4.161E-06	-233.6443	-16.4373	2.802E-07	373.9163	2.936E+10	2.5748	3712500.0000
354.00	-2.624E-06	-228.1811	-8.8429	2.271E-07	373.5938	2.936E+10	1.6233	3712500.0000
360.00	-1.437E-06	-280.2198	3.6938	1.692E-07	373.9850	2.936E+10	0.8889	3712500.0000
366.00	-5.934E-07	-242.1389	7.4621	1.158E-07	373.9289	2.936E+10	0.3672	3712500.0000
372.00	-4.755E-08	-190.9089	8.6314	7.152E-08	373.8534	2.936E+10	0.0292	3712500.0000
378.00	2.648E-07	-138.5269	8.2475	3.786E-08	373.7762	2.936E+10	-0.1639	3712500.0000
384.00	4.070E-07	-76.0527	7.0003	1.433E-08	373.7076	2.936E+10	-0.2518	3712500.0000
390.00	4.364E-07	-54.5507	5.4349	-6.831E-10	373.6524	2.936E+10	-0.2700	3712500.0000
396.00	3.988E-07	-26.7951	3.8846	-8.996E-09	373.6115	2.936E+10	-0.2468	3712500.0000
402.00	3.284E-07	-7.9178	2.5346	-1.254E-08	373.5837	2.936E+10	-0.2032	3712500.0000

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Load No.	Load Type	Condition 1	Condition 2	Bent 4R_transv_crit length	Compute			
1	V	V = 77000. lbs	M = 0.000 in-lbs	169000.	True			
408.000	2.483E-07	3.6458	1.4641	-1.298E-08	373.5774	2.936E+10	-0.1536	3712500.0000
414.000	1.727E-07	9.6778	0.6827	-1.162E-08	373.5863	2.936E+10	-0.1068	3712500.0000
420.000	1.089E-07	11.8620	0.1601	-9.417E-09	373.5895	2.936E+10	-0.0674	3712500.0000
426.000	5.864E-08	11.6186	0.1527	-7.018E-09	373.5891	2.936E+10	-0.0369	3712500.0000
432.000	2.466E-08	10.0443	-0.3091	-4.804E-09	373.5868	2.936E+10	-0.0153	3712500.0000
438.000	1.994E-09	7.9186	-0.3586	-2.968E-09	373.5837	2.936E+10	-0.001234	3712500.0000
444.000	-1.096E-08	5.7469	0.3420	-1.572E-09	373.5805	2.936E+10	0.006781	3712500.0000
450.000	-1.687E-08	3.8180	-0.2903	-5.942E-10	373.5776	2.936E+10	0.0104	3712500.0000
456.000	-1.809E-08	2.2641	-0.2254	-2.736E-11	373.5754	2.936E+10	0.0112	3712500.0000
462.000	-1.654E-08	1.1127	-0.1612	3.725E-10	373.5737	2.936E+10	0.0102	3712500.0000
468.000	-1.362E-08	0.3295	-0.1052	5.198E-10	373.5725	2.936E+10	0.008428	3712500.0000
474.000	-1.030E-08	-0.1504	-0.0608	5.381E-10	373.5722	2.936E+10	0.006373	3712500.0000
480.000	-7.163E-09	-0.4009	-0.0284	4.818E-10	373.5726	2.936E+10	0.004432	3712500.0000
486.000	-4.518E-09	-0.4917	-0.006672	3.906E-10	373.5727	2.936E+10	0.002796	3712500.0000
492.000	-2.476E-09	-0.4817	0.006311	2.911E-10	373.5727	2.936E+10	0.001532	3712500.0000
498.000	-1.025E-09	-0.4165	0.0128	1.993E-10	373.5726	2.936E+10	0.000634	3712500.0000
504.000	-8.413E-11	-0.328	0.0149	1.232E-10	373.5725	2.936E+10	5.206E-05	3712500.0000
510.000	-6.537E-10	-0.2384	0.0142	6.528E-11	373.5724	2.936E+10	-0.000281	3712500.0000
516.000	6.992E-10	-0.1584	0.0120	2.474E-11	373.5723	2.936E+10	-0.000433	3712500.0000
522.000	7.958E-10	-0.0939	0.009350	-1.044E-12	373.5722	2.936E+10	-0.000464	3712500.0000
528.000	0.867E-10	-0.0462	0.006683	-1.536E-11	373.5721	2.936E+10	-0.000425	3712500.0000
534.000	5.662E-10	-0.0137	0.004357	-2.147E-11	373.5720	2.936E+10	-0.000350	3712500.0000
540.000	4.290E-10	0.006169	0.002508	-2.224E-11	373.5720	2.936E+10	-0.000265	3712500.0000
546.000	2.973E-10	0.0165	0.001157	-1.993E-11	373.5720	2.936E+10	-0.000185	3712500.0000
552.000	1.899E-							

Bent 4R_transv_ave P

Pile Plus for windows, version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Bent 4\
 Name of input data file: Bent 4R_transv_ave P.lp6d
 Name of output report file: Bent 4R_transv_ave P.lp6o
 Name of plot output file: Bent 4R_transv_ave P.lp6p
 Name of runtime message file: Bent 4R_transv_ave P.lp6r

Date and Time of Analysis

Date: September 13, 2014 Time: 21:09:13

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 4R_transv_ave P
 = Circular
 Section Length = 50.0000000 ft
 Top width = 24.0000000 in
 Bottom Width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 2 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Rock Emass	Layer Depth ft	Effective unit wt. Test	Undrained Cohesion Test	Angle of Friction Mod. deg.	Elastic Mod. psi	Uniaxial qu psi	RQD or GSI	Epsilon
1	Stiff Clay w/o Free water	--	-5.0000	120.0000	4500.0000	--	--	--	--	--
0.00700	--	--	0.100000	120.0000	4500.0000	--	--	--	--	--
2	Stiff Clay w/o Free water	--	0.100000	125.0000	4500.0000	--	--	--	--	--
0.00500	--	--	80.0000	125.0000	4500.0000	--	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.0000	0.4400	1.0000
2	50.0000	0.4400	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No.	Load Type	Condition		Axial Thrust Force, lbs	Compute Top y vs. Pile Length
		1	2		
1	4	y = 0.25000 in	M = 0.0000 in-lbs	169000.	False
2	4	y = 0.50000 in	M = 0.0000 in-lbs	169000.	False
3	4	y = 1.00000 in	M = 0.0000 in-lbs	169000.	False

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
e = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed values of Pile Loading and Deflection
For Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.250000 inches
Moment at pile head = 0.0000 in-lbs
Axial load at pile head = 169000.000 lbs

Depth X inches	Deflect. Y inches	Bending Moment in-lbs	Shear Force lbs	Slope psi	Total Stress psi	Bending Stiffness lb-in ²	Soil Res. p lb/in	Soil Spr. e ^{5h} lb/inch	Distrib. Lat. Load lb/inch
0.00	0.2500	0.000	41415.	-0.003872	373.5720	2.936E+10	-635.2741	7623.2887	0.000
6.000	0.2268	240982.	37424.	-0.003848	728.6961	2.936E+10	-695.0375	18390.	0.000
0.00	0.2031	647595.	29060.	-0.003663	1327.9051	2.936E+10	-697.7813	23073.	0.000
18.000	0.1815	647595.	29060.	-0.003663	1327.9051	2.936E+10	-697.7813	23073.	0.000
24.000	0.1599	610444.	24880.	-0.003514	1571.7202	2.936E+10	-695.6169	26107.	0.000
30.000	0.1393	581283.	20720.	-0.003334	1778.3834	2.936E+10	-690.8708	29267.	0.000
36.000	0.1199	1068448.	16596.	-0.003127	1948.0983	2.936E+10	-683.7382	34226.	0.000
42.000	0.1016	1284684.	12524.	-0.002899	2081.2135	2.936E+10	-673.8013	39370.	0.000
48.000	0.0851	1224611.	8519.0719	-0.002656	2178.2285	2.936E+10	-661.0238	46622.	0.000
54.000	0.0699	1266393.	4600.2675	-0.002401	2239.8010	2.936E+10	-645.2443	53997.	0.000
60.000	0.0563	1284684.	785.7434	-0.002141	2266.7355	2.936E+10	-626.2637	66796.	0.000
66.000	0.0442	1280163.	2904.5234	-0.001878	2260.0933	2.936E+10	-603.8252	81970.	0.000
72.000	0.0337	1253639.	6448.7367	-0.001620	2221.0062	2.936E+10	-577.5792	102794.	0.000
78.000	0.0248	1206063.	9222.5201	-0.001368	2150.8947	2.936E+10	-547.0133	132534.	0.000
84.000	0.0173	1138544.	-12998.	-0.001129	2051.3948	2.936E+10	-511.3203	177390.	0.000
90.000	0.0112	1052381.	-15939.	-0.000905	1924.4207	2.936E+10	-469.0404	230789.	0.000
96.000	0.006439	949115.	-18597.	-0.000700	1772.2419	2.936E+10	-417.0961	288662.	0.000
102.000	0.002820	830637.	-20888.	-0.000518	1597.6456	2.936E+10	-346.7019	373589.	0.000
108.000	0.000220	699505.	-22441.	-0.000362	1404.4024	2.936E+10	-304.1666	4837471.	0.000
114.000	-0.001522	564478.	-21629.	-0.000233	1205.4194	2.936E+10	-308.2517	1215247.	0.000
120.000	-0.002572	440432.	-19628.	-0.000130	1022.6173	2.936E+10	-358.7484	836938.	0.000
126.000	-0.003082	329209.	-17403.	-5.133E-05	858.7128	2.936E+10	-382.7043	745120.	0.000
132.000	-0.003188	231695.	-15075.	5.995E-06	715.0109	2.936E+10	-393.3129	740288.	0.000
138.000	-0.003010	148292.	-12711.	4.483E-05	592.1041	2.936E+10	-394.9277	787279.	0.000
144.000	-0.002630	79076.	-10377.	6.806E-05	490.1031	2.936E+10	-389.5039	881947.	0.000
150.000	-0.002193	23866.	-8054.5308	7.858E-05	408.7417	2.936E+10	-378.1180	1034535.	0.000
156.000	0.001707	-17178.	-5836.1745	7.921E-05	399.7112	2.936E+10	-361.3441	1270191.	0.000
162.000	-0.001242	-46329.	-3733.8926	7.266E-05	441.8452	2.936E+10	-339.4265	1639151.	0.000
168.000	-0.000835	-62692.	-1778.4333	6.152E-05	465.9580	2.936E+10	-312.3933	2245076.	0.000
174.000	0.000504	-67095.	-1.9074	4.818E-05	473.4787	2.936E+10	-279.7820	3329111.	0.000
180.000	-0.000257	62812.	1289.7561	3.484E-05	466.1358	2.936E+10	-150.7724	5249740.	0.000
186.000	-8.612E-05	-52389.	1896.3182	2.307E-05	450.7749	2.936E+10	-51.4149	9382262.	0.000
192.000	0.016105	-40103.	2013.8800	1.361E-05	452.6704	2.936E+10	-12.2273	16466800.	0.000
198.000	7.725E-05	28250.	1834.4040	6.629E-06	415.2024	2.936E+10	-47.5977	3696845.	0.000
204.000	9.970E-05	-18104.	1106.5414	1.891E-06	400.2509	2.936E+10	-61.6899	3712500.	0.000
210.000	9.995E-05	-10175.	1135.9419	-9.985E-07	388.5666	2.936E+10	-61.8433	3712500.	0.000
216.000	8.772E-05	-4470.5127	787.5844	-2.495E-06	380.1600	2.936E+10	-54.2759	3712500.	0.000
222.000	7.001E-05	-718.9790	494.8000	-3.026E-06	374.6215	2.936E+10	-43.3163	3712500.	0.000
228.000	5.141E-05	1473.3187	269.4260	-2.948E-06	375.7432	2.936E+10	-31.8111	3712500.	0.000
234.000	3.462E-05	2520.1130	109.7214	-2.540E-06	377.2688	2.936E+10	-21.4238	3712500.	0.000
240.000	2.093E-05	2795.6177	6.4033	-1.997E-06	373.6013	2.936E+10	-12.9488	3712500.	0.000
246.000	1.066E-05	2603.4048	-52.0275	-1.445E-06	377.4085	2.936E+10	-6.5948	3712500.	0.000
252.000	3.582E-06	2173.7279	-78.4606	-9.573E-07	376.7754	2.936E+10	-2.2162	3712500.	0.000
258.000	8.498E-07	1663.8191	83.5706	-6.451E-07	376.0239	2.936E+10	0.8889	3712500.	0.000
264.000	-3.199E-06	1172.0285	-76.0932	-2.753E-07	375.2992	2.936E+10	1.9795	3712500.	0.000
270.000	-4.132E-06	713.4268	-56.6841	-2.566E-08	374.6791	2.936E+10	2.5468	3712500.	0.000
276.000	-4.144E-06	422.3792	-47.1213	4.121E-08	374.1943	2.936E+10	2.5641	3712500.	0.000
282.000	-3.638E-06	185.7194	-32.6766	1.034E-07	373.8457	2.936E+10	2.7508	3712500.	0.000
288.000	2.904E-06	0.05008	20.5341	1.234E-07	373.6183	2.936E+10	1.7967	3712500.	0.000
294.000	-2.133E-06	-60.9446	-11.1852	1.223E-07	373.6183	2.936E+10	1.3197	3712500.	0.000
300.000	-1.437E-06	-104.4196	-4.5594	1.054E-07	373.7259	2.936E+10	0.8889	3712500.	0.000
306.000	8.696E-07	-11.5716	0.8023	-4.386E-08	375.4278	2.936E+10	0.0038	3712500.	0.000
312.000	-4.426E-07	-107.9525	2.1534	5.897E-08	373.7311	2.936E+10	0.2738	3712500.	0.000
318.000	1.490E-07	-4.0490	-0.4969	2.314E-08	374.6791	2.936E+10	0.9277	3712500.	0.000
324.000	3.409E-08	-69.0167	3.4646	2.345E-08	373.6737	2.936E+10	-0.0211	3712500.	0.000
330.000	1.325E-07	-68.4253	3.1554	1.143E-08	373.6437	2.936E+10	-0.0820	3712500.	0.000
336.000	1.718E-07	-59.3102	1.9110	3.271E-09	375.6183	2.936E+10	-0.1060	3712500.	0.000
342.000	1.718E-07	-47.5335	1.9547	-1.701E-09	373.5879	2.936E+10	-0.1063	3712500.	0.000
348.000	1.509E-07	-7.7154	1.3557	-4.281E-09	375.8364	2.936E+10	-0.0933	3712500.	0.000
354.000	1.094E-07	-1.2559	0.8023	-1.198E-09	373.6183	2.936E+10	-0.879E-05	3712500.	0.000
360.000	8.848E-08	2.5210	0.4644	-5.069E-09	373.5757	2.936E+10	-0.0547	3712500.	0.000
366.000	4.890E-08	1.8940	0.3895	-4.036E-09	375.5784	2.936E+10	-0.0318	3712500.	0.000
372.000	3.605E-08	4.8034	0.0119	-3.436E-09	373.5791	2.936E+10	-0.0223	3712500.	0.000
378.000	1.838E-08	4.4763	-0.0891	-2.488E-09	373.5786	2.936E+10	-0.0114	3712500.	0.000
384.000	6.195E-09	3.7590	-0.1347	-1.648E-09	373.5775	2.936E+10	-0.003833	3712500.	0.000

390.000	-1.401E-09	2.8629	-0.1436	-9.735E-10	Bent 4R_transv_ave P	0.000867	3712500.	0.000	
									371.5762
396.000	-5.487E-09	2.0174	-0.1308	-4.478E-10	373.5790	2.936E+10	0.003395	3712500.	0.000
402.000	-7.099E-09	1.2937	-0.1075	-1.364E-10	373.5739	2.936E+10	0.004392	3712500.	0.000
408.000	-7.124E-09	0.7778	-0.0811	7.021E-11	373.9039	2.936E+10	0.016040	3712500.	0.000
414.000	-6.258E-09	0.3205	-0.0562	1.773E-10	373.5725	2.936E+10	0.003871	3712500.	0.000
420.000	-4.995E-09	0.0525	-0.0354	2.155E-10	373.5721	2.936E+10	0.003991	3712500.	0.000
426.000	-3.670E-09	-0.1043	-0.0193	2.102E-10	373.5722	2.936E+10	0.002171	3712500.	0.000
432.000	-2.473E-09	-0.1793	-0.007873	1.812E-10	373.5723	2.936E+10	0.001390	3712500.	0.000
438.000	-1.496E-09	-0.1991	-0.000055	1.425E-10	373.5722	2.936E+10	0.000926	3712500.	0.000
444.000	-7.631E-10	-0.1856	0.003689	1.032E-10	373.5723	2.936E+10	0.000472	3712500.	0.000
450.000	-2.576E-10	-0.1551	0.005583	6.839E-11	373.5722	2.936E+10	0.000159	3712500.	0.000
456.000	5.762E-11	-0.1188	0.001955	4.041E-11	373.5722	2.936E+10	-3.565E-05	3712500.	0.000
462.000	2.272E-11	-0.0837	0.005426	1.972E-11	373.5721	2.936E+10	-0.000141	3712500.	0.000
468.000	2.942E-11	-0.0537	0.004458	5.676E-12	373.5721	2.936E+10	-0.000182	3712500.	0.000
474.000	2.934E-11	-0.0302	0.003364	-2.897E-12	373.5721	2.936E+10	-0.000183	3712500.	0.000
480.000	2.594E-11	-0.0133	0.002334	-7.346E-12	373.5720	2.936E+10	-0.000161	3712500.	0.000
486.000	2.072E-11	-0.002394	0.001467	-8.931E-12	373.5720	2.936E+10	-0.000128	3712500.	0.000
492.000	1.573E-11	0.004912	0.000809	-8.714E-12	373.5720	2.936E+10	-9.472E-05	3712500.	0.000
498.000	1.026E-11	0.007426	0.000327	-7.515E-12	373.5720	2.936E+10	-6.350E-05	3712500.	0.000
504.000	6.210E-11	0.008252	2.126E-05	-5.912E-12	373.5720	2.936E+10	-3.842E-05	3712500.	0.000
510.000	3.168E-11	0.007693	-0.000153	-4.283E-12	373.5720	2.936E+10	-1.960E-05	3712500.	0.000
516.000	1.070E-11	0.006427	-0.000231	-2.840E-12	373.5720	2.936E+10			

Table with columns for pile ID, lateral force (k), moment (k-ft), and deflection (in). Includes data for various load cases and a summary of total stress.

* The above values of total stress are combined axial and bending stress.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Table listing pile head conditions (displacement, slope, moment), maximum bending moment, shear force, and number of iterations.

Computed values of Pile Loading and Deflection for Lateral Loading for Load Case Number 3

Table showing pile head conditions (displacement, slope, moment) and axial load at pile head for various depths.

Table with columns for pile ID, lateral force (k), moment (k-ft), and deflection (in). Includes data for various load cases and a summary of total stress.

* The above values of total stress are combined axial and bending stress.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

Table listing pile head conditions (displacement, slope, moment), maximum bending moment, shear force, and number of iterations.

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

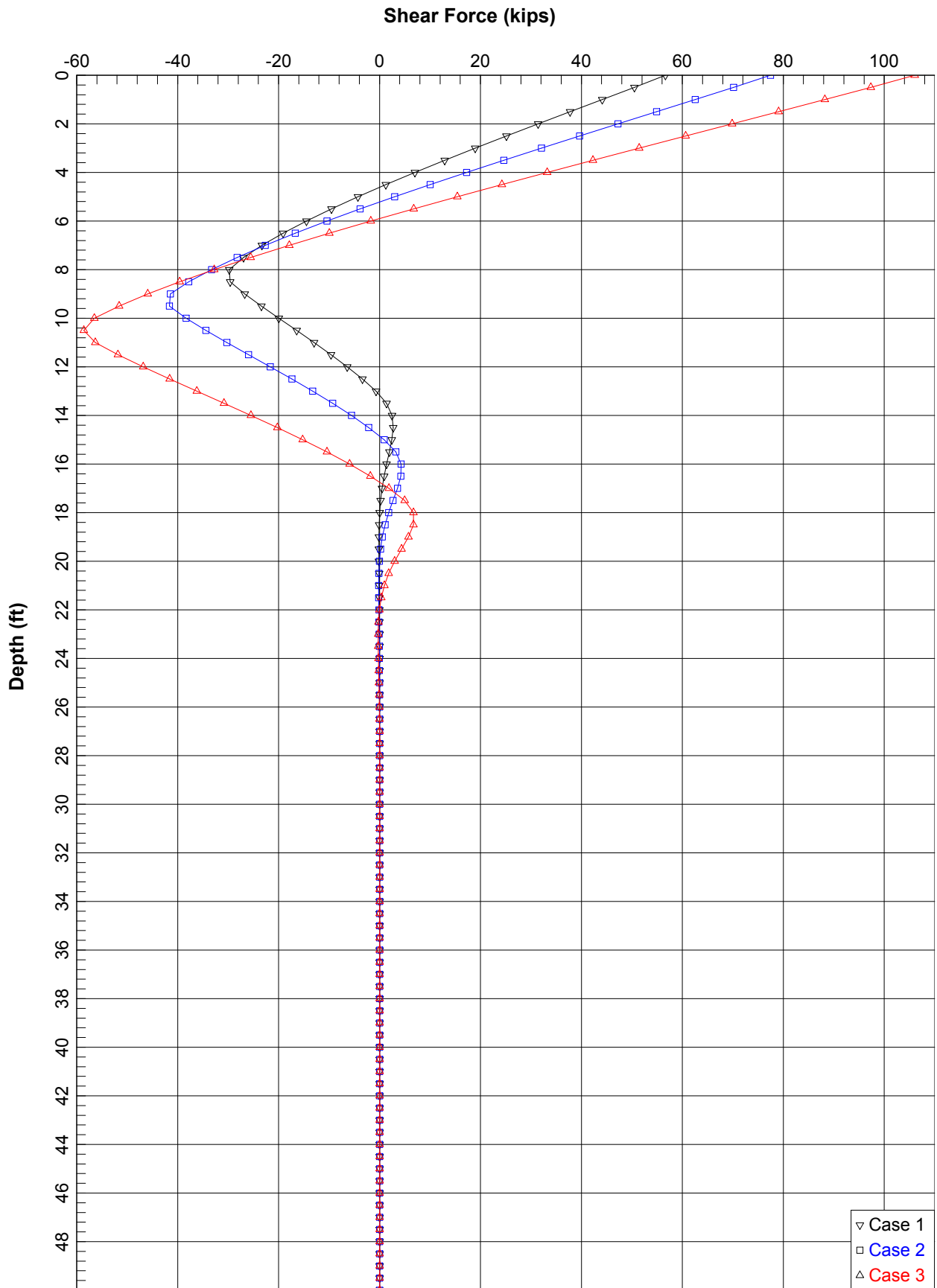
Load Type 1: Load 1 = shear, lbs, and Load 2 = Moment, in-lbs
Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians

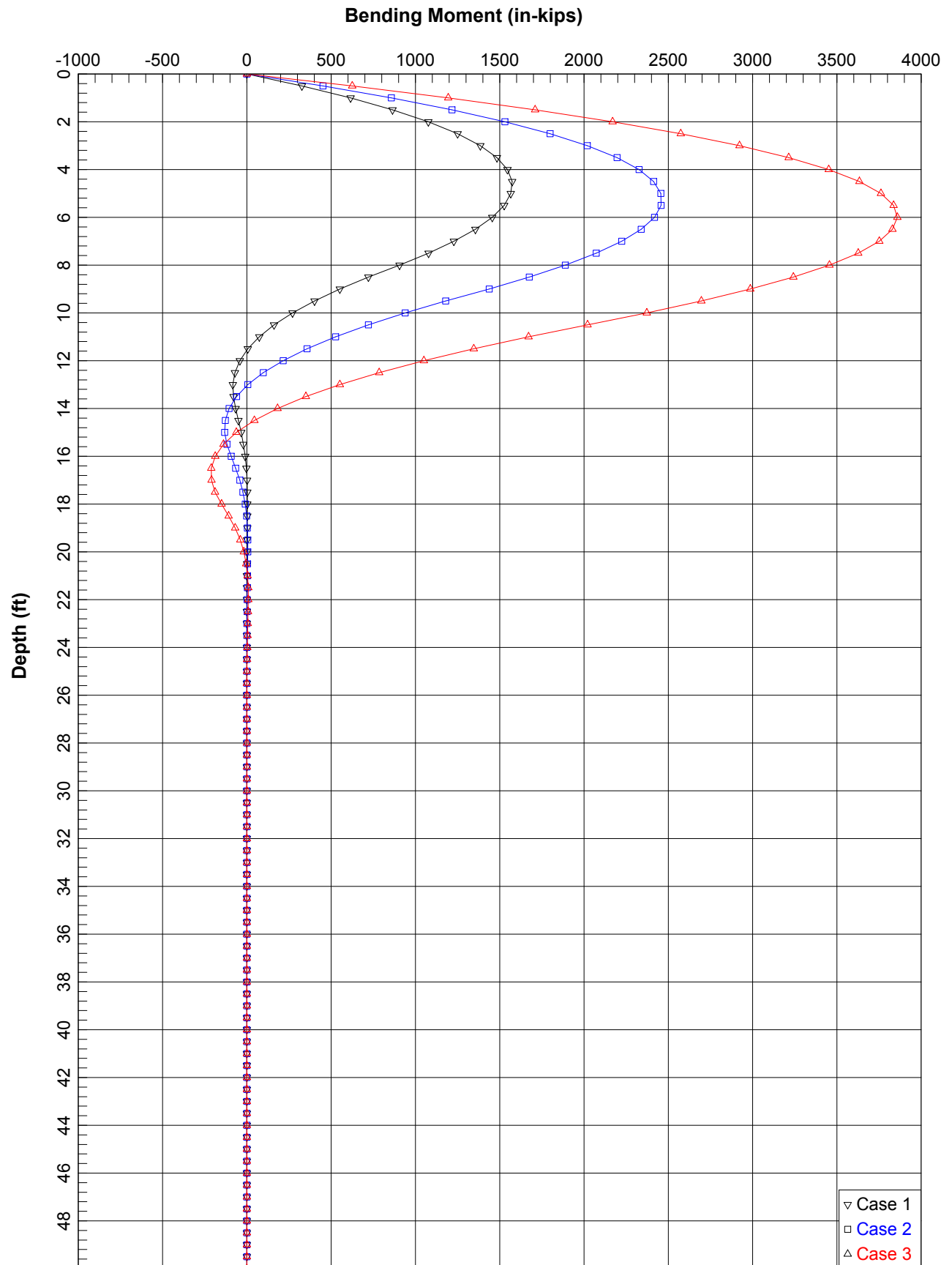
Bent 4R_transv_ave P

Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.		Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y =	0.2500	M = 0.000	169000.	0.25000000	1284684.	41415.	-0.00387226
2	4	y =	0.5000	M = 0.000	169000.	0.50000000	2012302.	56686.	-0.00654807
3	4	y =	1.0000	M = 0.000	169000.	1.00000000	3163188.	77650.	-0.01213114

The analysis ended normally.





Bent 4R_transv_Max P

Pile Plus for windows, version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Bent 4\
 Name of input data file: Bent 4R_transv_Max P.lp6d
 Name of output report file: Bent 4R_transv_Max P.lp6o
 Name of plot output file: Bent 4R_transv_Max P.lp6p
 Name of runtime message file: Bent 4R_transv_Max P.lp6r

Date and Time of Analysis

Date: September 13, 2014 Time: 21:12:27

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 4R_transv_Max P
 = Circular
 Section Length = 50.0000000 ft
 Top width = 24.0000000 in
 Bottom width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 2 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer Factor Num.	Layer Soil Type (p-y Curve Criteria) pcf	Rock Mass Rock Emass psi	Layer Depth ft	Effective unit wt. pcf Type	Undrained Cohesion psf Property	Angle of Friction deg. Mod. pci	Elastic Subgrade psi	Uniaxial qu psi	RQD % or GSI	Epsilon
1	Stiff Clay w/o Free water	--	-5.0000	120.0000	4500.0000	--	--	--	--	--
0.00700	--	--	0.100000	120.0000	4500.0000	--	--	--	--	--
2	Stiff Clay w/o Free water	--	0.100000	125.0000	4500.0000	--	--	--	--	--
0.00500	--	--	80.0000	125.0000	4500.0000	--	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.0000	0.6750	1.0000
2	50.0000	0.6750	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Bent 4R_transv_Max P Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4	y = 0.25000 in M = 0.0000 in-lbs	N = 0.0000 in-lbs	169000.	False
2	4	y = 0.50000 in M = 0.0000 in-lbs	N = 0.0000 in-lbs	169000.	False
3	4	y = 1.00000 in M = 0.0000 in-lbs	N = 0.0000 in-lbs	169000.	False

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
E = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations Nominal Moment Capacity and Nonlinear Bending Stiffness

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed values of Pile Loading and Deflection
For Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.250000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 169000.000 lbs

Depth inches	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi	Bending Stiffness lb-in ²	Soil Res. lb/in	Soil Spr. lb/inch	Distrib. Lat. Load lb/inch
0.00	0.2500	0.000	56626.	-0.004288	373.5720	2.936E+10	-974.5682	11695.	0.000
6.000	0.2243	326563.	50513.	-0.004254	854.8139	2.936E+10	-1063.3113	28447.	0.000
0.188	0.1899	6142779.	-24694.	-0.001131	2370.3682	2.936E+10	-736.7229	300795.	0.000
18.000	0.1744	864576.	37761.	-0.004007	1647.6606	2.936E+10	-1059.8807	36468.	0.000
24.000	0.1509	1076038.	31426.	-0.003808	1955.2831	2.936E+10	-1051.8045	41830.	0.000
30.000	0.1287	1249414.	25133.	-0.003571	2214.7770	2.936E+10	-1039.2488	48459.	0.000
36.000	0.1080	1385114.	18969.	-0.003302	2414.7555	2.936E+10	-1022.0036	56768.	0.000
42.000	0.0893	1477747.	12904.	-0.003008	2560.0919	2.936E+10	-999.8231	67360.	0.000
48.000	0.0719	1546059.	6986.9475	-0.002699	2651.9329	2.936E+10	-972.4099	81128.	0.000
54.000	0.0567	1573054.	1251.5520	-0.002380	2691.7138	2.936E+10	-939.3886	99455.	0.000
60.000	0.0434	1565995.	-4267.3929	-0.002059	2681.1781	2.936E+10	-900.2597	124584.	0.000
66.000	0.0320	1526021.	-9531.1120	-0.001743	2622.4039	2.936E+10	-854.3133	160376.	0.000
72.000	0.0224	1455067.	-14495.	-0.001439	2517.8409	2.936E+10	-800.4510	214046.	0.000
78.000	0.0147	1354994.	-19107.	-0.001131	2370.3682	2.936E+10	-736.7229	300795.	0.000
84.000	0.008621	1228117.	-23296.	-0.000887	2181.3947	2.936E+10	-659.4326	439899.	0.000
90.000	0.004049	1077245.	-26949.	-0.000652	1961.0621	2.936E+10	-558.2611	627357.	0.000
96.000	0.000798	906051.	-29771.	-0.000449	1708.7804	2.936E+10	-482.2321	897382.	0.000
102.000	-0.001341	720909.	-29599.	-0.000283	1435.9439	2.936E+10	-439.3404	1265735.	0.000
108.000	-0.002596	551433.	-26691.	-0.000153	1186.1950	2.936E+10	-330.0255	1248661.	0.000
114.000	-0.003175	400924.	-23394.	-5.554E-05	964.3964	2.936E+10	-268.9174	1074973.	0.000
120.000	-0.003263	270813.	-19935.	-1.310E-05	772.6573	2.936E+10	-284.2358	1074338.	0.000
126.000	-0.003018	161678.	-16430.	5.730E-05	611.8302	2.936E+10	-344.1172	1161200.	0.000
132.000	-0.002575	73538.	-12961.	8.134E-05	481.9421	2.936E+10	-572.0797	1332899.	0.000
138.000	-0.002024	5977.8533	-9595.3290	8.947E-05	382.3833	2.936E+10	-549.9048	1615723.	0.000
144.000	-0.001502	-41787.	-6390.0789	9.881E-05	435.1520	2.936E+10	-518.5119	2071852.	0.000
150.000	-0.001012	-70877.	-3399.8365	7.429E-05	478.0206	2.936E+10	-478.2556	2834332.	0.000
156.000	0.000610	-82736.	-678.9868	5.860E-05	495.4963	2.936E+10	-428.7143	4216373.	0.000
162.000	-0.000309	-79144.	1402.4799	4.205E-05	490.2028	2.936E+10	-265.1079	5143953.	0.000
168.000	-0.000105	-65991.	2473.6270	2.722E-05	470.8207	2.936E+10	-91.9411	5231844.	0.000
174.000	1.742E-05	-49515.	2703.1203	1.542E-05	446.5408	2.936E+10	-15.4433	5197246.	0.000
180.000	7.955E-05	-33585.	2441.6927	6.924E-06	423.0651	2.936E+10	-71.6992	5406725.	0.000
186.000	0.000101	-20229.	1950.4405	1.424E-06	403.3629	2.936E+10	-92.0515	5495515.	0.000
192.000	8.664E-05	-10185.	1404.4900	-1.684E-06	388.5780	2.936E+10	-89.9329	5695312.	0.000
198.000	8.029E-05	-3371.9005	907.0062	3.069E-06	378.5410	2.936E+10	-75.8959	5671297.	0.000
204.000	3.581E-05	107.4215	468.9134	-3.341E-06	374.6164	2.936E+10	-66.7750	5695312.	0.000
210.000	4.020E-05	2742.7967	224.1996	-2.989E-06	377.6140	2.936E+10	-38.1562	5695312.	0.000
216.000	2.295E-05	3403.9285	41.5400	-2.361E-06	378.5882	2.936E+10	-22.7303	5695312.	0.000
222.000	1.187E-05	3246.0645	-60.4511	-1.681E-06	378.3556	2.936E+10	-11.8667	5695312.	0.000
228.000	3.773E-06	2681.9249	-104.9968	-1.075E-06	377.5243	2.936E+10	-3.5818	5695312.	0.000
234.000	-1.034E-06	1988.2834	-117.7989	-5.980E-07	376.5021	2.936E+10	0.9811	5695312.	0.000
240.000	-3.464E-06	129.5593	-100.1668	-9.386E-07	375.5313	2.936E+10	3.7286	5695312.	0.000
246.000	-4.141E-06	786.8068	-78.6870	-4.264E-08	374.7315	2.936E+10	3.9306	5695312.	0.000
252.000	-3.914E-06	385.3933	-55.7502	7.716E-08	374.1400	2.936E+10	3.7152	5695312.	0.000
258.000	-3.216E-06	117.6480	-35.4500	1.286E-07	373.7434	2.936E+10	3.5030	5695312.	0.000
264.000	-2.371E-06	-40.2680	-19.5432	1.365E-07	373.6314	2.936E+10	2.2508	5695312.	0.000
270.000	-1.380E-06	-11.0208	-8.0278	5.366E-08	373.7447	2.936E+10	1.4970	5695312.	0.000
276.000	-9.266E-07	-140.1113	-1.1705	9.410E-08	373.7785	2.936E+10	0.8795	5695312.	0.000
282.000	-4.479E-07	-131.3840	2.7435	6.635E-08	373.7636	2.936E+10	0.4252	5695312.	0.000
288.000	1.304E-07	-107.3241	4.3901	4.189E-08	373.7805	2.936E+10	0.1237	5695312.	0.000
294.000	5.537E-08	-78.7874	4.6031	2.294E-08	373.6881	2.936E+10	-0.1277	5695312.	0.000
300.000	1.469E-07	52.1334	4.0323	5.556E-07	373.6488	2.936E+10	-0.0535	5695312.	0.000
306.000	1.702E-07	-30.4193	-1.1249	-1.120E-09	373.6188	2.936E+10	0.00244	5695312.	0.000
312.000	1.583E-07	-14.5166	2.1993	-3.472E-09	373.5934	2.936E+10	-0.1503	5695312.	0.000
318.000	5.860E-08	3.1812	1.3122	7.910E-09	373.5778	2.936E+10	0.00711	5695312.	0.000
324.000	9.391E-08	2.0819	0.7487	-5.565E-09	373.5751	2.936E+10	-0.0891	5695312.	0.000
330.000	6.180E-08	4.9750	0.3053	-4.844E-09	373.5794	2.936E+10	-0.0587	5695312.	0.000
336.000	2.402E-07	5.8082	0.1274	-7.476E-09	373.5805	2.936E+10	0.0349	5695312.	0.000
342.000	1.684E-08	5.5111	-0.1225	-2.616E-09	373.5798	2.936E+10	-0.0160	5695312.	0.000
348.000	4.396E-09	4.2907	-0.1830	-1.635E-09	373.5783	2.936E+10	-0.00473	5695312.	0.000
354.000	-1.836E-08	2.9090	-0.1875	-8.777E-07	373.5766	2.936E+10	0.00244	5695312.	0.000
360.000	-6.136E-09	2.0419	-0.1621	-3.503E-10	373.5750	2.936E+10	-0.005825	5695312.	0.000
366.000	-1.078E-08	1.4010	-0.1489	-1.120E-09	373.5744	2.936E+10	-0.006631	5695312.	0.000
372.000	-6.396E-09	0.5446	-0.0867	1.540E-10	373.5728	2.936E+10	0.006071	5695312.	0.000
378.000	-5.138E-09	0.1336	-0.0538	2.233E-10	373.5722	2.936E+10	0.004877	5695312.	0.000
384.000	-3.716E-09	-0.1018	-0.0286	2.266E-10	373.5722	2.936E+10	0.003527	5695312.	0.000

Page 3

390.000	-2.419E-09	-0.2102	-0.0111	1.947E-10	Bent 4R_transv_Max P	0.002296	5695312.	0.000	
396.000	-1.380E-09	-0.2359	-0.000326	1.491E-10	373.5724	2.936E+10	0.001310	5695312.	0.000
402.000	-6.302E-10	-0.2144	0.000398	1.031E-10	373.5723	2.936E+10	0.000598	5695312.	0.000
408.000	-1.344E-10	-0.1714	0.000001	6.362E-11	373.5723	2.936E+10	0.000035	5695312.	0.000
414.000	0.1332E-10	-0.1234	0.007630	3.350E-11	373.5722	2.936E+10	-0.000127	5695312.	0.000
420.000	2.587E-10	-0.0799	0.006513	1.275E-11	373.5721	2.936E+10	-0.000246	5695312.	0.000
426.000	2.861E-10	-0.0452	0.004962	0.000	373.5721	2.936E+10	-0.000195	5695312.	0.000
432.000	2.581E-10	-0.0203	0.000342	-6.751E-12	373.5720	2.936E+10	-0.000245	5695312.	0.000
438.000	2.051E-10	-0.004264	0.002093	-9.265E-12	373.5720	2.936E+10	-0.000139	5695312.	0.000
444.000	1.469E-10	0.004801	0.001091	-9.210E-12	373.5720	2.936E+10	-0.000139	5695312.	0.000
450.000	9.458E-11	0.008844	0.000403	-7.816E-12	373.5720	2.936E+10	-8.978E-05	5695312.	0.000
456.000	5.111E-11	0.000655	1.736E-05	-5.926E-12	373.5720	2.936E+10	-5.041E-05	5695312.	0.000
462.000	2.347E-11	0.008648	-0.000235	-4.055E-12	373.5720	2.936E+10	-2.228E-05	5695312.	0.000
468.000	4.445E-12	0.006838	-0.000315	-2.472E-12	373.5720	2.936E+10	-4.220E-06	5695312.	0.000
474.000	-6.106E-12	0.004874	-0.000310	-1.276E-12	373.5720	2.936E+10	5.882E-06	5695312.	0.000
480.000	-1.086E-11	0.003121	-0.000261	0.000	373.5720	2.936E+10	1.031E-05	5695312.	0.000
486.000	-1.170E-11	0.001739	-0.000187	0.000	373.5720	2.936E+10	1.110E-05	5695312.	0.000
492.000	-1.040E-11	0.000756	-0.000134	0.000	373.5720	2.936E+10	9.874E-06	5695312.	0.000
498.000	-8.180E-12	0.000128	-8.128E-05	0.000	373.5720	2.936E+10	7.765E-06	5695312.	0.000
504.000	-5.802E-12	-0.000221	-4.148E-05	0.000	373.5720	2.936E+10	5.507E-06	5695312.	0.000
510.000	-3.693E-12	-0.000371	-1.442E-05	0.000	373.5720	2.936E+10	3.506E-06	5695312.	0.000
516.000	-2.040E-12	-0.000394	1.902E-06	0.000	373.5720	2.936E+10	1.936E-06	5695312.	0.000
522.000	0.000	-0.001348	1.019E-05	0.000	373.5720	2.936E+10	8.251E-07	5695312.	0.000
528.000	0.000	-0.000272	1.302E-05	0.000	373.5720	2.936E+10	1.195E-07	5695312.	0.000
534.000	0.000	-0.000152							

252.000		1.706E-06		3698.2845		-176.7033		-1.301E-06		Bent 4R_transv_Max P		375.9222		2.936E+10		-1.6196		5695312.0		0.000	
258.000	-6.832E-06	2609.9472	-170.6507	-6.563E-07	377.4182	2.936E+10	3.6372	5695312.0	0.000												
264.000	-6.169E-06	1651.9076	-142.1716	-2.207E-07	376.0064	2.936E+10	5.8558	5695312.0	0.000												
270.000	-6.483E-06	1511.1850	-106.1484	-4.049E-07	375.1511	2.936E+10	1.1702	5695312.0	0.000												
276.000	-4.422E-06	485.8565	-42.7346	-2.149E-07	373.6396	2.936E+10	4.1975	5695312.0	0.000												
282.000	-3.105E-06	-218.3276	-21.3080	-2.057E-07	373.7838	2.936E+10	2.9471	5695312.0	0.000												
294.000	-1.933E-06	-210.1684	-6.8970	-1.704E-07	373.8817	2.936E+10	1.8541	5695312.0	0.000												
300.000	-1.060E-06	-102.9183	6.9134	2.483E-08	373.7237	2.936E+10	1.0057	5695312.0	0.000												
306.000	-4.335E-07	-190.2354	5.9342	8.489E-08	373.8524	2.936E+10	0.4115	5695312.0	0.000												
312.000	-4.081E-08	-147.2894	7.2849	5.040E-08	373.7891	2.936E+10	0.0387	5695312.0	0.000												
318.000	-1.713E-07	-102.9183	6.9134	2.483E-08	373.7237	2.936E+10	0.1626	5695312.0	0.000												
324.000	2.572E-07	-64.3787	5.6934	7.733E-09	373.6669	2.936E+10	-0.2441	5695312.0	0.000												
330.000	2.641E-07	-34.6132	4.2091	-2.383E-09	373.6230	2.936E+10	-0.2507	5695312.0	0.000												
336.000	2.786E-07	-15.8645	2.8063	-7.338E-09	373.5925	2.936E+10	-0.2169	5695312.0	0.000												
342.000	1.760E-07	-0.9230	1.6542	-8.849E-09	373.5734	2.936E+10	-0.1671	5695312.0	0.000												
348.000	1.224E-07	6.0036	0.8045	-8.330E-09	373.5809	2.936E+10	-0.1167	5695312.0	0.000												
354.000	7.607E-08	8.7474	0.2394	-6.827E-09	373.5849	2.936E+10	-0.0722	5695312.0	0.000												
360.000	4.050E-08	8.8999	-0.0926	-5.020E-09	373.5851	2.936E+10	-0.0384	5695312.0	0.000												
366.000	1.584E-08	7.6485	-0.2530	-3.330E-09	373.5833	2.936E+10	-0.0150	5695312.0	0.000												
372.000	5.468E-10	5.8603	-0.2997	-1.949E-09	373.5807	2.936E+10	-0.000519	5695312.0	0.000												
378.000	-7.536E-09	4.0543	-0.2797	-9.361E-10	373.5780	2.936E+10	0.007172	5695312.0	0.000												
384.000	-1.060E-08	2.5056	-0.2278	-2.637E-10	373.5757	2.936E+10	0.0101	5695312.0	0.000												
390.000	-1.074E-08	1.3216	-0.1667	-1.254E-10	373.5740	2.936E+10	0.0102	5695312.0	0.000												
396.000	-9.182E-09	0.5044	-0.1100	-3.120E-10	373.5728	2.936E+10	0.008715	5695312.0	0.000												
402.000	-7.000E-09	0.000889	-0.0639	-3.636E-10	373.5720	2.936E+10	0.006845	5695312.0	0.000												
408.000	-4.818E-09	-0.2634	-0.0303	-3.368E-10	373.5724	2.936E+10	0.004573	5695312.0	0.000												
414.000	-2.959E-09	-0.3630	-0.008124	-2.728E-10	373.5726	2.936E+10	0.002808	5695312.0	0.000												
420.000	-1.544E-09	-0.3614	0.004699	-1.988E-10	373.5726	2.936E+10	0.001466	5695312.0	0.000												
426.000	-5.734E-10	-0.3070	0.0107	-1.304E-10	373.5725	2.936E+10	0.000544	5695312.0	0.000												
432.000	2.176E-10	-0.1811	-0.0112	-3.164E-10	373.5724	2.936E+10	0.000193	5695312.0	0.000												
438.000	3.298E-10	-0.1595	0.0113	-3.515E-11	373.5723	2.936E+10	-0.000313	5695312.0	0.000												
444.000	4.429E-10	-0.0974	0.009103	-8.896E-12	373.5722	2.936E+10	-0.000420	5695312.0	0.000												
450.000	6.365E-10	0.0503	0.003939	-3.066E-12	373.5712	2.936E+10	-0.000144	5695312.0	0.000												
456.000	3.685E-10	-0.0182	0.004307	-1.320E-11	373.5720	2.936E+10	-0.000350	5695312.0	0.000												
462.000	2.781E-10	0.003388	0.002466	-1.491E-11	373.5720	2.936E+10	-0.000264	5695312.0	0.000												
468.000	1.895E-10	0.0114	0.001134	-1.360E-11	373.5720	2.936E+10	-0.000180	5695312.0	0.000												
474.000	1.149E-10	0.0150	0.000267	-1.090E-11	373.5720	2.936E+10	-0.000109	5695312.0	0.000												
480.000	3.872E-11	0.0147	-0.000227	-7.863E-12	373.5720	2.936E+10	-5.574E-05	5695312.0	0.000												
486.000	2.054E-11	0.0123	-0.000453	-5.105E-12	373.5720	2.936E+10	-1.950E-05	5695312.0	0.000												
492.000	-2.536E-12	0.009251	-0.000504	-2.901E-12	373.5720	2.936E+10	2.407E-06	5695312.0	0.000												
498.000	-1.477E-11	0.006572	-0.000672	-1.314E-12	373.5720	2.936E+10	1.354E-05	5695312.0	0.000												
504.000	-1.831E-11	0.003779	-0.000363	0.0000	373.5720	2.936E+10	1.738E-05	5695312.0	0.000												
510.000	-1.771E-11	0.003191	-0.000361	0.0000	373.5720	2.936E+10	1.681E-05	5695312.0	0.000												
516.000	-1.447E-11	0.000648	-0.000168	0.0000	373.5720	2.936E+10	1.407E-05	5695312.0	0.000												
522.000	-1.104E-11	-0.000111	-9.490E-05	0.0000	373.5720	2.936E+10	1.048E-05	5695312.0	0.000												
528.000	-7.444E-12	-0.000492	-4.226E-05	0.0000	373.5720	2.936E+10	7.066E-06	5695312.0	0.000												
534.000	-4.451E-12	-0.000619	-8.388E-06	0.0000	373.5720	2.936E+10	4.225E-06	5695312.0	0.000												
540.000	-2.219E-12	-0.000594	-1.061E-05	0.0000	373.5720	2.936E+10	2.106E-06	5695312.0	0.000												
546.000	0.0000	-0.000493	-1.896E-05	0.0000	373.5720	2.936E+10	6.777E-07	5695312.0	0.000												
552.000	0.0000	-0.000367	-2.046E-05	0.0000	373.5720	2.936E+10	-1.768E-07	5695312.0	0.000												
558.000	0.0000	-0.000247	-1.812E-05	0.0000	373.5720	2.936E+10	-6.043E-07	5695312.0	0.000												
564.000	0.0000	-0.000150	-1.407E-05	0.0000	373.5720	2.936E+10	-7.437E-07	5695312.0	0.000												
570.000	0.0000	-7.858E-05	-9.713E-06	0.0000	373.5720	2.936E+10	-7.090E-07	5695312.0	0.000												
576.000	0.0000	-3.304E-05	-0.000006	0.0000	373.5720	2.936E+10	-5.828E-07	5695312.0	0.000												
582.000	0.0000	-8.473E-06	-2.835E-06	0.0000	373.5720	2.936E+10	-4.181E-07	5695312.0	0.000												
588.000	0.0000	1.042E-06	8.498E-07	0.0000	373.5720	2.936E+10	-2.436E-07	5695312.0	0.000												
594.000	0.0000	1.786E-07	-9.132E-08	0.0000	373.5720	2.936E+10	3.866E-08	5695312.0	0.000												
600.000	0.0000	0.0000	0.0000	0.0000	373.5720	2.936E+10	1.009E-07	2847656.0	0.000												

* The above values of total stress are combined axial and bending stress.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Pile-head deflection	=	0.5000000	inches
Computed slope at pile head	=	-0.0075752	radians
Maximum bending moment	=	2457428.	inch-lbs
Maximum shear force	=	17450.	lbs
Depth of maximum bending moment	=	66.0000000	inches below pile head
Depth of maximum shear force	=	0.0000000	inches below pile head
Number of iterations	=	20	
Number of zero deflection points	=	9</	

Bent 4R_transv_Max P

Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

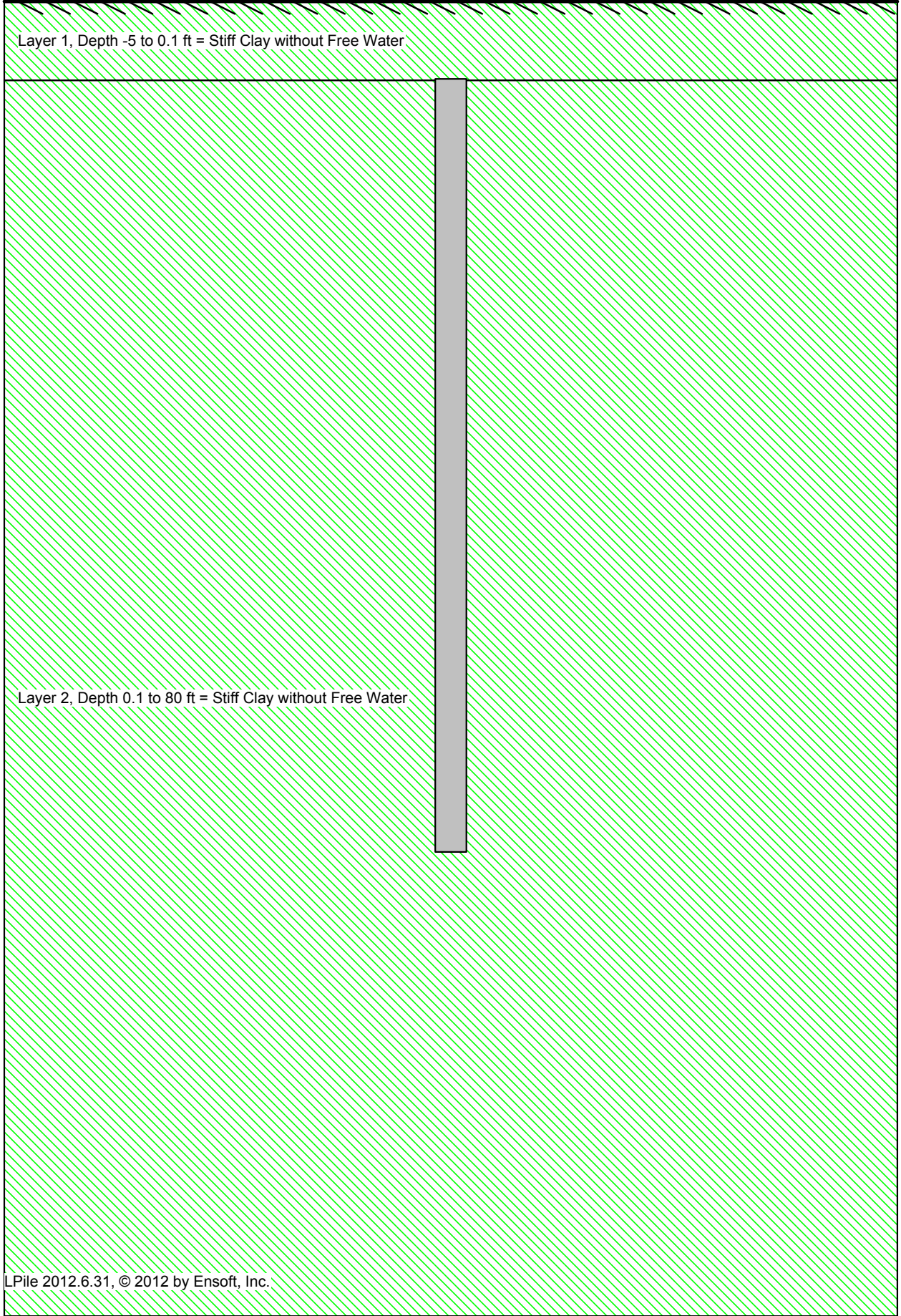
Load Case No.	Load Type No.		Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y =	0.2500	M = 0.000	169000.	0.25000000	1573054.	56626.	-0.00428756
2	4	y =	0.5000	M = 0.000	169000.	0.50000000	2457428.	77450.	-0.00757520
3	4	y =	1.0000	M = 0.000	169000.	1.00000000	3858368.	106014.	-0.01340138

The analysis ended normally.

SUPPORT: BENT 4L

LOAD DIRECTION: LONGITUDE

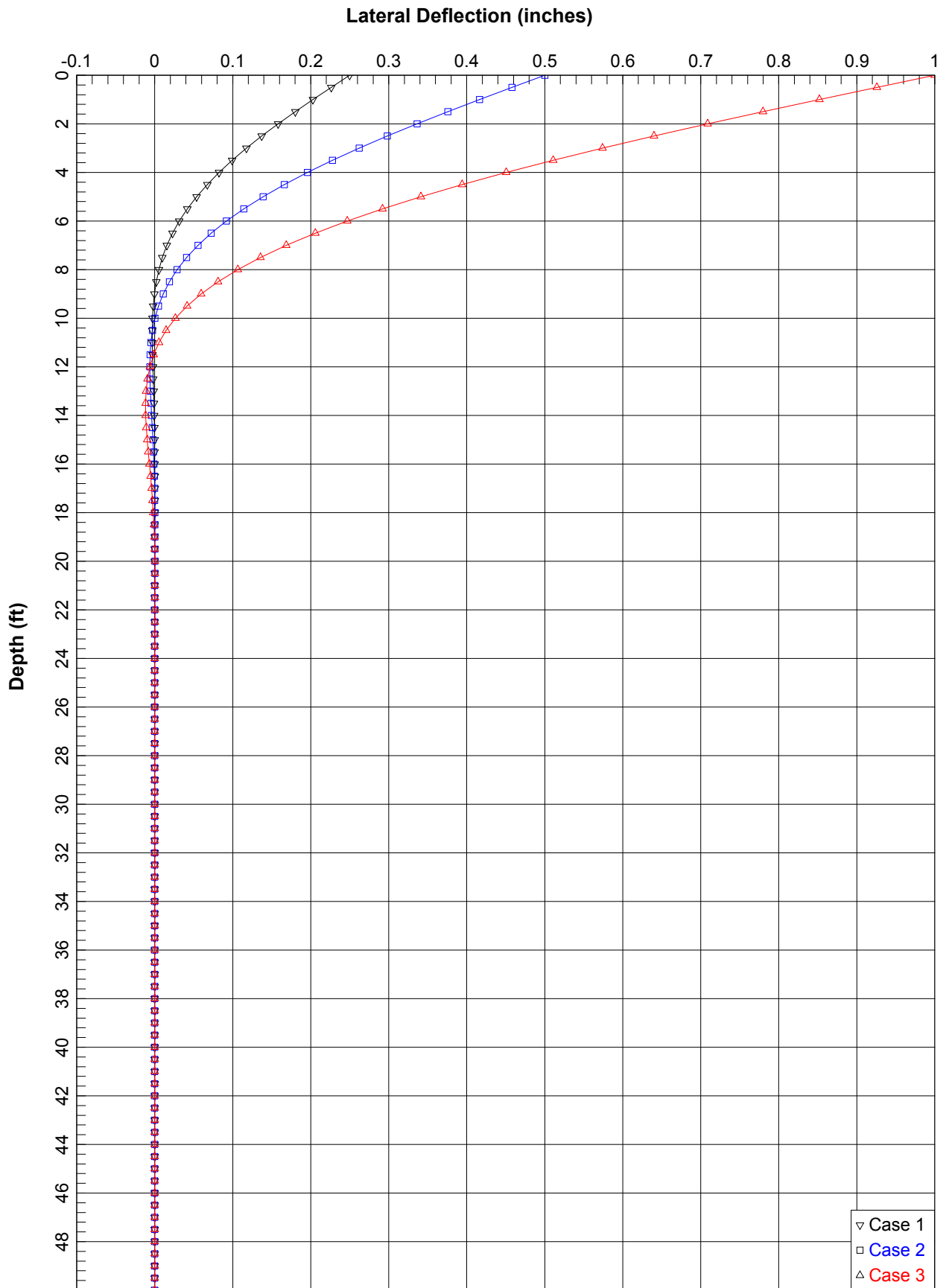
1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE

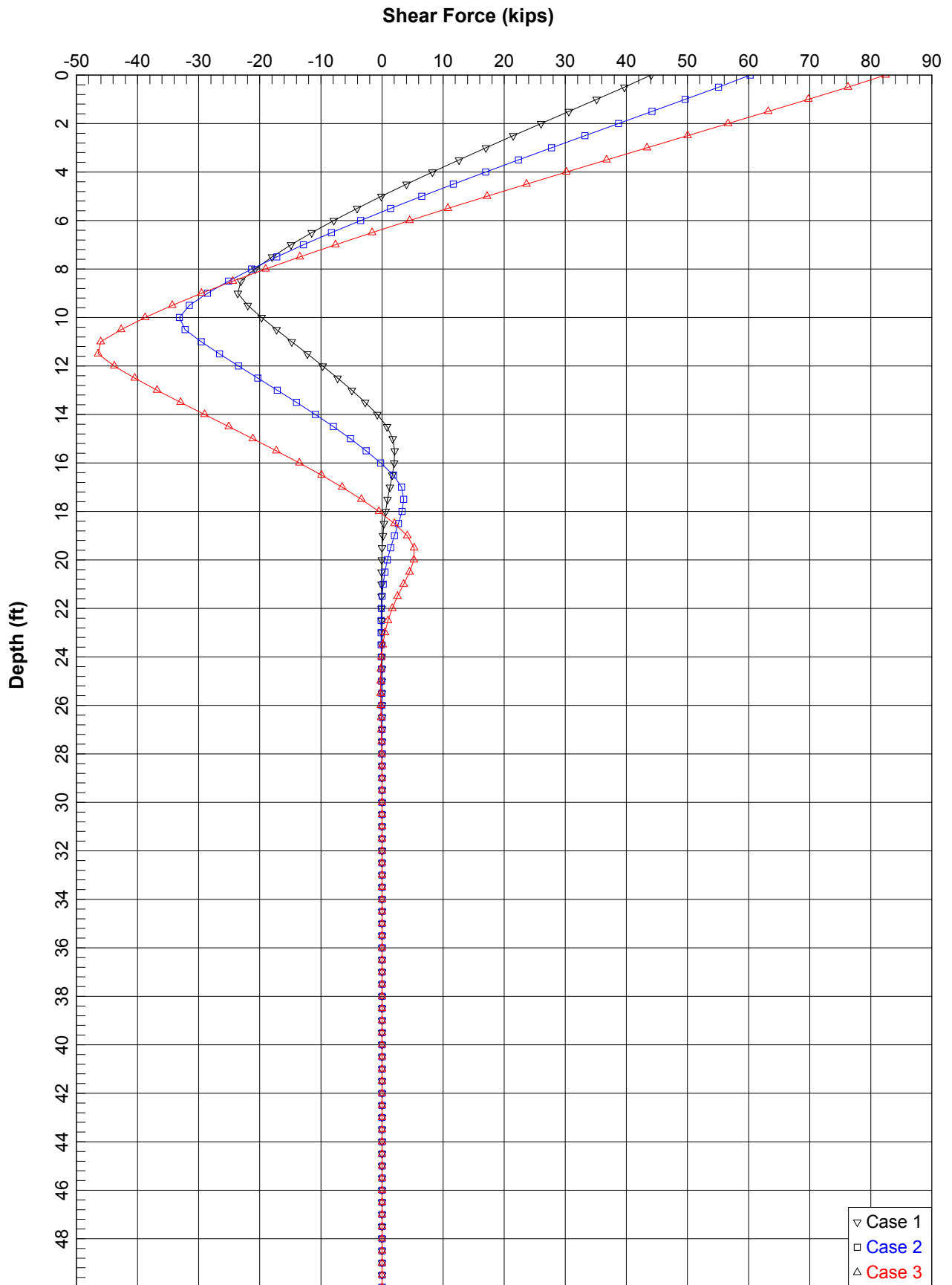


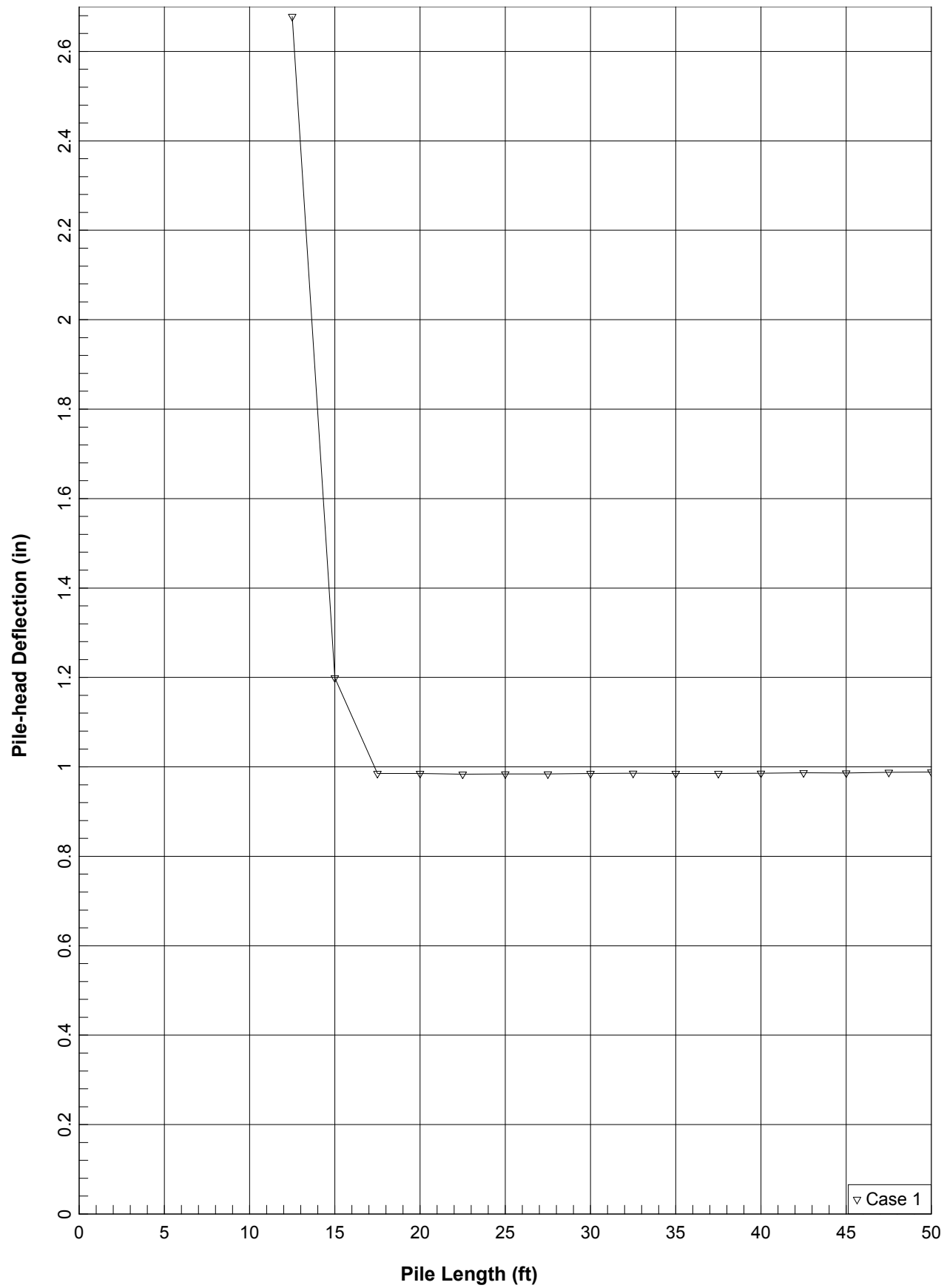
A cross-sectional diagram of a pile foundation. The pile is a vertical grey rectangle extending from the ground surface down into two soil layers. The top layer is labeled 'Layer 1, Depth -5 to 0.1 ft = Stiff Clay without Free Water' and is filled with a light green diagonal hatching pattern. The bottom layer is labeled 'Layer 2, Depth 0.1 to 80 ft = Stiff Clay without Free Water' and is filled with a darker green diagonal hatching pattern. The ground surface is indicated by a horizontal line with a hatched area above it representing the ground above the surface.

Layer 1, Depth -5 to 0.1 ft = Stiff Clay without Free Water

Layer 2, Depth 0.1 to 80 ft = Stiff Clay without Free Water







Bent 4L_long_crit length

Pile Plus for windows, version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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gdc
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Bent 4\
 Name of input data file: Bent 4L_long_crit length.lpd
 Name of output report file: Bent 4L_long_crit length.lpr
 Name of plot output file: Bent 4L_long_crit length.lpp
 Name of runtime message file: Bent 4L_long_crit length.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 21:15:45

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 4L_long_crit length
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top width = 24.0000000 in
 Bottom width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 2 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer	Rock Mass	Layer	Effective	Undrained	Angle of	Elastic	Uniaxial	RQD %
Factor	Soil Type	Rock Emass	Depth	unit wt.	In-situ Cohesion	Friction	Mod.	qu	or
50	(p-y Curve Criteria)	ft	ft	pcf	psf	deg.	psi	psi	GSI
Num.	psi		Type	Test	Property	psi			Epsilon
1	Stiff Clay w/o Free water	--	-5.0000	120.0000	4500.0000	--	--	--	--
0.00700	--	--	0.100000	120.0000	4500.0000	--	--	--	--
0.00700	--	--	0.100000	125.0000	4500.0000	--	--	--	--
2	Stiff Clay w/o Free water	--	0.100000	125.0000	4500.0000	--	--	--	--
0.00500	--	--	80.0000	125.0000	4500.0000	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.0000	0.4800	1.0000
2	50.0000	0.4800	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Load No.	Load Type	Bent 4L Long Crit Length		Compute Top y vs. Pile Length
		Condition 1	Condition 2	
V	1	V = 82000. lbs	M = 0.0000 in-lbs	198000.

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection
for Lateral Loading for Load Case Number 1

Pile-head conditions are shear and Moment (Loading Type 1)

Shear force at pile head = 82000.000 lbs
Applied moment at pile head = 0.000 in-lbs
Axial thrust load on pile head = 198000.000 lbs

Depth inches	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi*	Bending lb-in/2	Soil Res. lb/in	Soil Spr. lb/in2	Distrib. Lat. Load lb/inch
0.00	0.9882	0.000	82000.	-0.0123	437.6761	2.936E+10	-977.3960	2966.5238	0.000
6.00	0.9147	488969.	75845.	-0.0122	1158.2490	2.936E+10	-1074.5434	7048.5422	0.000
12.00	0.8418	939136.	63967.	-0.0121	1821.6406	2.936E+10	-1181.0844	1084.8094	0.000
18.00	0.7700	1350022.	62835.	-0.0118	2427.1453	2.936E+10	-1092.5489	8513.5145	0.000
24.00	0.6999	1722448.	56264.	-0.0115	2974.2054	2.936E+10	-1097.6742	9410.4575	0.000
30.00	0.6319	2052340.	49671.	-0.0111	3482.4161	2.936E+10	-1100.0938	10446.	0.000
36.00	0.5664	2343730.	43071.	-0.0107	3891.5306	2.936E+10	-1099.7115	11650.	0.000
42.00	0.5037	2594762.	36483.	-0.0102	4261.4649	2.936E+10	-1096.4249	13059.	0.000
48.00	0.4443	2803692.	29923.	-0.009620	4572.3036	2.936E+10	-1090.1241	14721.	0.000
54.00	0.3883	2976697.	23411.	-0.009029	4824.3055	2.936E+10	-1080.6887	16699.	0.000
60.00	0.3360	3097936.	16965.	-0.008407	5017.9099	2.936E+10	-1067.9858	19074.	0.000
66.00	0.2874	3200248.	10605.	-0.007762	5153.7438	2.936E+10	-1051.8633	21958.	0.000
72.00	0.2428	3253779.	4353.1660	-0.007103	5232.6294	2.936E+10	-1032.1468	25505.	0.000
78.00	0.2022	3269362.	-1769.1546	-0.006436	5255.5937	2.936E+10	-1008.6268	29531.	0.000
84.00	0.1656	3247841.	-7738.1706	-0.005770	5223.8788	2.936E+10	-981.0452	33550.	0.000
90.00	0.1330	3190215.	-13529.	-0.005112	5138.9557	2.936E+10	-949.0709	42831.	0.000
96.00	0.1042	3097644.	-21311.	-0.004469	5002.5412	2.936E+10	-912.5376	52111.	0.000
102.00	0.0793	2971482.	-24459.	-0.003849	4816.6215	2.936E+10	-869.9694	63808.	0.000
108.00	0.0580	2813280.	-29513.	-0.003258	4583.4853	2.936E+10	-821.2336	84888.	0.000
114.00	0.0402	2624830.	-34290.	-0.002702	4305.7746	2.936E+10	-764.4208	114207.	0.000
120.00	0.0256	2408223.	-38672.	-0.002188	3996.5709	2.936E+10	-696.4361	163105.	0.000
126.00	0.0140	2165960.	-42592.	-0.001720	3629.5383	2.936E+10	-610.1110	262064.	0.000
132.00	0.004974	1901207.	-45864.	-0.001305	3239.4033	2.936E+10	-480.4182	579492.	0.000
138.00	-0.001689	1618698.	-46186.	-0.000945	2823.0811	2.936E+10	-372.9013	1324977.	0.000
144.00	-0.006366	1349219.	-43478.	-0.000642	2425.9626	2.936E+10	-279.6640	489183.	0.000
150.00	-0.009390	1098482.	-40107.	-0.000392	2056.4609	2.936E+10	-194.2817	179751.	0.000
156.00	-0.0111	868872.	-36433.	-0.000191	1718.0938	2.936E+10	-130.1740	341694.	0.000
162.00	-0.0117	661786.	-32953.	-0.000105	1412.8476	2.936E+10	-69.8091	533158.	0.000
168.00	-0.0115	477833.	-28670.	-8.233E-05	1141.8380	2.936E+10	-658.0574	344080.	0.000
174.00	-0.0107	217504.	-24723.	0.000164	905.5684	2.936E+10	657.3372	869011.	0.000
180.00	-0.009512	180763.	-20804.	0.000215	704.0580	2.936E+10	649.0024	409391.	0.000
186.00	-0.008114	67341.	-16956.	0.000240	536.9137	2.936E+10	633.8528	468729.	0.000
192.00	-0.006633	-23278.	-13277.	0.000244	471.9001	2.936E+10	612.3542	533912.	0.000
198.00	-0.005181	-91847.	-9626.0019	0.000233	373.0269	2.936E+10	584.7350	677173.	0.000
204.00	-0.003842	-139345.	-6237.1030	0.000209	304.0197	2.936E+10	544.8980	851067.	0.000
210.00	-0.002673	-167189.	-3109.4247	0.000178	246.0349	2.936E+10	497.6613	1117.0000	0.000
216.00	-0.001709	-177078.	-281.3381	0.000142	198.6285	2.936E+10	445.0341	1562054.	0.000
222.00	-0.000963	-179093.	-120.4236	0.000107	169.5290	2.936E+10	385.5352	2402090.	0.000
228.00	-0.000426	-150807.	4230.2518	7.405E-05	139.9140	2.936E+10	287.7229	4050000.	0.000
234.00	-7.441E-05	-120316.	5244.0994	4.635E-05	110.9810	2.936E+10	20.2264	4050000.	0.000
240.00	0.000130	-87988.	5131.7553	2.506E-05	86.3403	2.936E+10	-67.6745	4050000.	0.000
246.00	0.000226	-58795.	4410.5105	1.006E-05	54.3194	2.936E+10	-152.7404	4050000.	0.000
252.00	0.000251	-35086.	3444.8783	4.630E-07	489.3805	2.936E+10	-169.1370	4050000.	0.000
258.00	0.000232	17452.	2467.9963	-4.907E-06	463.4022	2.936E+10	-156.4903	4050000.	0.000
264.00	0.000192	5458.1901	1610.3473	-7.249E-06	445.7196	2.936E+10	-129.3927	4050000.	0.000
270.00	0.000145	1884.0990	928.8384	-7.614E-06	440.4526	2.936E+10	-87.7769	4050000.	0.000
276.00	0.000100	5705.9610	432.3452	-6.838E-06	446.0847	2.936E+10	-67.7208	4050000.	0.000
282.00	6.280E-05	7088.4894	102.0191	-5.531E-06	448.1221	2.936E+10	-42.3879	4050000.	0.000
288.00	3.396E-05	6945.3313	93.3012	-4.097E-06	447.9082	2.936E+10	-22.8228	4050000.	0.000
294.00	1.364E-05	5971.2668	-190.2971	-2.777E-06	446.4757	2.936E+10	9.2052	4050000.	0.000
300.00	6.379E-07	4666.3643	-219.2044	-1.690E-06	444.5527	2.936E+10	-0.4306	4050000.	0.000
306.00	6.639E-06	3144.8282	-207.0521	-8.710E-07	442.6052	2.936E+10	4.4814	4050000.	0.000
312.00	9.814E-06	2183.8087	-173.7346	-3.060E-07	440.8943	2.936E+10	6.6245	4050000.	0.000
318.00	-1.031E-05	1260.7404	-132.9814	4.602E-08	439.5340	2.936E+10	6.9399	4050000.	0.000
324.00	9.462E-05	587.9226	-93.3466	2.349E-07	438.5425	2.936E+10	6.5117	4050000.	0.000
330.00	-7.492E-06	140.0231	-59.4210	3.093E-07	437.8824	2.936E+10	5.0568	4050000.	0.000
336.00	5.550E-06	-125.8617	-33.0124	3.108E-07	437.8616	2.936E+10	3.7460	4050000.	0.000
342.00	-3.762E-06	-256.8646	-14.1560	2.717E-07	438.0546	2.936E+10	2.5394	4050000.	0.000
348.00	-2.290E-06	-296.3820	-1.9012	2.151E-07	438.1129	2.936E+10	1.5455	4050000.	0.000
354.00	1.181E-06	-258.1904	3.2828	1.562E-07	438.0890	2.936E+10	0.7968	4050000.	0.000
360.00	-4.150E-07	-235.2441	8.3568	1.035E-07	438.0228	2.936E+10	0.2802	4050000.	0.000
366.00	6.193E-08	-180.1551	9.0718	6.109E-08	437.9416	2.936E+10	-0.0418	4050000.	0.000
372.00	3.180E-07	-128.5271	3.3023	2.974E-08	437.8432	2.936E+10	0.1246	4050000.	0.000
378.00	4.189E-07	-80.5953	6.8105	8.577E-09	437.7949	2.936E+10	-0.2827	4050000.	0.000
384.00	4.209E-07	-44.8810	11.0174	3.247E-09	437.7421	2.936E+10	-0.2841	4050000.	0.000
390.00	3.680E-07	-19.2657	3.5125	-1.079E-08	437.7045	2.936E+10	-0.2484	4050000.	0.000
396.00	2.914E-07	-2.6465	2.1772	-1.303E-08	437.6800	2.936E+10	-0.1967	4050000.	0.000
402.00	2.116E-07	6.8919	1.1586	-1.260E-08	437.6662	2.936E+10	-0.1428	4050000.	0.000

Page 3

Load No.	Load Type	Condition 1	Condition 2	Force, lbs	Top y vs. Pile Length				
408.000	1.403E-07	11.2861	0.4459	-1.074E-08	-0.0947	4050000.	0.000		
414.000	8.278E-08	12.2688	-0.005742	-8.330E-09	437.6942	2.936E+10	-0.0559	4050000.	0.000
420.000	4.032E-08	11.2370	-0.2550	-5.928E-09	437.6927	2.936E+10	-0.0272	4050000.	0.000
426.000	1.164E-08	9.2228	-0.3602	-3.837E-09	437.6897	2.936E+10	-0.007857	4050000.	0.000
432.000	-5.728E-09	6.9235	-0.3722	-2.187E-09	437.6863	2.936E+10	0.003866	4050000.	0.000
438.000	-1.460E-08	4.7617	-0.3310	-9.929E-10	437.6831	2.936E+10	0.009588	4050000.	0.000
444.000	-1.764E-08	2.9536	-0.2657	-2.044E-10	437.6804	2.936E+10	0.0111	4050000.	0.000
450.000	-1.706E-08	1.5736	-0.1954	2.582E-10	437.6784	2.936E+10	0.0115	4050000.	0.000
456.000	-1.454E-08	0.6076	-0.1115	4.811E-10	437.6770	2.936E+10	0.009817	4050000.	0.000
462.000	-1.128E-08	-0.005029	-0.0792	5.427E-10	437.6761	2.936E+10	0.007617	4050000.	0.000
468.000	-8.031E-09	-0.3435	-0.0400	5.071E-10	437.6766	2.936E+10	0.005421	4050000.	0.000
474.000	-5.199E-09	-0.4867	-0.0132	4.223E-10	437.6768	2.936E+10	0.003509	4050000.	0.000
480.000	-2.964E-09	-0.5035	0.003282	3.211E-10	437.6768	2.936E+10	0.002001	4050000.	0.000
486.000	-1.346E-09	-0.4481	0.0120	2.238E-10	437.6768	2.936E+10	0.000909	4050000.	0.000
492.000	-2.777E-10	-0.3599	0.0153	1.413E-10	437.6766	2.936E+10	0.000187	4050000.	0.000
498.000	3.492E-10	-0.2648	0.0152	7.743E-11	437.6765	2.936E+10	-0.000236	4050000.	0.000
504.000	6.524E-10	-0.1782	0.0131	3.215E-11	437.6764	2.936E+10	-0.000440	4050000.	0.000
510.000	7.350E-10	-0.1074	0.0103	2.958E-12	437.6763	2.936E+10	-0.000496	4050000.	0.000
516.000	6.869E-10	-0.0544	0.007439	-1.358E-11	437.6762	2.936E+10	-0.000464	4050000.	0.000
522.000	5.721E-10	-0.0181	0.004890	-2.099E-11	437.6761	2.936E+10	-0.000386	4050000.	0.000
528.000	4.350E-10	0.004322	0.002851	-2.240E-11	437.6761	2.936E+10	-0.000294	4	

Pile Plus for windows, version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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gdc
 gdc
 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\updated_ET 9-14-14\Bent 4\
 Name of input data file: Bent 4L_long_ave P.lpd
 Name of output report file: Bent 4L_long_ave P.lpd
 Name of plot output file: Bent 4L_long_ave P.lpd
 Name of runtime message file: Bent 4L_long_ave P.lpd

Date and Time of Analysis

Date: September 13, 2014 Time: 21:14:28

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 4L_long_ave P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top width = 24.0000000 in
 Bottom width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 2 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer	Rock Mass	Layer	Effective	Undrained	In-situ	Angle of	Elastic	Uniaxial	RQD %
Factor	Soil Type	Rock Emass	Depth	unit wt.	Cohesion	In-situ	Friction	Mod.	qu	or
50	(p-y Curve Criteria)	ft	ft	pcf	psf	Test	Subgrade	psi	psi	GSI
Num.	psi		krm	Type	Property	Test	Mod. pci			Epsilon
1	Stiff Clay w/o Free water	--	-5.0000	120.0000	4500.0000	--	--	--	--	--
0.00700	--	--	0.100000	120.0000	4500.0000	--	--	--	--	--
2	Stiff Clay w/o Free water	--	0.100000	125.0000	4500.0000	--	--	--	--	--
0.00500	--	--	80.0000	125.0000	4500.0000	--	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.0000	0.4800	1.0000
2	50.0000	0.4800	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Bent 4L Long Ave P Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4	y = 0.25000 in	M = 0.0000 in-lbs	198000.	False
2	4	y = 0.50000 in	M = 0.0000 in-lbs	198000.	False
3	4	y = 1.00000 in	M = 0.0000 in-lbs	198000.	False

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
e = rotational stiffness apply to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations Nominal Moment Capacity and Non-linear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed values of Pile Loading and Deflection
For Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.250000 inches
Moment at pile head = 0.0000 in-lbs
Axial load at pile head = 198000.000 lbs

Depth inches	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil Res. lb/in	Soil Spr. lb ² /in	Distrib. Lat. Load lb/inch
0.00	0.2500	0.000	44036.	-0.003951	437.6761	2.936E+10	-693.0262	8316.3150	0.000
6.00	0.2263	256435.	39683.	-0.003925	815.5736	2.936E+10	-757.8267	20932.	0.000
0.00	0.2029	483529.	13130.	-0.003849	1151.1754	2.936E+10	-760.1060	22477.	0.000
18.00	0.1801	687136.	30570.	-0.003729	1450.2786	2.936E+10	-759.7991	25312.	0.000
24.00	0.1581	861226.	26020.	-0.003571	1706.8273	2.936E+10	-756.8076	28733.	0.000
30.00	0.1372	1007861.	21497.	-0.003380	1922.9178	2.936E+10	-751.0245	32711.	0.000
36.00	0.1176	1127215.	17016.	-0.003162	2098.8048	2.936E+10	-742.3314	37879.	0.000
42.00	0.0999	1207861.	12947.	-0.002922	2234.9065	2.936E+10	-730.5949	44143.	0.000
48.00	0.0825	1285331.	8258.9310	-0.002666	2331.8125	2.936E+10	-715.6584	52037.	0.000
54.00	0.0673	1325014.	4019.9411	-0.002399	2390.2918	2.936E+10	-697.3382	62161.	0.000
60.00	0.0537	1338271.	98.2842	-0.002127	2411.3020	2.936E+10	-675.4036	75425.	0.000
66.00	0.0418	1328888.	-4073.1579	-0.001854	2396.0016	2.936E+10	-649.5543	93274.	0.000
72.00	0.0315	1294799.	-879.9470	-0.001586	2345.7659	2.936E+10	-619.5754	118082.	0.000
78.00	0.0227	1238098.	-11491.	-0.001327	2262.2079	2.936E+10	-584.2477	154102.	0.000
84.00	0.0155	1160603.	-14873.	-0.001082	2147.2116	2.936E+10	-543.1563	209882.	0.000
90.00	0.009759	1062194.	-17985.	-0.000855	2002.9849	2.936E+10	-494.2062	303837.	0.000
96.00	0.005279	946274.	-20767.	-0.000650	1832.1596	2.936E+10	-433.0979	452258.	0.000
102.00	0.001959	814534.	-23103.	-0.000470	1638.0192	2.936E+10	-345.6150	1038548.	0.000
108.00	0.000362	6701531.	-23880.	-0.000318	1425.2158	2.936E+10	-186.7700	3095423.	0.000
114.00	0.0001861	532334.	-21958.	-0.000195	1222.1532	2.936E+10	353.7013	11402331.	0.000
120.00	0.0002708	407118.	-19708.	-9.945E-05	1037.6285	2.936E+10	396.4149	878462.	0.000
126.00	0.0003055	296075.	-17269.	-2.759E-05	871.9886	2.936E+10	416.5571	818209.	0.000
132.00	0.0003039	199955.	-14748.	2.310E-05	732.3417	2.936E+10	423.9406	837097.	0.000
138.00	0.002777	119890.	-12059.	5.570E-05	613.1141	2.936E+10	422.3885	812247.	0.000
144.00	0.001270	53135.	-9702.6148	0.342E-04	516.2449	2.936E+10	431.2210	1046029.	0.000
150.00	0.001898	2443.8275	-7269.4313	7.902E-05	441.2775	2.936E+10	397.8402	1257904.	0.000
156.00	0.001422	-34106.	-4946.0901	7.578E-05	487.9363	2.936E+10	376.6069	1589010.	0.000
162.00	0.000988	-57089.	-2767.1261	6.646E-05	521.8061	2.936E+10	349.7144	2123171.	0.000
168.00	0.000625	-67469.	-767.0529	5.373E-05	537.1026	2.936E+10	316.9766	3045282.	0.000
174.00	0.000344	-66422.	833.6205	4.003E-05	535.5457	2.936E+10	216.3812	3782922.	0.000
180.00	0.000144	-57561.	1760.1527	2.738E-05	522.5012	2.936E+10	92.2628	3845422.	0.000
186.00	-1.499E-05	-45365.	2066.2315	1.886E-05	504.5283	2.936E+10	9.7634	3907322.	0.000
192.00	5.534E-05	-32806.	1979.6963	8.870E-06	486.0212	2.936E+10	-38.6088	4039302.	0.000
198.00	9.145E-05	21630.	1679.4720	3.307E-06	469.5506	2.936E+10	-61.4663	4032922.	0.000
204.00	0.000220	12660.	1296.5743	-1.976E-07	456.3332	2.936E+10	-66.1663	4050000.	0.000
210.00	8.908E-05	6070.1773	917.6974	-2.112E-06	446.6215	2.936E+10	-60.1260	4050000.	0.000
216.00	7.688E-05	1643.0147	590.1369	-2.900E-06	440.0973	2.936E+10	-49.0609	4050000.	0.000
222.00	5.428E-05	1018.3557	437.1872	-2.964E-06	439.1768	2.936E+10	-36.6357	4050000.	0.000
228.00	3.712E-05	2360.5938	147.9796	-2.619E-06	441.1548	2.936E+10	-25.0335	4050000.	0.000
234.00	2.285E-05	2800.3324	26.5430	-2.091E-06	441.8028	2.936E+10	-15.4254	4050000.	0.000
240.00	1.402E-05	2684.0778	-44.0791	-1.531E-06	440.6102	2.936E+10	-8.1133	4050000.	0.000
246.00	4.485E-06	2275.0206	-77.5061	-1.024E-06	441.0287	2.936E+10	-3.0271	4050000.	0.000
252.00	-2.636E-07	1756.4367	-86.0535	-6.119E-07	440.2645	2.936E+10	0.1780	4050000.	0.000
258.00	-2.936E-08	1243.8326	-79.7356	-4.052E-07	439.5091	2.936E+10	1.9290	4050000.	0.000
264.00	-3.927E-08	800.3712	-65.9941	-9.634E-08	438.8556	2.936E+10	2.6505	4050000.	0.000
270.00	-4.274E-08	416.4322	-49.4466	-6.169E-08	438.2424	2.936E+10	2.7094	4050000.	0.000
276.00	-3.547E-08	201.3211	-34.6044	-9.844E-08	437.9728	2.936E+10	2.3940	4050000.	0.000
282.00	-2.833E-08	36.6460	-21.6862	-5.278E-07	437.7301	2.936E+10	1.9120	4050000.	0.000
288.00	-2.074E-08	59.2054	-11.7311	-1.703E-07	437.7483	2.936E+10	1.3987	4050000.	0.000
294.00	-1.387E-08	-104.6538	-4.7430	1.037E-07	437.8303	2.936E+10	0.9364	4050000.	0.000
300.00	-8.291E-07	-116.3682	-0.2550	8.112E-08	437.8476	2.936E+10	0.5967	4050000.	0.000
306.00	4.137E-07	-107.9069	2.2618	-8.820E-08	437.8316	2.936E+10	-0.3059	4050000.	0.000
312.00	-1.307E-07	-89.3654	3.3643	3.804E-08	437.8078	2.936E+10	0.0882	4050000.	0.000
318.00	-5.631E-08	-74.2862	2.5474	-1.164E-07	437.7366	2.936E+10	-0.2738	4050000.	0.000
324.00	1.323E-07	-46.9084	3.1861	1.029E-08	437.7452	2.936E+10	-0.0899	4050000.	0.000
330.00	1.662E-07	-29.4172	2.5797	2.491E-09	437.7194	2.936E+10	-0.1122	4050000.	0.000
336.00	1.631E-07	-19.2054	1.9127	-2.146E-09	437.6753	2.936E+10	-0.1517	4050000.	0.000
342.00	1.405E-07	-6.4593	1.2979	-4.437E-09	437.6856	2.936E+10	-0.0948	4050000.	0.000
348.00	1.099E-07	-0.3723	0.7910	-5.135E-09	437.6766	2.936E+10	-0.0742	4050000.	0.000
354.00	7.852E-08	0.0446	0.4088	-4.862E-09	437.6836	2.936E+10	-0.0532	4050000.	0.000
360.00	5.154E-08	4.5448	0.1448	-4.087E-09	437.6828	2.936E+10	-0.0348	4050000.	0.000
366.00	2.734E-08	4.4332	-0.0059	-3.509E-09	437.6824	2.936E+10	0.0201	4050000.	0.000
372.00	1.395E-08	4.3126	-0.1086	-2.202E-09	437.6824	2.936E+10	-0.009417	4050000.	0.000
378.00	3.382E-09	3.4937	-0.1437	-1.404E-09	437.6812	2.936E+10	-0.00283	4050000.	0.000
384.00	-2.901E-09	2.5918	-0.1447	-7.824E-10	437.6799	2.936E+10	0.001958	4050000.	0.000

390.00	-6.007E-09	1.7597	-0.1266	-3.377E-10	437.6787 <th>2.936E+10</th> <th>0.004054</th> <th>4050000.</th> <th>0.000</th>	2.936E+10	0.004054	4050000.	0.000
396.00	-6.954E-09	1.0732	-0.1004	-4.821E-11	437.6777	2.936E+10	0.004694	4050000.	0.000
402.00	-6.585E-09	0.5554	-0.0730	1.182E-10	437.6769	2.936E+10	0.004445	4050000.	0.000
408.00	-5.353E-09	0.1974	-0.0484	1.931E-10	437.6764	2.936E+10	0.003166	4050000.	0.000
414.00	-4.243E-09	-0.0260	-0.0286	2.127E-10	437.6761	2.936E+10	0.002864	4050000.	0.000
420.00	-2.983E-09	-0.1464	-0.0140	1.951E-10	437.6763	2.936E+10	0.002034	4050000.	0.000
426.00	-1.803E-09	-0.1842	-0.004079	1.603E-10	437.6764	2.936E+10	0.001284	4050000.	0.000
432.00	-1.060E-09	-0.1957	0.001921	1.204E-10	437.6764	2.936E+10	0.000716	4050000.	0.000
438.00	-4.579E-10	-0.1714	0.004995	8.289E-11	437.6763	2.936E+10	0.000309	4050000.	0.000
444.00	-6.362E-11	-0.1359	0.006055	5.148E-11	437.6763	2.936E+10	4.430E-05	4050000.	0.000
450.00	1.599E-10	-0.0989	0.005864	2.749E-11	437.6762	2.936E+10	-0.000108	4050000.	0.000
456.00	2.642E-10	-0.0656	0.005006	1.067E-11	437.6762	2.936E+10	-0.000178	4050000.	0.000
462.00	2.880E-10	-0.0388	0.003887	0.0000	437.6762	2.936E+10	-0.000194	4050000.	0.000
468.00	2.642E-10	-0.0190	0.002769	-5.911E-12	437.6761	2.936E+10	-0.000178	4050000.	0.000
474.00	2.171E-10	-0.003579	0.001795	-8.422E-12	437.6761	2.936E+10	-0.000147	4050000.	0.000
480.00	1.631E-10	0.002562	0.001025	-8.730E-12	437.6761	2.936E+10	-0.000110	4050000.	0.000
486.00	1.123E-10	0.006739	0.000467	-7.780E-12	437.6761	2.936E+10	-7.581E-05	4050000.	0.000
492.00	6.976E-11	0.008185	9.837E-05	-6.254E-12	437.6761	2.936E+10	-4.709E-05	4050000.	0.000
498.00	3.725E-11	0.007934	-0.000118	-4.607E-12	437.6761	2.936E+10	-2.515E-05	4050000.	0.000
504.00	1.448E-11	0.006776	-0.000223	-3.104E-12	437.6761	2.936E+10	-9.771E-06	4050000.	0.000
510.00	0.000	0.005265	-0.000252	-1.873E-12	437.6761	2.936E+10	-5.549E-09	4050000.	0.000
516.00	-8.003E-12	0.003752	-0.000236	0.000	437.6761	2.936E+10	5.402E-06	4050000.	0.000
522.00	-1.141E-11	0.002452	-0.000197</						

Table with columns for Load Case No. 2, Pile-head deflection, Computed slope at pile head, Maximum bending moment, Depth of maximum bending moment, Depth of maximum shear force, Number of iterations, and Number of zero deflection points. Includes a section for 'Computed values of Pile Loading and Deflection For Lateral Loading For Load Case Number 3'.

* The above values of total stress are combined axial and bending stress.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Table with columns: Pile-head deflection, Computed slope at pile head, Maximum bending moment, Depth of maximum bending moment, Depth of maximum shear force, Number of iterations, Number of zero deflection points.

Computed values of Pile Loading and Deflection For Lateral Loading For Load Case Number 3

Table with columns: Pile-head conditions are Displacement and Moment (Loading Type 4), Displacement of pile head, Moment at pile head, Axial load at pile head, Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Soil Res., Soil Spr., Distrib. Lat. Load.

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Table with columns for Load Case No. 3, Pile-head deflection, Computed slope at pile head, Maximum bending moment, Depth of maximum bending moment, Depth of maximum shear force, Number of iterations, and Number of zero deflection points. Includes a section for 'Computed values of Pile Loading and Deflection For Lateral Loading For Load Case Number 3'.

* The above values of total stress are combined axial and bending stress.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

Table with columns: Pile-head deflection, Computed slope at pile head, Maximum bending moment, Depth of maximum bending moment, Depth of maximum shear force, Number of iterations, Number of zero deflection points.

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = shear, lbs, and Load 2 = Moment, in-lbs
Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radian

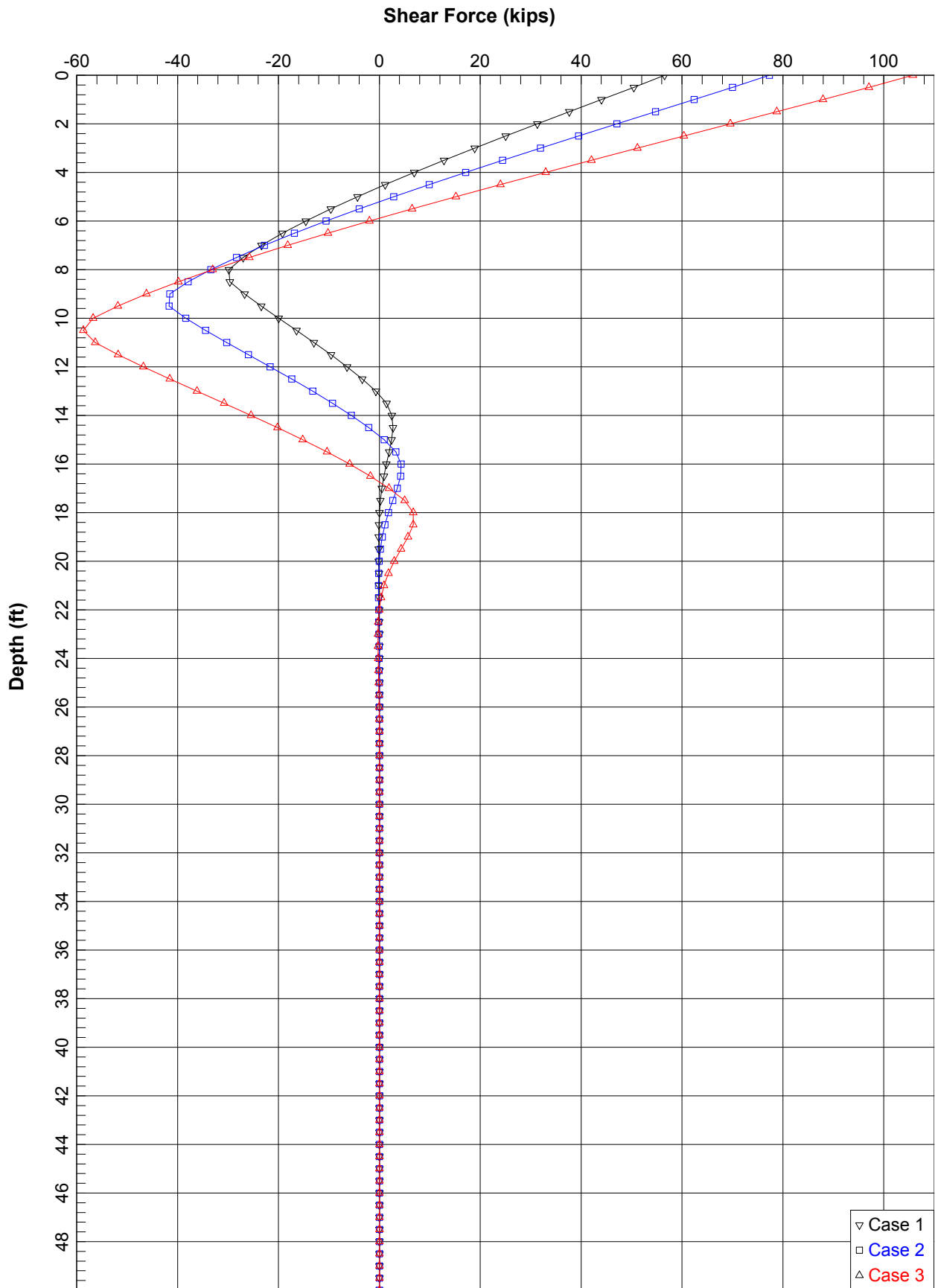
Page 6

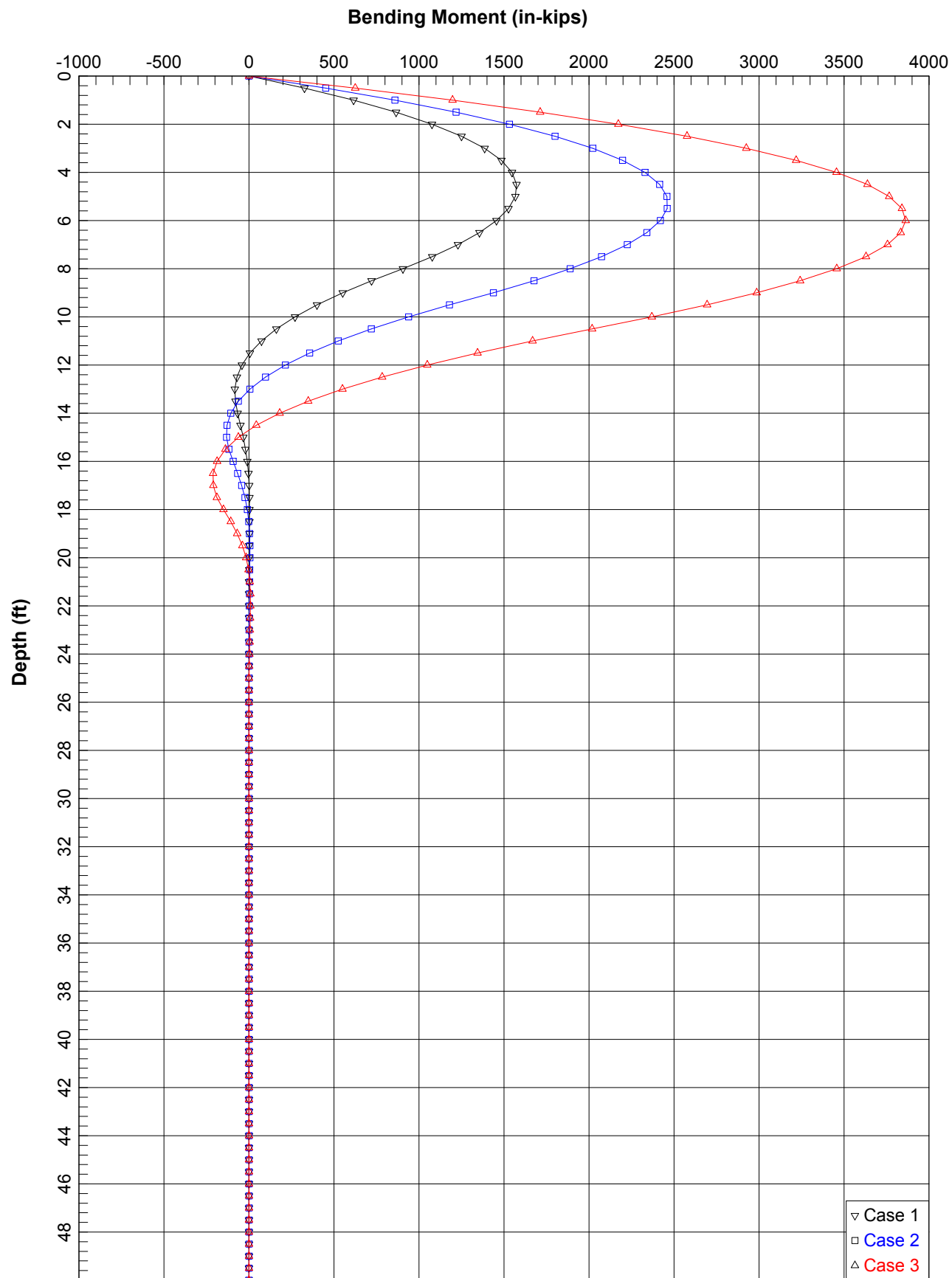
Bent 4L_Long_ave P

Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.		Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y =	0.2500	M = 0.000	198000.	0.25000000	1339271.	44036.	-0.00395130
2	4	y =	0.5000	M = 0.000	198000.	0.50000000	2098018.	60267.	-0.00699538
3	4	y =	1.0000	M = 0.000	198000.	1.00000000	3294324.	82436.	-0.01237389

The analysis ended normally.





Pile Plus for windows, version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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This copy of LPILE is licensed to:

gdc
 gdc
 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\updated_ET 9-14-14\Bent 4\
 Name of input data file: Bent 4L_Long_Max P.lpd
 Name of output report file: Bent 4L_Long_Max P.lpd
 Name of plot output file: Bent 4L_Long_Max P.lpd
 Name of runtime message file: Bent 4L_Long_Max P.lpd

Date and Time of Analysis

Date: September 13, 2014 Time: 21:17:04

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 4L_Long_Max P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top width = 24.0000000 in
 Bottom width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 2 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer	Rock Mass	Layer	Effective	Undrained	Angle of	Elastic	Uniaxial	RQD %
Factor	Soil Type	Rock Emass	Depth	unit wt.	In-situ Cohesion	Friction	Mod.	qu	or
50	(p-y Curve Criteria)	ft	ft	pcf	psf	deg.	psi	psi	GSI
Num.	psi		Type	Test	Property	psi			Epsilon
1	Stiff Clay w/o Free water	--	-5.0000	120.000	4500.000	--	--	--	--
0.00700	--	--	0.10000	120.000	4500.000	--	--	--	--
2	Stiff Clay w/o Free water	--	0.10000	125.000	4500.000	--	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.6750	1.0000
2	50.000	0.6750	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No.	Load Type	Condition 1	Bent 4L Long_Max P		Compute Top y vs. Pile Length
			Condition 2	Axial Thrust Force, lbs	
1	4	y = 0.25000 in	M = 0.0000 in-lbs	198000.	False
2	4	y = 0.50000 in	M = 0.0000 in-lbs	198000.	False
3	4	y = 1.00000 in	M = 0.0000 in-lbs	198000.	False

v = perpendicular shear force applied to pile head

M = bending moment applied to pile head

y = lateral deflection relative to pile axis

S = pile slope relative to original pile batter angle

r = rotational stiffness applied to pile head

Axial thrust is assumed to be acting axially for all pile batter angles.

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.250000 inches
 Moment at pile head = 0.000 in-lbs
 Axial load at pile head = 198000.000 lbs

Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil Res.	Soil Spr.	Distrib.
inches	inches	in-lbs	lbs	radians	Stress	Stiffness	p	lb/inch	Lat. Load
					psi ²	lb-in ²	lb/in	lb/inch	lb/inch
0.00	0.2500	0.000	56543.	-0.004289	437.6761	2.936E+10	-974.5682	11695.	0.000
6.000	0.2243	326810.	50429.	-0.004256	919.2818	2.936E+10	-1063.2998	28448.	0.000
0.1989	0.1849	1604159	1344.3608	-0.004159	1344.3608	3.2081	0.000	61363.6338	32081.
18.000	0.1744	865273.	37678.	-0.004008	1712.7920	2.936E+10	-1059.8383	36473.	0.000
24.000	0.1508	1076920.	31343.	-0.003810	2024.6874	2.936E+10	-1051.7421	4137.	0.000
30.000	0.1286	1230444.	12823.	-0.003572	2280.4008	2.936E+10	-1039.1626	48470.	0.000
36.000	0.1080	1386253.	18887.	-0.003302	2480.5375	2.936E+10	-1021.8894	56787.	0.000
42.000	0.0890	1542244.	26423.	-0.003009	2625.9652	2.936E+10	-999.6759	67389.	0.000
48.000	0.0719	1547274.	6906.9378	-0.002699	2717.8271	2.936E+10	-972.2335	81173.	0.000
54.000	0.0566	1574234.	1172.8021	-0.002380	2757.5573	2.936E+10	-939.3551	99527.	0.000
60.000	0.0433	1567003.	4344.3690	-0.002059	2746.9005	2.936E+10	-899.9686	124702.	0.000
66.000	0.0319	1526992.	-9606.3230	-0.001743	2687.9381	2.936E+10	-853.9494	160576.	0.000
72.000	0.0224	1455868.	-14568.	-0.001438	2584.1259	2.936E+10	-799.9905	214406.	0.000
78.000	0.0147	1353931.	-19177.	-0.001131	2495.3128	2.936E+10	-736.1739	301473.	0.000
84.000	0.008578	1228482.	-23361.	-0.000887	2248.0377	2.936E+10	-658.6064	406645.	0.000
90.000	0.004012	1077366.	-27008.	-0.000651	2025.3437	2.936E+10	-557.0119	533042.	0.000
96.000	0.000767	905935.	-29814.	-0.000448	1772.7137	2.936E+10	-378.3325	7061484.	0.000
102.000	-0.001368	720665.	-29624.	-0.000282	1499.6885	2.936E+10	441.6441	1937195.	0.000
108.000	-0.002618	531118.	-26705.	-0.000152	1249.8353	2.936E+10	531.2105	1217210.	0.000
114.000	-0.003193	400562.	-23402.	-5.486E-05	1027.9665	2.936E+10	569.7579	1070555.	0.000
120.000	-0.003277	270419.	-19938.	1.371E-05	836.1810	2.936E+10	584.8964	1070986.	0.000
126.000	-0.003029	161267.	-16430.	5.783E-05	675.3284	2.936E+10	584.6605	118253.	0.000
132.000	-0.002583	73124.	-12958.	8.178E-05	545.4354	2.936E+10	574.3353	1330036.	0.000
138.000	-0.002047	5573.8704	-9589.7727	8.983E-05	488.8901	2.936E+10	550.2875	1612762.	0.000
144.000	-0.001505	42167.	-6382.4258	8.609E-05	499.8158	2.936E+10	518.8282	2068001.	0.000
150.000	-0.001014	-71220.	-3390.4855	7.450E-05	542.6296	2.936E+10	478.4853	2830729.	0.000
156.000	-0.000611	-83030.	-668.3621	5.874E-05	560.0336	2.936E+10	428.8892	4212616.	0.000
162.000	-0.000309	-79380.	-1433.9612	4.214E-05	554.6545	2.936E+10	265.2185	5142993.	0.000
168.000	-0.000105	-66162.	2484.7967	2.727E-05	535.1768	2.936E+10	91.7267	5231844.	0.000
174.000	1.783E-05	-49627.	2712.5331	1.543E-05	510.8091	2.936E+10	-15.8078	5139746.	0.000
180.000	7.999E-05	-33648.	2448.8431	6.922E-06	487.2623	2.936E+10	-27.0955	5407625.	0.000
186.000	0.000101	-20257.	1955.3285	1.413E-06	467.5283	2.936E+10	-92.4094	5495515.	0.000
192.000	8.693E-05	-10188.	1407.4464	-1.698E-06	446.6895	2.936E+10	-90.7189	5495115.	0.000
198.000	8.051E-05	-3363.8471	908.4871	3.083E-06	442.6332	2.936E+10	-76.1018	5671297.	0.000
204.000	5.995E-05	721.3149	-99.4634	-3.353E-06	438.7391	2.936E+10	-56.9061	5695312.	0.000
210.000	4.027E-05	2757.6816	224.0616	-2.998E-06	441.7400	2.936E+10	-38.2278	5695312.	0.000
216.000	2.398E-05	3417.1762	41.0989	-2.367E-06	442.7118	2.936E+10	-22.7597	5695312.	0.000
222.000	1.187E-05	3256.4913	-60.9885	-1.685E-06	442.4750	2.936E+10	-11.7694	5695312.	0.000
228.000	3.761E-06	2689.3170	-105.5064	-1.077E-06	441.6392	2.936E+10	-3.5699	5695312.	0.000
234.000	-1.053E-06	1992.9738	-113.2188	-5.986E-07	440.6131	2.936E+10	0.9991	5695312.	0.000
240.000	-3.427E-07	132.6132	-100.4772	-9.388E-07	439.6304	2.936E+10	3.2481	5695312.	0.000
246.000	-4.158E-08	787.8623	-78.8935	-4.210E-08	438.8371	2.936E+10	3.9464	5695312.	0.000
252.000	-3.327E-08	385.4937	-55.8732	-7.781E-08	438.2442	2.936E+10	3.7277	5695312.	0.000
258.000	-3.240E-08	52.2351	35.3045	-1.924E-07	437.8498	2.936E+10	3.9020	5695312.	0.000
264.000	-2.377E-08	-40.9081	19.5588	1.370E-07	437.6934	2.936E+10	2.2562	5695312.	0.000
270.000	-1.890E-08	-117.9976	1.700E-07	1.700E-07	437.8497	2.936E+10	1.1498	5695312.	0.000
276.000	-9.272E-07	-140.6854	-1.1497	9.435E-08	437.8834	2.936E+10	0.8806	5695312.	0.000
282.000	-4.479E-07	-131.8277	2.7675	6.650E-08	437.8704	2.936E+10	0.4251	5695312.	0.000
288.000	-1.297E-07	-107.6132	4.4123	4.703E-08	437.8347	2.936E+10	0.1210	5695312.	0.000
294.000	5.643E-08	-78.9795	4.6211	2.296E-08	437.7925	2.936E+10	-0.0536	5695312.	0.000
300.000	2.421E-08	52.2351	4.0464	9.546E-09	437.7353	2.936E+10	-0.1384	5695312.	0.000
306.000	1.710E-07	-30.1450	-1.435	1.095E-09	437.6892	2.936E+10	0.00578	5695312.	0.000
312.000	1.589E-07	-14.5161	2.2042	-3.501E-09	437.6975	2.936E+10	-0.1508	5695312.	0.000
318.000	3.580E-08	1.1304	1.3845	-6.820E-08	437.6820	2.936E+10	0.1224	5695312.	0.000
324.000	9.415E-08	2.1111	0.7492	-5.587E-09	437.6792	2.936E+10	-0.0894	5695312.	0.000
330.000	6.192E-08	5.0040	0.3048	-4.860E-09	437.6835	2.936E+10	-0.0588	5695312.	0.000
336.000	1.938E-08	1.0216	0.0264	-7.576E-08	437.6847	2.936E+10	0.0440	5695312.	0.000
342.000	1.683E-08	5.3299	-0.1236	-2.622E-09	437.6839	2.936E+10	-0.0160	5695312.	0.000
348.000	4.366E-09	4.2035	-0.1839	-1.638E-09	437.6824	2.936E+10	-0.004144	5695312.	0.000
354.000	-6.174E-09	-10.1259	-0.1883	-8.783E-07	437.6807	2.936E+10	0.00278	5695312.	0.000
360.000	-6.174E-09	2.0459	-0.1627	-3.497E-10	437.6791	2.936E+10	0.005860	5695312.	0.000
366.000	-1.020E-07	1.5654	1.3413	-6.820E-07	437.6784	2.936E+10	0.006661	5695312.	0.000
372.000	-6.419E-09	0.5444	-0.0869	1.553E-10	437.6769	2.936E+10	0.006093	5695312.	0.000
378.000	-5.154E-09	0.1326	-0.0539	2.245E-10	437.6763	2.936E+10	0.004892	5695312.	0.000
384.000	-3.725E-09	-0.1031	-0.0286	2.275E-10	437.6762	2.936E+10	0.005356	5695312.	0.000

390.000	-2.424E-09	-0.2215	-0.0111	1.953E-10	Bent 4L Long_Max P			
					Axial Thrust	Force, lbs	0.002301	5695312.
396.000	-1.381E-09	-0.2370	-0.000282	1.495E+10	437.6764	2.936E+10	0.001131	5695312.
402.000	-6.297E-10	-0.2152	0.005445	1.035E+10	437.6764	2.936E+10	0.000598	5695312.
408.000	1.419E-10	-0.1719	0.007642	6.375E+11	437.6762	2.936E+10	-0.000247	5695312.
414.000	1.370E-10	-0.1237	0.007662	3.352E+11	437.6763	2.936E+10	-0.000128	5695312.
420.000	2.603E-10	-0.0800	0.006536	1.270E+11	437.6762	2.936E+10	-0.000247	5695312.
426.000	2.874E-10	-0.0453	0.004976	0.000	437.6762	2.936E+10	-0.000273	5695312.
432.000	2.591E-10	-0.0203	0.003420	-6.808E+12	437.6761	2.936E+10	-0.000246	5695312.
438.000	2.058E-10	-0.04236	0.002096	-9.315E+12	437.6761	2.936E+10	-0.000273	5695312.
444.000	1.473E-10	0.004858	0.001091	-9.250E+12	437.6761	2.936E+10	-0.000140	5695312.
450.000	9.476E-11	0.008899	0.000402	7.844E+12	437.6761	2.936E+10	-8.995E-05	5695312.
456.000	5.215E-11	0.005700	1.933E-05	-5.945E+12	437.6761	2.936E+10	-5.045E-05	5695312.
462.000	2.344E-11	0.008681	-0.000237	-4.064E+12	437.6761	2.936E+10	-2.225E-05	5695312.
468.000	4.379E-12	0.006860	-0.000317	-2.476E+12	437.6761	2.936E+10	-4.157E-06	5695312.
474.000	-6.272E-12	0.004987	-0.000311	-1.276E+12	437.6761	2.936E+10	5.935E-06	5695312.
480.000	-1.093E-11	0.003127	-0.000262	0.000	437.6761	2.936E+10	1.038E-05	5695312.
486.000	-1.175E-11	0.001740	-0.000198	0.000	437.6761	2.936E+10	1.116E-05	5695312.
492.000	-1.044E-11	0.000755	-0.000155	0.000	437.6761	2.936E+10	9.913E-06	5695312.
498.000	-8.207E-12	0.000126	-8.139E-05	0.000	437.6761	2.936E+10	7.790E-06	5695312.
504.000	-8.171E-12	-0.000223	-4.146E-05	0.000	437.6761	2.936E+10	5.571E-06	5695312.
510.000	-3.700E-12	-0.000373	-1.436E-05	0.000	437.6761	2.936E+10	3.512E-06	5695312.
516.000	-2.041E-12	-0.000396	1					

252.000	1.681E+06	3710.5888	-177.5787	-1.304E-06	441.1442	2.936E+10	-1.5956	5695312.	0.000
258.000	3.866E+06	2617.4933	-171.3566	-6.570E-07	441.5334	2.936E+10	3.6697	5695312.	0.000
264.000	-6.203E+06	1655.8701	-142.6836	-2.203E-07	440.1163	2.936E+10	5.8880	5695312.	0.000
270.000	6.387E+06	219.3799	-106.4848	-4.131E-07	437.6971	2.936E+10	2.0167	5695312.	0.000
276.000	-5.705E+06	377.9756	-71.7008	1.727E-07	438.3321	2.936E+10	5.4152	5695312.	0.000
282.000	-4.437E+06	-144.9940	-42.8202	2.159E-07	437.7424	2.936E+10	4.2116	5695312.	0.000
288.000	3.114E+06	-136.3799	-21.3184	2.066E-07	437.9793	2.936E+10	2.9526	5695312.	0.000
294.000	-1.938E+06	-211.3173	-6.8761	1.711E-07	437.9875	2.936E+10	1.8584	5695312.	0.000
300.000	1.1061E+06	-219.3000	7.1207	1.271E-07	437.9391	2.936E+10	1.0072	5695312.	0.000
306.000	-4.332E+07	-190.9707	5.9760	8.512E-08	437.9575	2.936E+10	0.4112	5695312.	0.000
312.000	-3.960E+08	-147.7905	7.3225	5.050E-08	437.8939	2.936E+10	0.0376	5695312.	0.000
318.000	1.728E+07	-103.2213	6.9431	2.485E-08	437.8282	2.936E+10	-0.1640	5695312.	0.000
324.000	2.586E+07	-64.5320	5.7146	7.708E-09	437.7712	2.936E+10	-0.2455	5695312.	0.000
330.000	2.635E+07	-34.6646	4.2227	-2.430E-09	437.7272	2.936E+10	-0.2518	5695312.	0.000
336.000	2.295E+07	-15.8543	2.8138	-7.388E-09	437.6965	2.936E+10	-0.2178	5695312.	0.000
342.000	1.766E+07	-0.8816	1.6574	-8.894E-09	437.6774	2.936E+10	-0.1677	5695312.	0.000
348.000	1.227E+07	6.0533	0.8049	-8.366E-09	437.6850	2.936E+10	-0.1165	5695312.	0.000
354.000	7.625E+06	8.7970	0.2384	-6.848E-09	437.6891	2.936E+10	0.0724	5695312.	0.000
360.000	4.055E+08	8.9310	-0.0943	-5.036E-09	437.6893	2.936E+10	-0.0385	5695312.	0.000
366.000	1.581E+08	7.6771	-0.2548	-3.339E-09	437.6874	2.936E+10	0.0150	5695312.	0.000
372.000	4.900E+10	5.8808	-0.3013	-1.953E-09	437.6848	2.936E+10	-0.000465	5695312.	0.000
378.000	-7.623E+09	4.0664	-0.2810	-9.366E-10	437.6821	2.936E+10	0.007236	5695312.	0.000
384.000	1.057E+08	2.1515	-0.2286	-2.644E-10	437.6798	2.936E+10	0.0102	5695312.	0.000
390.000	1.0780	1.3233	-0.1673	1.275E-10	437.6780	2.936E+10	0.0102	5695312.	0.000
396.000	-9.219E+09	0.5037	-0.1103	3.142E-10	437.6768	2.936E+10	0.00571	5695312.	0.000
402.000	-7.025E+09	-0.001045	-0.0640	3.656E-10	437.6761	2.936E+10	0.00668	5695312.	0.000
408.000	-4.832E+09	-0.2657	-0.0303	3.383E-10	437.6765	2.936E+10	0.00487	5695312.	0.000
414.000	2.365E+09	-0.3851	-0.00870	-2.739E-10	437.6766	2.936E+10	0.002815	5695312.	0.000
420.000	-1.546E+09	-0.3632	0.00477	1.994E-10	437.6766	2.936E+10	0.001467	5695312.	0.000
426.000	-5.721E+10	-0.3083	0.0108	1.308E-10	437.6765	2.936E+10	0.000543	5695312.	0.000
432.000	2.464E+10	-0.2727	-0.0043	7.344E-10	437.6761	2.936E+10	-0.244E-05	5695312.	0.000
438.000	3.327E+10	-0.1600	0.0114	3.516E-11	437.6763	2.936E+10	-0.000316	5695312.	0.000
444.000	4.455E+10	-0.0976	0.009139	8.830E-12	437.6762	2.936E+10	-0.000423	5695312.	0.000
450.000	6.387E+10	-0.0504	0.006621	6.233E-08	437.6762	2.936E+10	-0.000416	5695312.	0.000
456.000	3.700E+10	-0.0181	0.004319	-1.329E-11	437.6761	2.936E+10	-0.000351	5695312.	0.000
462.000	2.791E+10	0.001476	0.002470	-1.500E-11	437.6761	2.936E+10	-0.000265	5695312.	0.000
468.000	1.901E+10	0.0115	0.001134	-1.367E-11	437.6761	2.936E+10	-0.000180	5695312.	0.000
474.000	1.151E+10	0.0151	0.000265	-1.094E-11	437.6761	2.936E+10	-0.000109	5695312.	0.000
480.000	5.877E+11	0.0147	-0.000231	-7.889E-12	437.6761	2.936E+10	-5.578E-05	5695312.	0.000
486.000	2.047E+11	0.0124	-0.000456	-5.118E-12	437.6761	2.936E+10	-9.143E-05	5695312.	0.000
492.000	-2.654E+12	0.009285	-0.000507	-2.906E-12	437.6761	2.936E+10	-2.519E-06	5695312.	0.000
498.000	-1.39E+11	0.006291	-0.004861	-1.311E-06	437.6761	2.936E+10	1.366E-05	5695312.	0.000
504.000	-1.842E+11	0.003788	-0.000365	0.000	437.6761	2.936E+10	1.748E-05	5695312.	0.000
510.000	-1.782E+11	0.001913	-0.000162	0.000	437.6761	2.936E+10	-1.690E-05	5695312.	0.000
516.000	-1.484E+11	0.000645	-0.000169	0.000	437.6761	2.936E+10	-4.684E-05	5695312.	0.000
522.000	-1.108E+11	-0.000115	-9.505E-05	0.000	437.6761	2.936E+10	1.052E-05	5695312.	0.000
528.000	7.466E+12	-0.000497	-4.223E-06	0.000	437.6761	2.936E+10	6.487E-06	5695312.	0.000
534.000	-4.461E+12	-0.000623	-8.268E-06	0.000	437.6761	2.936E+10	4.234E-06	5695312.	0.000
540.000	-2.220E+12	-0.000597	-1.076E-05	0.000	437.6761	2.936E+10	2.107E-06	5695312.	0.000
546.000	0.000	-0.000495	-1.910E-05	0.000	437.6761	2.936E+10	6.745E-07	5695312.	0.000
552.000	0.000	-0.000368	-2.058E-05	0.000	437.6761	2.936E+10	-1.820E-07	5695312.	0.000
558.000	0.000	-0.000248	-1.820E-05	0.000	437.6761	2.936E+10	-6.097E-07	5695312.	0.000
564.000	0.000	-0.000150	-1.818E-05	0.000	437.6761	2.936E+10	-7.485E-07	5695312.	0.000
570.000	0.000	-7.867E-05	9.745E-06	0.000	437.6761	2.936E+10	-7.127E-07	5695312.	0.000
576.000	0.000	-3.100E-05	6.063E-06	0.000	437.6761	2.936E+10	-5.854E-07	5695312.	0.000
582.000	0.000	-8.399E-06	2.835E-06	0.000	437.6761	2.936E+10	-4.196E-07	5695312.	0.000
588.000	0.000	1.097E-06	8.443E-07	0.000	437.6761	2.936E+10	-2.441E-07	5695312.	0.000
594.000	0.000	1.870E-06	-9.744E-07	0.000	437.6761	2.936E+10	-4.984E-07	5695312.	0.000
600.000	0.000	0.000	0.000	0.000	437.6761	2.936E+10	1.023E-07	2847656.	0.000

* The above values of total stress are combined axial and bending stress.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Pile-head deflection	=	0.5000000 inches
Computed slope at pile head	=	-0.0075788 radians
Maximum bending moment	=	2439705. inch-lbs
Maximum shear force	=	77923 lbs
Depth of maximum bending moment	=	66.000000 inches below pile head
Depth of maximum shear force	=	0.000000 inches below pile head
Number of iterations	=	20
Number of zero deflection points	=	9

Computed values of Pile Loading and Deflection
For Lateral Loading For Load Case Number 3

Pile-head conditions are Displacement and Moment (Loading Type 4)	=	
Displacement of pile head	=	1.000000 inches
Moment at pile head	=	0.000 in-lbs
Axial load at pile head	=	198000.000 lbs

Depth inches	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil Res. lb/in	Soil Spr. lb/inch	Distrib. Lat. Load lb/inch
0.00	1.0000	0.000	0.000	105745.	-0.0134	437.6761	2.936E+10	-1378.2475	4374.7425
6.000	0.9196	625592.	97071.	-0.0133	1359.5838	2.936E+10	-1513.0681	9827.6151	0.000
6.839	1196692.	19160.	-106.4848	-0.0132	2200.9070	2.936E+10	-1574.6442	29159.8892	0.000
18.000	0.7617	1712533.	78788.	-0.0129	2961.0971	2.936E+10	-1532.2154	12070.	0.000
6.6856	2172569.	69394.	-0.0125	3639.2799	2.936E+10	-1535.6381	13440.	0.000	
61.21	2576974.	60324.	-0.0120	4295.2531	2.936E+10	-1534.7611	15040.	0.000	
36.000	0.5418	292504.	51180.	-0.0114	4748.8647	2.936E+10	-1529.4231	16936.	0.000
42.000	0.4751	3218263.	42034.	-0.0108	5180.2910	2.936E+10	-1529.4498	18881.	0.000
48.000	0.4124	3455540.	32961.	-0.0101	5529.9564	2.936E+10	-1504.6501	21893.	0.000
54.000	0.3539	3637811.	23993.	-0.009381	5798.5611	2.936E+10	-1484.8101	25176.	0.000
60.000	0.2993	3765745.	15160.	-0.008624	5987.0925	2.936E+10	-1468.6856	28259.6858	0.000
66.000	0.2504	3840217.	6493.5642	-0.007847	6096.8377	2.936E+10	-1428.9906	32425.	0.000
72.000	0.2056	3862312.	-1970.5407	-0.007060	6129.3985	2.936E+10	-1392.3777	40625.	0.000
78.000	0.1657	3833444.	-10196.	-0.006273	6086.7093	2.936E+10	-1349.4102	48376.	0.000
84.000	0.1304	3754866.	-18143.	-0.005498	5971.0599	2.936E+10	-1299.5133	59809.	0.000
90.000	0.0997	3638844.	-25767.	-0.004757	5785.1219	2.936E+10	-1241.8937	74872.	0.000
96.000	0.0735	3456933.	-33019.	-0.004019	5532.0089	2.936E+10	-1175.3335	96011.	0.000
102.000	0.0515	3242020.	-39838.	-0.003334	5215.3018	2.936E+10	-1097.9158	128021.	0.000
108.000	0.0334	2986796.	-46150.	-0.002698	4839.1883	2.936E+10	-1006.0891	180527.	0.000

114.000	0.0191	2694627.	-51845.	-0.002117	4408.6314	2.936E+10	-892.1506	280501.	0.000
120.000	0.008033	2369686.	-56720.	-0.001600	3929.7802	2.936E+10	-732.9411	547464.	0.000
126.000	-0.000112	2017784.	-58861.	-0.001151	3411.1973	2.936E+10	-86.0169	4616610.	0.000
132.000	0.000132	1668458.	-59862.	-0.000774	2896.4538	2.936E+10	707.1953	3047973.	0.000
138.000	-0.009406	1344016.	-61779.	-0.000467	2418.2950	2.936E+10	806.3267	514362.	0.000
144.000	-0.0114	1048246.	-64777.	-0.000272	1982.4303	2.936E+10	861.2092	454008.	0.000
150.000	-0.0121	783224.	-68324.	-0.000193	1591.8794	2.936E+10	889.6931	442208.	0.000
156.000	-0.0118	550041.	-76154.	0.000101	1248.2473	2.936E+10	900.2742	457717.	0.000
162.000	-0.0109	349134.	-80762.	0.000193	952.1797	2.936E+10	896.9473	472308.	0.000
168.000	-0.009483	180433.	-84354.	0.000247	703.5718	2.936E+10	881.3628	557944.	0.000
174.000	-0.007889	44344.	-86254.	0.000270	501.6836	2.936E+10	856.2419	651212.	

Bent 4L_Long_Max P

Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

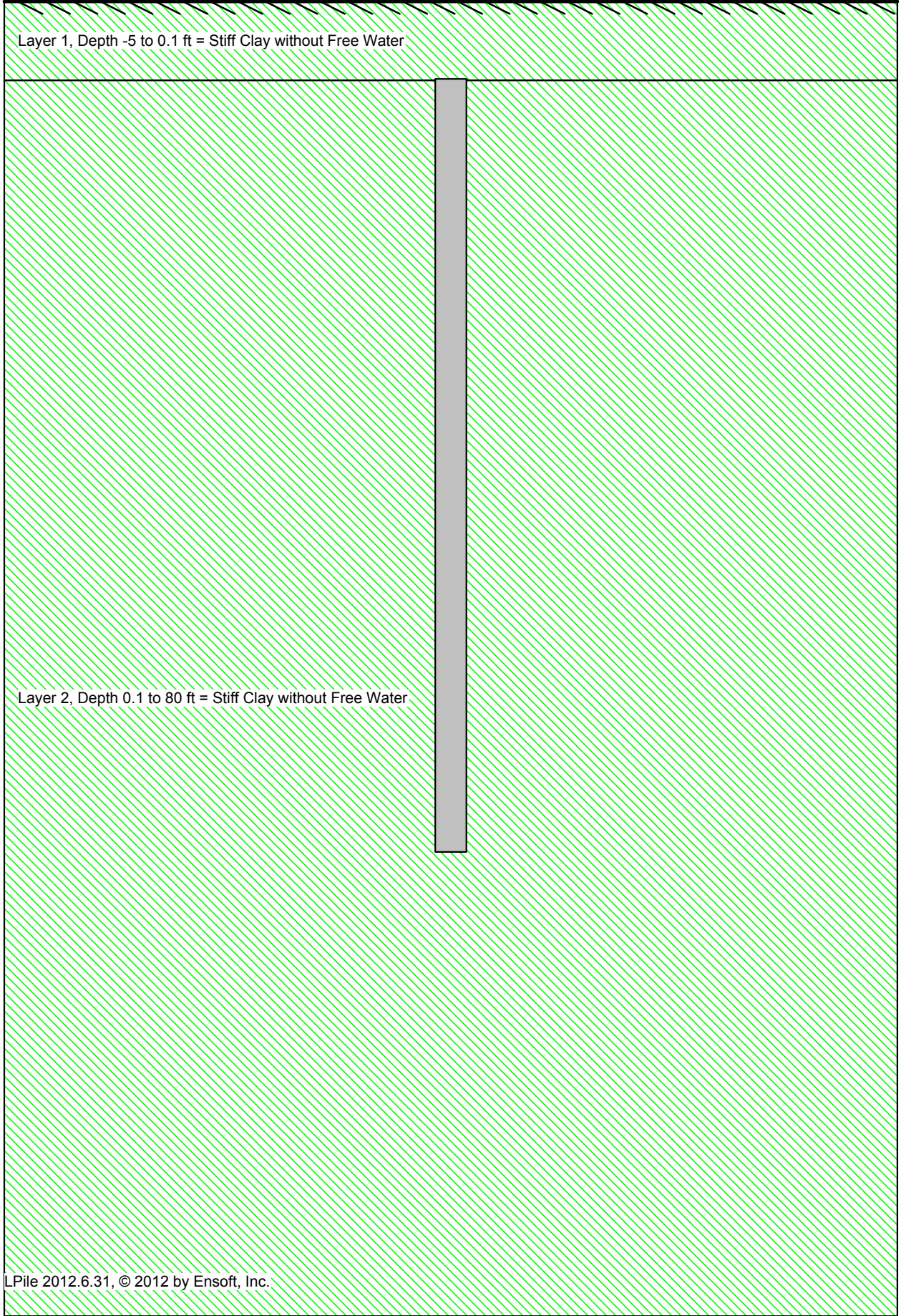
Load Case No.	Load Type No.		Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y =	0.2500	M = 0.000	198000.	0.25000000	1574234.	56543.	-0.00428916
2	4	y =	0.5000	M = 0.000	198000.	0.50000000	2459705.	77303.	-0.00757685
3	4	y =	1.0000	M = 0.000	198000.	1.00000000	3862312.	105745.	-0.01340756

The analysis ended normally.

SUPPORT: BENT 4L

LOAD DIRECTION: TRANSVERSE

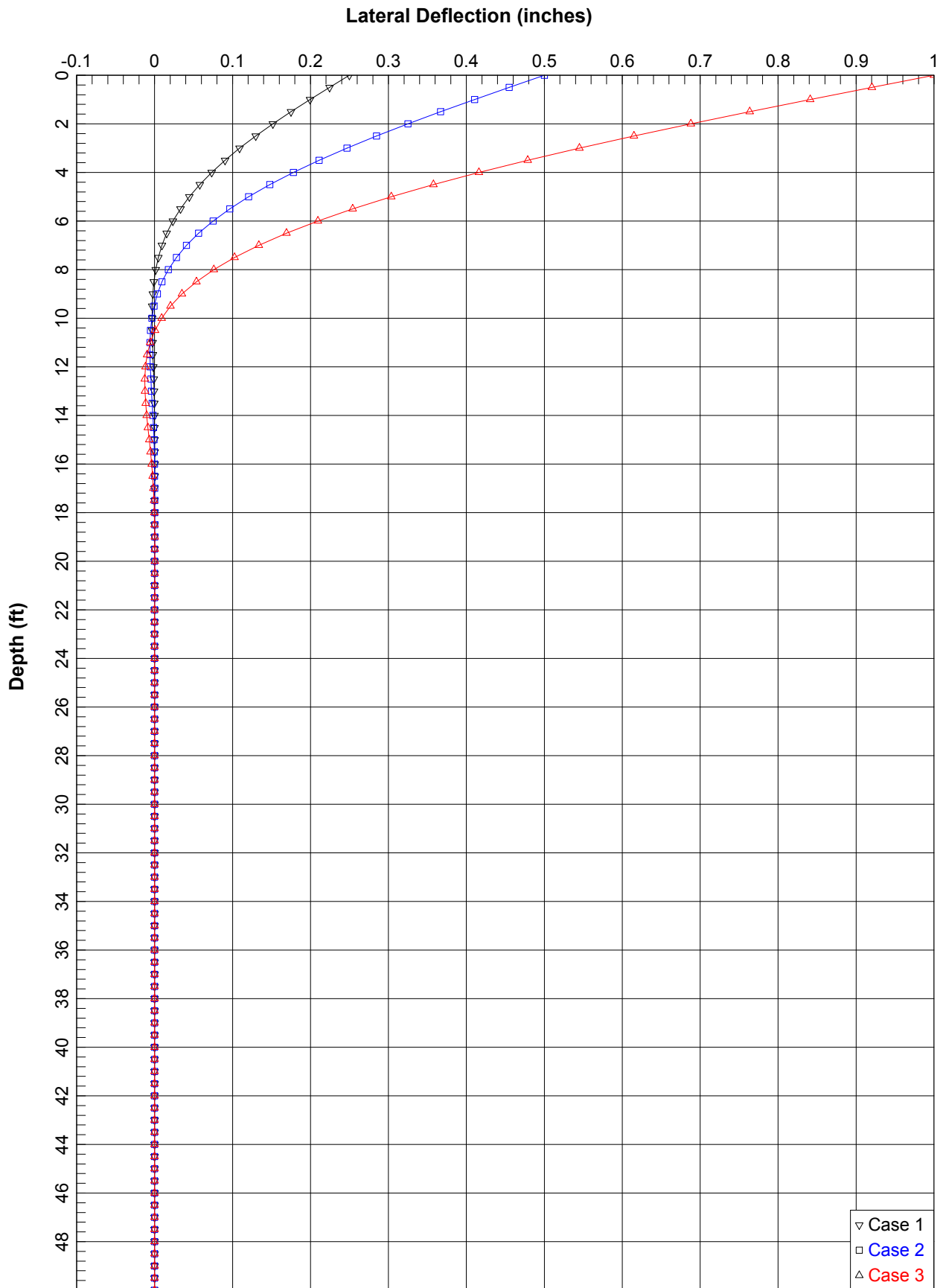
1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE

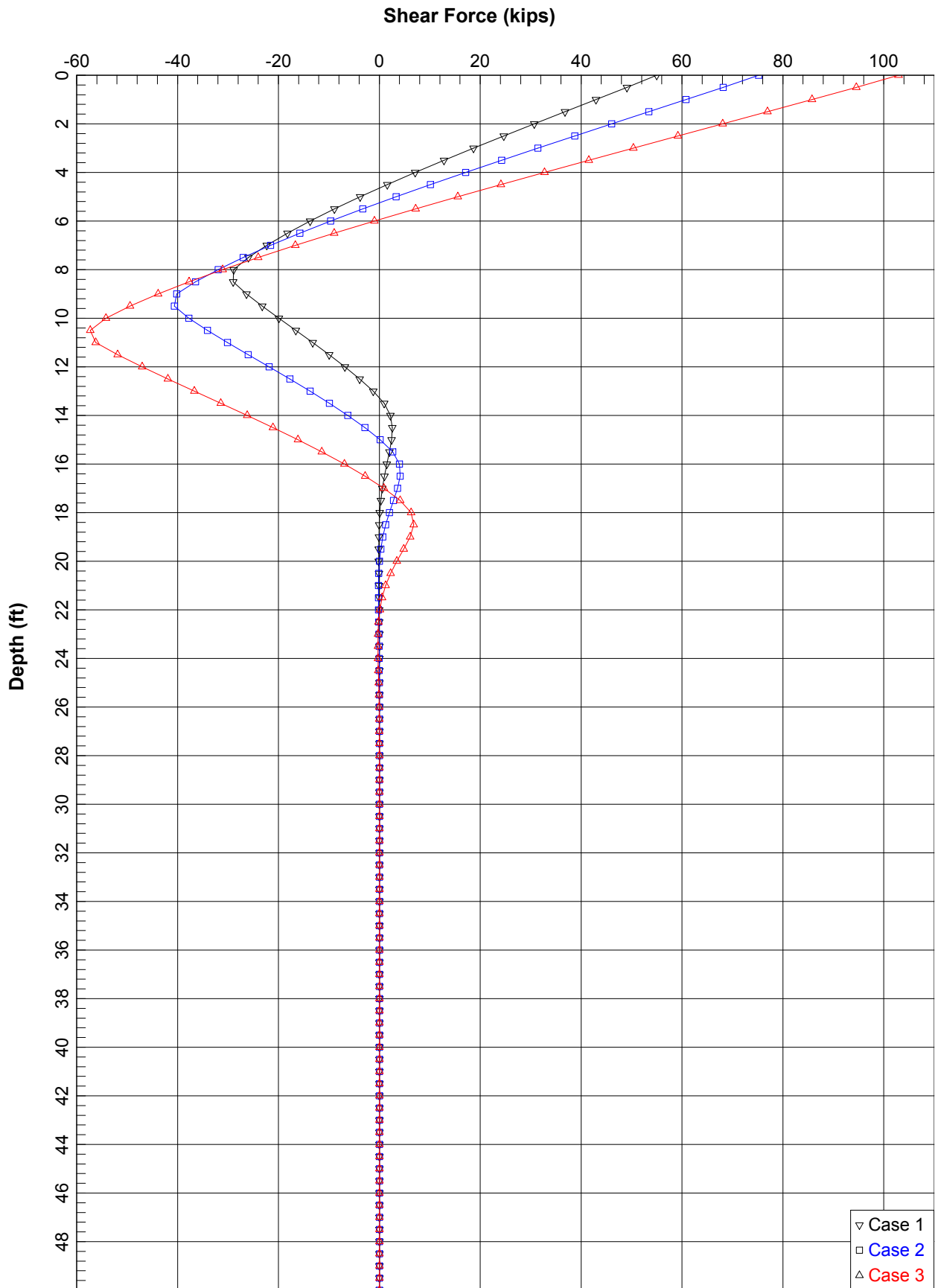


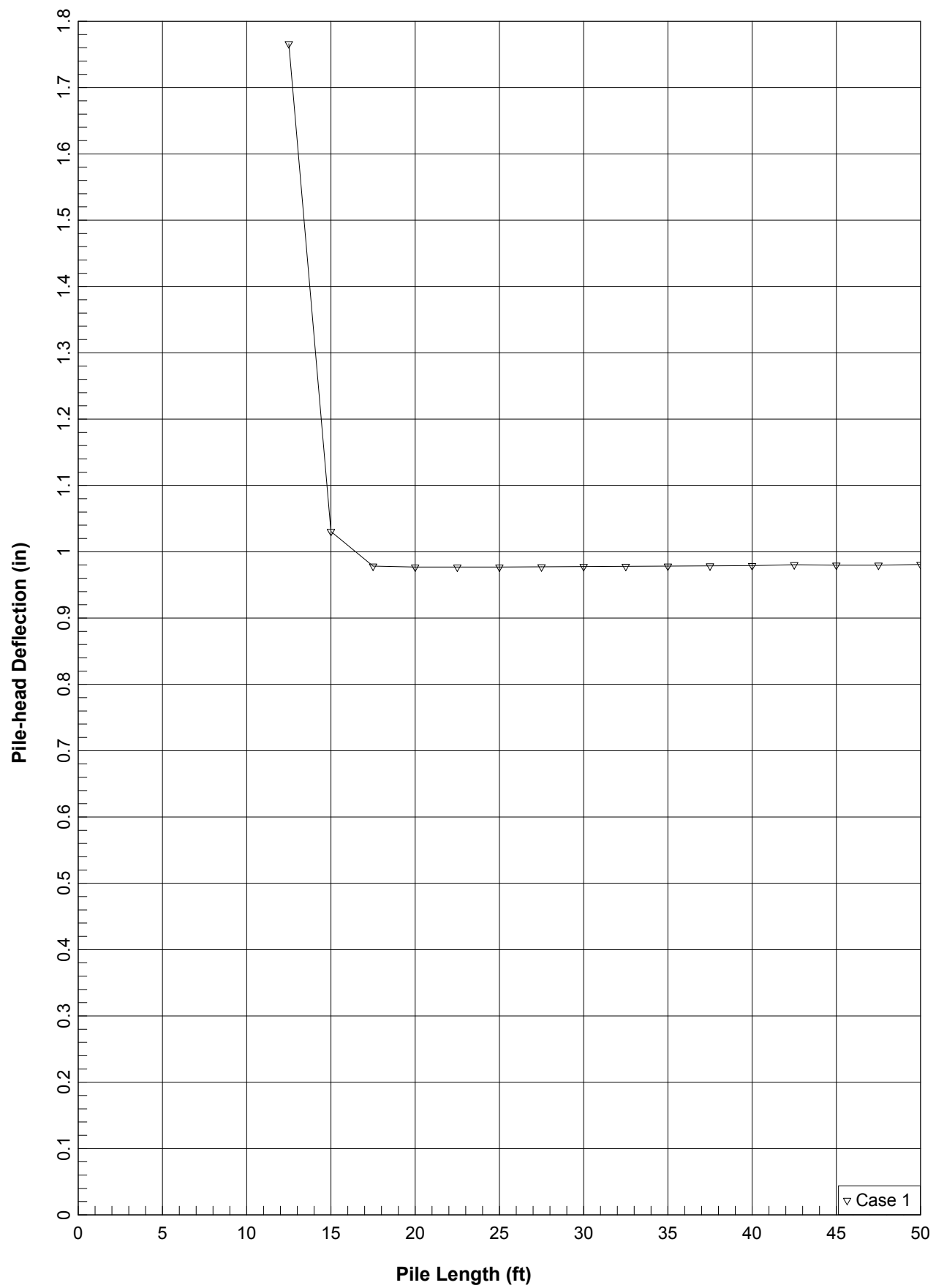
A cross-sectional diagram of a pile foundation. The pile is a vertical grey rectangle extending from the ground surface down into two soil layers. The top layer is labeled 'Layer 1, Depth -5 to 0.1 ft = Stiff Clay without Free Water' and is filled with a light green diagonal hatching pattern. The bottom layer is labeled 'Layer 2, Depth 0.1 to 80 ft = Stiff Clay without Free Water' and is filled with a darker green diagonal hatching pattern. The ground surface is indicated by a horizontal line with a hatched area above it representing the ground above the surface.

Layer 1, Depth -5 to 0.1 ft = Stiff Clay without Free Water

Layer 2, Depth 0.1 to 80 ft = Stiff Clay without Free Water







Bent 4L_transv_crit length

Pile Plus for windows, version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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gdc
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Bent 4\
 Name of input data file: Bent 4L_transv_crit length.ip6d
 Name of output report file: Bent 4L_transv_crit length.ip6o
 Name of plot output file: Bent 4L_transv_crit length.ip6p
 Name of runtime message file: Bent 4L_transv_crit length.ip6r

Date and Time of Analysis

Date: September 13, 2014 Time: 21:23:01

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 4L_transv_crit length
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top width = 24.0000000 in
 Bottom width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 2 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer Factor Num.	Layer Soil Type (p-y Curve Criteria)	Rock Mass Rock Emass	Layer Depth ft	Effective unit wt. Test	Undrained Cohesion Test	Angle of Friction Mod. deg.	Elastic Subgrade psi	Uniaxial qu psi	RQD or GSI	Epsilon
50	1	Stiff Clay w/o Free water	-5.0000	120.000	4500.000	--	--	--	--	--
0.00700	--	--	0.10000	120.000	4500.000	--	--	--	--	--
0.00700	--	--	0.10000	125.000	4500.000	--	--	--	--	--
2	2	Stiff Clay w/o Free water	0.10000	125.000	4500.000	--	--	--	--	--
0.00500	--	--	80.000	125.000	4500.000	--	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.6500	1.0000
2	50.000	0.6500	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Load No.	Load Type	Condition		Compute Top y vs. Pile Length
		1	2	
1	V	102000. lbs	M = 0.000 in-lbs	198000. True

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
R = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed values of Pile Loading and Deflection
For Lateral Loading for Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head	=	102000.000 lbs
Applied moment at pile head	=	0.000 in-lbs
Axial thrust load on pile head	=	198000.000 lbs

Depth	Deflect.	Bending	Shear	Slope	Total	Soil Res.	Soil Spr.	Distrib.
inches	inches	in-lbs	lbs	radians	psi*	lb/in ²	lb/in	lb/inch
0.00	-0.9808	-1.811E-07	102000.	-0.0131	437.6761	2.936E+10	-1320.7799	4040.0587
6.00	-0.9023	603771.	93687.	-0.0130	1327.4273	2.936E+10	-1450.1353	9643.4289
12.00	-0.8245	115190.	84951.	-0.0128	2140.0304	2.936E+10	-1461.4118	10635.
18.00	-0.7481	1653719.	76162.	-0.0126	2874.6898	2.936E+10	-1468.8778	11780.
24.00	-0.6738	2098966.	67338.	-0.0122	3530.8511	2.936E+10	-1472.3965	13111.
30.00	-0.6021	2490967.	58505.	-0.0117	4108.1083	2.936E+10	-1471.8234	14668.
36.00	-0.5334	2828837.	49689.	-0.0112	4606.4116	2.936E+10	-1467.0045	16503.
42.00	-0.4681	3113479.	40914.	-0.0106	5025.8756	2.936E+10	-1457.7735	18684.
48.00	-0.4067	3344885.	32209.	-0.0099	5366.8883	2.936E+10	-1443.9477	21301.
54.00	-0.3494	3523496.	23601.	-0.0091	5630.1002	2.936E+10	-1425.3228	24475.
60.00	-0.2963	3659405.	15112.	-0.0082	5816.4537	2.936E+10	-1401.6654	28371.
66.00	-0.2479	3725038.	6797.4035	-0.007704	5927.1044	2.936E+10	-1372.7015	33221.
72.00	-0.2040	3749815.	-1334.9989	-0.006940	5963.6161	2.936E+10	-1338.0993	39360.
78.00	-0.1646	3725509.	-9241.6219	-0.006176	5927.7977	2.936E+10	-1297.4417	47295.
84.00	-0.1299	3653590.	-16884.	-0.005422	5821.8147	2.936E+10	-1250.1796	57763.
90.00	-0.0996	3535778.	-24222.	-0.004688	5648.2003	2.936E+10	-1195.3499	70246.
96.00	-0.0746	3374068.	-31206.	-0.003981	5409.8949	2.936E+10	-1132.4189	82308.
102.00	-0.0518	3170772.	-37780.	-0.003313	5110.3054	2.936E+10	-1058.8524	92689.
108.00	-0.0339	2928583.	-43872.	-0.002689	4753.4621	2.936E+10	-971.8250	101230.
114.00	-0.0219	2650697.	-49379.	-0.002119	4343.8940	2.936E+10	-863.8894	126690.
120.00	-0.008426	2341068.	-54113.	-0.001609	3887.6066	2.936E+10	-734.1394	150830.
126.00	-0.002007	2003161.	-56717.	-0.001165	3392.5953	2.936E+10	-553.6429	18445625.
132.00	-0.000552	1663236.	-55172.	-0.000790	2888.7155	2.936E+10	668.3772	227286.
138.00	-0.000272	1344969.	-50845.	-0.000483	2419.6990	2.936E+10	774.0026	508663.
144.00	-0.0113	1034259.	-46936.	-0.000237	1991.2634	2.936E+10	828.3333	438495.
150.00	-0.0121	793096.	-40976.	-4.855E-05	1606.4269	2.936E+10	857.9730	424737.
156.00	-0.0119	562646.	-35793.	9.000E-05	1266.8235	2.936E+10	869.6214	437354.
162.00	-0.0110	363367.	-30581.	0.000185	971.1336	2.936E+10	867.8498	471657.
168.00	-0.009709	195241.	-25413.	0.000242	725.3946	2.936E+10	854.7921	528227.
174.00	-0.008139	57841.	-20353.	0.000268	522.9139	2.936E+10	831.6643	613072.
180.00	-0.006498	-49633.	-15461.	0.000268	310.8186	2.936E+10	799.1386	737858.
186.00	-0.004918	-128327.	-10791.	0.000250	626.7855	2.936E+10	757.4961	924117.
192.00	-0.003495	-179719.	-6398.4867	0.000219	702.5011	2.936E+10	706.6467	1212980.
198.00	-0.002293	-205628.	-2340.5818	0.000179	740.7016	2.936E+10	645.8990	1690286.
204.00	-0.001343	-208232.	-1299.9486	0.000137	744.5588	2.936E+10	567.5212	2355701.
210.00	-0.000648	-190355.	-421.6882	9.635E-05	718.1935	2.936E+10	473.0520	4379300.
216.00	-0.000187	-155401.	6352.6896	6.102E-05	666.6839	2.936E+10	170.6218	5484375.
222.00	8.415E-05	-114267.	6633.8080	3.346E-05	606.0669	2.936E+10	-76.9156	5484375.
228.00	0.000215	-75875.	5813.9676	1.403E-05	549.4896	2.936E+10	-196.3645	5484375.
234.00	0.000252	-44533.	4532.5909	1.721E-06	503.3023	2.936E+10	-230.7611	5484375.
240.00	0.000235	-21488.	3194.5932	-5.026E-06	469.3418	2.936E+10	-215.2381	5484375.
246.00	0.000192	-6185.9708	2021.9939	-7.854E-06	446.7921	2.936E+10	-175.8283	5484375.
252.00	0.000141	2794.7653	1107.8562	-8.201E-06	441.7946	2.936E+10	-129.0843	5484375.
258.00	9.373E-05	7127.7891	463.3843	-7.187E-06	446.1800	2.936E+10	-85.6730	5484375.
264.00	5.498E-05	8374.8527	55.8099	-5.603E-06	450.0178	2.936E+10	-50.2517	5484375.
270.00	2.650E-05	7810.8137	-167.6002	-3.949E-06	449.1866	2.936E+10	-24.2183	5484375.
276.00	7.939E-06	6273.0316	-261.0764	-2.499E-06	447.0478	2.936E+10	6.9404	5484375.
282.00	-3.494E-06	4683.8412	-272.3168	-1.369E-06	444.5785	2.936E+10	3.1936	5484375.
288.00	-8.137E-06	3108.4816	-238.5045	-5.728E-07	442.2569	2.936E+10	6.0772	5484375.
294.00	-1.037E-05	1823.1487	-185.8438	-6.880E-08	440.3628	2.936E+10	9.4764	5484375.
300.00	-9.662E-06	878.5209	-130.9192	2.073E-07	438.9707	2.936E+10	8.8318	5484375.
306.00	7.980E-07	241.6261	-82.8160	3.228E-07	437.6761	2.936E+10	10.2822	5484375.
312.00	5.789E-06	-116.0384	-45.3349	3.367E-07	437.8471	2.936E+10	5.2912	5484375.
318.00	-3.940E-06	-293.1922	-18.9316	2.948E-07	438.1082	2.936E+10	3.5099	5484375.
324.00	2.231E-06	-343.9167	2.2302	-1.876E-07	438.1829	2.936E+10	-0.0573	5484375.
330.00	-1.083E-06	-320.5003	6.9120	1.618E-07	438.1484	2.936E+10	0.9901	5484375.
336.00	3.088E-07	-261.3588	10.7294	1.024E-07	438.0632	2.936E+10	1.2823	5484375.
342.00	1.450E-07	-191.9912	11.1785	5.603E-08	437.9590	2.936E+10	-0.1326	5484375.
348.00	6.635E-07	-127.3497	9.7941	2.339E-08	437.8638	2.936E+10	-0.3322	5484375.
354.00	4.257E-06	-74.6380	7.6109	7.986E-09	437.7861	2.936E+10	-0.5892	5484375.
360.00	3.965E-07	-35.9176	5.3652	-8.549E-09	437.7290	2.936E+10	-0.3624	5484375.
366.00	3.231E-07	-10.2347	3.3919	-1.327E-08	437.6912	2.936E+10	-0.2954	5484375.
372.00	2.376E-07	7.8171	2.1619	-8.851E-09	437.6761	2.936E+10	-0.1169	5484375.
378.00	1.573E-07	12.0599	0.7731	-1.209E-08	437.6939	2.936E+10	-0.1438	5484375.
384.00	9.214E-08	14.2142	-0.6983	-9.418E-09	437.6969	2.936E+10	-0.0862	5484375.
390.00	4.429E-08	13.1510	-0.2850	-6.632E-09	437.6955	2.936E+10	-0.0405	5484375.
396.00	1.256E-08	10.7183	-0.4409	-4.192E-09	437.6919	2.936E+10	-0.0115	5484375.
402.00	-6.020E-09	7.8697	-0.4589	-2.293E-09	437.6877	2.936E+10	0.005503	5484375.

Page 3

Load No.	Load Type	Condition		Compute Top y vs. Pile Length
		1	2	
1	V	102000. lbs	M = 0.000 in-lbs	198000. True

Depth	Deflect.	Bending	Shear	Slope	Total	Soil Res.	Soil Spr.	Distrib.
inches	inches	in-lbs	lbs	radians	psi*	lb/in ²	lb/in	lb/inch
408.00	-1.495E-08	5.2173	-0.4014	-9.552E-10	437.6838	2.936E+10	0.0137	5484375.
414.00	-1.748E-08	3.0556	-0.3124	-1.098E-10	437.6806	2.936E+10	0.0160	5484375.
420.00	-1.627E-08	1.4684	-0.2199	3.526E-10	437.6783	2.936E+10	0.0149	5484375.
426.00	-1.325E-08	0.4163	-0.1389	5.452E-10	437.6767	2.936E+10	0.0121	5484375.
432.00	-9.726E-09	-0.1999	-0.0759	5.673E-10	437.6764	2.936E+10	0.00890	5484375.
438.00	-6.445E-09	-0.4961	-0.0316	4.962E-10	437.6768	2.936E+10	0.005891	5484375.
444.00	-3.772E-09	-0.3800	-0.00354	3.862E-10	437.6769	2.936E+10	0.003448	5484375.
450.00	-1.811E-09	-0.5396	0.0118	2.718E-10	437.6769	2.936E+10	0.001655	5484375.
456.00	-5.108E-10	-0.4396	0.0181	1.717E-10	437.6767	2.936E+10	0.000467	5484375.
462.00	2.499E-10	-0.3226	0.0188	9.382E-11	437.6766	2.936E+10	-0.000228	5484375.
468.00	6.150E-10	-0.2127	0.0165	3.901E-11	437.6764	2.936E+10	-0.000562	5484375.
474.00	7.179E-10	-0.1251	0.0128	4.380E-12	437.6763	2.936E+10	-0.000656	5484375.
480.00	6.675E-10	-0.0600	0.009011	-1.454E-11	437.6762	2.936E+10	-0.000610	5484375.
486.00	5.435E-10	-0.0169	0.005690	-2.240E-11	437.6761	2.936E+10	-0.000497	5484375.
492.00	3.987E-10	0.008297	0.003106	-2.329E-11	437.6761	2.936E+10	-0.000364	5484375.
498.00	2.640E-10	0.0204	0.001289	-2.035E-11	437.6761	2.936E+10	-0.000241	5484375.
504.00	1.544E-10	0.0238	0.000142	-1.585E-11	437.6761	2.936E+10	-0.000141	5484375.
510.00	7.403E-11	0.0221	-0.000485	-1.114E-11	437			

Bent 4L_transv_ave P

Pile Plus for windows, version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading using the p-y Method
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Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Bent 4\
 Name of input data file: Bent 4L_transv_ave P.lp6d
 Name of output report file: Bent 4L_transv_ave P.lp6o
 Name of plot output file: Bent 4L_transv_ave P.lp6p
 Name of runtime message file: Bent 4L_transv_ave P.lp6r

Date and Time of Analysis

Date: September 13, 2014 Time: 21:19:17

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
 - Maximum number of iterations allowed = 100
 - Deflection tolerance for convergence = 1.0000E-05 in
 - Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 4L_transv_ave P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top width = 24.0000000 in
 Bottom width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 2 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer Factor	Soil Type	Rock Mass Rock Emass	Layer Depth	Effective unit wt.	Undrained Cohesion	In-situ Friction	Angle of Elastic Mod.	Uniaxial qu	RQD or GSI	psi	Epsilon
1	50	Stiff Clay w/o Free water	--	-5.0000	120.0000	4500.0000	--	--	--	--	--	--
0.00700	--	--	--	0.100000	120.0000	4500.0000	--	--	--	--	--	--
0.00700	--	--	--	0.100000	125.0000	4500.0000	--	--	--	--	--	--
2	50	Stiff Clay w/o Free water	--	80.0000	125.0000	4500.0000	--	--	--	--	--	--
0.00500	--	--	--	80.0000	125.0000	4500.0000	--	--	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.0000	0.6500	1.0000
2	50.0000	0.6500	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No. Load Type Condition 1 Condition 2 Bent 4L_trans_vave P Axial Thrust Force, lbs Compute Top y vs. Pile Length

v = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
e = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed values of Pile Loading and Deflection
For Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.250000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 198000.000 lbs

Table with 13 columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load. Rows 0.00 to 384.00.

Table with 13 columns: 390.00 to 600.00. Columns include values for depth, deflection, bending moment, shear force, slope, total stress, bending stiffness, soil resistance, soil spring, and lateral load.

* The above values of total stress are combined axial and bending stress.

Output verification: computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Pile-head deflection = 0.2500000 inches
Computed slope at pile head = -0.002433 radians
Maximum bending moment = 1544366. inch-lbs
Maximum shear force = 54985. lbs
Depth of maximum bending moment = 54.000000 inches below pile head
Depth of maximum shear force = 0.000000 inches below pile head
Number of iterations = 9
Number of zero deflection points = 18

Computed values of Pile Loading and Deflection
For Lateral Loading for Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)
Displacement of pile head = 0.500000 inches
Moment at pile head = 0.000 in-lbs
Axial load at pile head = 198000.000 lbs

Table with 13 columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Bending Stiffness, Soil Res., Soil Spr., Distrib. Lat. Load. Rows 0.00 to 246.00.

Table of stress components for various pile types (252, 258, 264, 268, 270, 272, 276, 280, 284, 288, 292, 296, 300, 304, 308, 312, 316, 320, 324, 328, 332, 336, 340, 344, 348, 352, 356, 360, 364, 368, 372, 376, 380, 384, 388, 392, 396, 400, 404, 408, 412, 416, 420, 424, 428, 432, 436, 440, 444, 448, 452, 456, 460, 464, 468, 472, 476, 480, 484, 488, 492, 496, 500, 504, 508, 512, 516, 520, 524, 528, 532, 536, 540, 544, 548, 552, 556, 560, 564, 568, 572, 576, 580, 584, 588, 592, 596, 600, 604) and pile types (41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100). Columns include Y, X, Z coordinates, stress components (sigma_y, sigma_x, sigma_z, tau_yx, tau_yz, tau_xz), and pile type.

* The above values of total stress are combined axial and bending stress.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Pile-head deflection = 0.5000000 inches
Computed slope at pile head = -0.0075070 radians
Maximum bending moment = 2416239. inch-lbs
Maximum shear force = 52175. lbs
Depth of maximum bending moment = 66.0000000 inches below pile head
Depth of maximum shear force = 0.0000000 inches below pile head
Number of iterations = 21
Number of zero deflection points = 9

Computed values of Pile Loading and Deflection for Lateral Loading for Load Case Number 3

Table with columns: Depth, Deflect., Bending Moment, Shear Force, Slope, Total Stress, Soil Res., Soil Spr., Distrib. Lat. Load. Rows show data for depths from 0.00 to 108.00.

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 1.000000 inches
Moment at pile head = 198000.00 in-lbs
Axial load at pile head = 198000.00 lbs

Table of stress components for various pile types (114, 120, 126, 130, 134, 138, 142, 146, 150, 154, 158, 162, 166, 170, 174, 178, 182, 186, 190, 194, 198, 202, 206, 210, 214, 218, 222, 226, 230, 234, 238, 242, 246, 250, 254, 258, 262, 266, 270, 274, 278, 282, 286, 290, 294, 298, 302, 306, 310, 314, 318, 322, 326, 330, 334, 338, 342, 346, 350, 354, 358, 362, 366, 370, 374, 378, 382, 386, 390, 394, 398, 402, 406, 410, 414, 418, 422, 426, 430, 434, 438, 442, 446, 450, 454, 458, 462, 466, 470, 474, 478, 482, 486, 490, 494, 498, 502, 506, 510, 514, 518, 522, 526, 530, 534, 538, 542, 546, 550, 554, 558, 562, 566, 570, 574, 578, 582, 586, 590, 594, 598, 602, 606, 610, 614, 618, 622, 626, 630, 634, 638, 642, 646, 650, 654, 658, 662, 666, 670, 674, 678, 682, 686, 690, 694, 698, 702, 706, 710, 714, 718, 722, 726, 730, 734, 738, 742, 746, 750, 754, 758, 762, 766, 770, 774, 778, 782, 786, 790, 794, 798, 802, 806, 810, 814, 818, 822, 826, 830, 834, 838, 842, 846, 850, 854, 858, 862, 866, 870, 874, 878, 882, 886, 890, 894, 898, 902, 906, 910, 914, 918, 922, 926, 930, 934, 938, 942, 946, 950, 954, 958, 962, 966, 970, 974, 978, 982, 986, 990, 994, 998, 1000) and pile types (Bent 41, trans, ave P). Columns include Y, X, Z coordinates, stress components (sigma_y, sigma_x, sigma_z, tau_yx, tau_yz, tau_xz), and pile type.

* The above values of total stress are combined axial and bending stress.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

Pile-head deflection = 1.0000000 inches
Computed slope at pile head = -0.0133000 radians
Maximum bending moment = 3790233. inch-lbs
Maximum shear force = 102919. lbs
Depth of maximum bending moment = 72.0000000 inches below pile head
Depth of maximum shear force = 0.0000000 inches below pile head
Number of iterations = 15
Number of zero deflection points = 8

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

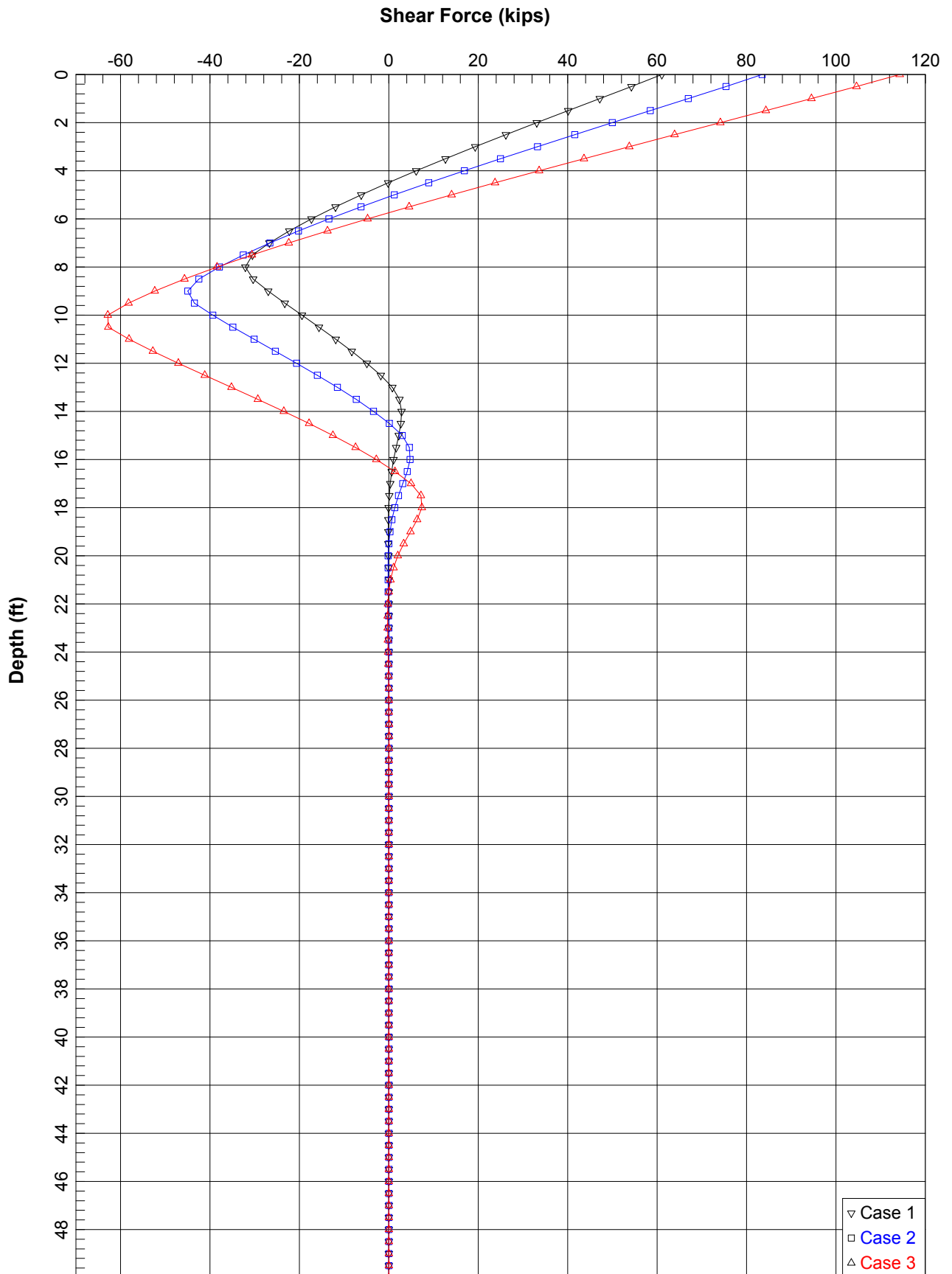
Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians

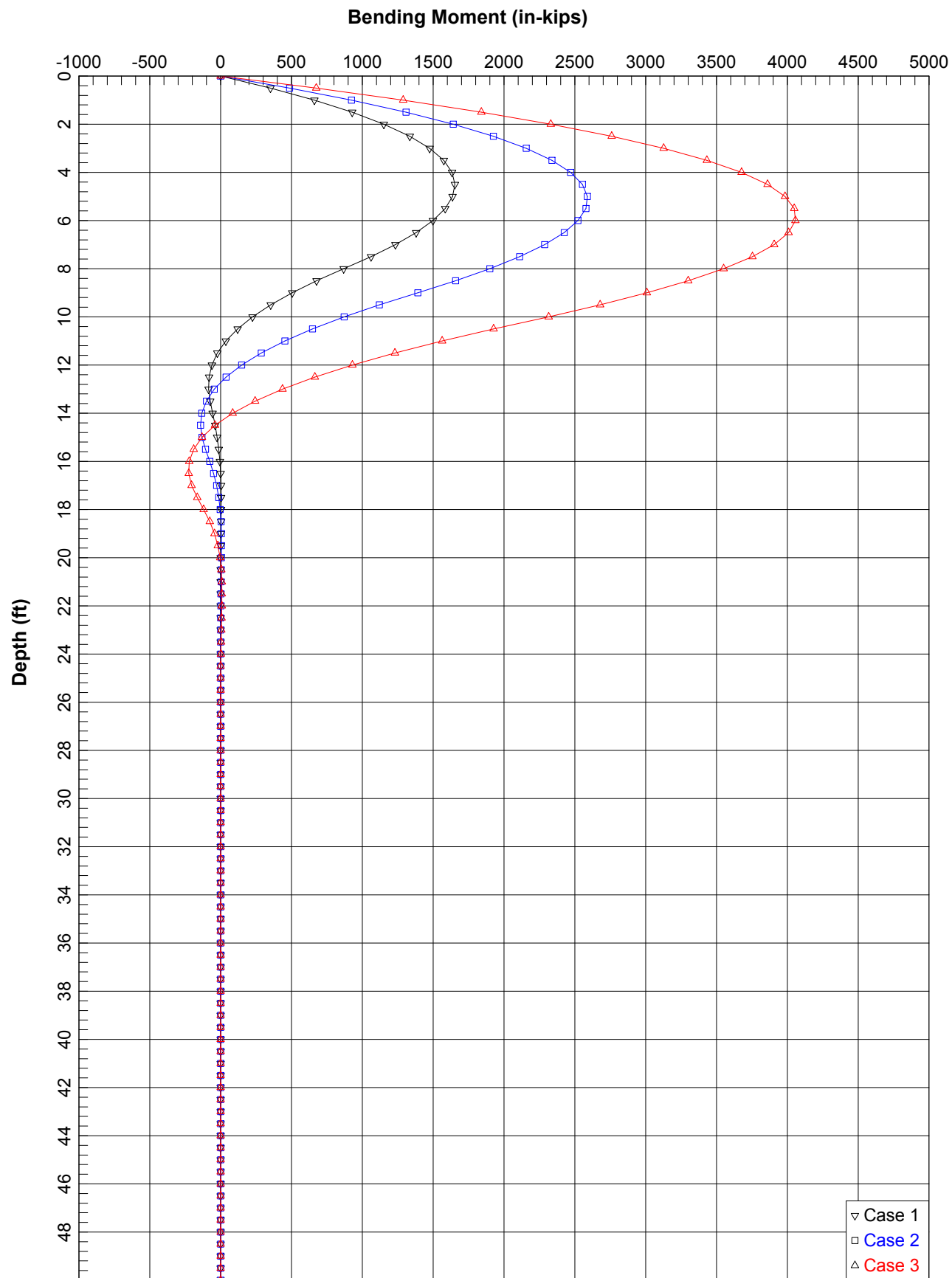
Bent 4L_transv_ave P

Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.		Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y =	0.2500	M = 0.000	198000.	0.25000000	1544366.	54985.	-0.00424813
2	4	y =	0.5000	M = 0.000	198000.	0.50000000	2416239.	75175.	-0.00750702
3	4	y =	1.0000	M = 0.000	198000.	1.00000000	3799023.	102919.	-0.01330061

The analysis ended normally.





Bent 4L_transv_Max P

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 Subjected to Lateral Loading using the p-y Method
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Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Bent 4\
 Name of input data file: Bent 4L_transv_Max P.lp6d
 Name of output report file: Bent 4L_transv_Max P.lp6o
 Name of plot output file: Bent 4L_transv_Max P.lp6p
 Name of runtime message file: Bent 4L_transv_Max P.lp6r

Date and Time of Analysis

Date: September 13, 2014 Time: 21:24:44

Problem Title

Project Name: Palo Comado OC Bridge widen
 Job Number: LA-1143
 Client: Parson Transportation
 Engineer: Mario DiNicola
 24inch CIDH Lateral Capacity Analysis-Bent 2-Free Head- Longit.-Avg Pm

Program Options

Engineering units are US Customary units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -5.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	24.0000000
2	50.00000	24.0000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Page 1

Bent 4L_transv_Max P
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top width = 24.0000000 in
 Bottom width = 24.0000000 in
 Top Area = 452.38934212 in
 Bottom Area = 452.38934212 in
 Moment of Inertia at Top = 8143.00815810 in
 Moment of Inertia at Bottom = 8143.00815810 in
 Elastic Modulus = 3605000. Tbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 2 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Strain Layer	Layer	Rock Mass	Layer	Effective	Undrained	Angle of	Elastic	Uniaxial	RQD %
Factor	Soil Type	Rock Emass	Depth	unit wt.	Cohesion	Friction	Mod.	qu	or
50	(p-y Curve Criteria)	ft	ft	pcf	psf	deg.	psi	psi	GSI
Num.	psi		Type	Test	Property	Subgrade			Epsilon
1	Stiff Clay w/o Free water	--	-5.0000	120.0000	4500.0000	--	--	--	--
0.00700	--	--	0.100000	120.0000	4500.0000	--	--	--	--
0.00700	--	--	0.100000	125.0000	4500.0000	--	--	--	--
2	Stiff Clay w/o Free water	--	80.0000	125.0000	4500.0000	--	--	--	--
0.00500	--	--	80.0000	125.0000	4500.0000	--	--	--	--
0.00500	--	--	--	--	--	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.0000	0.7500	1.0000
2	50.0000	0.7500	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Bent 4L _{transv} Max P	Compute
1	4	y = 0.25000 in	M = 0.0000 in-lbs	198000.	False
2	4	y = 0.50000 in	M = 0.0000 in-lbs	198000.	False
3	4	y = 1.00000 in	M = 0.0000 in-lbs	198000.	False

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
e = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Depth	Deflect.	Bending Moment	Shear Force	Slope	Total Stress	Bending Stiffness	Soil Res. p	Soil Spr. Es	Distrib. Lat. Load
inches	inches	in-lbs	lbs	radians	psi	lb-in ²	lb/in	lb/inch	Tb/inch
0.00	0.2500	0.000	61042.	-0.004394	437.6761	2.936E+10	-1082.8535	12994.	0.000
6.000	0.2236	351981.	54252.	-0.004358	956.3752	2.936E+10	-1180.6123	31675.	0.000
0.197	0.2225	189982.	54252.	-0.004355	912.0348	2.936E+10	-1179.9850	35811.	0.000
18.000	0.1726	928128.	40106.	-0.004092	1805.4177	2.936E+10	-1174.5904	40836.	0.000
24.000	0.1486	1152370.	33090.	-0.003880	2135.8745	2.936E+10	-1164.2377	47010.	0.000
30.000	0.1260	1334421.	28311.	-0.003625	2404.1543	2.936E+10	-1148.7129	54690.	0.000
36.000	0.1051	1474793.	19321.	-0.003338	2611.0154	2.936E+10	-1127.7702	64888.	0.000
42.000	0.0866	1567240.	12635.	-0.003027	2737.5187	2.936E+10	-1101.2156	76854.	0.000
48.000	0.0688	1633600.	6126.0518	-0.002699	2845.0425	2.936E+10	-1068.4066	93216.	0.000
54.000	0.0536	1654133.	-166.7024	-0.002363	2875.3011	2.936E+10	-1029.2781	115254.	0.000
60.000	0.0404	1637234.	-6202.8966	-0.002027	2850.3682	2.936E+10	-982.8200	145912.	0.000
66.000	0.0293	1584516.	-11936.	-0.001697	2772.7092	2.936E+10	-928.4383	190389.	0.000
72.000	0.0200	1498005.	-17316.	-0.001382	2645.2280	2.936E+10	-864.6026	258774.	0.000
78.000	0.0127	1380133.	-22276.	-0.001088	2471.3422	2.936E+10	-788.7167	373455.	0.000
84.000	0.006989	1233288.	-26727.	-0.000821	2255.1199	2.936E+10	-695.1123	539768.	0.000
90.000	0.002818	1061240.	-30251.	-0.000587	2001.5795	2.936E+10	-566.5148	820606.	0.000
96.000	-0.008205	868539.	-32094.	-0.000389	1717.6047	2.936E+10	-39.1998	4641286.	0.000
102.000	-0.001855	677039.	-30385.	-0.000231	1435.3988	2.936E+10	530.4496	1716256.	0.000
108.000	0.001828	504700.	-26988.	-0.000111	1181.0918	2.936E+10	601.9960	1277155.	0.000
114.000	-0.003183	353451.	-23284.	-2.304E-05	958.5412	2.936E+10	632.6526	1195519.	0.000
120.000	-0.003105	225121.	-19462.	3.609E-05	769.4274	2.936E+10	641.3406	1239092.	0.000
126.000	-0.002750	119818.	-15637.	7.134E-05	614.2466	2.936E+10	613.9940	1383271.	0.000
132.000	-0.002248	37309.	-11892.	8.740E-05	492.6573	2.936E+10	614.2376	1639097.	0.000
138.000	-0.001701	-23096.	-8299.1795	8.885E-05	471.7111	2.936E+10	583.4215	2057723.	0.000
144.000	-0.001182	-62492.	-4922.1077	8.011E-05	329.7677	2.936E+10	542.7691	2752151.	0.000
150.000	-0.000740	-82351.	-1822.9783	6.530E-05	559.0336	2.936E+10	490.7741	3979864.	0.000
156.000	-0.000399	-84523.	768.8530	4.825E-05	652.2337	2.936E+10	373.1697	5637848.	0.000
162.000	-0.000161	-73240.	2348.1090	3.213E-05	545.6062	2.936E+10	153.2490	5715504.	0.000
168.000	-1.302E-05	-56422.	2845.6910	1.888E-05	520.8225	2.936E+10	12.6116	5813160.	0.000
174.000	6.965E-05	-39136.	2689.5015	9.112E-06	495.3489	2.936E+10	-64.6748	5910816.	0.000
180.000	9.632E-05	-24169.	2206.0977	7.642E-06	473.2936	2.936E+10	-96.4598	6008472.	0.000
186.000	9.736E-05	-12669.	1619.4816	1.123E-06	456.3464	2.936E+10	-99.0789	6106128.	0.000
192.000	6.285E-05	-4732.9990	1085.2439	-2.901E-06	444.6099	2.936E+10	-85.6670	6216000.	0.000
198.000	6.254E-05	120.4795	611.1818	3.372E-06	437.8536	2.936E+10	-65.6870	6301441.	0.000
204.000	4.238E-05	2609.1950	280.0138	3.093E-06	441.5212	2.936E+10	-44.7023	6382125.	0.000
210.000	2.542E-05	3487.9956	65.4649	-2.470E-06	442.8162	2.936E+10	-26.8141	6382125.	0.000
216.000	1.274E-05	3400.6428	-55.2892	-1.766E-06	442.6875	2.936E+10	-13.4373	6382125.	0.000
222.000	4.228E-06	2828.7221	-107.9778	-1.130E-06	441.8447	2.936E+10	-4.4589	6382125.	0.000
228.000	-8.161E-07	2095.5933	-119.7724	-6.265E-07	440.7643	2.936E+10	0.8607	6382125.	0.000
234.000	-3.290E-06	1392.9422	-106.7803	-2.700E-07	439.7288	2.936E+10	3.4699	6382125.	0.000
240.000	-6.621E-06	814.8707	-83.3390	-4.434E-08	438.8769	2.936E+10	8.3293	6382125.	0.000
246.000	-3.822E-06	390.5912	-58.6123	7.885E-08	438.2517	2.936E+10	0.0311	6382125.	0.000
252.000	-3.109E-06	111.3360	-36.6805	1.301E-07	437.8402	2.936E+10	3.2795	6382125.	0.000
258.000	-2.906E-07	-49.8845	-19.6904	-5.364E-07	437.6298	2.936E+10	3.7819	6382125.	0.000
264.000	-1.472E-06	-125.2731	-7.8804	1.185E-07	437.8607	2.936E+10	1.5528	6382125.	0.000
270.000	8.051E-07	2.8284	1.3279	1.074E-08	437.8594	2.936E+10	0.2850	6382125.	0.000
276.000	-3.811E-07	-132.3375	3.2862	6.262E-08	437.8711	2.936E+10	0.4019	6382125.	0.000
282.000	-8.647E-08	-105.4444	4.7655	3.837E-08	437.8315	2.936E+10	0.0912	6382125.	0.000
288.000	7.890E-08	-75.2423	4.7908	1.986E-08	437.8070	2.936E+10	-0.0313	6382125.	0.000
294.000	1.518E-07	-48.0137	4.0602	7.259E-09	437.7468	2.936E+10	-0.1601	6382125.	0.000
300.000	-6.659E-07	-26.5369	3.0550	-3.594E-10	437.7452	2.936E+10	-0.1750	6382125.	0.000
306.000	1.475E-07	11.5929	0.9634	-4.252E-09	437.6228	2.936E+10	0.00983	6382125.	0.000
312.000	1.151E-07	-1.7658	1.2325	-5.572E-09	437.6787	2.936E+10	-0.1214	6382125.	0.000
318.000	6.051E-08	2.8284	0.6132	6.452E-09	437.8259	2.936E+10	0.00437	6382125.	0.000
324.000	5.033E-08	5.6051	0.1989	-4.475E-09	437.6844	2.936E+10	-0.0531	6382125.	0.000
330.000	2.692E-08	5.8475	-0.0455	-3.304E-09	437.6847	2.936E+10	-0.0284	6382125.	0.000
336.000	1.068E-08	1.6162	-0.1652	-1.566E-09	437.6785	2.936E+10	-0.00752	6382125.	0.000
342.000	6.300E-10	3.8788	-0.2003	-1.275E-09	437.6818	2.936E+10	-0.000686	6382125.	0.000
348.000	-4.620E-09	2.8655	-0.1878	-6.059E-10	437.6800	2.936E+10	0.004873	6382125.	0.000
354.000	6.621E-06	11.5929	0.6273	-1.322E-07	437.6781	2.936E+10	-0.000886	6382125.	0.000
360.000	-6.627E-09	0.8396	-0.1103	8.483E-11	437.6773	2.936E+10	0.006989	6382125.	0.000
366.000	5.603E-09	1.2868	-0.0816	3.962E-11	437.6765	2.936E+10	0.001120	6382125.	0.000
372.000	-4.207E-09	-0.0199	-0.0405	2.306E-10	437.6761	2.936E+10	0.004437	6382125.	0.000
378.000	-2.836E-09	-0.1835	-0.0183	2.098E-10	437.6764	2.936E+10	0.002991	6382125.	0.000
384.000	-1.689E-09	-0.2395	-0.003939	1.666E-10	437.6764	2.936E+10	0.001782	6382125.	0.000

Load No.	Load Type	Condition 1	Condition 2	Bent 4L _{transv} Max P	Compute
1	4	y = 0.25000 in	M = 0.0000 in-lbs	198000.	False
2	4	y = 0.50000 in	M = 0.0000 in-lbs	198000.	False
3	4	y = 1.00000 in	M = 0.0000 in-lbs	198000.	False

V = perpendicular shear force applied to pile head
M = bending moment applied to pile head
y = lateral deflection relative to pile axis
S = pile slope relative to original pile batter angle
e = rotational stiffness applied to pile head
Axial thrust is assumed to be acting axially for all pile batter angles.

Depth	Deflect.	Bending Moment	Shear Force	Slope	Total Stress	Bending Stiffness	Soil Res. p	Soil Spr. Es	Distrib. Lat. Load
inches	inches	in-lbs	lbs	radians	psi	lb-in ²	lb/in	lb/inch	Tb/inch
0.00	0.2500	0.000	61042.	-0.004394	437.6761	2.936E+10	-1082.8535	12994.	0.000
6.000	0.2236	351981.	54252.	-0.004358	956.3752	2.936E+10	-1180.6123	31675.	0.000
0.197	0.2225	189982.	54252.	-0.004355	912.0348	2.936E+10	-1179.9850	35811.	0.000
18.000	0.1726	928128.	40106.	-0.004092	1805.4177	2.936E+10	-1174.5904	40836.	0.000
24.000	0.1486	1152370.	33090.	-0.003880	2135.8745	2.936E+10	-1164.2377	47010.	0.000
30.000	0.1260	1334421.	28311.	-0.003625	2404.1543	2.936E+10	-1148.7129	54690.	0.000
36.000	0.1051	1474793.	19321.	-0.003338	2611.0154	2.936E+10	-1127.7702	64888.	0.000
42.000	0.0866	1567240.	12635.	-0.003027	2737.5187	2.936E+10	-1101.2156	76854.	0.000
48.000	0.0688	1633600.	6126.0518	-0.002699	2845.0425	2.936E+10	-1068.4066	93216.	0.000
54.000	0.0536	1654133.	-166.7024	-0.002363	2875.3011	2.936E+10	-1029.2781	115254.	0.000
60.000	0.0404	1637234.	-6202.8966	-0.002027	2850.3682	2.936E+10	-982.8200	145912.	0.000
66.000	0.0293	1584516.	-11936.	-0.001697	2772.7092	2.936E+10	-928.4383	190389.	0.000
72.000	0.0200	1498005.	-17316.	-0.001382	2645.2280	2.936E+10	-864.6026	258774.	0.000
78.000	0.0127	1380133.	-22276.	-0.001088	2471.3422	2.936E+10	-788.7167	373455.	0.000
84.000	0.006989	1233288.	-26727.	-0.000821	2255.1199	2.936E+10	-695.1123	539768.	0.000
90.000	0.002818	1061240.	-30251.	-0.000587	2001.5795	2.936E+10	-566.5148	820606.	0.000
96.000	-0.008205	868539.	-32094.	-0.000389	1717.6047	2.936E+10	-39.1998	4641286.	0.000
102.000	-0.001855	677039.	-30385.	-0.000231	1435.3988	2.936E+10	530.4496	1716256.	0.000
108.000	0.001828	504700.	-26988.	-0.000111	1181.0918	2.936E+10	601.9960	1277155.	0.000
114.000	-0.003183	353451.	-23284.	-2.304E-05	958.5412	2.936E+10	632.6526	1195519.	0.000
120.000	-0.003105	225121.	-19462.	3.609E-05	769.4274	2.936E+10	641.3406	1239092.	0.000
126.000	-0.002750	119818.	-15637.	7.134E-05	614.2466	2.936E+10	613.9940	1383271.	0.000
132.000	-0.002248	37309.	-11892.	8.740E-05	492.6573	2.936E+10	614.2376	1639097.	0.000
138.000	-0.001701	-23096.	-8299.1795						

		Bent 4L_transv_Max P												
252.000	-4.990E-06	2742.6177	-186.6362	-6.588E-07	441.7178	2.936E+10	4.3140	6328125.	0.000					
258.000	-6.361E-06	1700.9022	-153.5661	-2.047E-07	440.1826	2.936E+10	6.7094	6328125.	0.000					
264.000	-6.547E-06	900.3111	-112.7236	6.113E-08	439.0028	2.936E+10	6.9048	6328125.	0.000					
274.000	-5.628E-06	346.2132	-74.7026	1.887E-07	437.6197	2.936E+10	6.8186	6328125.	0.000					
276.000	-4.282E-06	9.4365	-42.8457	2.252E-07	437.6900	2.936E+10	4.5164	6328125.	0.000					
282.000	-2.925E-06	-166.6103	-20.0414	2.092E-07	437.9216	2.936E+10	3.0850	6328125.	0.000					
288.000	-1.772E-06	-182.4243	-5.1795	1.685E-07	438.0173	2.936E+10	1.8690	6328125.	0.000					
294.000	-9.031E-07	-229.1642	3.2851	1.214E-07	438.0138	2.936E+10	0.9525	6328125.	0.000					
300.000	-3.152E-07	-192.4243	7.1401	7.805E-07	437.9597	2.936E+10	0.3325	6328125.	0.000					
306.000	6.673E-08	-143.6693	8.0212	4.397E-08	437.8878	2.936E+10	-0.0387	6328125.	0.000					
312.000	2.125E-07	-96.2739	7.2327	1.945E-08	437.8180	2.936E+10	-0.2241	6328125.	0.000					
318.000	2.702E-07	-56.9277	5.7056	3.798E-09	437.7600	2.936E+10	-0.2849	6328125.	0.000					
324.000	2.581E-07	-27.8157	4.0343	-4.862E-09	437.7171	2.936E+10	-0.2722	6328125.	0.000					
330.000	2.118E-07	-8.4998	2.5476	-8.573E-09	437.6886	2.936E+10	-0.2234	6328125.	0.000					
336.000	1.532E-07	2.7734	1.3864	-9.158E-09	437.6802	2.936E+10	-0.1637	6328125.	0.000					
342.000	1.019E-07	8.1584	0.5729	-8.041E-09	437.6881	2.936E+10	-0.1075	6328125.	0.000					
348.000	5.666E-08	9.6696	0.0648	-6.219E-09	437.6903	2.936E+10	-0.0619	6328125.	0.000					
354.000	2.798E-08	8.9505	-0.2072	-4.316E-09	437.6893	2.936E+10	0.0288	6328125.	0.000					
360.000	6.582E-09	7.1930	-0.3154	-2.666E-09	437.6867	2.936E+10	-0.007258	6328125.	0.000					
366.000	-4.706E-09	5.1724	-0.3222	-1.403E-09	437.6837	2.936E+10	0.004964	6328125.	0.000					
372.000	-9.952E-09	3.3293	-0.2759	-5.340E-10	437.6810	2.936E+10	0.0105	6328125.	0.000					
378.000	-1.111E-08	1.8633	-0.2092	-3.297E-12	437.6788	2.936E+10	0.0117	6328125.	0.000					
384.000	-9.991E-09	0.8188	-0.1424	2.708E-10	437.6773	2.936E+10	0.0105	6328125.	0.000					
390.000	-7.864E-09	0.1534	-0.0859	3.702E-10	437.6763	2.936E+10	0.008294	6328125.	0.000					
396.000	-5.549E-09	-0.2134	-0.0435	3.640E-10	437.6764	2.936E+10	0.005853	6328125.	0.000					
402.000	-3.966E-09	-0.3694	-0.0149	3.045E-10	437.6764	2.936E+10	0.003687	6328125.	0.000					
408.000	-1.896E-09	-0.3926	0.002183	2.266E-10	437.6767	2.936E+10	0.002000	6328125.	0.000					
414.000	-7.771E-10	-0.3438	0.0106	1.513E-10	437.6766	2.936E+10	0.000820	6328125.	0.000					
420.000	-7.991E-11	-0.2653	0.0134	8.908E-11	437.6765	2.936E+10	8.428E-05	6328125.	0.000					
426.000	2.939E-10	-0.1838	0.0127	4.319E-11	437.6764	2.936E+10	-0.000308	6328125.	0.000					
432.000	4.384E-10	-0.1073	0.0066	1.513E-10	437.6764	2.936E+10	-0.000462	6328125.	0.000					
438.000	4.460E-10	-0.0593	0.005753	-4.799E-12	437.6762	2.936E+10	-0.000470	6328125.	0.000					
444.000	3.808E-10	-0.0224	0.004957	-1.315E-11	437.6761	2.936E+10	-0.000402	6328125.	0.000					
450.000	2.882E-10	0.000172	0.002840	-1.542E-11	437.6761	2.936E+10	-0.000304	6328125.	0.000					
456.000	1.958E-10	0.0118	0.001309	-1.420E-11	437.6761	2.936E+10	-0.000206	6328125.	0.000					
462.000	1.178E-10	0.0159	0.000317	-1.137E-11	437.6761	2.936E+10	-0.000124	6328125.	0.000					
468.000	5.937E-11	0.0156	-0.000244	-8.148E-12	437.6761	2.936E+10	-6.261E-05	6328125.	0.000					
474.000	2.004E-11	0.0130	-0.000495	-5.226E-12	437.6761	2.936E+10	-2.113E-05	6328125.	0.000					
480.000	-3.346E-12	0.039659	-0.000548	-2.910E-12	437.6761	2.936E+10	3.329E-06	6328125.	0.000					
486.000	-1.488E-11	0.006437	-0.000490	-1.265E-12	437.6761	2.936E+10	-5.170E-05	6328125.	0.000					
492.000	-1.852E-11	0.003779	-0.000385	0.0000	437.6761	2.936E+10	1.954E-05	6328125.	0.000					
498.000	-1.738E-11	0.001823	-0.000281	0.0000	437.6761	2.936E+10	1.849E-05	6328125.	0.000					
504.000	-1.430E-11	0.000532	-0.000170	0.0000	437.6761	2.936E+10	1.309E-05	6328125.	0.000					
510.000	-1.042E-11	-0.000216	-9.351E-05	0.0000	437.6761	2.936E+10	1.099E-06	6328125.	0.000					
516.000	6.409E-12	-0.000368	-3.971E-06	0.0000	437.6761	2.936E+10	7.180E-06	6328125.	0.000					
522.000	-3.899E-12	-0.0000661	-3.165E-06	0.0000	437.6761	2.936E+10	4.102E-06	6328125.	0.000					
528.000	-1.781E-12	-0.000007	-1.477E-06	0.0000	437.6761	2.936E+10	3.788E-06	6328125.	0.000					
534.000	0.0000	-0.0000485	2.172E-05	0.0000	437.6761	2.936E+10	4.391E-07	6328125.	0.000					
540.000	0.0000	-0.000347	2.192E-05	0.0000	437.6761	2.936E+10	-3.727E-07	6328125.	0.000					
546.000	0.0000	0.000113	1.860E-04	0.0000	437.6761	2.936E+10	1.364E-07	6328125.	0.000					
552.000	0.0000	-0.000124	1.395E-05	0.0000	437.6761	2.936E+10	-8.131E-07	6328125.	0.000					
558.000	0.0000	-5.444E-05	9.318E-06	0.0000	437.6761	2.936E+10	-7.301E-07	6328125.	0.000					
564.000	0.0000	1.116E-05	0.0000	0.0000	437.6761	2.936E+10	5.767E-07	6328125.	0.000					
570.000	0.0000	1.039E-05	2.442E-06	0.0000	437.6761	2.936E+10	-4.082E-07	6328125.	0.000					
576.000	0.0000	1.772E-05	6.917E-07	0.0000	437.6761	2.936E+10	-2.332E-07	6328125.	0.000					
582.000	0.0000	1.594E-05	-6.651E-07	0.0000	437.6761	2.936E+10	-1.211E-07	6328125.	0.000					
588.000	0.0000	9.789E-06	-1.057E-06	0.0000	437.6761	2.936E+10	-9.640E-09	6328125.	0.000					
594.000	0.0000	-2.792E-06	-8.188E-07	0.0000	437.6761	2.936E+10	-9.586E-07	6328125.	0.000					
600.000	0.0000	0.0000	0.0000	0.0000	437.6761	2.936E+10	1.837E-07	3164062.	0.000					

* The above values of total stress are combined axial and bending stress.

Output verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Pile-head deflection	=	0.5000000	inches
Computed slope at pile head	=	-0.0077255	radians
Maximum bending moment	=	2586656.	inch-lbs
Maximum shear force	=	60.0000000	inches below pile head
Depth of maximum bending moment	=	0.0000000	inches below pile head
Number of iterations	=	15	
Number of zero deflection points	=	9	

Computed values of Pile Loading and Deflection
For Lateral Loading for Load Case Number 3

		Pile-head conditions are Displacement and Moment (Loading Type 4)									
Depth X inches	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi ²	Bending Stiffness lb-in ²	Soil Res. lb/in	Soil Spr. lb/inch	Distrib. Lat/Lat lb/inch		
0.00	1.0000	0.000	114237.	-0.0138	437.6761	2.936E+10	-1531.3661	4594.1884	0.000		
6.00	0.9175	674292.	104602.	-0.0137	1431.2044	2.936E+10	-1680.2469	10998.0000	0.000		
12.00	0.8338	1827732.	144485.	-0.0135	2335.3316	2.936E+10	-1892.0036	36365.0000	0.000		
18.00	0.7557	1840047.	84312.	-0.0132	3149.2744	2.936E+10	-1699.1366	13490.0000	0.000		
24.00	0.6779	2330742.	74116.	-0.0127	3872.3968	2.936E+10	-1701.4786	15060.0000	0.000		
30.00	0.6029	2792627.	63909.	-0.0122	4504.4130	2.936E+10	-1698.8315	16907.0000	0.000		
36.00	0.5313	3126678.	53739.	-0.0116	5045.3268	2.936E+10	-1691.0645	19097.0000	0.000		
42.00	0.4635	3432092.	43622.	-0.0109	5495.4027	2.936E+10	-1677.9101	21377.0000	0.000		
48.00	0.4000	3672628.	33621.	-0.0102	5855.2334	2.936E+10	-1659.1586	24888.0000	0.000		
54.00	0.3409	3839821.	23740.	-0.009446	6125.7281	2.936E+10	-1634.5506	28765.0000	0.000		
60.00	0.2863	3935931.	14025.	-0.008645	6308.1260	2.936E+10	-1603.7863	33126.0000	0.000		
66.00	0.2372	4048662.	4514.1819	-0.007824	6404.0150	2.936E+10	-1566.5082	39624.0000	0.000		
72.00	0.1927	4056354.	-4752.1703	-0.006996	6415.3494	2.936E+10	-1522.2758	47387.0000	0.000		
78.00	0.1533	4008259.	-11721.	-0.006172	6344.4732	2.936E+10	-1470.5219	57140.0000	0.000		
84.00	0.1187	3906250.	-22374.	-0.005363	6194.1490	2.936E+10	-1410.4784	71035.0000	0.000		
90.00	0.0880	3755253.	-30626.	-0.004618	5967.5989	2.936E+10	-1341.0380	88143.0000	0.000		
96.00	0.0637	3549595.	-38433.	-0.003834	5668.5617	2.936E+10	-1260.4765	118679.0000	0.000		
102.00	0.0429	3300434.									

Bent 4L_transv_Max P

Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type No.		Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad., or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y =	0.2500	M = 0.000	198000.	0.25000000	1654133.	61042.	-0.00439415
2	4	y =	0.5000	M = 0.000	198000.	0.50000000	2588656.	83499.	-0.00772248
3	4	y =	1.0000	M = 0.000	198000.	1.00000000	4056354.	114237.	-0.01375038

The analysis ended normally.

SUPPORT: ABUTMENT 5R

LOAD DIRECTION: LONGITUDE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE

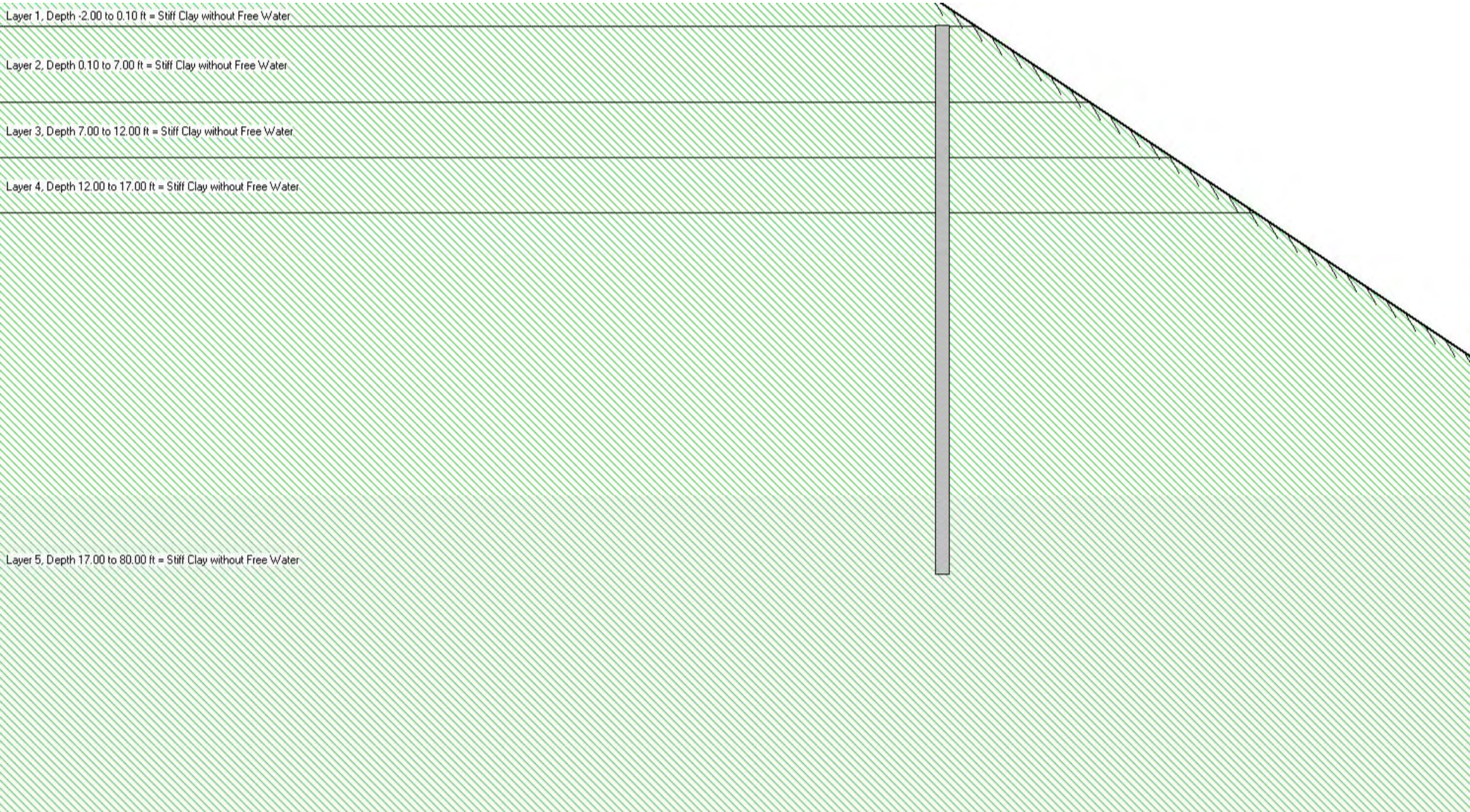
Layer 1, Depth -2.00 to 0.10 ft = Stiff Clay without Free Water

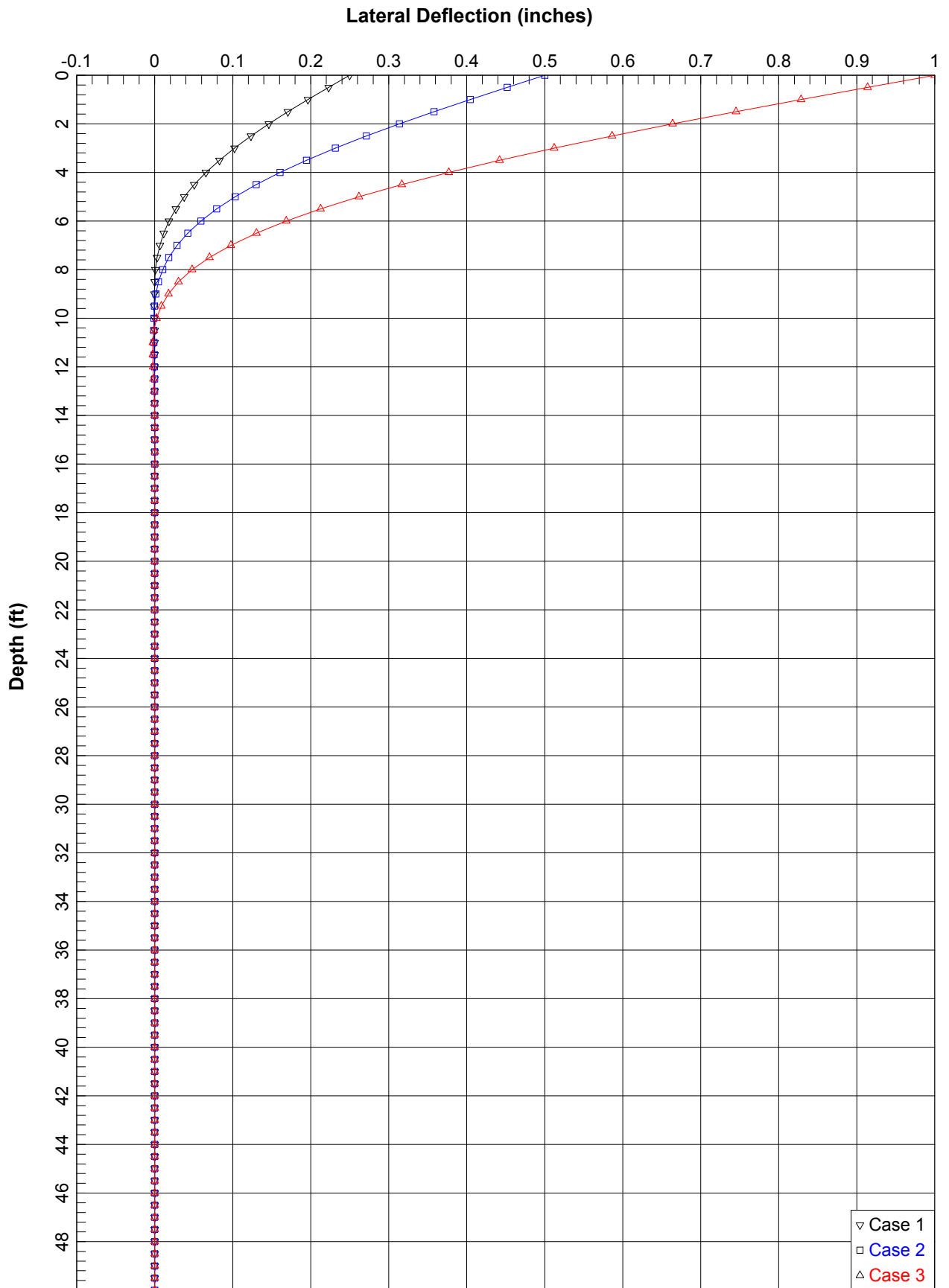
Layer 2, Depth 0.10 to 7.00 ft = Stiff Clay without Free Water

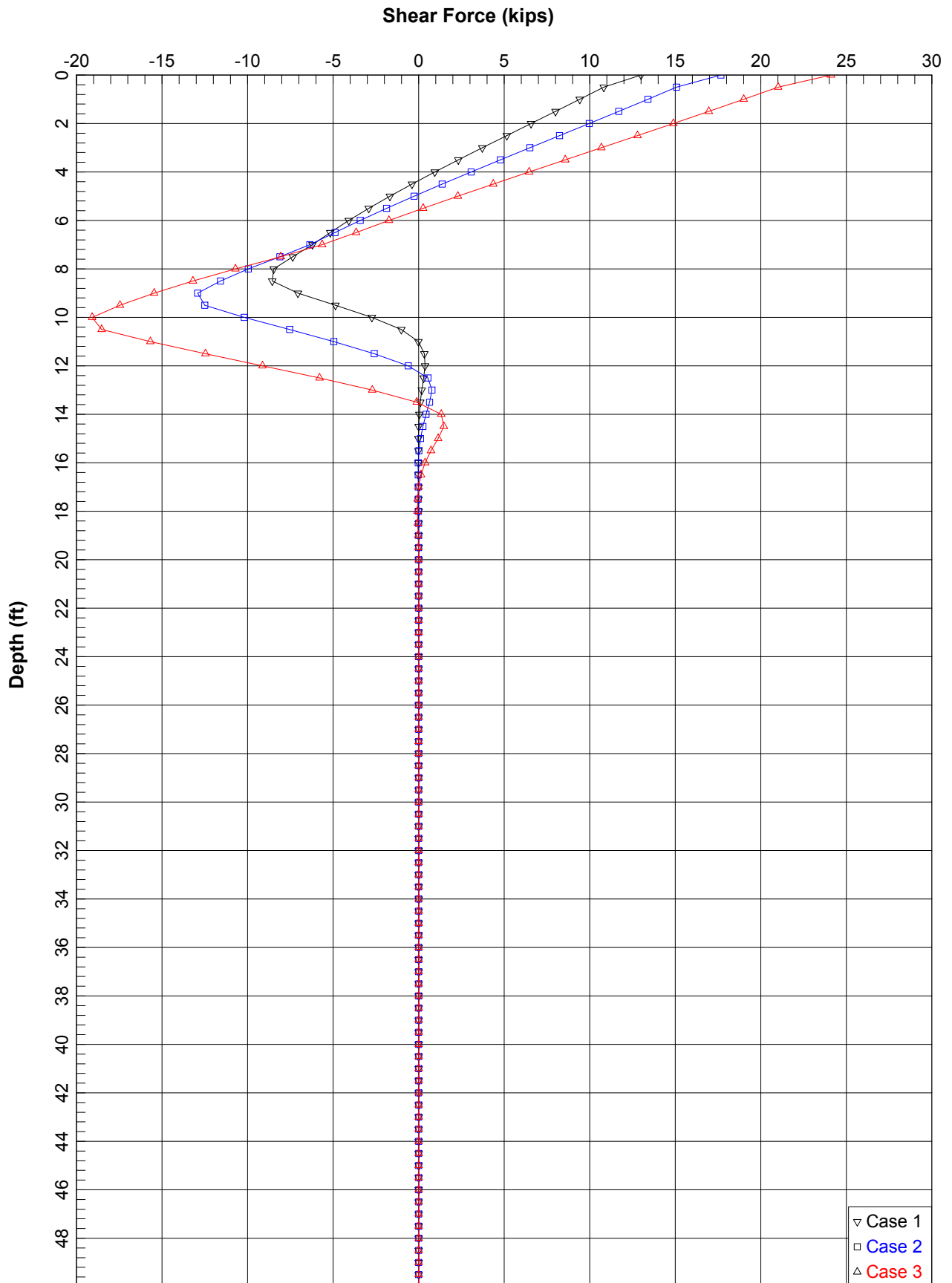
Layer 3, Depth 7.00 to 12.00 ft = Stiff Clay without Free Water

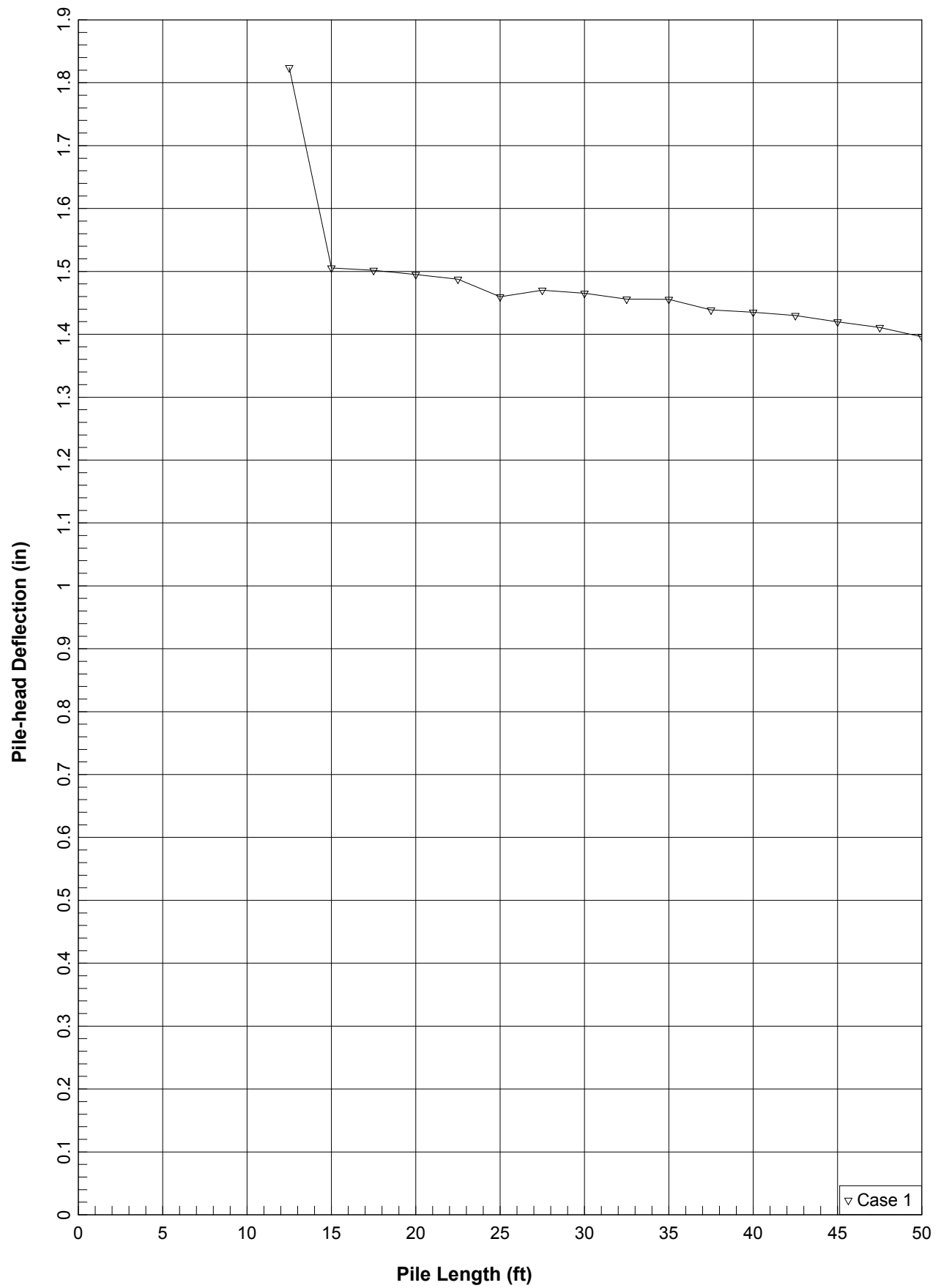
Layer 4, Depth 12.00 to 17.00 ft = Stiff Clay without Free Water

Layer 5, Depth 17.00 to 80.00 ft = Stiff Clay without Free Water









 Abut 5R_long_Critical Length

Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

 Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 5\
 Name of input data file: Abut 5R_long_Critical Length.lp6d
 Name of output report file: Abut 5R_long_Critical Length.lp6o
 Name of plot output file: Abut 5R_long_Critical Length.lp6p
 Name of runtime message file: Abut 5R_long_Critical Length.lp6r

 Date and Time of Analysis

Date: September 13, 2014 Time: 9:40:38

 Problem Title

Project Name: Palo Comado OC Bridge Widen

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

 Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

 Pile Structural Properties and Geometry

Page 1

 Abut 5R_long_Critical Length

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

 Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 16.0000000 in
 Bottom Width = 16.0000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

 Ground Slope and Pile Batter Angles

Ground Slope Angle = 33.700 degrees
 = 0.588 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

 Soil and Rock Layering Information

The soil profile is modelled using 5 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 7.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 7.00000 ft
 Distance from top of pile to bottom of layer = 12.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi

Page 2

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 12.00000 ft
 Distance from top of pile to bottom of layer = 17.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 17.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Uniaxial Elastic Mod.	ROD % or GSI
Num.	Epsilon 50	psi	ft	pcf	psf	deg.	psi	
1	0.00700	Stiff Clay w/o Free Water	2.000	120.000	4000.000			
2	0.00700	Stiff Clay w/o Free Water	0.10000	120.000	4000.000			
3	0.00700	Stiff Clay w/o Free Water	7.000	120.000	1500.000			
4	0.00700	Stiff Clay w/o Free Water	7.000	120.000	3500.000			
5	0.00500	Stiff Clay w/o Free Water	12.000	125.000	4000.000			
	0.00500	Stiff Clay w/o Free Water	17.000	125.000	4500.000			
	0.00500	Stiff Clay w/o Free Water	80.000	125.000	4500.000			

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X Ft	p-mult	y-mult
1	0.000	1.0000	1.0000
2	50.000	1.0000	1.0000

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Abut 5R_long_Critical Length

Number of loads specified = 1

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	V	28000. lbs	0.0000 in-lbs	157000.	True

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head = 28000.000 lbs
 Applied moment at pile head = 0.000 in-lbs
 Axial thrust load on pile head = 157000.000 lbs

Depth inches	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress lb-in ²	Bending Stiffness lb-in ²	Soil Res. lb/in	Spr. lb/inch	Distrib. Lat. Load lb/inch
0.00	1.3960	2.504E-07	28000.	-0.0190	780.8539	5.799E+09	-758.9903	1631.0111	0.000
6.00	1.2819	172259.	24643.	-0.0189	1637.6019	5.799E+09	-359.9358	1684.6973	0.000
12.00	1.1688	331393.	22459.	-0.0187	2429.0686	5.799E+09	-367.9781	1888.9689	0.000
18.00	1.0578	476957.	20231.	-0.0183	3153.0425	5.799E+09	-374.7666	2125.7301	0.000
24.00	0.9497	608564.	17966.	-0.0177	3807.6024	5.799E+09	-380.2403	2402.1720	0.000
30.00	0.8455	725889.	15672.	-0.0170	4391.1305	5.799E+09	-384.3357	2727.5280	0.000
36.00	0.7457	828671.	13359.	-0.0162	4902.3244	5.799E+09	-386.9863	3173.8092	0.000
42.00	0.6511	916713.	11033.	-0.0153	5340.2115	5.799E+09	-388.1217	3576.8641	0.000
48.00	0.5621	989890.	8705.8438	-0.0143	5704.1616	5.799E+09	-387.6661	4137.9413	0.000
54.00	0.4793	1048145.	6386.2344	-0.0133	5993.9016	5.799E+09	-385.5371	4826.0421	0.000
60.00	0.4030	1091500.	4084.6916	-0.0121	6209.5301	5.799E+09	-381.6439	5681.5578	0.000
66.00	0.3335	1120052.	1812.1046	-0.0110	6351.5342	5.799E+09	-375.8851	6762.0530	0.000
72.00	0.2710	1133980.	-419.9862	-0.009839	6420.8065	5.799E+09	-368.1452	8151.7690	0.000
78.00	0.2155	1133549.	-2599.2945	-0.008666	6418.6653	5.799E+09	-358.2909	9977.8284	0.000
84.00	0.1670	1119115.	-4860.4313	-0.007501	6346.8772	5.799E+09	-395.4213	14209.	0.000
90.00	0.1254	1089356.	-7629.1860	-0.006358	6198.8638	5.799E+09	-527.4969	25230.	0.000
96.00	0.0907	1039544.	-10725.	-0.005267	5951.1215	5.799E+09	-504.3965	33376.	0.000
102.00	0.0624	970561.	-13665.	-0.004217	5608.0278	5.799E+09	-475.7378	45772.	0.000
108.00	0.0401	883505.	-16414.	-0.003258	5175.0484	5.799E+09	-440.6331	65974.	0.000
114.00	0.0233	779726.	-18929.	-0.002397	4658.8909	5.799E+09	-397.4763	102484.	0.000
120.00	0.0113	660877.	-21149.	-0.001652	4067.7856	5.799E+09	-342.5852	181767.	0.000
126.00	0.003449	529051.	-22964.	-0.001036	3412.1368	5.799E+09	-262.6084	456802.	0.000
132.00	-0.001125	387255.	-22432.	-0.000562	2706.9035	5.799E+09	-440.2299	2347188.	0.000
138.00	-0.003296	260930.	-19382.	-0.000227	2078.6156	5.799E+09	576.2748	1049120.	0.000
144.00	-0.003846	155097.	-15728.	-0.000150	1552.2444	5.799E+09	641.7981	1001185.	0.000
150.00	-0.003434	72218.	-11806.	0.000106	1140.0348	5.799E+09	665.4631	1162787.	0.000
156.00	-0.002573	13224.	-7952.2590	0.000150	846.6259	5.799E+09	619.1487	1443789.	0.000
162.00	-0.001630	28230.	-4437.6651	0.000145	897.6970	5.799E+09	552.3826	2033146.	0.000
168.00	-0.000833	-40301.	-1379.3926	0.000112	981.2943	5.799E+09	467.0415	3366348.	0.000
174.00	-0.000286	-40256.	1008.6282	7.031E-05	981.0728	5.799E+09	328.9654	6894920.	0.000
180.00	1.064E-05	28330.	1976.9925	3.483E-05	921.7550	5.799E+09	-6.1173	3484581.	0.000
186.00	0.000132	-16598.	1722.9326	1.158E-05	863.4060	5.799E+09	-78.5093	3577858.	0.000
192.00	0.000150	-7676.4787	1212.7414	-9.757E-07	819.0336	5.799E+09	-91.5544	3671140.	0.000
198.00	0.000120	-2043.3493	712.3059	-6.004E-06	791.0167	5.799E+09	-75.2574	3764426.	0.000
204.00	7.758E-05	882.5049	325.8519	6.050E-06	785.2432	5.799E+09	-52.3173	4046127.	0.000
210.00	4.069E-05	1924.0777	79.3233	-5.153E-06	790.4235	5.799E+09	-31.1023	4586121.	0.000
216.00	1.575E-05	1844.0927	50.9814	-3.203E-06	790.0257	5.799E+09	-12.3326	4699310.	0.000
222.00	2.250E-06	1318.3358	-93.3934	-1.567E-06	787.4108	5.799E+09	-1.8047	4812503.	0.000
228.00	-3.061E-06	726.3247	-85.8924	5.995E-07	784.4664	5.799E+09	4.3050	8437500.	0.000
234.00	-3.863E-06	288.5867	-56.6785	1.563E-08	782.2893	5.799E+09	5.4329	8437500.	0.000
240.00	-2.874E-06	46.1534	-28.2556	1.888E-07	781.0835	5.799E+09	4.0413	8437500.	0.000
246.00	-1.598E-06	-50.8363	-9.3911	1.864E-07	781.1068	5.799E+09	2.2468	8437500.	0.000
252.00	-6.372E-07	-66.8914	0.0376	1.255E-07	781.1866	5.799E+09	0.8961	8437500.	0.000

Abut SR Long Critical Length									
258.000	-9.201E-08	-50.6217	3.1140	6.468E-08	781.1051	5.799E+09	0.1294	8437500.	0.000
264.000	1.389E-07	-29.6448	3.1128	2.315E-08	781.0014	5.799E+09	-0.1298	5604937.	0.000
270.000	1.858E-07	-13.3113	2.1922	9.292E-10	780.9201	5.799E+09	-0.1771	5718152.	0.000
276.000	1.501E-07	-3.3405	1.2233	-7.686E-09	780.8706	5.799E+09	-0.1459	5831369.	0.000
282.000	9.360E-08	1.3824	0.5075	-8.699E-09	780.8603	5.799E+09	-0.0927	5944587.	0.000
288.000	4.570E-08	2.7654	0.0908	-6.553E-09	780.8677	5.799E+09	-0.0461	6057807.	0.000
294.000	1.497E-08	2.4847	-0.0938	-3.837E-09	780.8663	5.799E+09	-0.0154	6171029.	0.000
300.000	-3.405E-10	1.6474	-0.1385	-1.699E-09	780.8621	5.799E+09	0.000479	6437500.	0.000
306.000	-5.420E-09	0.8257	-0.1142	-4.194E-10	780.8580	5.799E+09	0.007622	8437500.	0.000
312.000	-5.373E-09	0.2776	-0.0687	1.514E-10	780.8553	5.799E+09	0.007556	8437500.	0.000
318.000	-3.603E-09	0.001264	-0.0308	2.957E-10	780.8539	5.799E+09	0.005067	8437500.	0.000
324.000	-1.625E-09	-0.0927	-0.007914	2.484E-10	780.8544	5.799E+09	0.002566	8437500.	0.000
330.000	-6.220E-10	-0.0942	0.002408	1.517E-10	780.8544	5.799E+09	0.000875	8437500.	0.000
336.000	-3.985E-12	-0.0641	0.005049	6.986E-11	780.8543	5.799E+09	5.603E-06	8437500.	0.000
342.000	2.162E-10	-0.0337	0.004301	1.926E-11	780.8541	5.799E+09	-0.000255	7076854.	0.000
348.000	2.271E-10	-0.0125	0.002719	-4.653E-12	780.8540	5.799E+09	-0.000272	7190087.	0.000
354.000	1.604E-10	-0.001080	0.001317	-1.168E-11	780.8539	5.799E+09	-0.000195	7303321.	0.000
360.000	8.697E-11	0.003317	0.000408	-1.052E-11	780.8540	5.799E+09	-0.000107	7416557.	0.000
366.000	3.412E-11	0.003841	-4.253E-05	-6.821E-12	780.8540	5.799E+09	-4.281E-05	7529793.	0.000
372.000	5.110E-12	0.002819	-0.000191	-3.376E-12	780.8540	5.799E+09	-6.509E-06	7643030.	0.000
378.000	-6.394E-12	0.001561	-0.000183	-1.110E-12	780.8539	5.799E+09	8.991E-06	8437500.	0.000
384.000	-8.207E-12	0.000625	-0.000121	0.000	780.8539	5.799E+09	1.154E-05	8437500.	0.000
390.000	-6.143E-12	0.000103	-6.092E-05	0.000	780.8539	5.799E+09	8.638E-06	8437500.	0.000
396.000	-3.437E-12	-0.000107	-2.051E-05	0.000	780.8539	5.799E+09	4.834E-06	8437500.	0.000
402.000	-1.398E-12	-0.000144	-1.090E-07	0.000	780.8539	5.799E+09	1.966E-06	8437500.	0.000
408.000	0.000	-0.000109	6.843E-06	0.000	780.8539	5.799E+09	3.516E-07	8437500.	0.000
414.000	0.000	1.174E-05	6.967E-06	0.000	780.8539	5.799E+09	-3.105E-07	8435710.	0.000
420.000	0.000	-2.554E-05	4.734E-06	0.000	780.8539	5.799E+09	-4.337E-07	8437500.	0.000
426.000	0.000	-4.927E-06	2.432E-06	0.000	780.8539	5.799E+09	-3.339E-07	8437500.	0.000
432.000	0.000	3.670E-06	8.572E-07	0.000	780.8539	5.799E+09	-1.910E-07	8437500.	0.000
438.000	0.000	5.387E-06	4.342E-08	0.000	780.8539	5.799E+09	-8.023E-08	8437500.	0.000
444.000	0.000	4.211E-06	-2.467E-07	0.000	780.8539	5.799E+09	-1.647E-08	8437500.	0.000
450.000	0.000	2.437E-06	-2.645E-07	0.000	780.8539	5.799E+09	1.053E-08	8437500.	0.000
456.000	0.000	1.040E-06	-1.842E-07	0.000	780.8539	5.799E+09	1.624E-08	8437500.	0.000
462.000	0.000	2.269E-07	-9.685E-08	0.000	780.8539	5.799E+09	1.288E-08	8437500.	0.000
468.000	0.000	-1.229E-07	-3.561E-08	0.000	780.8539	5.799E+09	7.534E-09	8437500.	0.000
474.000	0.000	-2.014E-07	-3.217E-09	0.000	780.8539	5.799E+09	3.262E-09	8437500.	0.000
480.000	0.000	-1.623E-07	8.815E-09	0.000	780.8539	5.799E+09	7.487E-10	8437500.	0.000
486.000	0.000	-9.603E-08	1.002E-08	0.000	780.8539	5.799E+09	-3.480E-10	8437500.	0.000
492.000	0.000	-4.222E-08	7.155E-09	0.000	780.8539	5.799E+09	-6.062E-10	8437500.	0.000
498.000	0.000	-1.019E-08	3.849E-09	0.000	780.8539	5.799E+09	-4.959E-10	8437500.	0.000
504.000	0.000	3.997E-09	4.471E-09	0.000	780.8539	5.799E+09	-2.966E-10	8437500.	0.000
510.000	0.000	7.503E-09	1.846E-10	0.000	780.8539	5.799E+09	-1.322E-10	8437500.	0.000
516.000	0.000	6.242E-09	-3.118E-10	0.000	780.8539	5.799E+09	-3.329E-11	8437500.	0.000
522.000	0.000	3.777E-09	-3.784E-10	0.000	780.8539	5.799E+09	1.111E-11	8437500.	0.000
528.000	0.000	1.708E-09	-2.774E-10	0.000	780.8539	5.799E+09	2.254E-11	8437500.	0.000
534.000	0.000	4.489E-10	-1.526E-10	0.000	780.8539	5.799E+09	1.906E-11	8437500.	0.000
540.000	0.000	-1.245E-10	-6.048E-11	0.000	780.8539	5.799E+09	1.166E-11	8437500.	0.000
546.000	0.000	-2.783E-10	-9.488E-12	0.000	780.8539	5.799E+09	5.341E-12	8437500.	0.000
552.000	0.000	-2.395E-10	1.090E-11	0.000	780.8539	5.799E+09	-1.455E-12	8437500.	0.000
558.000	0.000	-1.482E-10	1.425E-11	0.000	780.8539	5.799E+09	0.000	8437500.	0.000
564.000	0.000	-6.880E-11	1.072E-11	0.000	780.8539	5.799E+09	0.000	8437500.	0.000
570.000	0.000	-1.957E-11	5.987E-12	0.000	780.8539	5.799E+09	0.000	8437500.	0.000
576.000	0.000	3.092E-12	2.370E-12	0.000	780.8539	5.799E+09	0.000	8437500.	0.000
582.000	0.000	8.927E-12	0.000	0.000	780.8539	5.799E+09	0.000	8437500.	0.000
588.000	0.000	6.718E-12	0.000	0.000	780.8539	5.799E+09	0.000	8437500.	0.000
594.000	0.000	2.451E-12	0.000	0.000	780.8539	5.799E+09	0.000	8437500.	0.000
600.000	0.000	0.000	0.000	0.000	780.8539	5.799E+09	0.000	4218750.	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Pile-head deflection = 1.3960487 inches
 Computed slope at pile head = -0.0190247 radians
 Maximum bending moment = 1133980. inch-lbs
 Maximum shear force = 28000. lbs
 Depth of maximum bending moment = 72.0000000 inches below pile head
 Depth of maximum shear force = 0.000000 inches below pile head
 Number of iterations = 35
 Number of zero deflection points = 13

Pile-head Deflection vs. Pile Length for Load Case 1

Boundary Condition Type 1, Shear and Moment

Shear = 28000. lbs
 Moment = 0. in-lbs
 Axial Load = 157000. lbs

Pile Length	Pile Head Deflection	Maximum Moment	Maximum Shear

feet	inches	In-lbs	Abut SR Long Critical Length lbs
50.000	1.3960487	1133980.	28000.
47.500	1.4108173	1137782.	28000.
45.000	1.4199638	1141270.	28000.
42.500	1.4298070	1144054.	28000.
40.000	1.4349594	1148183.	28000.
37.500	1.4388000	1152954.	28000.
35.000	1.4556777	1155589.	28000.
32.500	1.4558633	1160429.	28000.
30.000	1.4653221	1164174.	28000.
27.500	1.4702558	1168522.	28000.
25.000	1.4896166	1175571.	28000.
22.500	1.4875131	1176170.	28000.
20.000	1.4950895	1179975.	28000.
17.500	1.5018350	1184295.	28000.
15.000	1.5053539	1188996.	28000.
12.500	1.8238960	1158218.	-28914.

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	1	V = 28000.	M = 0.000	157000.	1.3960487	1133980.	28000.	-0.01902466

The analysis ended normally.

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Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 5
 Name of input data file: Abut 5R_long_Ave P.lpd
 Name of output report file: Abut 5R_long_Ave P.lpo
 Name of plot output file: Abut 5R_long_Ave P.lpp
 Name of runtime message file: Abut 5R_long_Ave P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 9:30:36

Problem Title

Project Name: Palo Comado OC Bridge Widened

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

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Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 16.0000000 in
 Bottom Width = 16.0000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 33.700 degrees
 = 0.588 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 5 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 7.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 7.00000 ft
 Distance from top of pile to bottom of layer = 12.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 12.00000 ft
 Distance from top of pile to bottom of layer = 17.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 17.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 130.00000 pcf
 Effective unit weight at bottom of layer = 130.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Rock Emass	Layer Depth ft	Effective Unit Wt. krm pcf	Undrained Cohesion Test psf	In-situ Friction Test deg.	Angle of Friction Property	Uniaxial Elastic Mod. psi	ROD % or GSI
1	0.00700	Stiff Clay w/o Free Water	--	-2.000	120.000	4000.000	--	--	--	--
2	0.00700	Stiff Clay w/o Free Water	--	0.10000	120.000	4000.000	--	--	--	--
3	0.00700	Stiff Clay w/o Free Water	--	7.000	120.000	1500.000	--	--	--	--
4	0.00700	Stiff Clay w/o Free Water	--	12.000	125.000	4000.000	--	--	--	--
5	0.00500	Stiff Clay w/o Free Water	--	17.000	130.000	4000.000	--	--	--	--
	0.00500		--	80.000	130.000	4000.000	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X Ft	p-mult	y-mult
1	0.000	1.0000	1.0000
2	50.000	1.0000	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

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Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4 y =	0.25000 in	M = 0.0000 in-lbs	157000.	False
2	4 y =	0.50000 in	M = 0.0000 in-lbs	157000.	False
3	4 y =	1.00000 in	M = 0.0000 in-lbs	157000.	False

V = perpendicular shear force applied to pile head

M = bending moment applied to pile head

y = lateral deflection relative to pile axis

S = pile slope relative to original pile batter angle

R = rotational stiffness applied to pile head

Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection

For Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.250000 inches

Moment at pile head = 0.000 in-lbs

Axial load at pile head = 157000.000 lbs

Depth X inches	Deflect. Y inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil Res. p lb/in	Soil Spr. Es ^h lb/inch	Distrib. Lat. Load lb/inch
0.00	0.2500	0.000	13005.	-0.004496	780.8539	5.799E+09	-493.7350	5924.8206	0.000
6.000	0.2230	-73377	10826.	-0.004458	1145.7991	5.799E+09	-232.4603	6253.8493	0.000
12.000	0.1965	138313.	9421.9233	-0.004348	1468.7667	5.799E+09	-235.6292	7194.6133	0.000
18.000	0.1708	194632.	8002.2910	-0.004176	1748.8745	5.799E+09	-237.5815	8343.8304	0.000
24.000	0.1464	242208.	6574.7830	-0.003950	1985.5000	5.799E+09	-238.2545	9765.1496	0.000
30.000	0.1234	280972.	5147.2757	-0.003679	2178.2920	5.799E+09	-237.5813	11548.	0.000
36.000	0.1022	310908.	3728.0617	-0.003373	2327.1831	5.799E+09	-235.4900	13820.000	0.000
42.000	0.0830	332064.	2325.8873	-0.003041	2432.4026	5.799E+09	-231.9014	16772.000	0.000
48.000	0.0657	344547.	950.0048	-0.002691	2494.4906	5.799E+09	-226.7260	20690.000	0.000
54.000	0.0507	348533.	-389.7529	-0.002332	2514.3132	5.799E+09	-219.8599	26031.000	0.000
60.000	0.0378	344264.	-1682.8639	-0.001974	2493.0803	5.799E+09	-211.1772	33551.000	0.000
66.000	0.0270	332056.	-2917.9512	-0.001624	2432.3674	5.799E+09	-200.5186	44572.000	0.000
72.000	0.0183	312307.	-4082.5121	-0.001290	2334.1420	5.799E+09	-187.6684	61593.000	0.000
78.000	0.0115	285497.	-5162.4400	-0.000981	2200.8068	5.799E+09	-172.3076	89827.000	0.000
84.000	0.006509	252206.	-6206.7531	-0.000703	2035.2239	5.799E+09	-175.7968	162039.000	0.000
90.000	0.003075	212340.	-7360.9239	-0.000462	1836.9481	5.799E+09	-208.9268	407607.000	0.000
96.000	0.000960	164746.	-8474.2534	-0.000267	1600.2347	5.799E+09	-162.1831	1013989.000	0.000
102.000	-0.000133	111153.	-8558.8236	-0.000125	1333.6838	5.799E+09	133.9930	6033055.000	0.000
108.000	-0.000536	62275.	-7062.0025	-3.492E-05	1090.5855	5.799E+09	364.9474	4084377.000	0.000
114.000	-0.000552	26475.	-4863.4884	1.099E-05	912.5288	5.799E+09	367.8907	3996363.000	0.000
120.000	-0.000404	3892.6514	-2739.0138	2.670E-05	800.2144	5.799E+09	340.2675	5050992.000	0.000
126.000	-0.000232	-6443.6678	-1018.7013	2.538E-05	812.9021	5.799E+09	233.1700	6033055.000	0.000
132.000	-9.959E-05	-8379.5871	-18.7732	1.771E-05	822.5306	5.799E+09	100.1394	6033055.000	0.000
138.000	-1.931E-05	-6702.3215	339.9017	9.912E-06	814.1886	5.799E+09	19.4189	6033055.000	0.000
144.000	1.936E-05	-4319.4417	368.5030	4.210E-06	802.3371	5.799E+09	-9.8851	3064339.000	0.000
150.000	3.121E-05	-2288.2165	286.5364	7.913E-07	792.2346	5.799E+09	-17.4371	3326219.000	0.000
156.000	2.885E-05	-882.4958	184.5161	-8.491E-07	785.2431	5.799E+09	-16.5697	3445901.000	0.000
162.000	2.027E-05	-72.4237	97.6151	-1.343E-06	781.2141	5.799E+09	-12.3973	3529189.000	0.000
168.000	1.273E-05	291.4159	37.2958	-2.300E-06	782.3033	5.799E+09	-7.7091	3632480.000	0.000
174.000	6.259E-06	377.4433	2.5081	-8.838E-07	782.7312	5.799E+09	-3.8868	3725775.000	0.000
180.000	2.128E-06	323.1784	-13.2163	-5.213E-07	782.4613	5.799E+09	-1.3547	3819074.000	0.000
186.000	3.640E-05	219.8304	-17.2874	-2.404E-07	781.9473	5.799E+09	-0.002373	3912376.000	0.000
192.000	-7.562E-07	116.1827	-14.6875	-6.653E-08	781.4318	5.799E+09	0.8690	6894920.000	0.000
198.000	-7.947E-07	43.7053	9.3408	1.619E-08	781.0713	5.799E+09	0.9133	6894920.000	0.000
204.000	-5.619E-07	4.0630	-4.5876	4.090E-08	780.8741	5.799E+09	0.6711	7165821.000	0.000
210.000	-3.039E-07	-11.4235	-1.4347	3.710E-08	780.9108	5.799E+09	0.3799	7500000.000	0.000
216.000	-1.168E-07	-13.2236	0.1428	2.434E-08	780.9197	5.799E+09	0.1460	7500000.000	0.000
222.000	-1.177E-08	-9.7556	0.6249	1.245E-08	780.9025	5.799E+09	0.0147	7500000.000	0.000
228.000	3.268E-08	-5.7483	0.5935	4.434E-09	780.8255	5.799E+09	-0.0252	4625398.000	0.000
234.000	4.143E-08	-2.6423	0.4200	9.276E-11	780.8671	5.799E+09	-0.0326	4727130.000	0.000

Abut SR_Long_Ave P									
240.000	3.379E-08	-0.7089	0.2405	-1.641E-10	780.8539	5.799E-09	-0.0272	4828868.	0.000
246.000	2.174E-08	0.2462	0.1053	-1.880E-09	780.8552	5.799E-09	-0.0179	4930216.	0.000
252.000	1.122E-08	0.5579	0.0234	-1.464E-09	780.8567	5.799E-09	-0.009414	5032360.	0.000
258.000	4.169E-09	0.5301	-0.0155	-9.015E-10	780.8566	5.799E-09	-0.003567	5134113.	0.000
264.000	4.051E-10	0.3734	-0.0273	-4.341E-10	780.8558	5.799E-09	-0.003353	5235871.	0.000
270.000	-1.040E-09	0.2037	-0.0244	-1.355E-10	780.8550	5.799E-09	0.001300	5300000.	0.000
276.000	-1.221E-09	0.0805	-0.0160	-1.148E-11	780.8543	5.799E-09	0.001526	5300000.	0.000
282.000	-9.024E-10	0.0122	-0.007950	5.943E-11	780.8540	5.799E-09	0.001128	5300000.	0.000
288.000	-5.080E-10	-0.0155	-0.002700	5.771E-11	780.8540	5.799E-09	0.000635	5300000.	0.000
294.000	-2.099E-10	-0.0203	-0.00268	-0.929E-10	780.8540	5.799E-09	0.000262	5300000.	0.000
300.000	-3.789E-11	-0.0157	0.000921	2.056E-11	780.8540	5.799E-09	4.737E-05	5300000.	0.000
306.000	6.678E-11	-0.009308	0.000954	7.631E-12	780.8540	5.799E-09	-3.647E-05	5948278.	0.000
312.000	5.368E-11	-0.004244	0.000682	0.0000	780.8540	5.799E-09	-5.412E-05	6050063.	0.000
318.000	4.422E-11	-0.001125	0.000384	-2.158E-12	780.8539	5.799E-09	-4.534E-05	6151851.	0.000
324.000	2.778E-11	0.000363	0.000161	-2.552E-12	780.8539	5.799E-09	-2.895E-05	6253641.	0.000
330.000	1.359E-11	0.000809	3.069E-05	-1.945E-12	780.8539	5.799E-09	-1.440E-05	6355433.	0.000
336.000	4.433E-12	0.0000735	-2.683E-05	-1.146E-12	780.8539	5.799E-09	-4.771E-06	6457228.	0.000
342.000	0.000	0.000489	-4.053E-05	0.000	780.8539	5.799E-09	2.038E-07	7500000.	0.000
348.000	-1.722E-12	0.000250	-3.346E-05	0.000	780.8539	5.799E-09	2.153E-06	7500000.	0.000
354.000	-1.730E-12	8.794E-05	-2.051E-05	0.000	780.8539	5.799E-09	2.162E-06	7500000.	0.000
360.000	-1.191E-12	3.678E-06	-9.562E-06	0.000	780.8539	5.799E-09	1.489E-06	7500000.	0.000
366.000	0.000	-2.698E-05	-2.734E-06	0.000	780.8539	5.799E-09	7.872E-07	7500000.	0.000
372.000	0.000	-2.928E-05	5.119E-07	0.000	780.8539	5.799E-09	2.949E-07	7500000.	0.000
378.000	0.000	-2.094E-05	1.486E-06	0.000	780.8539	5.799E-09	2.984E-08	7500000.	0.000
384.000	0.000	-1.150E-05	1.364E-06	0.000	780.8539	5.799E-09	-7.051E-08	7271654.	0.000
390.000	0.000	-4.584E-06	8.986E-07	0.000	780.8539	5.799E-09	-8.461E-08	7373464.	0.000
400.000	0.000	-1.722E-07	-4.539E-08	0.000	780.8539	5.799E-09	-6.362E-08	7475276.	0.000
406.000	0.000	8.695E-07	-1.548E-07	0.000	780.8539	5.799E-09	-3.608E-08	7500000.	0.000
412.000	0.000	1.152E-06	1.374E-09	0.000	780.8539	5.799E-09	-1.507E-08	7500000.	0.000
418.000	0.000	8.901E-07	-5.280E-08	0.000	780.8539	5.799E-09	-2.993E-09	7500000.	0.000
424.000	0.000	-4.350E-08	-1.083E-09	0.000	780.8539	5.799E-09	2.173E-09	7500000.	0.000
430.000	0.000	2.277E-07	-3.884E-08	0.000	780.8539	5.799E-09	3.303E-09	7500000.	0.000
436.000	0.000	5.408E-08	-2.093E-08	0.000	780.8539	5.799E-09	2.665E-09	7500000.	0.000
442.000	0.000	-2.367E-08	-8.112E-09	0.000	780.8539	5.799E-09	1.608E-09	7500000.	0.000
448.000	0.000	-4.350E-08	-1.083E-09	0.000	780.8539	5.799E-09	7.548E-10	7500000.	0.000
454.000	0.000	-3.684E-08	1.718E-09	0.000	780.8539	5.799E-09	1.989E-09	7500000.	0.000
460.000	0.000	-2.988E-08	2.162E-09	0.000	780.8539	5.799E-09	-5.102E-11	7500000.	0.000
466.000	0.000	-1.094E-08	1.641E-09	0.000	780.8539	5.799E-09	-1.226E-10	7500000.	0.000
472.000	0.000	-3.296E-09	9.452E-10	0.000	780.8539	5.799E-09	-1.093E-10	7500000.	0.000
478.000	0.000	4.118E-10	4.057E-10	0.000	780.8539	5.799E-09	-7.048E-11	7500000.	0.000
484.000	0.000	1.582E-09	8.981E-11	0.000	780.8539	5.799E-09	-3.482E-11	7500000.	0.000
490.000	0.000	-1.497E-09	-4.835E-11	0.000	780.8539	5.799E-09	-1.143E-11	7500000.	0.000
496.000	0.000	9.988E-10	-8.225E-11	0.000	780.8539	5.799E-09	0.000	7500000.	0.000
502.000	0.000	5.119E-10	-6.818E-11	0.000	780.8539	5.799E-09	4.354E-12	7500000.	0.000
508.000	0.000	1.812E-10	-4.192E-11	0.000	780.8539	5.799E-09	4.399E-12	7500000.	0.000
514.000	0.000	8.628E-12	-1.951E-11	0.000	780.8539	5.799E-09	3.039E-12	7500000.	0.000
520.000	0.000	-5.451E-11	-5.658E-12	0.000	780.8539	5.799E-09	1.612E-12	7500000.	0.000
526.000	0.000	-5.958E-11	0.000	0.000	780.8539	5.799E-09	0.000	7500000.	0.000
532.000	0.000	-4.271E-11	3.019E-12	0.000	780.8539	5.799E-09	0.000	7500000.	0.000
538.000	0.000	-2.344E-11	2.782E-12	0.000	780.8539	5.799E-09	0.000	7500000.	0.000
544.000	0.000	-9.359E-12	1.829E-12	0.000	780.8539	5.799E-09	0.000	7500000.	0.000
550.000	0.000	-1.498E-12	0.000	0.000	780.8539	5.799E-09	0.000	7500000.	0.000
556.000	0.000	-1.724E-12	0.000	0.000	780.8539	5.799E-09	0.000	7500000.	0.000
562.000	0.000	2.312E-12	0.000	0.000	780.8539	5.799E-09	0.000	7500000.	0.000
568.000	0.000	1.794E-12	0.000	0.000	780.8539	5.799E-09	0.000	7500000.	0.000
574.000	0.000	1.053E-12	0.000	0.000	780.8539	5.799E-09	0.000	7500000.	0.000
580.000	0.000	0.000	0.000	0.000	780.8539	5.799E-09	0.000	7500000.	0.000
586.000	0.000	0.000	0.000	0.000	780.8539	5.799E-09	0.000	7500000.	0.000
592.000	0.000	0.000	0.000	0.000	780.8539	5.799E-09	0.000	7500000.	0.000
598.000	0.000	0.000	0.000	0.000	780.8539	5.799E-09	0.000	7500000.	0.000
604.000	0.000	0.000	0.000	0.000	780.8539	5.799E-09	0.000	3750000.	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Pile-head deflection	=	0.2500000 inches
Computed slope at pile head	=	-0.0044959 radians
Maximum bending moment	=	348533.3 inch-lbs
Maximum shear force	=	13005.5 lbs
Depth of maximum bending moment	=	54.000000 inches below pile head
Depth of maximum shear force	=	0.000000 inches below pile head
Number of iterations	=	14
Number of zero deflection points	=	14

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)	=	0.500000 inches
Displacement of pile head	=	0.000 inches
Moment at pile head	=	1570000.0 lbs
Axial load at pile head	=	1570000.0 lbs

Depth y inches	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Abut SR_Long_Ave P Stress psi*	Bending Stiffness lb-in ²	Soil Res. p lb/in	Soil Spr. Es* lb/inch	Distri b. Lat. Load lb/inch
0.00	0.5000	0.000	17669.	-0.008019	780.8539	5.799E-09	-55.1552	3522.9194	0.000
6.00	0.4519	102999.	15076.	-0.007966	1293.1296	5.799E-09	-277.3429	3682.4736	0.000
12.00	0.4044	195914.	13397.	-0.007811	1755.2479	5.799E-09	-282.2212	4187.1461	0.000
18.00	0.3582	278477.	11693.	-0.007566	2165.8850	5.799E-09	-285.8754	4789.1697	0.000
24.00	0.3136	350478.	9970.1645	-0.007240	2523.9862	5.799E-09	-288.2436	5514.4652	0.000
30.00	0.2713	411760.	8237.6506	-0.006846	2828.7786	5.799E-09	-289.2610	6397.9524	0.000
36.00	0.2315	462227.	6503.2914	-0.006394	3079.7828	5.799E-09	-288.8587	7487.5364	0.000
42.00	0.1945	501845.	4775.8292	-0.005895	3276.8263	5.799E-09	-286.9621	8850.3021	0.000
48.00	0.1607	530643.	3064.4759	-0.005361	3420.0565	5.799E-09	-283.4891	10282.	0.000
54.00	0.1302	548718.	1378.9662	-0.004802	3509.9558	5.799E-09	-278.3475	11686.	0.000
60.00	0.1031	556238.	-270.3690	-0.004231	3547.3571	5.799E-09	-271.4309	15796.	0.000
66.00	0.0794	553445.	-1872.5013	-0.003657	3533.4623	5.799E-09	-262.6132	19833.	0.000
72.00	0.0592	540657.	-3415.5581	-0.003091	3469.8637	5.799E-09	-251.7391	25504.	0.000
78.00	0.0428	518281.	-4886.6034	-0.002543	3358.5705	5.799E-09	-238.6094	33798.	0.000
84.00	0.0287	486809.	-6366.4661	-0.002023	3202.0419	5.799E-09	-254.6782	53222.	0.000
90.00	0.0181	445694.	-8105.9249	-0.001540	2997.5533	5.799E-09	-325.1414	107864.	0.000
96.00	0.0102	392439.	-9958.7302	-0.001107	2732.6878	5.799E-09	-292.4604	171562.	0.000
102.00	0.004807	328274.	-11589.	-0.000734	2413.5549	5.799E-09	-250.9200	313226.	0.000
108.00	0.001423	254755.	-12917.	-0.000432	2047.9036	5.799E-09	-191.8776	809111.	0.000
114.00	-0.000379	174081.	-12496.	-0.000210	1646.6618	5.799E-09	-332.2398	5257853.	0.000
120.00	-0.001100	105197.	-10189.	-6.578E-05	1304.0633	5.799E-09	436.8696	3282083.	0.000
126.00	-0.001169	51939.	-7546.7088	1.551E-05	1039.1760	5.799E-09	443.8438	2278970.	0.000
132.00	-0.00314	14608.	-4968.5042	4.995E-05	819.5249	5.799E-09	117.5283	2140187.	0.000
138.00	-0.000649	-7706.4653	-2597.2518	5.351E-05	591.8228	5.799E-09	370.9127	3099676.	0.000
144.00	-0.000272	-16660.	-605.1255	4.091E-05	483.7144	5.799E-09	293.1255	6463988.	0.000
150.00	-7.837E-05	-15045.	544.4190	2.450E-05	855.6814	5.799E-09	90.0538	6894920.	0.000
156.00	-2.195E-05	10173.	778.2368	1.144E-05	783.4514	5.799E-09	-12.1152	7391758.	0.000
162.00	5.911E-05	-5727.7266	641.2616	3.229E-06	809.3413	5.799E-09	-33.5425	3405033.	0.000
168.00	6.070E-05	-4844.1724	434.						

Abut	SR	long	Ave	P	780.8539	5.799E+09	6.437E-12	7500000.	0.000
522.000	0.000	6.708E-11	-4.545E-11	0.000	780.8539	5.799E+09	6.437E-12	7500000.	0.000
528.000	0.000	-9.014E-11	-1.529E-11	0.000	780.8539	5.799E+09	3.618E-12	7500000.	0.000
534.000	0.000	-1.170E-10	0.000	0.000	780.8539	5.799E+09	1.499E-12	7500000.	0.000
540.000	0.000	-8.982E-11	5.420E-12	0.000	780.8539	5.799E+09	0.000	7500000.	0.000
546.000	0.000	-5.219E-11	5.601E-12	0.000	780.8539	5.799E+09	0.000	7500000.	0.000
550.000	0.000	-2.268E-11	3.913E-12	0.000	780.8539	5.799E+09	0.000	7500000.	0.000
558.000	0.000	-5.249E-12	2.096E-12	0.000	780.8539	5.799E+09	0.000	7500000.	0.000
564.000	0.000	2.495E-12	0.000	0.000	780.8539	5.799E+09	0.000	7500000.	0.000
570.000	0.000	4.413E-12	0.000	0.000	780.8539	5.799E+09	0.000	7500000.	0.000
576.000	0.000	3.676E-12	0.000	0.000	780.8539	5.799E+09	0.000	7500000.	0.000
582.000	0.000	2.227E-12	0.000	0.000	780.8539	5.799E+09	0.000	7500000.	0.000
588.000	0.000	0.000	0.000	0.000	780.8539	5.799E+09	0.000	7500000.	0.000
594.000	0.000	0.000	0.000	0.000	780.8539	5.799E+09	0.000	7500000.	0.000
600.000	0.000	0.000	0.000	0.000	780.8539	5.799E+09	0.000	3750000.	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Pile-head deflection = 0.5000000 inches
 Computed slope at pile head = -0.0080190 radians
 Maximum bending moment = 556238. inch-lbs
 Maximum shear force = 766.0 lbs
 Depth of maximum bending moment = 60.000000 inches below pile head
 Depth of maximum shear force = 0.000000 inches below pile head
 Number of iterations = 20
 Number of zero deflection points = 13

Computed Values of Pile Loading and Deflection
 For Lateral Loading for Load Case Number 3

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 1.000000 inches
 Moment at pile head = 0.000000 in-lbs
 Axial load at pile head = 157000.000 lbs

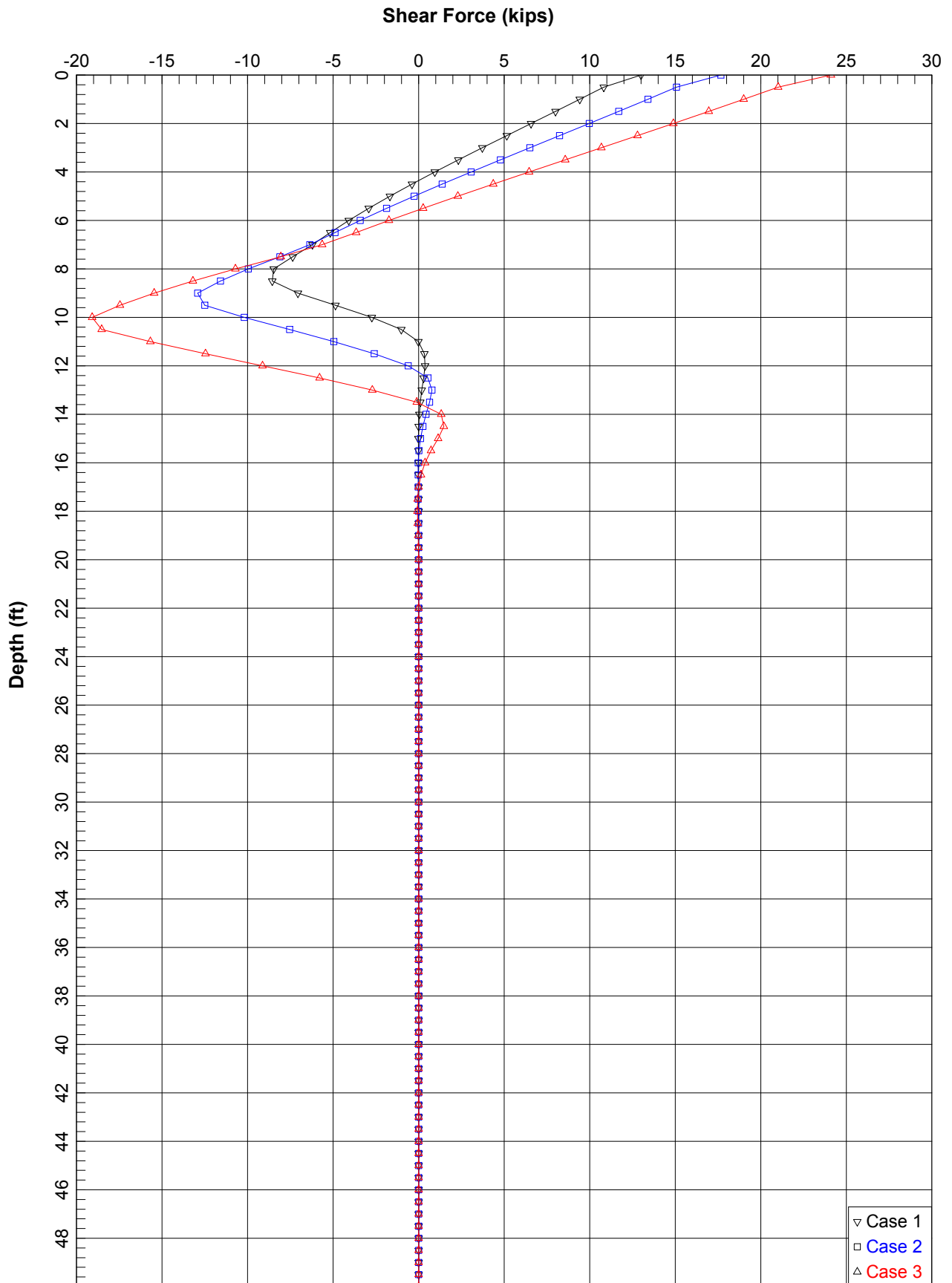
Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil Res.	Soil Spr.	Distrib.
x	y	Moment	Force	S	Stiffness	Stiffness	p	E*s ^h	Lat. Load
inches	inches	in-lbs	lbs	radians	psi*	lb/in ²	lb/in	lb/inch	lb/inch
0.00	1.0000	0.000	24095.	-0.0144	780.8539	5.799E+09	-698.2468	2094.7404	0.000
6.00	0.9138	145529.	21008.	-0.0143	1504.6582	5.799E+09	-330.7329	2171.4860	0.000
12.00	0.8286	279011.	19003.	-0.0141	2168.5394	5.799E+09	-337.6510	2445.0054	0.000
18.00	0.7451	400065.	16960.	-0.0137	2770.6119	5.799E+09	-343.3267	2764.7931	0.000
24.00	0.6640	508369.	14887.	-0.0132	3309.2725	5.799E+09	-347.6985	3141.7077	0.000
30.00	0.5861	603660.	12792.	-0.0127	3783.2134	5.799E+09	-350.7027	3589.8957	0.000
36.00	0.5120	685738.	10683.	-0.0120	4191.4349	5.799E+09	-352.2718	4128.0553	0.000
42.00	0.4421	754466.	8569.1703	-0.0113	4533.2579	5.799E+09	-352.3339	4781.3007	0.000
48.00	0.3769	809774.	6459.7350	-0.0104	4808.3383	5.799E+09	-350.8112	5583.9802	0.000
54.00	0.3168	851663.	4364.4461	-0.009587	5016.6806	5.799E+09	-347.6184	6584.0434	0.000
60.00	0.2619	880209.	2293.6112	-0.008691	5158.6533	5.799E+09	-342.6599	7850.0150	0.000
66.00	0.2125	895560.	258.1507	-0.007772	5235.0059	5.799E+09	-335.8270	9482.5149	0.000
72.00	0.1686	897949.	-1730.3100	-0.006844	5246.8874	5.799E+09	-326.9533	11634.	0.000
78.00	0.1304	887691.	-3659.3159	-0.005920	5195.8678	5.799E+09	-316.0087	14545.	0.000
84.00	0.0976	865192.	-5644.6205	-0.005014	5083.9638	5.799E+09	-345.7595	21257.	0.000
90.00	0.0702	829401.	-8050.7033	-0.004137	4905.9574	5.799E+09	-456.2681	38998.	0.000
96.00	0.0480	776377.	-10710.	-0.003306	4642.2358	5.799E+09	-430.1768	53825.	0.000
102.00	0.0305	707109.	-13195.	-0.002539	4297.7276	5.799E+09	-397.9951	78226.	0.000
108.00	0.0175	622825.	-15463.	-0.001850	3878.5306	5.799E+09	-358.2484	122896.	0.000
114.00	0.008321	525036.	-17461.	-0.001257	3392.1702	5.799E+09	-307.5414	221764.	0.000
120.00	0.002411	415664.	-19083.	-0.000770	2848.1995	5.799E+09	-233.2477	580484.	0.000
126.00	-0.000918	297491.	-18533.	-0.000401	2260.4508	5.799E+09	416.7335	2722557.	0.000
132.00	-0.002401	194029.	-15687.	-0.000147	1745.8758	5.799E+09	531.6378	1328668.	0.000
138.00	-0.002679	109518.	-12453.	1.037E-05	1325.5495	5.799E+09	546.6130	1224431.	0.000
144.00	-0.002276	44577.	-9125.7878	9.009E-05	1002.5630	5.799E+09	562.3568	1482245.	0.000
150.00	-0.001597	-161.6326	-5791.7868	0.000113	781.6578	5.799E+09	548.9769	2061939.	0.000
156.00	-0.000920	-25137.	-2710.6414	9.998E-05	605.8761	5.799E+09	478.0716	3119392.	0.000
162.00	-0.000398	-32878.	-113.9437	6.997E-05	444.3742	5.799E+09	387.4943	5846051.	0.000
168.00	-7.997E-05	-26636.	1324.2195	3.917E-05	313.3322	5.799E+09	91.8934	6894920.	0.000
174.00	7.240E-05	-17061.	1474.7261	1.657E-05	865.7077	5.799E+09	-41.7245	3457929.	0.000
180.00	0.000184	-8910.0024	1135.5360	3.099E-06	825.4512	5.799E+09	-30.3288	3551207.	0.000
186.00	0.000110	-3404.2702	727.8161	3.303E-06	797.7854	5.799E+09	-66.5678	3644490.	0.000
192.00	7.921E-05	-230.8231	380.0841	-5.184E-06	782.0020	5.799E+09	-49.3429	3737776.	0.000
198.00	4.739E-05	1166.5047	141.2809	-4.700E-06	786.6557	5.799E+09	-30.2582	3831066.	0.000
204.00	2.281E-05	1473.4011	5.8031	-3.334E-06	798.1820	5.799E+09	-14.9011	3919175.	0.000
210.00	7.384E-06	1242.4225	-54.4198	-1.929E-06	787.0332	5.799E+09	-5.1732	4203635.	0.000
216.00	-3.313E-07	823.9971	-68.6969	-8.596E-07	784.9522	5.799E+09	0.4142	4506500.	0.000
222.00	-2.931E-06	419.6785	-56.4636	-2.161E-07	782.9412	5.799E+09	3.6636	7500000.	0.000
228.00	-2.925E-06	146.8414	-4.5041	7.696E-08	781.5843	5.799E+09	3.6542	7500000.	0.000
234.00	-2.007E-06	5.4840	-16.0079	1.558E-07	780.8812	5.799E+09	2.5092	7500000.	0.000
240.00	-1.056E-06	-45.5475	-4.5214	1.350E-07	781.0805	5.799E+09	1.3197	7500000.	0.000
246.00	-3.869E-07	-49.0271	0.8883	6.811E-08	781.0978	5.799E+09	0.4836	7500000.	0.000
252.00	-2.237E-08	-35.0505	2.4229	4.261E-08	781.0283	5.799E+09	0.0280	7500000.	0.000

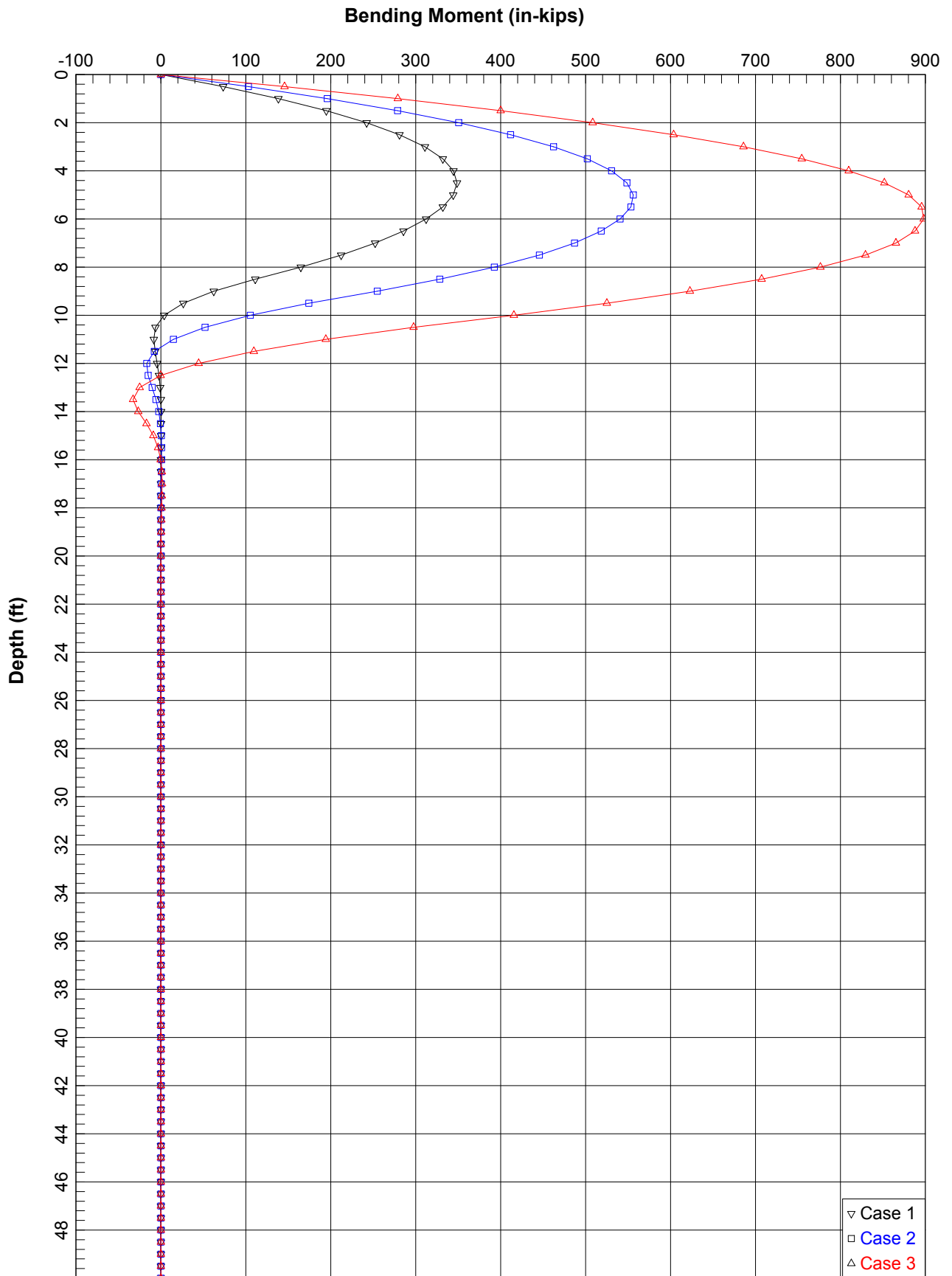
Abut	SR	long	Ave	P	780.8539	5.799E+09	-0.1041	5017404.	0.000
258.000	1.245E-07	-20.0330	2.1944	1.412E-10	780.8539	5.799E+09	-0.1041	5017404.	0.000
264.000	1.470E-07	-8.7444	1.5057	-7.728E-10	780.8974	5.799E+09	-0.1254	5119151.	0.000
270.000	1.152E-07	-1.9628	0.8286	-6.312E-09	780.8637	5.799E+09	-0.1003	52520902.	0.000
276.000	7.147E-08	1.2108	0.3381	-6.701E-09	780.8600	5.799E+09	-0.0632	5322658.	0.000
282.000	3.482E-08	2.1071	0.0540	-4.985E-09	780.8644	5.799E+09	-0.0315	5424419.	0.000
288.000	1.125E-08	1.8681	-0.0721	-2.928E-09	780.8632	5.799E+09	-0.0105	5526182.	0.000
294.000	-3.154E-10	1.2475	-0.1026	-1.316E-09	780.8601	5.799E+09	0.000394	7500000.	0.000
300.000	-4.340E-09	0.6398	-0.0851	-3.397E-10	780.8571	5.799E+09	0.005425	7500000.	0.000
306.000	-4.392E-09	0.2268	-0.0524	-1.086E-10	780.8551	5.799E+09	0.005490	7500000.	0.000
312.000	-3.036E-09	0.0113	-0.0245	-2.319E-10	780.8540	5.799E+09	0.003795	7500000.	0.000
318.000	-1.610E-09	-0.0676	-0.007080	2.027E-10	780.8543	5.799E+09	0.002012	7500000.	0.000
324.000	-6.036E-10	0.0740	0.001221	1.294E-10	780.8543	5.799E+09	0.000755	7500000.	0.000
330.000	-5.701E-11	-0.0532	0.003698	6.357E-11	780.8542	5.799E+09	7.124E-05	7500000.	0.000
336.000	1.592E-10	-0.0298	0.003407	2.062E-11	780.8541	5.799E+09	-0.000168	6340409.	0.000
342.000	1.905E-10	-0.0124	0.002289	-1.188E-12	780.8540	5.799E+09	-0.000205	6442199.	0.000
348.000	1.449E-10	-0.002314	0.001201	-8.787E-12	780.8540	5.799E+09	-0.000158	6543992.	0.000
354.000	8.504E-11	0.002057	0.000444	-8.920E-12	780.8539	5.799E+09	-9.420E-05	6645786.	0.000
360.000	3.791E-11	0.003035	3.389E-05	-6.285E-12	780.8540	5.799E+09	-4.263E-05	6747583.	0.000
366.000	9.620E-12	0.002476	-0.000127	-3.434E-12	780.8540	5.799E+09	-1.098E-05	6849382.	0.000
372.000	-3.300E-12	0.001518	-0.000148	-1.368E-12	780.8539	5.799E+09	4.125E-06	7500000.	0.000
378.000	-6.793E-12	0.000708	-0.000110	0.000	780.8539	5.799E+09	8.492E-06	7500000.	0.000
384.000	-5.892E-12	0.000203	-6.211E-05	0.000	780.8539	5.799E+09	7.365E-06	7500000.	0.000
390.000	-3.733E-12	-3.783E-05	-2.601E-05	0.000	780.8539	5.799E+09	4.666E-06	7500000.	0.000
396.000	-1.809E-12	-0.000110	-5.230E-06	0.000	780.8539	5.799E+09			

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Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 M = in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection in-lb	Maximum Moment in-lb	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	157000.	0.25000000	348533.	13005.	-0.00449590
2	4	y = 0.5000	M = 0.000	157000.	0.50000000	556238.	17669.	-0.00801905
3	4	y = 1.0000	M = 0.000	157000.	1.00000000	897949.	24095.	-0.01435949

The analysis ended normally.





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Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 5R
 Name of input data file: Abut 5R_long_Ave P.lpd
 Name of output report file: Abut 5R_long_Ave P.lpo
 Name of plot output file: Abut 5R_long_Ave P.lpp
 Name of runtime message file: Abut 5R_long_Ave P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 9:30:36

Problem Title

Project Name: Palo Comado OC Bridge Widened

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

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Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 16.0000000 in
 Bottom Width = 16.0000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 33.700 degrees
 = 0.588 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 5 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 7.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 7.00000 ft
 Distance from top of pile to bottom of layer = 12.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 12.00000 ft
 Distance from top of pile to bottom of layer = 17.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 17.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 130.00000 pcf
 Effective unit weight at bottom of layer = 130.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Rock Emass	Layer Depth ft	Effective Unit Wt. krm	Undrained Cohesion Test psf	In-situ Friction Test deg.	Angle of Friction Property	Uniaxial Elastic Mod. psi	ROD % or GSI
1	0.00700	Stiff Clay w/o Free Water	--	-2.000	120.000	4000.000	--	--	--	--
2	0.00700	Stiff Clay w/o Free Water	--	0.10000	120.000	4000.000	--	--	--	--
3	0.00700	Stiff Clay w/o Free Water	--	7.000	120.000	1500.000	--	--	--	--
4	0.00700	Stiff Clay w/o Free Water	--	12.000	125.000	4000.000	--	--	--	--
5	0.00500	Stiff Clay w/o Free Water	--	17.000	130.000	4000.000	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X Ft	p-mult	y-mult
1	0.000	1.0000	1.0000
2	50.000	1.0000	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

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Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4 y =	0.25000 in	M = 0.0000 in-lbs	157000.	False
2	4 y =	0.50000 in	M = 0.0000 in-lbs	157000.	False
3	4 y =	1.00000 in	M = 0.0000 in-lbs	157000.	False

V = perpendicular shear force applied to pile head

M = bending moment applied to pile head

y = lateral deflection relative to pile axis

S = pile slope relative to original pile batter angle

R = rotational stiffness applied to pile head

Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection

For Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.250000 inches

Moment at pile head = 0.000 in-lbs

Axial load at pile head = 157000.000 lbs

Depth X inches	Deflect. Y inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil Res. p lb/in	Soil Spr. Es ^h lb/inch	Distrib. Lat. Load lb/inch
0.00	0.2500	0.000	13005.	-0.004496	780.8539	5.799E+09	-493.7350	5924.8206	0.000
6.00	0.2230	-73377	10826.	-0.004458	1145.7991	5.799E+09	-232.4603	6253.8493	0.000
12.00	0.1965	138313.	9421.9233	-0.004348	1468.7667	5.799E+09	-235.6292	7194.6133	0.000
18.00	0.1708	194632.	8002.2910	-0.004176	1748.8745	5.799E+09	-237.5815	8343.8304	0.000
24.00	0.1464	242208.	6574.7830	-0.003950	1985.5000	5.799E+09	-238.2545	9765.1496	0.000
30.00	0.1234	280972.	5147.2757	-0.003679	2178.2920	5.799E+09	-237.5813	11548.	0.000
36.00	0.1022	310908.	3728.0617	-0.003373	2327.1831	5.799E+09	-235.4900	13820.000	0.000
42.00	0.0830	332064.	2325.8873	-0.003041	2432.4026	5.799E+09	-231.9014	16772.000	0.000
48.00	0.0657	344547.	950.0048	-0.002691	2494.4906	5.799E+09	-226.7260	20690.000	0.000
54.00	0.0507	348533.	-389.7529	-0.002332	2514.3132	5.799E+09	-219.8599	26031.000	0.000
60.00	0.0378	344264.	-1682.8639	-0.001974	2493.0803	5.799E+09	-211.1772	33551.000	0.000
66.00	0.0270	332056.	-2917.9512	-0.001624	2432.3674	5.799E+09	-200.5186	44572.000	0.000
72.00	0.0183	312307.	-4082.5121	-0.001290	2334.1420	5.799E+09	-187.6684	61593.000	0.000
78.00	0.0115	285497.	-5162.4400	-0.000981	2200.8068	5.799E+09	-172.3076	89827.000	0.000
84.00	0.006509	252206.	-6206.7531	-0.000703	2035.2239	5.799E+09	-175.7968	162039.000	0.000
90.00	0.003075	212340.	-7360.9239	-0.000462	1836.9481	5.799E+09	-208.9268	407607.000	0.000
96.00	0.000960	164746.	-8474.2534	-0.000267	1600.2347	5.799E+09	-162.1831	1013989.000	0.000
102.00	-0.000133	111153.	-8558.8236	-0.000125	1333.6838	5.799E+09	133.9930	6033055.000	0.000
108.00	-0.000536	62275.	-7062.0025	-3.492E-05	1090.5855	5.799E+09	364.9474	4084377.000	0.000
114.00	-0.000552	26475.	-4863.4884	1.099E-05	912.5288	5.799E+09	367.8907	3996363.000	0.000
120.00	-0.000404	3892.6514	-2739.0138	2.670E-05	800.2144	5.799E+09	340.2675	5050992.000	0.000
126.00	-0.000232	-6443.6678	-1018.7013	2.538E-05	812.9021	5.799E+09	233.1700	6033055.000	0.000
132.00	-9.959E-05	-8379.5871	-18.7732	1.771E-05	822.5306	5.799E+09	100.1394	6033055.000	0.000
138.00	-1.931E-05	-6702.3215	339.9017	9.912E-06	814.1886	5.799E+09	19.4189	6033055.000	0.000
144.00	1.936E-05	-4319.4417	368.5030	4.210E-06	802.3371	5.799E+09	-9.8851	3064339.000	0.000
150.00	3.121E-05	-2288.2165	286.5364	7.913E-07	792.2346	5.799E+09	-17.4371	3352619.000	0.000
156.00	2.885E-05	-882.4958	184.5161	-8.491E-07	785.2431	5.799E+09	-16.5697	3445901.000	0.000
162.00	2.027E-05	-72.4237	97.6151	-1.343E-06	781.2141	5.799E+09	-12.3973	3529189.000	0.000
168.00	1.273E-05	291.4159	37.2958	-2.300E-06	782.3033	5.799E+09	-7.7091	3632480.000	0.000
174.00	6.259E-06	377.4433	2.5081	-8.838E-07	782.7312	5.799E+09	-3.8868	3725775.000	0.000
180.00	2.128E-06	323.1784	-13.2163	-5.213E-07	782.4613	5.799E+09	-1.3547	3819074.000	0.000
186.00	3.640E-05	219.8304	-17.2874	-2.404E-07	781.9473	5.799E+09	-0.002373	3912376.000	0.000
192.00	-7.562E-07	116.1827	-14.6875	-6.653E-08	781.4318	5.799E+09	0.8690	6894920.000	0.000
198.00	-7.947E-07	43.7053	9.3408	1.619E-08	781.0713	5.799E+09	0.9133	6894920.000	0.000
204.00	-5.619E-07	4.0630	-4.5876	4.090E-08	780.8741	5.799E+09	0.6711	7165821.000	0.000
210.00	-3.039E-07	-11.4235	-1.4347	3.710E-08	780.9108	5.799E+09	0.3799	7500000.000	0.000
216.00	-1.166E-07	-13.2236	0.1428	2.434E-08	780.9197	5.799E+09	0.1460	7500000.000	0.000
222.00	-1.177E-08	-9.7556	0.6249	1.245E-08	780.9025	5.799E+09	0.0147	7500000.000	0.000
228.00	3.268E-08	-5.7483	0.5935	4.434E-09	780.8255	5.799E+09	-0.0252	4625398.000	0.000
234.00	4.143E-08	-2.6423	0.4200	9.276E-11	780.8671	5.799E+09	-0.0326	4727130.000	0.000

			Abut SR Long Ave P						
240.000	3.379E-08	-0.7089	0.2405	-1.641E-10	780.8539	5.799E-09	-0.0272	4828868.0	0.000
246.000	2.174E-08	0.2462	0.1053	-1.880E-09	780.8552	5.799E-09	-0.0179	4930216.0	0.000
252.000	1.122E-08	0.5579	0.0234	-1.464E-09	780.8567	5.799E-09	-0.009414	5032360.0	0.000
258.000	4.169E-09	0.5301	-0.0155	-9.015E-10	780.8566	5.799E-09	-0.003567	5134113.0	0.000
264.000	4.051E-10	0.3734	-0.0273	-4.341E-10	780.8558	5.799E-09	-0.003353	5235871.0	0.000
270.000	-1.040E-09	0.2037	-0.0244	-1.355E-10	780.8550	5.799E-09	0.001300	5300000.0	0.000
276.000	-1.221E-09	0.0805	-0.0160	-1.148E-11	780.8543	5.799E-09	0.001526	5300000.0	0.000
282.000	-9.024E-10	0.0122	-0.007950	5.943E-11	780.8540	5.799E-09	0.001128	5300000.0	0.000
288.000	-5.080E-10	-0.0155	-0.002700	5.771E-11	780.8540	5.799E-09	0.000635	7500000.0	0.000
294.000	-2.099E-10	-0.0203	-8.092E-06	3.918E-11	780.8540	5.799E-09	0.000262	7500000.0	0.000
300.000	-3.789E-11	-0.0157	0.000921	2.056E-11	780.8540	5.799E-09	4.737E-05	7500000.0	0.000
306.000	6.678E-11	-0.009308	0.000954	7.631E-12	780.8540	5.799E-09	-3.647E-05	5948278.0	0.000
312.000	5.368E-11	-0.004244	0.000682	0.000000	780.8540	5.799E-09	-5.412E-05	6050063.0	0.000
318.000	4.422E-11	-0.001125	0.000384	-2.158E-12	780.8539	5.799E-09	-4.534E-05	6151851.0	0.000
324.000	2.778E-11	0.000363	0.000161	-2.552E-12	780.8539	5.799E-09	-2.895E-05	6253641.0	0.000
330.000	1.359E-11	0.000809	3.069E-05	-1.945E-12	780.8539	5.799E-09	-1.440E-05	6355433.0	0.000
336.000	4.433E-12	0.0000735	-2.683E-05	-1.146E-12	780.8539	5.799E-09	-4.771E-06	6457228.0	0.000
342.000	0.000	0.000489	-4.053E-05	0.000000	780.8539	5.799E-09	2.038E-07	7500000.0	0.000
348.000	-1.722E-12	0.000250	-3.346E-05	0.000000	780.8539	5.799E-09	2.153E-06	7500000.0	0.000
354.000	-1.730E-12	8.794E-05	-2.051E-05	0.000000	780.8539	5.799E-09	2.162E-06	7500000.0	0.000
360.000	-1.191E-12	3.678E-06	-9.562E-06	0.000000	780.8539	5.799E-09	1.489E-06	7500000.0	0.000
366.000	0.000	-2.698E-05	-2.734E-06	0.000000	780.8539	5.799E-09	7.872E-07	7500000.0	0.000
372.000	0.000	-2.928E-05	5.119E-07	0.000000	780.8539	5.799E-09	2.949E-07	7500000.0	0.000
378.000	0.000	-2.094E-05	1.486E-06	0.000000	780.8539	5.799E-09	2.984E-08	7500000.0	0.000
384.000	0.000	-1.150E-05	1.364E-06	0.000000	780.8539	5.799E-09	-7.051E-08	7271654.0	0.000
390.000	0.000	-4.584E-06	8.986E-07	0.000000	780.8539	5.799E-09	-8.461E-08	7373464.0	0.000
400.000	0.000	-1.722E-07	-5.526E-08	0.000000	780.8539	5.799E-09	-6.362E-08	7475276.0	0.000
402.000	0.000	8.695E-07	1.548E-07	0.000000	780.8539	5.799E-09	-3.608E-08	7500000.0	0.000
408.000	0.000	1.152E-06	1.374E-09	0.000000	780.8539	5.799E-09	-1.507E-08	7500000.0	0.000
414.000	0.000	8.901E-07	-5.280E-08	0.000000	780.8539	5.799E-09	-2.993E-09	7500000.0	0.000
420.000	0.000	4.350E-08	-1.083E-09	0.000000	780.8539	5.799E-09	2.173E-09	7500000.0	0.000
426.000	0.000	2.277E-07	-3.884E-08	0.000000	780.8539	5.799E-09	3.303E-09	7500000.0	0.000
432.000	0.000	5.408E-08	-2.093E-08	0.000000	780.8539	5.799E-09	2.665E-09	7500000.0	0.000
438.000	0.000	-2.367E-08	-8.112E-09	0.000000	780.8539	5.799E-09	1.608E-09	7500000.0	0.000
444.000	0.000	-4.350E-08	-1.083E-09	0.000000	780.8539	5.799E-09	7.548E-10	7500000.0	0.000
450.000	0.000	-3.684E-08	1.718E-09	0.000000	780.8539	5.799E-09	1.989E-10	7500000.0	0.000
456.000	0.000	-2.988E-08	2.162E-09	0.000000	780.8539	5.799E-09	-5.102E-11	7500000.0	0.000
462.000	0.000	-1.094E-08	1.641E-09	0.000000	780.8539	5.799E-09	-1.226E-10	7500000.0	0.000
468.000	0.000	-3.296E-09	9.453E-10	0.000000	780.8539	5.799E-09	-1.093E-10	7500000.0	0.000
474.000	0.000	4.118E-10	4.057E-10	0.000000	780.8539	5.799E-09	-7.048E-11	7500000.0	0.000
480.000	0.000	1.582E-09	8.981E-11	0.000000	780.8539	5.799E-09	-3.482E-11	7500000.0	0.000
486.000	0.000	-1.497E-09	-4.835E-11	0.000000	780.8539	5.799E-09	-1.143E-11	7500000.0	0.000
492.000	0.000	9.988E-10	-8.225E-11	0.000000	780.8539	5.799E-09	0.000000	7500000.0	0.000
498.000	0.000	5.119E-10	-6.818E-11	0.000000	780.8539	5.799E-09	4.354E-12	7500000.0	0.000
504.000	0.000	1.812E-10	-4.192E-11	0.000000	780.8539	5.799E-09	4.399E-12	7500000.0	0.000
510.000	0.000	8.628E-12	-1.951E-11	0.000000	780.8539	5.799E-09	3.039E-12	7500000.0	0.000
516.000	0.000	-5.451E-11	-5.658E-12	0.000000	780.8539	5.799E-09	1.612E-12	7500000.0	0.000
522.000	0.000	-5.958E-11	0.000000	0.000000	780.8539	5.799E-09	0.000000	7500000.0	0.000
528.000	0.000	-4.271E-11	3.019E-12	0.000000	780.8539	5.799E-09	0.000000	7500000.0	0.000
534.000	0.000	-2.344E-11	2.782E-12	0.000000	780.8539	5.799E-09	0.000000	7500000.0	0.000
540.000	0.000	-9.359E-12	1.829E-12	0.000000	780.8539	5.799E-09	0.000000	7500000.0	0.000
546.000	0.000	-1.498E-12	0.000000	0.000000	780.8539	5.799E-09	0.000000	7500000.0	0.000
552.000	0.000	-1.724E-12	0.000000	0.000000	780.8539	5.799E-09	0.000000	7500000.0	0.000
558.000	0.000	2.312E-12	0.000000	0.000000	780.8539	5.799E-09	0.000000	7500000.0	0.000
564.000	0.000	1.794E-12	0.000000	0.000000	780.8539	5.799E-09	0.000000	7500000.0	0.000
570.000	0.000	1.053E-12	0.000000	0.000000	780.8539	5.799E-09	0.000000	7500000.0	0.000
576.000	0.000	0.000000	0.000000	0.000000	780.8539	5.799E-09	0.000000	7500000.0	0.000
582.000	0.000	0.000000	0.000000	0.000000	780.8539	5.799E-09	0.000000	7500000.0	0.000
588.000	0.000	0.000000	0.000000	0.000000	780.8539	5.799E-09	0.000000	7500000.0	0.000
594.000	0.000	0.000000	0.000000	0.000000	780.8539	5.799E-09	0.000000	7500000.0	0.000
600.000	0.000	0.000000	0.000000	0.000000	780.8539	5.799E-09	0.000000	3750000.0	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Pile-head deflection	=	0.2500000	inches
Computed slope at pile head	=	-0.0044959	rad
Maximum bending moment	=	348533.	inch-lbs
Maximum shear force	=	13005.	lbs
Depth of maximum bending moment	=	54.0000000	inches below pile head
Depth of maximum shear force	=	0.0000000	inches below pile head
Number of iterations	=	14	
Number of zero deflection points	=	14	

Computed Values of Pile Loading and Deflection For Lateral Loading for Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)	=		
Displacement of pile head	=	0.500000	inches
Moment at pile head	=	0.000	in-lbs
Axial load at pile head	=	157000.0	lbs

Depth	Deflect.	Bending	Shear	Slope	Abut	SR Long Ave P	Bending	Soil Res.	Soil Spr.	Di Stri b.
y	inches	Moment	Force	radi	Stress	Stiffness	Stiffness	p	Es/h	Lat. Load
inches	inches	in-lbs	lbs	ans	psi*	lb-in ²	lb-in ²	lb/in	lb/inch	lb/inch
0.00	0.5000	0.000	17669.	-0.008019	780.8539	5.799E-09	-58.1152	3522.9194	0.000	0.000
6.00	0.4519	102999.	15076.	-0.007966	1293.1296	5.799E-09	-277.3429	3682.4736	0.000	0.000
12.00	0.4044	195914.	13397.	-0.007811	1755.2479	5.799E-09	-282.2212	4187.1461	0.000	0.000
18.00	0.3582	278477.	11693.	-0.007566	2165.8850	5.799E-09	-285.8754	4789.1697	0.000	0.000
24.00	0.3136	350478.	9970.1645	-0.007240	2523.9862	5.799E-09	-288.2436	5514.4652	0.000	0.000
30.00	0.2713	411760.	8237.6506	-0.006846	2828.7786	5.799E-09	-289.2610	6397.9524	0.000	0.000
36.00	0.2315	462227.	6503.2914	-0.006394	3079.7828	5.799E-09	-288.8587	7487.5364	0.000	0.000
42.00	0.1945	501845.	4775.8292	-0.005895	3276.8263	5.799E-09	-286.9621	8850.3021	0.000	0.000
48.00	0.1607	530643.	3064.4759	-0.005361	3420.0565	5.799E-09	-283.4891	10882.	0.000	0.000
54.00	0.1302	548718.	1378.9662	-0.004802	3509.9558	5.799E-09	-278.3475	12626.	0.000	0.000
60.00	0.1031	556238.	-270.3690	-0.004231	3547.3571	5.799E-09	-271.4309	15796.	0.000	0.000
66.00	0.0794	553445.	-1872.5013	-0.003657	3533.4623	5.799E-09	-262.6132	19833.	0.000	0.000
72.00	0.0592	540657.	-3415.5581	-0.003091	3469.8637	5.799E-09	-251.7391	25504.0	0.000	0.000
78.00	0.0428	518281.	-4886.6034	-0.002543	3358.5705	5.799E-09	-238.6094	33798.	0.000	0.000
84.00	0.0287	486809.	-6366.4661	-0.002023	3202.0419	5.799E-09	-254.6782	53222.	0.000	0.000
90.00	0.0181	445694.	-8105.9249	-0.001540	2997.5533	5.799E-09	-325.1414	107864.	0.000	0.000
96.00	0.0102	392439.	-9958.7302	-0.001107	2732.6878	5.799E-09	-292.4604	171562.	0.000	0.000
102.00	0.004807	328274.	-11589.	-0.000734	2413.5549	5.799E-09	-250.9200	313226.	0.000	0.000
108.00	0.001423	254755.	-12917.	-0.000432	2047.9036	5.799E-09	-191.8776	809111.	0.000	0.000
114.00	-0.000379	174081.	-12496.	-0.000210	1646.6618	5.799E-09	332.2398	5257853.	0.000	0.000
120										

Abut 5R_long_Ave P									
Depth	Deflect.	Bending Moment	Shear Force	Slope	Total Stiffness	Bending Stiffness	Soil Res.	Soil Spr.	Distrib. Lat. Load
inches	inches	in-lbs	lbs	radians	psi*	lb/in ²	lb/in	lb/inch	lb/inch
0.00	0.0000	0.0000	24095.	-0.0144	780.8539	5.799E+09	-698.2468	2094.7404	0.000
6.000	0.9138	145529.	21008.	-0.0143	1504.6582	5.799E+09	-330.7329	2171.4860	0.000
12.000	0.8286	279011.	19003.	-0.0141	2168.5394	5.799E+09	-337.6510	2445.0054	0.000
18.000	0.7451	400065.	16960.	-0.0137	2770.6119	5.799E+09	-343.3267	2764.7931	0.000
24.000	0.6640	508369.	14887.	-0.0132	3309.2725	5.799E+09	-347.6985	3141.7077	0.000
30.000	0.5861	603660.	12792.	-0.0127	3783.2134	5.799E+09	-350.7027	3589.8957	0.000
36.000	0.5120	685738.	10683.	-0.0120	4191.4349	5.799E+09	-352.2718	4128.0553	0.000
42.000	0.4421	754466.	8569.1703	-0.0113	4533.2579	5.799E+09	-352.3339	4781.3007	0.000
48.000	0.3769	809774.	6459.7350	-0.0104	4808.3383	5.799E+09	-350.8112	5583.9802	0.000
54.000	0.3168	851663.	4364.4461	-0.009587	5016.6806	5.799E+09	-347.6184	6584.0434	0.000
60.000	0.2619	880209.	2293.6112	-0.008691	5158.6533	5.799E+09	-342.6599	7850.0150	0.000
66.000	0.2125	895560.	258.1507	-0.007772	5235.0059	5.799E+09	-335.8270	9482.5149	0.000
72.000	0.1686	897949.	-1730.3100	-0.006844	5246.8874	5.799E+09	-326.9533	11634.	0.000
78.000	0.1304	887691.	-3659.3159	-0.005920	5195.8678	5.799E+09	-316.0087	14545.	0.000
84.000	0.0976	865192.	-5644.6205	-0.005014	5083.9638	5.799E+09	-345.7595	21257.	0.000
90.000	0.0702	829401.	-8050.7033	-0.004137	4905.9574	5.799E+09	-456.2681	38998.	0.000
96.000	0.0480	776377.	-10710.	-0.003306	4642.2358	5.799E+09	-430.1768	53825.	0.000
102.000	0.0305	707109.	-13195.	-0.002539	4297.7276	5.799E+09	-397.9951	78226.	0.000
108.000	0.0175	622825.	-15463.	-0.001850	3878.5306	5.799E+09	-358.2484	122896.	0.000
114.000	0.008321	525036.	-17461.	-0.001257	3392.1702	5.799E+09	-307.5414	221764.	0.000
120.000	0.002411	415664.	-19083.	-0.000770	2848.1995	5.799E+09	-233.2477	580484.	0.000
126.000	-0.000918	297491.	-18533.	-0.000401	2260.4508	5.799E+09	416.7335	2722557.	0.000
132.000	-0.002401	194029.	-15687.	-0.000147	1745.8758	5.799E+09	531.6378	1328668.	0.000
138.000	-0.002679	109518.	-12453.	1.037E-05	1325.5495	5.799E+09	546.6130	1224431.	0.000
144.000	-0.002276	44577.	-9125.7878	9.009E-05	1002.5630	5.799E+09	562.3568	1482245.	0.000
150.000	-0.001597	-161.6326	-5791.7868	0.000113	781.6578	5.799E+09	548.9769	2061939.	0.000
156.000	-0.000920	-25137.	-2710.6414	9.998E-05	605.8761	5.799E+09	478.0716	3119392.	0.000
162.000	-0.000398	-32878.	-113.9437	6.997E-05	444.3742	5.799E+09	387.4943	5846051.	0.000
168.000	-7.997E-05	-26636.	1324.2195	3.917E-05	313.3322	5.799E+09	91.8934	6894920.	0.000
174.000	7.240E-05	-17061.	1474.7261	1.657E-05	219.7077	5.799E+09	-41.7245	3457929.	0.000
180.000	0.000184	-8910.0024	1135.5360	3.999E-06	152.4512	5.799E+09	-70.3388	3551207.	0.000
186.000	0.000110	-3404.2702	727.8161	3.303E-06	97.7854	5.799E+09	-66.5678	3644490.	0.000
192.000	7.921E-05	-230.8231	380.0841	-5.184E-06	782.0020	5.799E+09	-49.3429	3737776.	0.000
198.000	4.739E-05	1166.5047	141.2809	-4.700E-06	786.6557	5.799E+09	-30.2582	3831066.	0.000
204.000	2.281E-05	1473.4011	5.8031	-3.334E-06	798.1820	5.799E+09	-14.9011	3919175.	0.000
210.000	7.384E-06	1242.4225	-54.4198	-1.929E-06	787.0332	5.799E+09	-5.1732	4203635.	0.000
216.000	-3.313E-07	823.9971	-68.6969	-8.596E-07	784.9522	5.799E+09	0.4142	5206500.	0.000
222.000	-2.931E-06	419.6785	-56.4636	-2.161E-07	782.9412	5.799E+09	3.6636	7500000.	0.000
228.000	-2.925E-06	146.8414	-44.5041	7.696E-08	781.5843	5.799E+09	3.6542	7500000.	0.000
234.000	-2.007E-06	5.4840	-16.0079	1.558E-07	780.8812	5.799E+09	2.5092	7500000.	0.000
240.000	-1.056E-06	-45.5475	-4.5214	1.350E-07	781.0050	5.799E+09	1.3197	7500000.	0.000
246.000	-3.869E-07	-49.0271	0.8883	6.811E-08	781.0978	5.799E+09	0.4836	7500000.	0.000
252.000	-2.237E-08	-35.0505	2.4229	4.261E-08	781.0283	5.799E+09	0.0280	7500000.	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Pile-head deflection	=	0.5000000 inches
Computed slope at pile head	=	-0.0080190 radians
Maximum bending moment	=	556238. inch-lbs
Maximum shear force	=	7660. lbs
Depth of maximum bending moment	=	60.000000 inches below pile head
Depth of maximum shear force	=	0.000000 inches below pile head
Number of iterations	=	20
Number of zero deflection points	=	13

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 3

Pile-head conditions are Displacement and Moment (Loading Type 4)									
Displacement of pile head = 1.000000 inches									
Moment at pile head = 1190000 in-lbs									
Axial load at pile head = 1570000.000 lbs									
Depth	Deflect.	Bending Moment	Shear Force	Slope	Total Stiffness	Bending Stiffness	Soil Res.	Soil Spr.	Distrib. Lat. Load
inches	inches	in-lbs	lbs	radians	psi*	lb/in ²	lb/in	lb/inch	lb/inch
0.00	0.0000	0.0000	24095.	-0.0144	780.8539	5.799E+09	-698.2468	2094.7404	0.000
6.000	0.9138	145529.	21008.	-0.0143	1504.6582	5.799E+09	-330.7329	2171.4860	0.000
12.000	0.8286	279011.	19003.	-0.0141	2168.5394	5.799E+09	-337.6510	2445.0054	0.000
18.000	0.7451	400065.	16960.	-0.0137	2770.6119	5.799E+09	-343.3267	2764.7931	0.000
24.000	0.6640	508369.	14887.	-0.0132	3309.2725	5.799E+09	-347.6985	3141.7077	0.000
30.000	0.5861	603660.	12792.	-0.0127	3783.2134	5.799E+09	-350.7027	3589.8957	0.000
36.000	0.5120	685738.	10683.	-0.0120	4191.4349	5.799E+09	-352.2718	4128.0553	0.000
42.000	0.4421	754466.	8569.1703	-0.0113	4533.2579	5.799E+09	-352.3339	4781.3007	0.000
48.000	0.3769	809774.	6459.7350	-0.0104	4808.3383	5.799E+09	-350.8112	5583.9802	0.000
54.000	0.3168	851663.	4364.4461	-0.009587	5016.6806	5.799E+09	-347.6184	6584.0434	0.000
60.000	0.2619	880209.	2293.6112	-0.008691	5158.6533	5.799E+09	-342.6599	7850.0150	0.000
66.000	0.2125	895560.	258.1507	-0.007772	5235.0059	5.799E+09	-335.8270	9482.5149	0.000
72.000	0.1686	897949.	-1730.3100	-0.006844	5246.8874	5.799E+09	-326.9533	11634.	0.000
78.000	0.1304	887691.	-3659.3159	-0.005920	5195.8678	5.799E+09	-316.0087	14545.	0.000
84.000	0.0976	865192.	-5644.6205	-0.005014	5083.9638	5.799E+09	-345.7595	21257.	0.000
90.000	0.0702	829401.	-8050.7033	-0.004137	4905.9574	5.799E+09	-456.2681	38998.	0.000
96.000	0.0480	776377.	-10710.	-0.003306	4642.2358	5.799E+09	-430.1768	53825.	0.000
102.000	0.0305	707109.	-13195.	-0.002539	4297.7276	5.799E+09	-397.9951	78226.	0.000
108.000	0.0175	622825.	-15463.	-0.001850	3878.5306	5.799E+09	-358.2484	122896.	0.000
114.000	0.008321	525036.	-17461.	-0.001257	3392.1702	5.799E+09	-307.5414	221764.	0.000
120.000	0.002411	415664.	-19083.	-0.000770	2848.1995	5.799E+09	-233.2477	580484.	0.000
126.000	-0.000918	297491.	-18533.	-0.000401	2260.4508	5.799E+09	416.7335	2722557.	0.000
132.000	-0.002401	194029.	-15687.	-0.000147	1745.8758	5.799E+09	531.6378	1328668.	0.000
138.000	-0.002679	109518.	-12453.	1.037E-05	1325.5495	5.799E+09	546.6130	1224431.	0.000
144.000	-0.002276	44577.	-9125.7878	9.009E-05	1002.5630	5.799E+09	562.3568	1482245.	0.000
150.000	-0.001597	-161.6326	-5791.7868	0.000113	781.6578	5.799E+09	548.9769	2061939.	0.000
156.000	-0.000920	-25137.	-2710.6414	9.998E-05	605.8761	5.799E+09	478.0716	3119392.	0.000
162.000	-0.000398	-32878.	-113.9437	6.997E-05	444.3742	5.799E+09	387.4943	5846051.	0.000
168.000	-7.997E-05	-26636.	1324.2195	3.917E-05	313.3322	5.799E+09	91.8934	6894920.	0.000
174.000	7.240E-05	-17061.	1474.7261	1.657E-05	219.7077	5.799E+09	-41.7245	3457929.	0.000
180.000	0.000184	-8910.0024	1135.5360	3.999E-06	152.4512	5.799E+09	-70.3388	3551207.	0.000
186.000	0.000110	-3404.2702	727.8161	3.303E-06	97.7854	5.799E+09	-66.5678	3644490.	0.000
192.000	7.921E-05	-230.8231	380.0841	-5.184E-06	782.0020	5.799E+09	-49.3429	3737776.	0.000
198.000	4.739E-05	1166.5047	141.2809	-4.700E-06	786.6557	5.799E+09	-30.2582	3831066.	0.000
204.000	2.281E-05	1473.4011	5.8031	-3.334E-06	798.1820	5.799E+09	-14.9011	3919175.	0.000
210.000	7.384E-06	1242.4225	-54.4198	-1.929E-06	787.0332	5.799E+09	-5.1732	4203635.	0.000
216.000	-3.313E-07	823.9971	-68.6969	-8.596E-07	784.9522	5.799E+09	0.4142	5206500.	0.000
222.000	-2.931E-06	419.6785	-56.4636	-2.161E-07	782.9412	5.799E+09	3.6636	7500000.	0.000
228.000	-2.925E-06	146.8414	-44.5041	7.696E-08	781.5843	5.799E+09	3.6542	7500000.	0.000
234.000	-2.007E-06	5.4840	-16.0079	1.558E-07	780.8812	5.799E+09	2.5092	7500000.	0.000
240.000	-1.056E-06	-45.5475	-4.5214	1.350E-07	781.0050	5.799E+09	1.3197	7500000.	0.000
246.000	-3.869E-07	-49.0271	0.8883	6.811E-08	781.0978	5.799E+09	0.4836	7500000.	0.000
252.000	-2.237E-08	-35.0505	2.4229	4.261E-08	781.0283	5.799E+09	0.0280	7500000.	0.000

Abut 5R_long_Ave P									
Depth	Deflect.	Bending Moment	Shear Force	Slope	Total Stiffness	Bending Stiffness	Soil Res.	Soil Spr.	Distrib. Lat. Load
inches	inches	in-lbs	lbs	radians	psi*	lb/in<			

Abut 5R_Long_Ave P

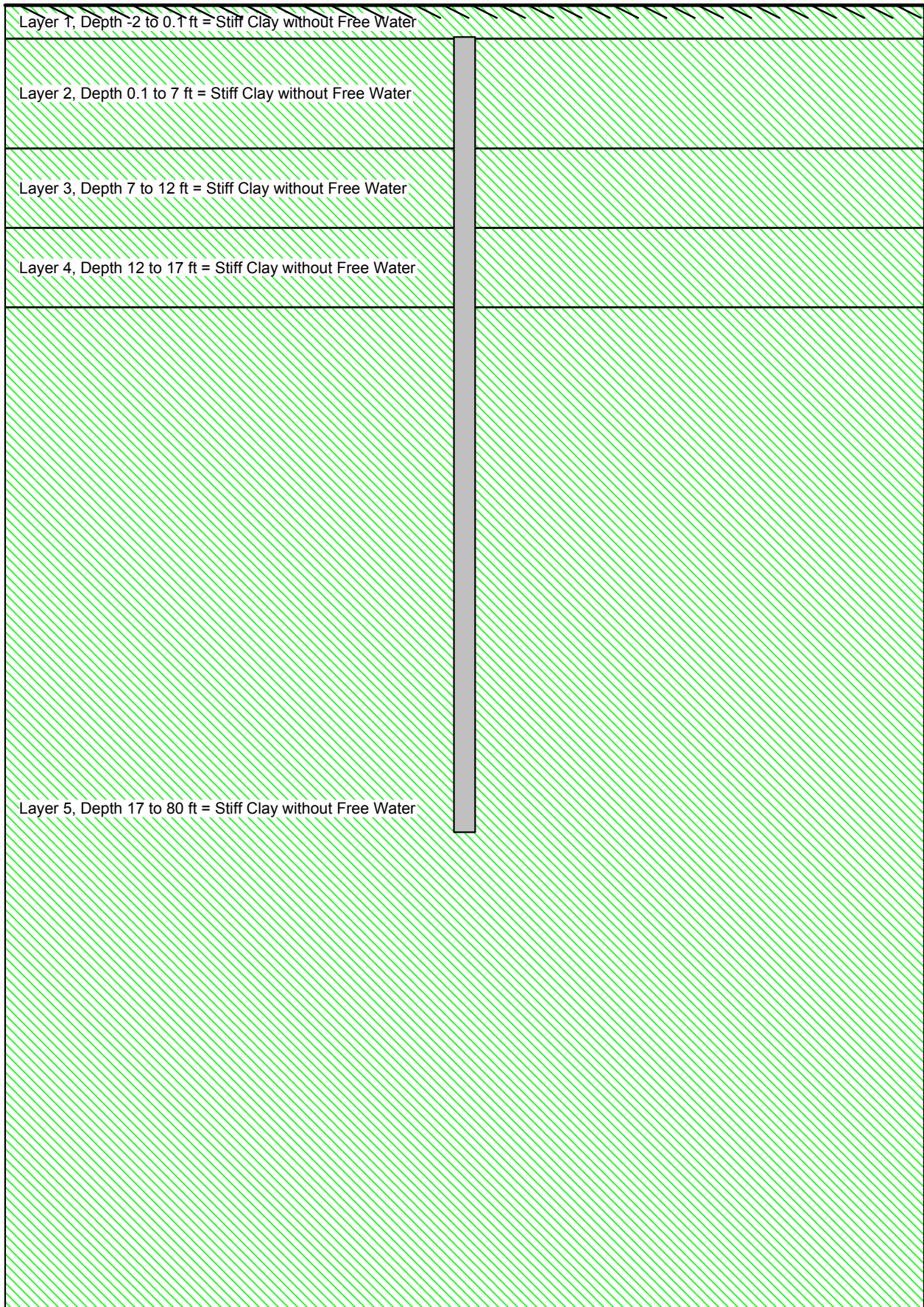
Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 M = in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection in-inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	157000.	0.25000000	348533.	13005.	-0.00449590
2	4	y = 0.5000	M = 0.000	157000.	0.50000000	556238.	17669.	-0.00801905
3	4	y = 1.0000	M = 0.000	157000.	1.00000000	897949.	24095.	-0.01435949

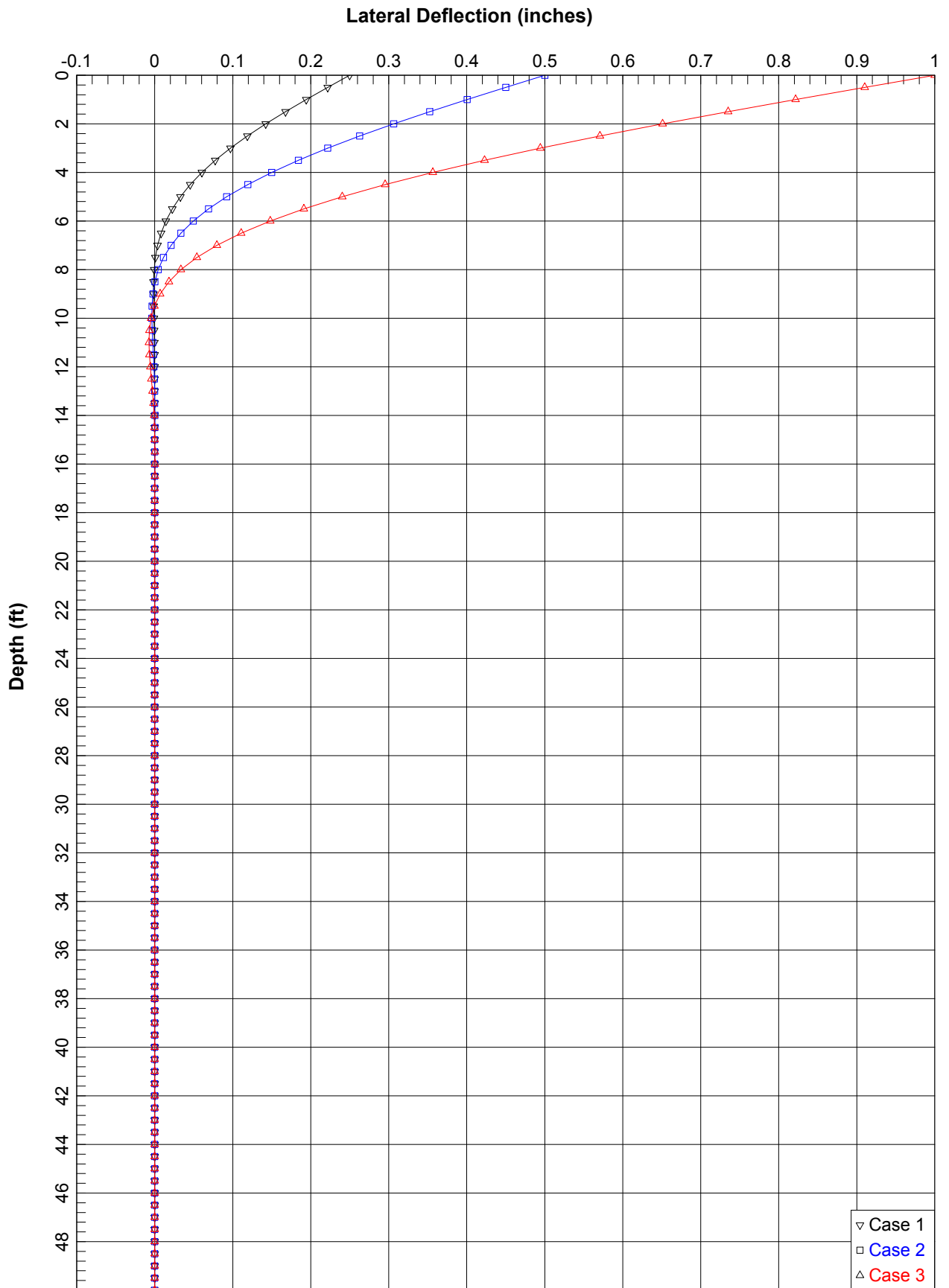
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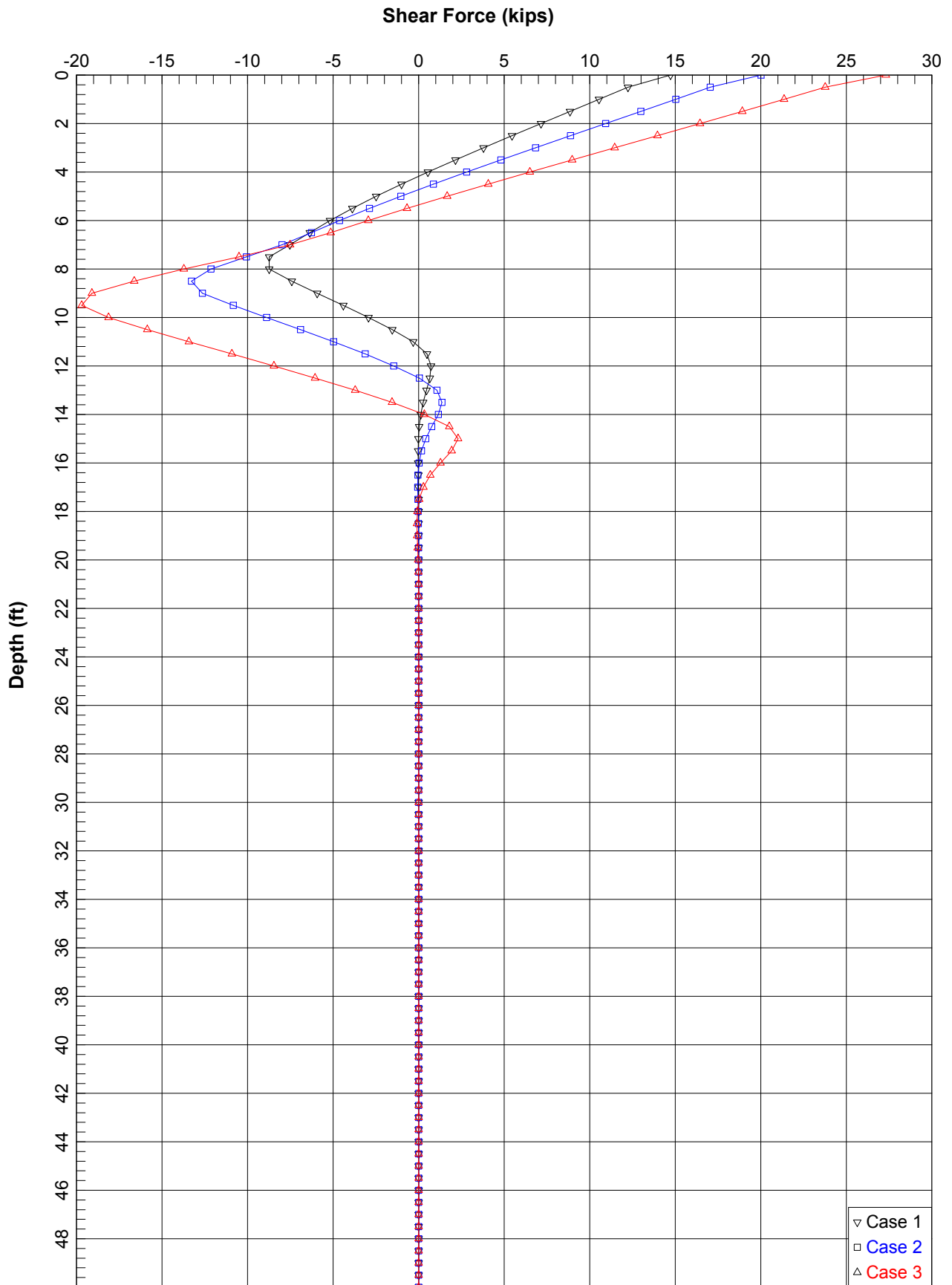
SUPPORT: ABUTMENT 5R

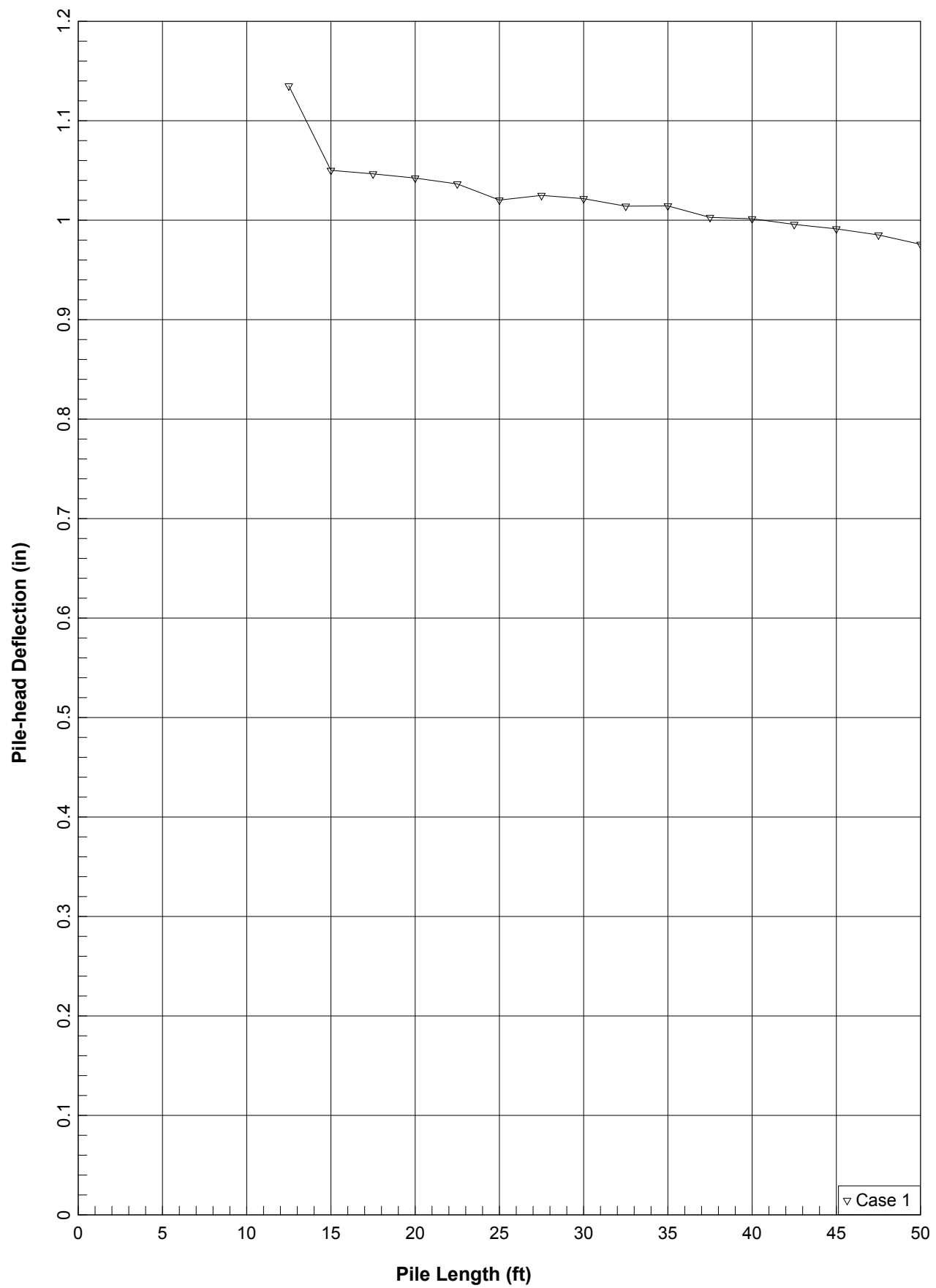
LOAD DIRECTION: TRANSVERSE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE









 Abut 5R_transv_Critical Length

Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 This copy of LPILE is licensed to:

gdc
 gdc
 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

 Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 5\
 Name of input data file: Abut 5R_transv_Critical Length.lpd
 Name of output report file: Abut 5R_transv_Critical Length.lpo
 Name of plot output file: Abut 5R_transv_Critical Length.lpp
 Name of runtime message file: Abut 5R_transv_Critical Length.lpr

 Date and Time of Analysis

Date: September 13, 2014 Time: 9:49:20

 Problem Title

Project Name: Palo Comado OC Bridge Widen

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

 Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

 Pile Structural Properties and Geometry

Page 1

 Abut 5R_transv_Critical Length

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

 Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 16.0000000 in
 Bottom Width = 16.0000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

 Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

 Soil and Rock Layering Information

The soil profile is modelled using 5 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 7.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 7.00000 ft
 Distance from top of pile to bottom of layer = 12.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi

Page 2

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 12.00000 ft
 Distance from top of pile to bottom of layer = 17.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 17.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Rock Emass	Layer Depth ft	Effective Unit Wt. krm	Undrained Cohesion Test psf	In-situ Friction Test deg.	Angle of Friction Property	Uniaxial Elastic Mod. psi	ROD % or GSI
1	0.00700	Stiff Clay w/o Free Water	--	-2.000	120.000	4000.000	--	--	--	--
	0.00700	--	--	0.10000	120.000	4000.000	--	--	--	--
2	0.00700	Stiff Clay w/o Free Water	--	0.10000	120.000	1500.000	--	--	--	--
	0.00700	--	--	7.000	120.000	1500.000	--	--	--	--
3	0.00700	Stiff Clay w/o Free Water	--	7.000	120.000	3500.000	--	--	--	--
	0.00700	--	--	12.000	120.000	3500.000	--	--	--	--
4	0.00700	Stiff Clay w/o Free Water	--	12.000	125.000	4000.000	--	--	--	--
	0.00700	--	--	17.000	125.000	4000.000	--	--	--	--
5	0.00500	Stiff Clay w/o Free Water	--	17.000	125.000	4500.000	--	--	--	--
	0.00500	--	--	80.000	125.000	4500.000	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X Ft	p-mult	y-mult
1	0.000	0.6700	1.0000
2	50.000	0.6700	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Abut 5R_transv_Critical Length

Number of loads specified = 1

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	1	V = 27000. lbs	M = 0.0000 in-lbs	157000.	True

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head = 27000.000 lbs
 Applied moment at pile head = 0.00000 in-lbs
 Axial thrust load on pile head = 157000.000 lbs

Depth inches	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress lb-in ²	Bending Stiffness lb-in ²	Soil Res. lb/in	Soil Spr. lb/inch	Distrib. Lat. Load lb/inch
0.00	0.9757	-1.431E-07	27000.	-0.0146	780.8539	5.799E+09	-775.0439	2383.1187	0.000
6.00	0.8878	161840.	23487.	-0.0146	1585.7797	5.799E+09	-396.0283	2676.3831	0.000
12.00	0.8010	309265.	21091.	-0.0143	2319.0122	5.799E+09	-402.4877	3014.9093	0.000
18.00	0.7161	441899.	18661.	-0.0139	2978.6804	5.799E+09	-407.4316	3413.6478	0.000
24.00	0.6339	559435.	16207.	-0.0134	3563.2560	5.799E+09	-410.7851	3888.1093	0.000
30.00	0.5552	661637.	13737.	-0.0128	4071.5687	5.799E+09	-412.4686	4457.4153	0.000
36.00	0.4806	748346.	11262.	-0.0120	4502.8218	5.799E+09	-412.3967	5148.2825	0.000
42.00	0.4107	819479.	8793.8532	-0.0112	4856.6076	5.799E+09	-410.4759	5997.0380	0.000
48.00	0.3458	875036.	6342.6192	-0.0104	5132.9253	5.799E+09	-406.6021	7054.5223	0.000
54.00	0.2864	915102.	3920.8438	-0.009430	5332.1991	5.799E+09	-400.6564	8393.6733	0.000
60.00	0.2327	939853.	1541.3747	-0.008471	5455.2995	5.799E+09	-392.4999	10122.	0.000
66.00	0.1847	949558.	-782.0195	-0.007493	5503.5668	5.799E+09	-381.9648	12405.	0.000
72.00	0.1427	944586.	-3034.4363	-0.006513	5478.8402	5.799E+09	-368.8408	15504.	0.000
78.00	0.1066	925416.	-5199.5156	-0.005546	5383.4937	5.799E+09	-352.8523	19862.	0.000
84.00	0.0762	892640.	-7550.1976	-0.004605	5220.4831	5.799E+09	-330.7084	33920.	0.000
90.00	0.0513	843490.	-10505.	-0.003707	4976.0270	5.799E+09	-554.3256	64801.	0.000
96.00	0.0317	773561.	-13689.	-0.002870	4628.2302	5.799E+09	-506.8564	95937.	0.000
102.00	0.0169	684630.	-16548.	-0.002116	4185.9239	5.799E+09	-446.2393	158611.	0.000
108.00	0.006310	578967.	-18965.	-0.001462	3660.3998	5.799E+09	-359.3048	341680.	0.000
114.00	-0.000667	459805.	-19412.	-0.000925	3067.7357	5.799E+09	210.2252	1890913.	0.000
120.00	-0.004789	347763.	-17718.	-0.000507	2510.4832	5.799E+09	354.4599	444094.	0.000
126.00	-0.006752	248142.	-15464.	-0.000199	2015.0106	5.799E+09	396.7919	352606.	0.000
132.00	-0.007174	162564.	-13033.	1.372E-05	1589.3804	5.799E+09	413.5365	345853.	0.000
138.00	-0.006587	91715.	-10547.	0.000145	1237.0055	5.799E+09	415.2528	378232.	0.000
144.00	-0.005431	35725.	-8121.4661	0.000211	958.5367	5.799E+09	393.2849	434493.	0.000
150.00	-0.004053	-6140.7906	-5743.9173	0.000227	811.3957	5.799E+09	399.2313	591040.	0.000
156.00	-0.002713	-33629.	-3434.4480	0.000206	698.1084	5.799E+09	370.5918	819639.	0.000
162.00	-0.001582	-47742.	-1326.3386	0.000164	6018.3039	5.799E+09	332.1114	1259887.	0.000
168.00	-0.000747	-49853.	516.4926	0.000113	5028.8036	5.799E+09	282.1657	2266973.	0.000
174.00	-0.000221	-41758.	1848.6569	6.595E-05	3988.5401	5.799E+09	161.8891	4385266.	0.000
180.00	4.456E-05	27794.	2234.2951	2.996E-05	3119.0880	5.799E+09	-33.2430	4489103.	0.000
186.00	0.000138	-15003.	1817.1406	7.823E-06	2555.4712	5.799E+09	-105.7085	4593702.	0.000
192.00	0.000138	-6002.6530	1180.2567	-3.045E-06	2100.7087	5.799E+09	-106.5861	4619597.	0.000
198.00	0.000102	-833.8697	625.9731	-6.582E-06	1785.0013	5.799E+09	-78.1751	4619597.	0.000
204.00	5.946E-05	1521.4239	237.7972	-2.266E-06	1523.2262	5.799E+09	-50.5502	5101169.	0.000
210.00	2.683E-05	2055.4257	12.3235	-4.375E-06	1291.0768	5.799E+09	-25.2743	5653125.	0.000
216.00	6.954E-06	1677.5489	-83.1550	-2.444E-06	1098.1974	5.799E+09	-6.5518	5653125.	0.000
222.00	-2.503E-06	1062.1707	-95.7368	-1.027E-06	948.1367	5.799E+09	2.3579	5653125.	0.000
228.00	-5.365E-06	530.6415	-73.4995	-2.025E-07	783.4931	5.799E+09	5.0545	5653125.	0.000
234.00	-4.932E-06	180.5581	-44.3943	1.655E-07	658.7520	5.799E+09	4.6472	5653125.	0.000
240.00	-3.379E-06	-2.4024	-20.9017	2.576E-07	568.8659	5.799E+09	3.1837	5653125.	0.000
246.00	-1.841E-06	-70.7473	-6.1478	2.198E-07	481.2058	5.799E+09	1.7343	5653125.	0.000
252.00	-7.415E-07	-76.5901	-1.1509	1.436E-07	408.2459	5.799E+09	0.6986	5653125.	0.000

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258.000	-1.179E-07	-57.2071	3.5799	7.435E-06	781.385	5.799E+09	0.1110	5653125.	0.000
264.000	1.506E-07	-33.7708	3.4873	2.728E-08	781.0719	5.799E+09	-0.1419	5653125.	0.000
270.000	2.095E-07	-15.4110	2.4694	1.832E-09	780.9306	5.799E+09	-0.1974	5653125.	0.000
276.000	1.726E-07	-4.1411	1.3894	-8.283E-09	780.8745	5.799E+09	-0.1626	5653125.	0.000
282.000	1.101E-07	1.2777	0.5904	-9.765E-09	780.8603	5.799E+09	-0.1037	5653125.	0.000
288.000	5.545E-08	2.9618	0.1225	-7.571E-09	780.8687	5.799E+09	-0.0522	5653125.	0.000
294.000	1.921E-08	2.7623	-0.0885	-4.610E-09	780.8677	5.799E+09	-0.0181	5653125.	0.000
300.000	1.281E-10	1.9085	-0.1432	-2.193E-09	780.8634	5.799E+09	-0.000121	5653125.	0.000
306.000	-7.108E-09	1.0485	-0.1234	-6.635E-10	780.8592	5.799E+09	0.006697	5653125.	0.000
312.000	-7.834E-09	0.4285	-0.0812	1.006E-10	780.8561	5.799E+09	0.007381	5653125.	0.000
318.000	-5.900E-09	0.0739	-0.0424	3.605E-10	780.8543	5.799E+09	0.005559	5653125.	0.000
324.000	-3.507E-09	-0.0808	-0.0158	3.570E-10	780.8543	5.799E+09	0.003305	5653125.	0.000
330.000	-1.616E-09	-0.1163	-0.001310	2.550E-10	780.8545	5.799E+09	0.001523	5653125.	0.000
336.000	-4.473E-10	-0.0970	0.004523	1.447E-10	780.8544	5.799E+09	0.000421	5653125.	0.000
342.000	1.198E-10	-0.0623	0.005449	6.227E-11	780.8542	5.799E+09	-0.000113	5653125.	0.000
348.000	3.000E-10	-0.0317	0.004262	1.363E-11	780.8541	5.799E+09	-0.000283	5653125.	0.000
354.000	2.834E-10	-0.0112	0.002613	-8.559E-12	780.8540	5.799E+09	-0.000267	5653125.	0.000
360.000	1.973E-10	-0.000316	0.001255	-1.452E-11	780.8539	5.799E+09	-0.000186	5653125.	0.000
366.000	1.092E-10	0.003880	0.000388	-1.267E-11	780.8540	5.799E+09	-0.000103	5653125.	0.000
372.000	4.517E-11	0.004369	-4.779E-05	-8.406E-12	780.8540	5.799E+09	-4.256E-05	5653125.	0.000
378.000	8.291E-12	0.003322	-0.000199	-4.427E-12	780.8540	5.799E+09	-7.812E-06	5653125.	0.000
384.000	-7.957E-12	0.001991	-0.000200	-1.678E-12	780.8539	5.799E+09	7.497E-06	5653125.	0.000
390.000	-1.184E-11	0.000928	-0.000144	0.000	780.8539	5.799E+09	1.116E-05	5653125.	0.000
396.000	-9.972E-12	0.000265	-8.220E-05	0.000	780.8539	5.799E+09	9.395E-06	5653125.	0.000
402.000	-6.455E-12	-5.970E-05	-3.577E-05	0.000	780.8539	5.799E+09	6.082E-06	5653125.	0.000
408.000	-3.309E-12	-0.000165	-8.173E-06	0.000	780.8539	5.799E+09	3.118E-06	5653125.	0.000
414.000	-1.189E-12	-0.000159	-4.542E-06	0.000	780.8539	5.799E+09	1.121E-06	5653125.	0.000
420.000	0.000	0.000111	8.059E-06	0.000	780.8539	5.799E+09	5.147E-08	5653125.	0.000
426.000	0.000	-6.214E-05	7.114E-06	0.000	780.8539	5.799E+09	-3.664E-07	5653125.	0.000
432.000	0.000	-2.606E-05	4.753E-06	0.000	780.8539	5.799E+09	-4.208E-07	5653125.	0.000
438.000	0.000	-5.106E-06	2.522E-06	0.000	780.8539	5.799E+09	-3.227E-07	5653125.	0.000
444.000	0.000	4.239E-06	9.698E-07	0.000	780.8539	5.799E+09	-1.947E-07	5653125.	0.000
450.000	0.000	6.570E-06	1.109E-07	0.000	780.8539	5.799E+09	-9.158E-08	5653125.	0.000
456.000	0.000	5.597E-06	-2.444E-07	0.000	780.8539	5.799E+09	-2.685E-08	5653125.	0.000
462.000	0.000	3.653E-06	-3.096E-07	0.000	780.8539	5.799E+09	5.137E-09	5653125.	0.000
468.000	0.000	1.890E-06	-2.469E-07	0.000	780.8539	5.799E+09	1.576E-08	5653125.	0.000
474.000	0.000	6.920E-07	-1.537E-07	0.000	780.8539	5.799E+09	1.532E-08	5653125.	0.000
480.000	0.000	4.506E-08	-7.518E-08	0.000	780.8539	5.799E+09	1.084E-08	5653125.	0.000
486.000	0.000	-2.117E-07	-2.438E-08	0.000	780.8539	5.799E+09	6.093E-09	5653125.	0.000
492.000	0.000	-2.489E-07	1.654E-09	0.000	780.8539	5.799E+09	2.585E-09	5653125.	0.000
498.000	0.000	-1.928E-07	1.101E-08	0.000	780.8539	5.799E+09	5.332E-10	5653125.	0.000
504.000	0.000	-1.173E-07	1.144E-08	0.000	780.8539	5.799E+09	-3.912E-10	5653125.	0.000
510.000	0.000	-5.573E-08	8.373E-09	0.000	780.8539	5.799E+09	-6.296E-10	5653125.	0.000
516.000	0.000	-1.681E-08	4.858E-09	0.000	780.8539	5.799E+09	-5.421E-10	5653125.	0.000
522.000	0.000	2.613E-09	2.163E-09	0.000	780.8539	5.799E+09	-3.563E-10	5653125.	0.000
528.000	0.000	9.202E-09	5.362E-10	0.000	780.8539	5.799E+09	-1.859E-10	5653125.	0.000
534.000	0.000	9.095E-09	-2.285E-10	0.000	780.8539	5.799E+09	-6.910E-11	5653125.	0.000
540.000	0.000	6.490E-09	-4.526E-10	0.000	780.8539	5.799E+09	-5.596E-12	5653125.	0.000
546.000	0.000	3.678E-09	-4.096E-10	0.000	780.8539	5.799E+09	1.994E-11	5653125.	0.000
552.000	0.000	1.581E-09	-2.779E-10	0.000	780.8539	5.799E+09	2.396E-11	5653125.	0.000
558.000	0.000	3.438E-10	-1.498E-10	0.000	780.8539	5.799E+09	1.874E-11	5653125.	0.000
564.000	0.000	-2.187E-10	-5.905E-11	0.000	780.8539	5.799E+09	1.150E-11	5653125.	0.000
570.000	0.000	-3.670E-10	-7.908E-12	0.000	780.8539	5.799E+09	5.545E-12	5653125.	0.000
576.000	0.000	-3.152E-10	1.394E-11	0.000	780.8539	5.799E+09	1.756E-12	5653125.	0.000
582.000	0.000	-2.007E-10	1.846E-11	0.000	780.8539	5.799E+09	0.000	5653125.	0.000
588.000	0.000	-9.424E-11	1.470E-11	0.000	780.8539	5.799E+09	-1.021E-12	5653125.	0.000
594.000	0.000	-2.443E-11	7.858E-12	0.000	780.8539	5.799E+09	-1.261E-12	5653125.	0.000
600.000	0.000	0.000	0.000	0.000	780.8539	5.799E+09	-1.358E-12	2826562.	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:
 Pile-head deflection = 0.9756677 inches
 Computed slope at pile head = -0.0146398 radians
 Maximum bending moment = 949558. inch-lbs
 Maximum shear force = 27000. lbs
 Depth of maximum bending moment = 66.000000 inches below pile head
 Depth of maximum shear force = 0.000000 inches below pile head
 Number of iterations = 33
 Number of zero deflection points = 12

 Pile-head Deflection vs. Pile Length for Load Case 1

Boundary Condition Type 1, Shear and Moment

Shear = 27000. lbs
 Moment = 0. in-lbs
 Axial Load = 157000. lbs

Pile Length Pile Head Deflection Maximum Moment Maximum Shear

Abut 5R_transv_Critical Length			
feet	inches	In-lbs	lbs
50.000	0.9756677	949558.	27000.
47.500	0.9850924	951245.	27000.
45.000	0.9912324	953694.	27000.
42.500	0.9957888	957848.	27000.
40.000	1.0013538	960731.	27000.
37.500	1.0029193	964810.	27000.
35.000	1.0144167	966471.	27000.
32.500	1.0140862	970659.	27000.
30.000	1.0215556	973083.	27000.
27.500	1.0249842	976575.	27000.
25.000	1.0202715	981986.	27000.
22.500	1.0365307	983137.	27000.
20.000	1.0423497	986145.	27000.
17.500	1.0466346	989608.	27000.
15.000	1.0501925	993343.	27000.
12.500	1.1351107	982517.	27000.

 Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	1	V = 27000.	M = 0.000	157000.	0.97566765	949558.	27000.	-0.01463982

The analysis ended normally.

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Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 5
 Name of input data file: Abut 5R_transv_Ave P.lpd
 Name of output report file: Abut 5R_transv_Ave P.lpp
 Name of plot output file: Abut 5R_transv_Ave P.lpp
 Name of runtime message file: Abut 5R_transv_Ave P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 9:45:25

Problem Title

Project Name: Palo Comado OC Bridge Widen

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

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Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 16.0000000 in
 Bottom Width = 16.0000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 5 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 7.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 7.00000 ft
 Distance from top of pile to bottom of layer = 12.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 12.00000 ft
 Distance from top of pile to bottom of layer = 17.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 17.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 130.00000 pcf
 Effective unit weight at bottom of layer = 130.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Uniaxial Elastic Mod.	ROD % or GSI
Num.	Epsilon 50	J (psi)	ft	pcf	psf	deg.	psi	
1	0.00700	Stiff Clay w/o Free Water	2.000	120.000	4000.000			
2	0.00700	Stiff Clay w/o Free Water	0.10000	120.000	4000.000			
3	0.00700	Stiff Clay w/o Free Water	7.000	120.000	1500.000			
4	0.00700	Stiff Clay w/o Free Water	12.000	125.000	4000.000			
5	0.00500	Stiff Clay w/o Free Water	17.000	130.000	4000.000			
	0.00500		80.000	130.000	4000.000			

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X Ft	p-mult	y-mult
1	0.000	0.6700	1.0000
2	50.000	0.6700	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

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Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4 y =	0.25000 in	M = 0.0000 in-lbs	157000.	False
2	4 y =	0.50000 in	M = 0.0000 in-lbs	157000.	False
3	4 y =	1.00000 in	M = 0.0000 in-lbs	157000.	False

V = perpendicular shear force applied to pile head

M = bending moment applied to pile head

y = lateral deflection relative to pile axis

S = pile slope relative to original pile batter angle

R = rotational stiffness applied to pile head

Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection

For Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.250000 inches

Moment at pile head = 0.000 in-lbs

Axial load at pile head = 157000.000 lbs

Depth X inches	Deflect. Y inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi	Bending Stiffness lb-in ²	Soil Res. p lb/in ²	Soil Spr. Es ^h lb/inch	Distrib. Lat. Load lb/inch
0.00	0.2500	0.000	14728.	-0.004683	780.8539	5.799E+09	-551.4203	6617.0437	0.000
6.000	0.2219	82851.	12233.	-0.004640	1192.9209	5.799E+09	-280.0159	7571.3288	0.000
12.000	0.1943	155541.	10546.	-0.004517	1554.4496	5.799E+09	-282.4711	8721.8793	0.000
18.000	0.1677	217910.	8848.0527	-0.004324	1864.6480	5.799E+09	-283.4332	10141.	0.000
24.000	0.1424	269863.	7149.2768	-0.004071	2123.0415	5.799E+09	-282.8254	11914.	0.000
30.000	0.1188	311371.	5459.1072	-0.003770	2329.4870	5.799E+09	-280.5644	14164.	0.000
36.000	0.0972	342476.	3787.7419	-0.003432	2484.1882	5.799E+09	-276.5574	17073.	0.000
42.000	0.0777	363290.	2145.9764	-0.003067	2587.7118	5.799E+09	-270.6978	20914.	0.000
48.000	0.0604	374006.	545.3050	-0.002686	2641.0059	5.799E+09	-262.8593	26118.	0.000
54.000	0.0454	374894.	-1001.9255	-0.002298	2645.4221	5.799E+09	-252.8842	33396.	0.000
60.000	0.0328	366312.	-2482.2672	-0.001915	2602.7421	5.799E+09	-240.5631	43994.	0.000
66.000	0.0225	348714.	-3880.7395	-0.001545	2515.2137	5.799E+09	-225.5944	60273.	0.000
72.000	0.0143	322654.	-5179.9973	-0.001197	2385.6023	5.799E+09	-207.4915	87235.	0.000
78.000	0.008088	288810.	-6358.4668	-0.000881	2217.2755	5.799E+09	-185.3316	137482.	0.000
84.000	0.003698	248012.	-7521.9380	-0.000603	2014.3650	5.799E+09	-202.4921	328507.	0.000
90.000	0.000848	199683.	-8729.6731	-0.000372	1773.9962	5.799E+09	-200.0862	1415217.	0.000
96.000	-0.000762	143956.	-8735.2483	-0.000194	1496.8341	5.799E+09	198.2278	1560615.	0.000
102.000	-0.001479	95225.	-7414.6062	-7.018E-05	1254.4666	5.799E+09	241.9862	981830.	0.000
108.000	-0.001604	55113.	-5925.3115	7.601E-06	1054.9650	5.799E+09	254.4454	951634.	0.000
114.000	-0.001388	24107.	-4404.5536	4.859E-05	900.7544	5.799E+09	252.4740	1091717.	0.000
120.000	-0.001021	2167.1114	-2926.0436	6.218E-05	791.6323	5.799E+09	240.3627	1412202.	0.000
126.000	-0.000641	-11122.	-1545.7489	5.755E-05	836.1715	5.799E+09	219.7355	2055468.	0.000
132.000	-0.000331	-16490.	-313.4917	4.326E-05	862.8699	5.799E+09	191.0169	3466094.	0.000
138.000	-0.000122	-14966.	483.0734	2.699E-05	855.2870	5.799E+09	74.5048	3655723.	0.000
144.000	6.815E-06	-10744.	718.9693	1.369E-05	834.2915	5.799E+09	4.1272	3633478.	0.000
150.000	4.195E-05	-6363.8083	648.1187	4.835E-06	812.5049	5.799E+09	-27.7440	3968431.	0.000
156.000	5.120E-05	-2975.9412	460.6260	2.602E-09	795.6551	5.799E+09	-34.7535	4072635.	0.000
162.000	4.198E-05	-835.3088	268.6970	-1.970E-06	785.0134	5.799E+09	-29.2288	4176842.	0.000
168.000	2.756E-05	252.1341	122.0272	-2.272E-06	782.1080	5.799E+09	-19.6672	4281053.	0.000
174.000	1.472E-05	632.3055	30.7610	-1.814E-06	783.9988	5.799E+09	-10.7549	4385266.	0.000
180.000	5.792E-06	624.6848	-14.5043	-1.164E-06	783.9609	5.799E+09	-4.3336	4489483.	0.000
186.000	7.465E-07	460.4466	-29.2197	-6.026E-07	783.1440	5.799E+09	-0.5715	4593702.	0.000
192.000	-1.440E-06	275.1840	-27.6082	-2.220E-07	782.2226	5.799E+09	1.1087	4619597.	0.000
198.000	-1.918E-06	129.5661	-19.8519	-1.264E-08	781.4983	5.799E+09	1.4768	4619597.	0.000
204.000	-1.592E-06	36.9852	-11.6006	7.352E-08	781.0379	5.799E+09	1.2737	4801100.	0.000
210.000	-1.036E-06	-9.7802	-5.1774	8.760E-08	780.9026	5.799E+09	0.8674	5025000.	0.000
216.000	-5.405E-07	-25.3085	-1.2171	6.945E-08	780.9798	5.799E+09	0.4527	5025000.	0.000
222.000	-2.024E-07	-24.5160	0.6494	4.367E-08	780.9759	5.799E+09	0.1695	5025000.	0.000
228.000	-1.648E-08	-17.5975	1.1993	2.188E-08	780.9415	5.799E+09	0.0138	5025000.	0.000
234.000	6.018E-08	-10.1650	1.0896	7.517E-09	780.9045	5.799E+09	-0.0504	5025000.	0.000

Abut	SR	transv	Ave	P	5.799E+09	-0.0617	5025000.	0.000
240.000	7.373E-08	-4.5370	0.7531	-8.893E-11	780.8545	5.799E+09	-0.0617	5025000.
246.000	5.911E-08	-1.1275	0.4194	-3.020E-09	780.8595	5.799E+09	-0.0495	5025000.
252.000	3.749E-08	0.5009	0.1766	-3.344E-09	780.8564	5.799E+09	-0.0314	5025000.
258.000	1.899E-08	0.9984	0.0347	-2.568E-09	780.8589	5.799E+09	-0.0159	5025000.
264.000	6.679E-09	0.9224	-0.0298	-1.574E-09	780.8585	5.799E+09	-0.005993	5025000.
270.000	9.657E-11	0.6442	-0.0468	-7.637E-10	780.8571	5.799E+09	-8.088E-05	5025000.
276.000	-2.486E-09	0.3624	-0.0408	-2.430E-10	780.8557	5.799E+09	0.002082	5025000.
282.000	-2.819E-09	0.1552	-0.0275	2.483E-11	780.8547	5.799E+09	0.002361	5025000.
288.000	-2.188E-09	0.0329	-0.0149	1.222E-10	780.8541	5.799E+09	0.001833	5025000.
294.000	-1.353E-09	-0.0235	-0.005976	1.270E-10	780.8541	5.799E+09	0.001133	5025000.
300.000	-6.639E-10	-0.0391	-0.000909	9.466E-11	780.8541	5.799E+09	0.000556	5025000.
306.000	-2.171E-10	-0.0346	0.001305	5.657E-11	780.8541	5.799E+09	0.000182	5025000.
312.000	1.444E-11	-0.0258	0.001813	2.652E-11	780.8541	5.799E+09	-1.252E-05	5025000.
318.000	1.011E-10	-0.0129	0.001521	7.693E-12	780.8540	5.799E+09	-8.464E-05	5025000.
324.000	1.073E-10	-0.005270	0.000998	-1.693E-12	780.8540	5.799E+09	-8.983E-05	5025000.
330.000	8.075E-11	-0.000895	0.000525	-4.882E-12	780.8539	5.799E+09	-6.763E-05	5025000.
336.000	4.868E-11	0.001045	0.000200	-4.805E-12	780.8539	5.799E+09	-4.077E-05	5025000.
342.000	2.309E-11	0.001517	1.997E-05	-3.479E-12	780.8539	5.799E+09	-1.934E-05	5025000.
348.000	6.928E-12	0.001291	-5.546E-05	-2.026E-12	780.8539	5.799E+09	-5.802E-06	5025000.
354.000	-1.219E-12	0.000855	-6.980E-05	0.0000	780.8539	5.799E+09	1.021E-06	5025000.
360.000	-4.055E-12	0.000455	-5.655E-05	0.0000	780.8539	5.799E+09	3.396E-06	5025000.
366.000	-4.063E-12	0.000177	-3.616E-05	0.0000	780.8539	5.799E+09	3.403E-06	5025000.
372.000	-2.971E-12	2.142E-05	-1.848E-05	0.0000	780.8539	5.799E+09	2.488E-06	5025000.
378.000	-1.745E-12	-4.490E-05	-6.636E-06	0.0000	780.8539	5.799E+09	1.462E-06	5025000.
384.000	0.000	-5.855E-05	-2.439E-07	0.0000	780.8539	5.799E+09	6.689E-07	5025000.
390.000	0.000	-4.807E-05	2.305E-06	0.0000	780.8539	5.799E+09	1.806E-07	5025000.
396.000	0.000	-3.103E-05	2.673E-06	0.0000	780.8539	5.799E+09	-5.777E-08	5025000.
402.000	0.000	-1.605E-05	0.996E-06	0.0000	780.8539	5.799E+09	-3.48E-07	5025000.
408.000	0.000	-5.901E-06	1.306E-06	0.0000	780.8539	5.799E+09	-1.284E-07	5025000.
414.000	0.000	-3.676E-07	6.473E-07	0.0000	780.8539	5.799E+09	-9.125E-08	5025000.
420.000	0.000	1.851E-06	2.168E-07	0.0000	780.8539	5.799E+09	-5.223E-08	5025000.
426.000	0.000	2.247E-06	-8.851E-09	0.0000	780.8539	5.799E+09	-2.299E-08	5025000.
432.000	0.000	1.783E-06	-9.412E-08	0.0000	780.8539	5.799E+09	-5.433E-09	5025000.
438.000	0.000	1.122E-06	-1.019E-07	0.0000	780.8539	5.799E+09	2.852E-09	5025000.
444.000	0.000	-7.729E-08	-6.962E-09	0.0000	780.8539	5.799E+09	1.860E-09	5025000.
450.000	0.000	1.939E-07	-4.703E-08	0.0000	780.8539	5.799E+09	4.823E-09	5025000.
456.000	0.000	-1.761E-09	-2.255E-08	0.0000	780.8539	5.799E+09	3.337E-09	5025000.
462.000	0.000	-7.729E-08	-6.962E-09	0.0000	780.8539	5.799E+09	1.860E-09	5025000.
468.000	0.000	-8.578E-08	9.711E-10	0.0000	780.8539	5.799E+09	1.846E-10	5025000.
474.000	0.000	-6.595E-08	3.791E-09	0.0000	780.8539	5.799E+09	1.553E-10	5025000.
480.000	0.000	-4.047E-08	3.864E-09	0.0000	780.8539	5.799E+09	-1.310E-10	5025000.
486.000	0.000	-1.965E-08	-2.069E-10	0.0000	780.8539	5.799E+09	2.069E-10	5025000.
492.000	0.000	-6.271E-09	1.688E-09	0.0000	780.8539	5.799E+09	-1.806E-10	5025000.
498.000	0.000	6.189E-10	7.815E-10	0.0000	780.8539	5.799E+09	-1.217E-10	5025000.
504.000	0.000	3.128E-09	2.186E-10	0.0000	780.8539	5.799E+09	-6.597E-11	5025000.
510.000	0.000	-1.232E-10	3.013E-12	0.0000	780.8539	5.799E+09	-2.655E-11	5025000.
516.000	0.000	2.431E-09	-1.509E-10	0.0000	780.8539	5.799E+09	-4.082E-12	5025000.
522.000	0.000	1.454E-09	-1.459E-10	0.0000	780.8539	5.799E+09	5.748E-12	5025000.
528.000	0.000	6.825E-10	-1.046E-10	0.0000	780.8539	5.799E+09	8.017E-12	5025000.
534.000	0.000	1.987E-10	-6.038E-11	0.0000	780.8539	5.799E+09	6.736E-12	5025000.
540.000	0.000	-4.274E-11	-2.691E-11	0.0000	780.8539	5.799E+09	4.422E-12	5025000.
546.000	0.000	-1.250E-10	-6.647E-12	0.0000	780.8539	5.799E+09	2.331E-12	5025000.
552.000	0.000	-1.232E-10	3.013E-12	0.0000	780.8539	5.799E+09	0.000	5025000.
558.000	0.000	-8.924E-11	5.945E-12	0.0000	780.8539	5.799E+09	0.000	5025000.
564.000	0.000	-5.205E-11	5.462E-12	0.0000	780.8539	5.799E+09	0.000	5025000.
570.000	0.000	-2.377E-11	3.766E-12	0.0000	780.8539	5.799E+09	0.000	5025000.
576.000	0.000	-6.850E-12	2.042E-12	0.0000	780.8539	5.799E+09	0.000	5025000.
582.000	0.000	0.000	0.000	0.0000	780.8539	5.799E+09	0.000	5025000.
588.000	0.000	2.389E-12	0.000	0.0000	780.8539	5.799E+09	0.000	5025000.
594.000	0.000	1.220E-12	0.000	0.0000	780.8539	5.799E+09	0.000	5025000.
600.000	0.000	0.000	0.000	0.0000	780.8539	5.799E+09	0.000	2512500.

Depth	Deflect.	Bendng	Shear	Sl	Abut	SR	transv	Ave	P	Bendng	Soil	Res.	Soil	Spr.	Di
inches	inches	Moment	Force	age	Total	Stress	Stiffness	Res.	Stress	Stiffness	p	p	Spr.	Stiffness	Stiffness
		in-lbs	lbs	radians	psi*	lb-in ²	lb-in ²	lb/in ²	psi	lb/in ²	lb/in ²	lb/in ²	lb/in ²	lb/in ²	lb/in ²
6.000	0.4499	116145.	17044.	-0.008294	780.8539	5.799E+09	-65.7530	3934.5177	0.000						
12.000	0.4005	220148.	15026.	-0.008120	1875.7818	5.799E+09	-338.4440	5070.6626	0.000						
18.000	0.3524	311753.	12987.	-0.007845	2331.3860	5.799E+09	-341.2587	5809.6996	0.000						
24.000	0.3063	390768.	10935.	-0.007481	2724.3768	5.799E+09	-342.4977	6708.2717	0.000						
30.000	0.2627	457073.	8881.7201	-0.007043	3054.1492	5.799E+09	-342.0794	7814.1505	0.000						
36.000	0.2218	510617.	6835.7376	-0.006542	3320.4567	5.799E+09	-339.9147	9194.1528	0.000						
42.000	0.1842	551427.	4808.2812	-0.005993	3523.4273	5.799E+09	-335.9040	10944.	0.000						
48.000	0.1499	579607.	2810.7709	-0.005407	3663.5813	5.799E+09	-329.9327	13205.	0.000						
54.000	0.1193	595344.	855.3785	-0.004799	3741.8512	5.799E+09	-321.8647	16192.	0.000						
60.000	0.0923	598914.	-1044.8100	-0.004182	3759.6054	5.799E+09	-311.5314	20247.	0.000						
66.000	0.0691	590684.	-2875.5439	-0.003566	3718.6766	5.799E+09	-298.7132	25941.	0.000						
72.000	0.0495	571126.	-4620.9965	-0.002965	3621.3999	5.799E+09	-283.1043	34298.	0.000						
78.000	0.0335	540819.	-6263.0395	-0.002390	3470.6648	5.799E+09	-264.2416	47315.	0.000						
84.000	0.0208	500472.	-7990.4698	-0.001851	3269.9957	5.799E+09	-231.5701	89667.	0.000						
90.000	0.0113	448420.	-10065.	-0.001360	3011.1139	5.799E+09	-379.7836	201736.	0.000						
96.000	0.004526	382260.	-12139.	-0.000930	2682.0583	5.799E+09	-311.8160	413234.	0.000						
102.000	0.000131	304051.	-13278.	-0.000575	2295.3191	5.799E+09	-67.5989	3104259.	0.000						
108.000	-0.002375	224012.	-12638.	-0.000302	1895.0003	5.799E+09	280.9484	709857.	0.000						
114.000	-0.003489	153419.	-10840.	-0.000106	1543.8990	5.799E+09	318.3489	540116.	0.000						
120.000	-0.003651	94137.	-8891.6059	2.168E-05	1249.0542	5.799E+09	330.9938	434890.	0.000						
126.000	-0.003229	46679.	-6909.6051	9.454E-05	1013.0172	5.799E+09	329.6732	612571.	0.000						
132.000	-0.002575	11044.	-4966.8722	0.000124	835.7871	5.799E+09	317.9045	800123.	0.000						
138.000	-0.001736	-18158.	-3121.8447	0.000123	646.2947	5.799E+09	297.1047	1026705.	0.000						
144.000	-0.001037	-26651.	-1452.0563	0.000103	913.4030	5.799E+09	259.4914	1510204.	0.000						
150.000	-0.000504	-30776.	35.6039	7.300E-05	933.9204	5.799E+09	236.3953	2815846.	0.000						
156.000	-0.000185	-10718.	1073.0885	4.344E-05	109.4396	5.799E+09	109.4396	4472635.	0.000						
162.000	0.1759E-05	-17980.	1364.6932	2.050E-05	870.2810	5.799E+09	-12.2447	4176842.	0.000						
168.000	8.478E-05	-10023	1146.4816	6.013E-06	830.7051	5.799E+09	-60.4925	4218053.	0.000						
174.000	8.975E-05	-4233.9249	768.2229	-1.363E-06	801.9118	5.799E+09	-65.5937	4385266.	0.000						
180.000	6.843E-05	801.9269	417.8491	-3.968E-06	784.8424	5.799E+09	-51.1902	4489483.							

Abut SR_transv_Ave P									
522.000	0.000	5.962E-09	1.711E-10	0.000	780.8539	5.799E+09	-8.962E-11	5025000.	0.000
528.000	0.000	5.386E-09	1.891E-10	0.000	780.8539	5.799E+09	-3.042E-11	5025000.	0.000
534.000	0.000	3.710E-09	-2.780E-10	0.000	780.8539	5.799E+09	0.000	5025000.	0.000
540.000	0.000	2.059E-09	-2.375E-10	0.000	780.8539	5.799E+09	1.269E-11	5025000.	0.000
546.000	0.000	8.621E-10	-1.578E-10	0.000	780.8539	5.799E+09	1.390E-11	5025000.	0.000
552.000	0.000	1.649E-10	-8.424E-11	0.000	780.8539	5.799E+09	1.062E-11	5025000.	0.000
558.000	0.000	-1.502E-10	-3.294E-11	0.000	780.8539	5.799E+09	6.483E-12	5025000.	0.000
564.000	0.000	-2.318E-10	-4.110E-12	0.000	780.8539	5.799E+09	3.129E-12	5025000.	0.000
570.000	0.000	-2.006E-10	8.216E-12	0.000	780.8539	5.799E+09	0.000	5025000.	0.000
576.000	0.000	-1.339E-10	1.078E-11	0.000	780.8539	5.799E+09	0.000	5025000.	0.000
582.000	0.000	-7.151E-11	8.797E-12	0.000	780.8539	5.799E+09	0.000	5025000.	0.000
588.000	0.000	-2.838E-11	5.471E-12	0.000	780.8539	5.799E+09	0.000	5025000.	0.000
594.000	0.000	-5.848E-12	2.361E-12	0.000	780.8539	5.799E+09	0.000	5025000.	0.000
600.000	0.000	0.000	0.000	0.000	780.8539	5.799E+09	0.000	2512500.	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Pile-head deflection	=	0.5000000	inches
Computed slope at pile head	=	-0.0083540	radians
Maximum bending moment	=	598914.	inch-lbs
Maximum shear force	=	60.0000000	inches below pile head
Depth of maximum bending moment	=	60.0000000	inches below pile head
Depth of maximum shear force	=	0.0000000	inches below pile head
Number of iterations	=	12	
Number of zero deflection points	=	12	

Computed Values of Pile Loading and Deflection
For Lateral Loading for Load Case Number 3

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 1.000000 inches
 Moment at pile head = 0.000000 in-lbs
 Axial load at pile head = 157000.000 lbs

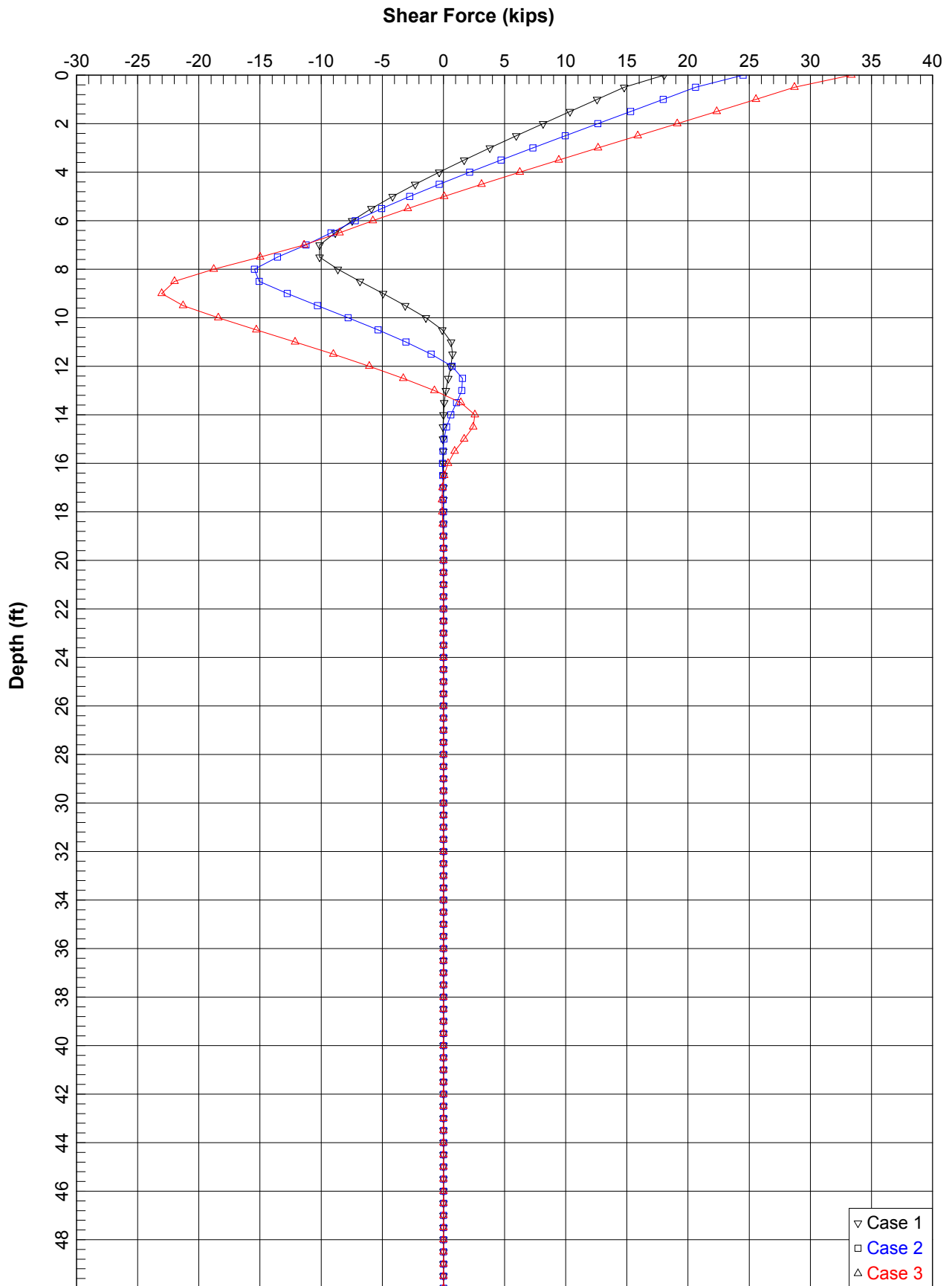
Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil Res.	Soil Spr.	Distrib.
x	y	Moment	Force	radians	Stress	Stiffness	lb/in	lb/inch	lb/inch
inches	inches	in-lbs	lbs		psi	lb-in ²			
0.00	1.0000	0.000	27301.	-0.0149	780.8539	5.799E+09	-779.8261	2359.4782	0.000
6.00	0.9103	163850.	-23766.	-0.0149	1595.7792	5.799E+09	-398.5101	2626.6182	0.000
12.00	0.8217	313195.	-21356.	-0.0146	2338.5571	5.799E+09	-405.0557	2957.8508	0.000
18.00	0.7349	447652.	-18910.	-0.0142	3007.2918	5.799E+09	-410.0851	3347.9238	0.000
24.00	0.6510	566970.	-16439.	-0.0137	3600.4309	5.799E+09	-413.5233	3811.2964	0.000
30.00	0.5706	670728.	-13953.	-0.0131	4116.7806	5.799E+09	-415.2908	4367.0704	0.000
36.00	0.4943	758942.	-11461.	-0.0123	4555.5213	5.799E+09	-415.3022	5040.8967	0.000
42.00	0.4228	831465.	-8974.7600	-0.0115	4916.2231	5.799E+09	-413.4644	5867.8650	0.000
48.00	0.3564	888294.	-6505.3468	-0.0106	5198.8637	5.799E+09	-409.6733	6897.0032	0.000
54.00	0.2955	925008.	-4064.8945	-0.009664	5403.8462	5.799E+09	-403.8108	8198.5144	0.000
60.00	0.2404	955279.	-1666.2467	-0.008689	5532.0205	5.799E+09	-395.7385	9875.8531	0.000
66.00	0.1913	965872.	-676.8386	-0.007695	5584.7072	5.799E+09	-385.2900	12087.	0.000
72.00	0.1481	961653.	-2949.4799	-0.006697	5563.7255	5.799E+09	-372.2571	15082.	0.000
78.00	0.1109	943096.	-5135.3563	-0.005712	5471.4296	5.799E+09	-356.3683	19282.	0.000
84.00	0.0795	910790.	-7510.6530	-0.004753	5310.7542	5.799E+09	-335.3972	24840.	0.000
90.00	0.0539	861923.	-10500.	-0.003836	5067.7058	5.799E+09	-301.0708	32505.	0.000
96.00	0.0335	792016.	-13725.	-0.002980	4720.0197	5.799E+09	-254.0598	42016.	0.000
102.00	0.0181	702832.	-16630.	-0.002207	4276.4519	5.799E+09	-204.1597	55064.	0.000
108.00	0.007040	596612.	-19101.	-0.001534	3748.1600	5.799E+09	-169.4532	71486.	0.000
114.00	0.003014	476511.	-19694.	-0.000979	3150.8254	5.799E+09	-117.8247	92849.	0.000
120.00	0.004710	362131.	-18120.	-0.000545	2581.9459	5.799E+09	-75.7374	119386.	0.000
126.00	-0.006857	260097.	-15867.	-0.000223	2074.4682	5.799E+09	-398.1542	148387.	0.000
132.00	-0.007390	172142.	-13424.	2.715E-07	1637.0189	5.799E+09	416.4561	138132.	0.000
138.00	-0.006854	99012.	-10917.	0.000141	1273.3012	5.799E+09	419.2457	97017.	0.000
144.00	-0.005703	40879.	-8464.8499	0.000213	984.1692	5.799E+09	397.9824	618698.	0.000
150.00	-0.004299	-2966.9714	-6055.9029	0.000233	795.6104	5.799E+09	404.9999	565293.	0.000
156.00	-0.002913	-32230.	-3709.8783	0.000214	641.1528	5.799E+09	377.0749	476783.	0.000
162.00	-0.001727	-47887.	-1560.5280	0.000173	509.0239	5.799E+09	339.3085	390885.	0.000
168.00	-0.000838	-51282.	-328.0858	0.000122	403.9100	5.799E+09	290.2294	2078144.	0.000
174.00	-0.000268	-44179.	1785.6421	7.219E-05	300.5620	5.799E+09	195.6227	1485266.	0.000
180.00	2.830	2390.	2390.	3.382E-05	230.8498	5.799E+09	-21.2202	448948.	0.000
186.00	5.405E-06	626.0251	6.7177	-3.381E-07	183.9675	5.799E+09	-53.3101	4801.0000	0.000
192.00	0.000145	-6875.0853	1274.7079	-2.364E-06	815.0478	5.799E+09	-111.9033	4619597.	0.000
198.00	0.000110	-1235.6200	685.3422	-6.560E-06	786.9988	5.799E+09	-84.5519	4619597.	0.000
204.00	6.642E-05	136.8206	271.7563	-6.495E-06	783.9249	5.799E+09	1.5266	5025000.	0.000
210.00	3.188E-05	2037.7913	31.7292	-4.736E-06	790.9891	5.799E+09	-26.6989	5025000.	0.000
216.00	9.788E-06	1751.0536	-72.9593	-2.776E-06	789.5630	5.799E+09	-8.1972	5025000.	0.000
222.00	-1.433E-06	1167.5098	-93.9511	-1.266E-06	786.6607	5.799E+09	1.1999	5025000.	0.000
228.00	-5.405E-06	626.0251	6.7177	-3.381E-07	783.9675	5.799E+09	4.5266	5025000.	0.000
234.00	-5.490E-06	246.8868	-49.3974	1.135E-07	782.0819	5.799E+09	4.5992	5025000.	0.000
240.00	-4.043E-06	33.0430	-25.4443	2.583E-07	781.0183	5.799E+09	3.3861	5025000.	0.000
246.00	-2.391E-06	-58.9320	-9.2791	2.449E-07	781.1470	5.799E+09	2.0023	5025000.	0.000
252.00	-1.104E-06	-78.7679	-0.4979	1.737E-07	781.2457	5.799E+09	0.9248	5025000.	0.000

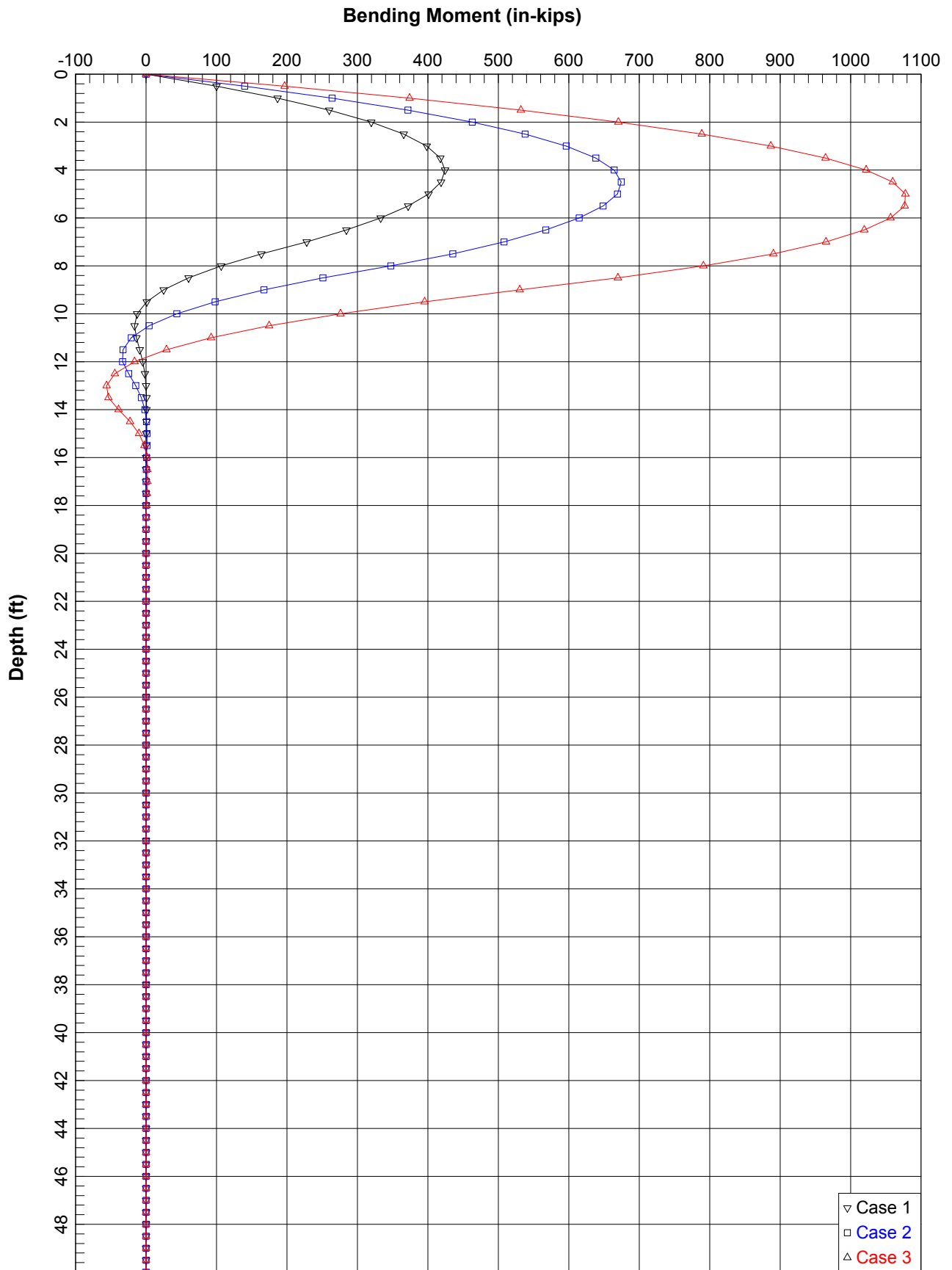
Abut SR_transv_Ave P									
258.000	-3.068E-07	-65.2335	3.0474	9.917E-08	781.1783	5.799E+09	0.2569	5025000.	0.000
264.000	8.752E-08	-42.3863	3.4028	4.349E-08	781.0648	5.799E+09	-0.0718	5025000.	0.000
270.000	2.151E-07	-22.0823	2.8470	1.013E-08	780.9638	5.799E+09	-0.1801	5025000.	0.000
276.000	2.073E-07	-8.2410	1.7858	-5.555E-09	780.8949	5.799E+09	-0.1736	5025000.	0.000
282.000	1.484E-07	-0.6424	0.8920	-1.015E-08	780.8571	5.799E+09	-0.1243	5025000.	0.000
288.000	8.550E-08	2.4824	0.3043	-9.199E-09	780.8663	5.799E+09	-0.0716	5025000.	0.000
294.000	3.802E-08	3.0268	-0.06019	-6.349E-09	780.8690	5.799E+09	-0.0318	5025000.	0.000
300.000	9.318E-09	2.4221	-0.1249	-3.530E-09	780.8660	5.799E+09	-0.007804	5025000.	0.000
306.000	-4.341E-09	1.5341	-0.1375	-1.483E-09	780.8616	5.799E+09	0.003636	5025000.	0.000
312.000	-8.477E-09	0.7755	-0.1052	-2.880E-10	780.8578	5.799E+09	0.007990	5025000.	0.000
318.000	-7.797E-09	0.2717	-0.0644	-2.538E-10	780.8553	5.799E+09	0.006530	5025000.	0.000
324.000	-5.431E-09	0.002772	-0.0311	-3.958E-10	780.8540	5.799E+09	0.004548	5025000.	0.000
330.000	-3.047E-09	-0.1025	-0.009818	-3.443E-10	780.8544	5.799E+09	0.002552	5025000.	0.000
336.000	-1.300E-09	-0.1157	0.001103	-2.314E-10	780.8545	5.799E+09	0.001089	5025000.	0.000
342.000	-2.704E-10	-0.0896	0.005048	-1.252E-10	780.8544	5.799E+09	0.000226	5025000.	0.000
348.000	2.023E-10	-0.0554	0.005219	-5.015E-11	780.8542	5.799E+09	-0.000169	5025000.	0.000
354.000	3.314E-10	-0.0271	0.003879	-7.488E-12	780.8541	5.799E+09	-0.000278	5025000.	0.000
360.000	2.922E-10	-0.008826	0.002312	-1.110E-11	780.8540	5.799E+09	-0.000245	5025000.	0.000
366.000	1.982E-10	0.000655	0.001080	-1.533E-11	780.8539	5.799E+09	-0.000166	5025000.	0.000
372.000	1.082E-10	0.004161	0.000310	-1.284E-11	780.8540	5.799E+09	-9.062E-05	5025000.	0.000
378.000	4.409E-11	0.004401	-7.246E-05	-8.409E-12	780.8540	5.799E+09	-3.692E-05	5025000.	0.000
384.000	7.293E-12	0.003308	-0.000202	-4.421E-12	780.8540	5.799E+09	-6.108E-06	5025000.	0.000
390.000	-8.965E-12	0.001991	-0.000197	-1.680E-12	780.8539	5.799E+09	7.509E-06	5025000.	0.000
396.000	-1.286E-11	0.000943	-0.000142	0.000	780.8539	5.799E+09	1.077E-05	5025000.	0.000
402.000	-1.091E-11	0.000281	-8.277E-05	0.000	780.8539	5.799E+09	9.136E-06	5025000.	0.000
408.000	-7.208E-12	-5.148E-05	3.725E-05	0.000	780.8539	5.799E+09	6.037E-06	5025000.	0.000
414.000	-3.827E-12	-0.000077	-9.525E-06	0.000	780.8539	5.799E+09	3.205E-06	5025000.	0.000
420.000	-1.482E-12	0.000167	3.813E-06	0.000	780.8539	5.799E+09	-1.241E-06	5025000.	0.000
426.000	0.000	-0.000122	7.966E-06	0.000	780.8539	5.799E+09	1.433E-07	5025000.	0.000
432.000	0.000	-7.137E-05	7.431E-06	0.000	780.8539	5.799E+09	-3.216E-07	5025000.	0.000
438.000	0.000	-3.259E-05	5.220E-06	0.000	780.8539	5.799E+09	-4.155E-07	5025000.	0.000
44									

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Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	157000.	0.25000000	374894.	14728.	-0.00468295
2	4	y = 0.5000	M = 0.000	157000.	0.50000000	598914.	20013.	-0.00835400
3	4	y = 1.0000	M = 0.000	157000.	1.00000000	965872.	27301.	-0.01494681

The analysis ended normally.





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Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 5
 Name of input data file: Abut 5R_transv_Max P.lpd
 Name of output report file: Abut 5R_transv_Max P.lpp
 Name of plot output file: Abut 5R_transv_Max P.lpp
 Name of runtime message file: Abut 5R_transv_Max P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 10:03:34

Problem Title

Project Name: Palo Comado OC Bridge Widen

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

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Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 16.0000000 in
 Bottom Width = 16.0000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 5 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 7.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 7.00000 ft
 Distance from top of pile to bottom of layer = 12.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 12.00000 ft
 Distance from top of pile to bottom of layer = 17.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 17.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Uniaxial Elastic Mod.	ROD % or GSI
Num.	Epsilon 50	J (psi)	Rock Mass Depth (ft)	pcf	psf	deg.	psi	
1	0.00700	Stiff Clay w/o Free Water	2.000	120.000	4000.000			
2	0.00700	Stiff Clay w/o Free Water	0.10000	120.000	4000.000			
3	0.00700	Stiff Clay w/o Free Water	7.000	120.000	1500.000			
4	0.00700	Stiff Clay w/o Free Water	12.000	125.000	4000.000			
5	0.00500	Stiff Clay w/o Free Water	17.000	125.000	4500.000			
	0.00500		80.000	125.000	4500.000			

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X (ft)	p-mult	y-mult
1	0.000	0.8800	1.0000
2	50.000	0.8800	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

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Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4 y =	0.25000 in	M = 0.0000 in-lbs	157000.	False
2	4 y =	0.50000 in	M = 0.0000 in-lbs	157000.	False
3	4 y =	1.00000 in	M = 0.0000 in-lbs	157000.	False

V = perpendicular shear force applied to pile head

M = bending moment applied to pile head

y = lateral deflection relative to pile axis

S = pile slope relative to original pile batter angle

R = rotational stiffness applied to pile head

Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.250000 inches
 Moment at pile head = 0.0000 in-lbs
 Axial load at pile head = 157000.000 lbs

Depth X (inches)	Deflect. y (inches)	Bending Moment (in-lbs)	Shear Force (lbs)	Slope S (radians)	Total Stress (psi)	Bending Stiffness (lb-in ²)	Soil Res. p (lb/in)	Soil Spr. Es ^h (lb/inch)	Distrib. Lat. Load (lb/inch)
0.00	0.2500	0.000	18057.	-0.004976	780.8539	5.799E+09	-724.2535	8691.0425	0.000
6.00	0.2201	99991.	14783.	-0.004925	1278.1693	5.799E+09	-367.0507	10004.	0.000
12.00	0.1909	186671.	12574.	-0.004776	1709.2798	5.799E+09	-369.3668	11609.	0.000
18.00	0.1628	259872.	10357.	-0.004545	2073.3504	5.799E+09	-369.5360	13617.	0.000
24.00	0.1364	319516.	8145.8597	-0.004245	2369.9961	5.799E+09	-367.4478	16168.	0.000
30.00	0.1119	365621.	5954.5718	-0.003891	2599.3015	5.799E+09	-362.9815	19466.	0.000
36.00	0.0897	398301.	3797.6232	-0.003496	2761.8429	5.799E+09	-356.0014	23820.	0.000
42.00	0.0699	417778.	1690.5679	-0.003074	2858.7116	5.799E+09	-346.3504	29716.	0.000
48.00	0.0528	424379.	-350.0003	-0.002638	2891.5411	5.799E+09	-333.8390	37944.	0.000
54.00	0.0383	418548.	-2306.1922	-0.002202	2862.5397	5.799E+09	-318.2250	49880.	0.000
60.00	0.0264	400853.	-4158.3920	-0.001778	2774.5313	5.799E+09	-299.1749	68077.	0.000
66.00	0.0169	371996.	-5884.4516	-0.001378	2631.0126	5.799E+09	-276.1783	97790.	0.000
72.00	0.009532	332835.	-7457.9642	-0.001013	2436.2410	5.799E+09	-248.3259	151541.	0.000
78.00	0.004785	284410.	-8843.6694	-0.000694	2195.3932	5.799E+09	-213.5758	267789.	0.000
84.00	0.001504	228019.	-10123.	-0.000429	1914.9261	5.799E+09	-212.8051	848787.	0.000
90.00	-0.000361	163744.	-10137.	-0.000226	1595.2510	5.799E+09	208.0605	3457183.	0.000
96.00	-0.001210	106800.	-8533.1981	-8.621E-05	1312.0351	5.799E+09	293.2221	1454114.	0.000
102.00	-0.001396	60308.	-6813.1505	2.426E-07	1080.8027	5.799E+09	313.4604	1347586.	0.000
108.00	-0.001207	25042.	-4938.8287	4.440E-05	905.4029	5.799E+09	311.3135	1547554.	0.000
114.00	-0.000863	958.6919	-3121.4050	5.785E-05	785.6221	5.799E+09	294.4944	2047812.	0.000
120.00	-0.000513	-12524.	-1440.6158	5.187E-05	843.1422	5.799E+09	265.7687	3109798.	0.000
126.00	-0.000240	-16426.	-95.1002	3.689E-05	862.5522	5.799E+09	182.7365	4560110.	0.000
132.00	-7.008E-05	-13735.	617.1374	2.129E-05	849.1638	5.799E+09	54.6760	4680829.	0.000
138.00	1.500E-05	-9660.8727	745.1580	9.493E-06	825.9190	5.799E+09	-12.0024	4801547.	0.000
144.00	4.383E-05	-4810.4947	604.5696	2.316E-06	804.7794	5.799E+09	-34.8604	4772330.	0.000
150.00	4.279E-05	-1810.4017	388.4647	-1.109E-06	789.8581	5.799E+09	-37.1746	5122268.	0.000
156.00	3.052E-05	-146.8283	195.3193	-2.122E-06	781.5842	5.799E+09	-27.2073	5349132.	0.000
162.00	1.733E-05	537.4269	66.1580	-1.920E-06	783.5269	5.799E+09	-15.8465	5486001.	0.000
168.00	7.481E-06	650.6848	-2.4142	-1.305E-06	784.0902	5.799E+09	-7.0109	5622875.	0.000
174.00	1.671E-06	510.9147	-28.2588	-7.041E-07	783.3950	5.799E+09	-1.6039	5759753.	0.000
180.00	-9.676E-07	312.9055	-30.2179	-2.778E-07	782.4102	5.799E+09	0.9509	5896634.	0.000
186.00	-1.663E-06	148.8338	-22.5473	-3.896E-08	781.5941	5.799E+09	1.6726	6033519.	0.000
192.00	-1.435E-06	44.8115	-12.9755	6.122E-08	781.0768	5.799E+09	1.4513	6067530.	0.000
198.00	-9.287E-07	-6.9979	-5.8041	8.078E-08	780.8887	5.799E+09	0.9392	6067530.	0.000
204.00	-4.658E-07	-24.8996	-1.4261	6.423E-08	780.9782	5.799E+09	0.5201	6700043.	0.000
210.00	-1.580E-07	-24.2320	0.7208	3.874E-08	780.9745	5.799E+09	0.1955	7425000.	0.000
216.00	-6.136E-10	-16.4128	1.3096	1.774E-08	780.9356	5.799E+09	0.000759	7425000.	0.000
222.00	5.486E-08	-8.5503	1.1082	4.821E-09	780.8965	5.799E+09	-0.0679	7425000.	0.000
228.00	5.724E-08	-3.1233	0.6921	-1.218E-09	780.8461	5.799E+09	-0.0708	7425000.	0.000
234.00	4.024E-08	-0.2434	0.3302	-2.960E-09	780.8552	5.799E+09	-0.0498	7425000.	0.000

	Abut SR_transv_Max P						
	0.00	0.5000	0.00	24507.0	0.008872	780.8539	5.799E-09
240.000	2.172E-08	0.8441	-0.1001	-2.640E-09	780.8539	5.799E-09	-0.0269
246.000	8.448E-09	0.9630	-0.0119	-1.714E-09	780.8541	5.799E-09	-0.0105
252.000	1.152E-09	0.7046	-0.0475	-8.515E-10	780.8574	5.799E-09	-0.001425
258.000	-1.770E-09	0.3942	-0.0452	-2.831E-10	780.8559	5.799E-09	0.002191
264.000	-2.245E-09	0.1623	-0.0303	4.867E-12	780.8547	5.799E-09	0.002778
270.000	-1.712E-09	0.0303	-0.0156	1.045E-10	780.8541	5.799E-09	0.002118
276.000	-9.911E-10	-0.0256	-0.005604	1.069E-10	780.8541	5.799E-09	0.001226
282.000	-4.289E-10	-0.0372	-0.000333	7.444E-11	780.8541	5.799E-09	0.000531
288.000	-9.779E-11	-0.0297	0.001623	3.983E-11	780.8541	5.799E-09	0.001121
294.000	4.902E-11	-0.0178	0.001804	1.526E-11	780.8540	5.799E-09	-6.066E-05
300.000	8.531E-11	-0.008075	0.001305	1.870E-12	780.8540	5.799E-09	-0.001016
306.000	7.147E-11	-0.002142	0.000723	-3.415E-12	780.8540	5.799E-09	-8.844E-05
312.000	4.433E-11	0.000610	0.000293	4.207E-12	780.8539	5.799E-09	-5.486E-05
318.000	2.098E-11	0.001387	5.091E-05	-3.174E-12	780.8539	5.799E-09	-2.596E-05
324.000	6.237E-12	0.001227	-5.012E-05	-1.822E-12	780.8539	5.799E-09	-7.718E-06
330.000	0.0000	0.000789	-6.999E-05	0.0000	780.8539	5.799E-09	1.096E-06
336.000	-3.111E-12	0.000389	-5.515E-05	0.0000	780.8539	5.799E-09	3.850E-06
342.000	-2.923E-12	0.000127	-3.275E-05	0.0000	780.8539	5.799E-09	3.618E-06
348.000	-1.946E-12	-4.401E-06	-1.467E-05	0.0000	780.8539	5.799E-09	2.408E-06
354.000	0.0000	-4.924E-05	-3.749E-06	0.0000	780.8539	5.799E-09	1.233E-06
360.000	0.0000	-4.964E-05	1.257E-06	0.0000	780.8539	5.799E-09	4.357E-07
366.000	0.0000	-3.431E-05	2.623E-06	0.0000	780.8539	5.799E-09	1.985E-08
372.000	0.0000	-1.823E-05	2.286E-06	0.0000	780.8539	5.799E-09	-1.324E-07
378.000	0.0000	-6.899E-06	1.455E-06	0.0000	780.8539	5.799E-09	-1.446E-07
384.000	0.0000	-7.685E-07	7.093E-07	0.0000	780.8539	5.799E-09	-1.038E-07
390.000	0.0000	1.624E-06	2.264E-07	0.0000	780.8539	5.799E-09	-5.714E-08
396.000	0.0000	1.959E-06	-1.380E-08	0.0000	780.8539	5.799E-09	-2.293E-08
402.000	0.0000	4.664E-06	-9.388E-08	0.0000	780.8539	5.799E-09	-3.764E-09
408.000	0.0000	8.355E-07	-9.275E-08	0.0000	780.8539	5.799E-09	4.141E-09
414.000	0.0000	3.538E-07	-6.344E-08	0.0000	780.8539	5.799E-09	5.627E-09
420.000	0.0000	7.429E-08	-3.337E-08	0.0000	780.8539	5.799E-09	4.395E-09
426.000	0.0000	-4.705E-08	-1.241E-08	0.0000	780.8539	5.799E-09	2.893E-09
432.000	0.0000	-7.500E-08	-1.176E-09	0.0000	780.8539	5.799E-09	1.151E-09
438.000	0.0000	-6.145E-08	3.136E-09	0.0000	780.8539	5.799E-09	2.860E-10
444.000	0.0000	-3.753E-08	3.673E-09	0.0000	780.8539	5.799E-09	-1.070E-10
450.000	0.0000	-1.743E-08	2.717E-09	0.0000	780.8539	5.799E-09	-2.117E-10
456.000	0.0000	-4.938E-09	1.534E-09	0.0000	780.8539	5.799E-09	-1.825E-10
462.000	0.0000	9.898E-10	6.405E-10	0.0000	780.8539	5.799E-09	-1.154E-10
468.000	0.0000	2.764E-09	1.269E-10	0.0000	780.8539	5.799E-09	-5.582E-11
474.000	0.0000	2.525E-09	-9.304E-11	0.0000	780.8539	5.799E-09	-1.750E-11
480.000	0.0000	1.654E-09	-1.413E-10	0.0000	780.8539	5.799E-09	7.617E-12
486.000	0.0000	8.328E-10	-1.142E-10	0.0000	780.8539	5.799E-09	4.466E-12
492.000	0.0000	2.846E-10	-6.910E-11	0.0000	780.8539	5.799E-09	7.422E-12
498.000	0.0000	3.356E-12	-3.171E-11	0.0000	780.8539	5.799E-09	5.040E-12
504.000	0.0000	-9.650E-11	-8.695E-12	0.0000	780.8539	5.799E-09	2.632E-12
510.000	0.0000	-1.015E-10	2.101E-12	0.0000	780.8539	5.799E-09	0.0000
516.000	0.0000	-7.162E-11	5.238E-12	0.0000	780.8539	5.799E-09	0.0000
522.000	0.0000	-3.880E-11	4.707E-12	0.0000	780.8539	5.799E-09	0.0000
528.000	0.0000	-1.518E-11	3.054E-12	0.0000	780.8539	5.799E-09	0.0000
534.000	0.0000	-2.148E-12	1.521E-12	0.0000	780.8539	5.799E-09	0.0000
540.000	0.0000	3.097E-12	0.0000	0.0000	780.8539	5.799E-09	0.0000
546.000	0.0000	3.974E-12	0.0000	0.0000	780.8539	5.799E-09	0.0000
552.000	0.0000	3.043E-12	0.0000	0.0000	780.8539	5.799E-09	0.0000
558.000	0.0000	1.766E-12	0.0000	0.0000	780.8539	5.799E-09	0.0000
564.000	0.0000	0.0000	0.0000	0.0000	780.8539	5.799E-09	0.0000
570.000	0.0000	0.0000	0.0000	0.0000	780.8539	5.799E-09	0.0000
576.000	0.0000	0.0000	0.0000	0.0000	780.8539	5.799E-09	0.0000
582.000	0.0000	0.0000	0.0000	0.0000	780.8539	5.799E-09	0.0000
588.000	0.0000	0.0000	0.0000	0.0000	780.8539	5.799E-09	0.0000
594.000	0.0000	0.0000	0.0000	0.0000	780.8539	5.799E-09	0.0000
600.000	0.0000	0.0000	0.0000	0.0000	780.8539	5.799E-09	0.0000

Depth y inches	Deflect. inches	Bendng Moment in-lbs	Shear Force lbs	Sl gpe radians	Abut SR_transv_Max Total Stress psi *	Bendng Stiffness lb-in ²	Soil p Res. lb/in	Soil Spr. Es/h lb/inch	Di stri b Lat. Load lb/inch
6.000	0.4468	139987.7	20609.0	-0.008800	1476.6427	5.799E-09	-86.2875	5167.7248	0.000
12.000	0.3944	263885.5	17966.0	-0.008591	2093.3123	5.799E-09	-442.8297	6736.6860	0.000
18.000	0.3437	371675.5	15301.0	-0.008262	2629.4144	5.799E-09	-445.4096	7776.0279	0.000
24.000	0.2953	463068.5	12628.0	-0.007830	3083.9643	5.799E-09	-445.7258	9057.5878	0.000
30.000	0.2497	537963.3	9959.8523	-0.007312	3456.4625	5.799E-09	-443.6585	10660.000	0.000
36.000	0.2075	596362.7	7311.6506	-0.006725	3746.9159	5.799E-09	-439.0754	12695.000	0.000
42.000	0.1690	638373.3	4698.9466	-0.006086	3955.8622	5.799E-09	-431.8260	15330.000	0.000
48.000	0.1345	664216.6	2138.2671	-0.005413	4084.3966	5.799E-09	-421.7339	18187.000	0.000
54.000	0.1041	674230.0	-352.6836	-0.004720	4134.1978	5.799E-09	-408.5830	23558.000	0.000
60.000	0.0778	668877.7	-2754.7184	-0.004025	4107.5750	5.799E-09	-392.0952	30225.000	0.000
66.000	0.0558	648757.7	-5046.6643	-0.003344	4007.5052	5.799E-09	-371.8867	40016.000	0.000
72.000	0.0377	614616.6	-7204.4637	-0.002690	3837.7042	5.799E-09	-347.3797	55266.000	0.000
78.000	0.0235	567371.1	-9199.3788	-0.002078	3602.7256	5.799E-09	-317.5920	81150.000	0.000
84.000	0.0128	508139.9	-11239.9	-0.001522	3308.1319	5.799E-09	-362.1656	170127.000	0.000
90.000	0.005218	435375.5	-13540.0	-0.001034	2946.2293	5.799E-09	-411.6236	473286.000	0.000
96.000	0.000367	347367.0	-15461.0	-0.000629	2508.5151	5.799E-09	-222.1824	3634651.000	0.000
102.000	-0.002328	251022.2	-15059.9	-0.000319	2029.3354	5.799E-09	356.2297	918057.000	0.000
108.000	-0.003465	167257.7	-12774.0	-0.000103	1612.7214	5.799E-09	405.5023	702240.000	0.000
114.000	-0.003563	97927.7	-10297.0	3.431E-05	1267.9015	5.799E-09	420.1813	707625.000	0.000
120.000	-0.003053	43628.0	-7789.7684	0.000108	997.8401	5.799E-09	415.5787	816761.000	0.000
126.000	-0.002722	4246.8860	-5353.6438	0.000132	801.9762	5.799E-09	396.4628	1046926.000	0.000
132.000	-0.002381	2076.2338	-3076.6297	0.000126	684.6297	5.799E-09	344.1605	1425000.000	0.000
138.000	-0.002078	-32831.1	-1010.1210	9.594E-05	444.4434	5.799E-09	320.1571	2439242.000	0.000
144.000	-0.000314	-33240.0	693.1183	6.176E-05	946.1739	5.799E-09	249.5893	4772330.000	0.000
150.000	-4.644E-05	-24630.0	1562.9104	3.182E-05	903.3546	5.799E-09	40.3415	5212268.000	0.000
156.000	6.803E-05	1452.0495	1502.0495	1.155E-05	915.0495	5.799E-09	-60.6284	5349132.000	0.000
162.000	9.215E-05	-6627.3823	1067.3933	5.955E-07	813.8158	5.799E-09	-84.2570	5486001.000	0.000
168.000	7.515E-05	-1736.9792	603.3379	-3.732E-06	789.4930	5.799E-09	-70.4282	5622875.000	0.000
174.000	4.737E-05	619.7032	258.6381	-4.310E-06	783.9361	5.799E-09	-45.4718	5759753.000	0.000
180.000	2.387E-05	1330.9719	30.3136	-3.89E-06	787.8146	5.799E-09	-22.0288	5826344.000	0.000
186.000	-7.808E-06	1227.5504	-42.5058	-1.969E-06	786.9593	5.799E-09	-7.8519	6033159.000	0.000
192.000	-1.948E-07	832.4375	-65.4705	-9.032E-07	784.9941	5.799E-09	0.1970	6067530.000	0.000
198.000	-3.030E-06	443.6064	-55.6875	-2.430E-07	783.0603	5.799E-09	3.0640	6067530.000	0.000
204.000	-3.111E-06	164.6484	-36.0742	-7.169E-08	781.6728	5.799E-09	3.4738	610043.000	0.000
210.000	-2.170E-06	10.5812	-17.5797	1.623E-07	780.9066	5.799E-09	2.6849	7425000.000	0.000
216.000	-1.163E-06	-46.8355	-5.2264	1.436E-07	781.0869	5.799E-09	1.4389	7425000.000	0.000
222.000	-4.466E-07	17.7485	9.224E-08	7.748E-08	781.5527	5.799E-09	1.2527	7425000.000	0.000
228.000	-5.586E-08	-38.0277	2.6140	4.545E-08	781.0431	5.799E-09	0.0691	7425000.000	0.000
234.000	9.882E-08	-21.1239	2.4545	1.485E-08	780.9590	5.799E-09	-0.1223	7425000.000	0.000
240.000	1.223E-07	-8.6018	1.6334	-5.280E-10	780.8967	5.799E-09	-0.1514	7425000.000	0.000
246.000	9.248E-08	-1.5219	0.8359	-5.766E-09	780.8265	5.799E-09	-0.1180	7425000.000	

Abut SR_transv_Max P							
Y	X	Moment	S	Stress	p		
522.000	0.000	-2.167E-10	0.000	780.8539	5.799E+09	2.656E-12	7425000.000
528.000	0.000	-1.645E-10	1.018E-11	0.000	780.8539	5.799E+09	7425000.000
534.000	0.000	-9.486E-11	1.031E-11	0.000	780.8539	5.799E+09	7425000.000
540.000	0.000	-4.084E-11	7.144E-12	0.000	780.8539	5.799E+09	7425000.000
546.000	0.000	-9.141E-12	3.804E-12	0.000	780.8539	5.799E+09	7425000.000
552.000	0.000	4.841E-12	1.445E-12	0.000	780.8539	5.799E+09	7425000.000
558.000	0.000	8.239E-12	0.000	0.000	780.8539	5.799E+09	7425000.000
564.000	0.000	6.863E-12	0.000	0.000	780.8539	5.799E+09	7425000.000
570.000	0.000	4.246E-12	0.000	0.000	780.8539	5.799E+09	7425000.000
576.000	0.000	2.026E-12	0.000	0.000	780.8539	5.799E+09	7425000.000
582.000	0.000	0.000	0.000	0.000	780.8539	5.799E+09	7425000.000
588.000	0.000	0.000	0.000	0.000	780.8539	5.799E+09	7425000.000
594.000	0.000	0.000	0.000	0.000	780.8539	5.799E+09	7425000.000
600.000	0.000	0.000	0.000	0.000	780.8539	5.799E+09	3712500.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Pile-head deflection	=	0.5000000	inches
Computed slope at pile head	=	-0.0088720	radians
Maximum bending moment	=	674230.	in-lb
Maximum shear force	=	33344.	lbs
Depth of maximum bending moment	=	54.0000000	inches below pile head
Depth of maximum shear force	=	0.0000000	inches below pile head
Number of iterations	=	13	
Number of zero deflection points	=	14	

Computed Values of Pile Loading and Deflection
For Lateral Loading for Load Case Number 3

Pile-head conditions are Displacement and Moment (Loading Type 4)										
Displacement of pile head			= 1.000000 inches							
Moment at pile head			= 157000.000 in-lbs							
Axial load at pile head			= 157000.000 lbs							
Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil Res.	Soil Spr.	Distrib.	
inches	inches	in-lbs	lbs	radians	Stress psi	Stiffness lb/in^2	lb/in	lb/inch	lb/inch	
0.00	1.0000	0.000	33344.	-0.0158	780.8539	5.799E+09	-1024.2492	3072.7475	0.000	
6.00	0.9050	196543.	28703.	-0.0157	1758.3793	5.799E+09	-522.6498	3465.0816	0.000	
12.00	0.8112	374079.	25545.	-0.0154	2641.3718	5.799E+09	-530.3158	3922.3562	0.000	
18.00	0.7198	532159.	22346.	-0.0150	3427.5981	5.799E+09	-535.8168	4466.6102	0.000	
24.00	0.6316	670432.	19122.	-0.0143	4115.3070	5.799E+09	-539.0445	5120.6747	0.000	
30.00	0.5476	788645.	15885.	-0.0136	4703.2502	5.799E+09	-539.8837	5915.2554	0.000	
36.00	0.4685	886653.	12650.	-0.0127	5190.7043	5.799E+09	-538.2097	6892.4171	0.000	
42.00	0.3949	964422.	9434.1809	-0.0118	5577.4941	5.799E+09	-533.8848	8111.0172	0.000	
48.00	0.3273	1022031.	6252.2668	-0.0107	5864.0168	5.799E+09	-526.7533	9655.4482	0.000	
54.00	0.2661	1059680.	3122.1027	-0.009661	6051.2700	5.799E+09	-516.6348	11650.	0.000	
60.00	0.2114	1077698.	62.2598	-0.008556	6140.8830	5.799E+09	-503.3129	14286.	0.000	
66.00	0.1634	1076546.	-2907.2319	-0.007441	6135.1537	5.799E+09	-486.5177	17884.	0.000	
72.00	0.1221	1056830.	-5764.4724	-0.006337	6037.0948	5.799E+09	-465.8958	22894.	0.000	
78.00	0.0874	1019312.	-8485.0249	-0.005263	5850.4943	5.799E+09	-440.9550	30286.	0.000	
84.00	0.0589	964925.	-11400.	-0.004237	5579.9996	5.799E+09	-530.5497	54007.	0.000	
90.00	0.0365	890499.	-14997.	-0.003277	5209.8326	5.799E+09	-668.6756	109864.	0.000	
96.00	0.0196	791132.	-18775.	-0.002407	4715.6227	5.799E+09	-590.5437	180571.	0.000	
102.00	0.007638	669735.	-21989.	-0.001651	4111.8411	5.799E+09	-480.7667	377652.	0.000	
108.00	-0.000188	530377.	-23036.	-0.001030	3418.7318	5.799E+09	131.5499	4197954.	0.000	
114.00	-0.004722	395238.	-21288.	-0.000551	2746.6053	5.799E+09	451.1483	573099.	0.000	
120.00	-0.006801	275955.	-18411.	-0.000204	2153.3404	5.799E+09	508.1067	448247.	0.000	
126.00	-0.007168	174695.	-15300.	2.930E-05	1649.7140	5.799E+09	528.7865	426239.	0.000	
132.00	-0.006450	92301.	-12128.	0.000167	1239.9195	5.799E+09	528.5823	491730.	0.000	
138.00	-0.005159	28846.	-9004.0613	0.000230	924.3198	5.799E+09	512.6668	596292.	0.000	
144.00	-0.003688	-16182.	-6060.8024	0.000237	661.3349	5.799E+09	468.4195	761998.	0.000	
150.00	-0.002319	-44330.	-3289.5316	0.000205	1001.3331	5.799E+09	455.3374	1178297.	0.000	
156.00	-0.001224	-56043.	-729.4877	0.000153	1059.5886	5.799E+09	398.0106	1950867.	0.000	
162.00	-0.000478	-53373.	1430.6286	9.682E-05	1046.3088	5.799E+09	322.0282	4046247.	0.000	
168.00	-6.230E-05	-39058.	2571.8592	4.900E-05	975.1114	5.799E+09	58.3820	5622875.	0.000	
174.00	0.000010	-22603.	2428.9486	1.710E-05	893.2714	5.799E+09	-106.0188	5759753.	0.000	
180.00	0.000143	-994.6060	1689.7169	2.500E-07	830.3044	5.799E+09	-440.3917	5964634.	0.000	
186.00	0.000014	-2326.7535	926.0276	-6.090E-06	792.4263	5.799E+09	-114.1714	6035519.	0.000	
192.00	6.978E-05	1181.1976	371.8291	-6.682E-06	786.7287	5.799E+09	-70.5615	6067530.	0.000	
198.00	3.335E-05	2147.7849	58.9733	-4.960E-06	791.5361	5.799E+09	-33.7238	6067530.	0.000	
204.00	1.026E-05	1898.2319	-76.5527	-2.867E-06	790.2949	5.799E+09	-11.4515	6700000.	0.000	
210.00	-1.054E-06	1234.5535	-106.9961	-1.246E-06	786.9941	5.799E+09	1.3037	7425000.	0.000	
216.00	-4.698E-06	616.6165	-85.6452	-2.883E-07	783.9207	5.799E+09	5.8132	7425000.	0.000	
222.00	-4.513E-06	207.3537	-51.4498	1.380E-07	781.8852	5.799E+09	5.5853	7425000.	0.000	
228.00	-3.042E-06	-1.0409	-23.4010	2.447E-07	780.8591	5.799E+09	3.7643	7425000.	0.000	
234.00	-1.577E-06	-73.9198	-6.2542	2.059E-07	781.2216	5.799E+09	1.9513	7425000.	0.000	
240.00	-5.707E-07	-76.4795	1.7184	1.281E-07	781.2343	5.799E+09	0.7062	7425000.	0.000	
246.00	-3.939E-08	-53.5401	3.9839E-08	6.085E-08	781.1202	5.799E+09	0.0487	7425000.	0.000	
252.00	-1.959E-07	-28.7937	3.5374	1.826E-08	780.9971	5.799E+09	-0.1974	7425000.	0.000	

Abut SR_transv_Max P										
Y	X	Moment	S	Stress	p					
258.000	1.797E-07	-11.1261	2.2781	-2.398E-09	780.8539	5.799E+09	-0.2223	7425000.	0.000	
264.000	1.307E-07	-1.4519	1.1257	-8.905E-09	780.8612	5.799E+09	-0.1618	7425000.	0.000	
270.000	7.281E-08	2.3989	0.3700	-8.415E-09	780.8659	5.799E+09	-0.0901	7425000.	0.000	
276.000	2.976E-08	3.0039	-0.0108	-5.620E-09	780.8689	5.799E+09	-0.0368	7425000.	0.000	
282.000	5.363E-09	2.2801	-0.1412	-2.887E-09	780.8653	5.799E+09	-0.0337	7425000.	0.000	
288.000	-4.879E-09	1.3151	-0.1430	-1.027E-09	780.8605	5.799E+09	0.006037	7425000.	0.000	
294.000	-6.956E-09	0.5662	-0.0990	-5.321E-11	780.8568	5.799E+09	0.008608	7425000.	0.000	
300.000	-5.517E-09	0.1267	-0.0527	3.053E-10	780.8546	5.799E+09	0.006827	7425000.	0.000	
306.000	-3.292E-09	-0.0672	-0.0200	3.361E-10	780.8543	5.799E+09	0.004074	7425000.	0.000	
312.000	-1.484E-09	-0.1144	-0.002302	2.421E-10	780.8545	5.799E+09	0.001837	7425000.	0.000	
318.000	-3.867E-10	-0.0953	0.004645	1.337E-10	780.8544	5.799E+09	0.000479	7425000.	0.000	
324.000	1.194E-10	0.0589	0.005637	5.389E-11	780.8542	5.799E+09	-0.000148	7425000.	0.000	
330.000	2.600E-10	-0.0277	0.004229	9.076E-12	780.8541	5.799E+09	-0.000322	7425000.	0.000	
336.000	2.283E-10	-0.08155	0.002416	-9.495E-12	780.8540	5.799E+09	-0.000283	7425000.	0.000	
342.000	1.460E-10	0.001267	0.001026	-1.306E-11	780.8539	5.799E+09	-0.000181	7425000.	0.000	
348.000	7.161E-11	0.004182	0.000218	-1.024E-11	780.8540	5.799E+09	-8.862E-05	7425000.	0.000	
354.000	2.315E-11	0.003902	-0.000134	-6.059E-12	780.8540	5.799E+09	-2.864E-05	7425000.	0.000	
360.000	-1.092E-12	0.002588	-0.000216	-2.701E-12	780.8540	5.799E+09	1.352E-06	7425000.	0.000	
366.000	-9.266E-12	0.001319	-0.000177	0.000	780.8539	5.799E+09	1.147E-05	7425000.	0.000	
372.000	-9.249E-12	0.000463	-0.000108	0.000	780.8539	5.799E+09	1.145E-05	7425000.	0.000	
378.000	-6.360E-12	1.745E-05	-5.050E-05	0.000	780.8539	5.799E+09	7.871E-06	7425000.	0.000	
384.000	-3.363E-12	0.000144	-1.440E-05	0.000	780.8539	5.799E+09	4.162E-06	7425000.	0.000	
390.000	-1.262E-12	-0.000156								

Abut SR_transv_Max P

Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	157000.	0.25000000	424379.	18057.	-0.00497627
2	4	y = 0.5000	M = 0.000	157000.	0.50000000	674230.	24507.	-0.00887202
3	4	y = 1.0000	M = 0.000	157000.	1.00000000	1077698.	33344.	-0.01583332

The analysis ended normally.

SUPPORT: ABUTMENT 5L

LOAD DIRECTION: LONGITUDE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE

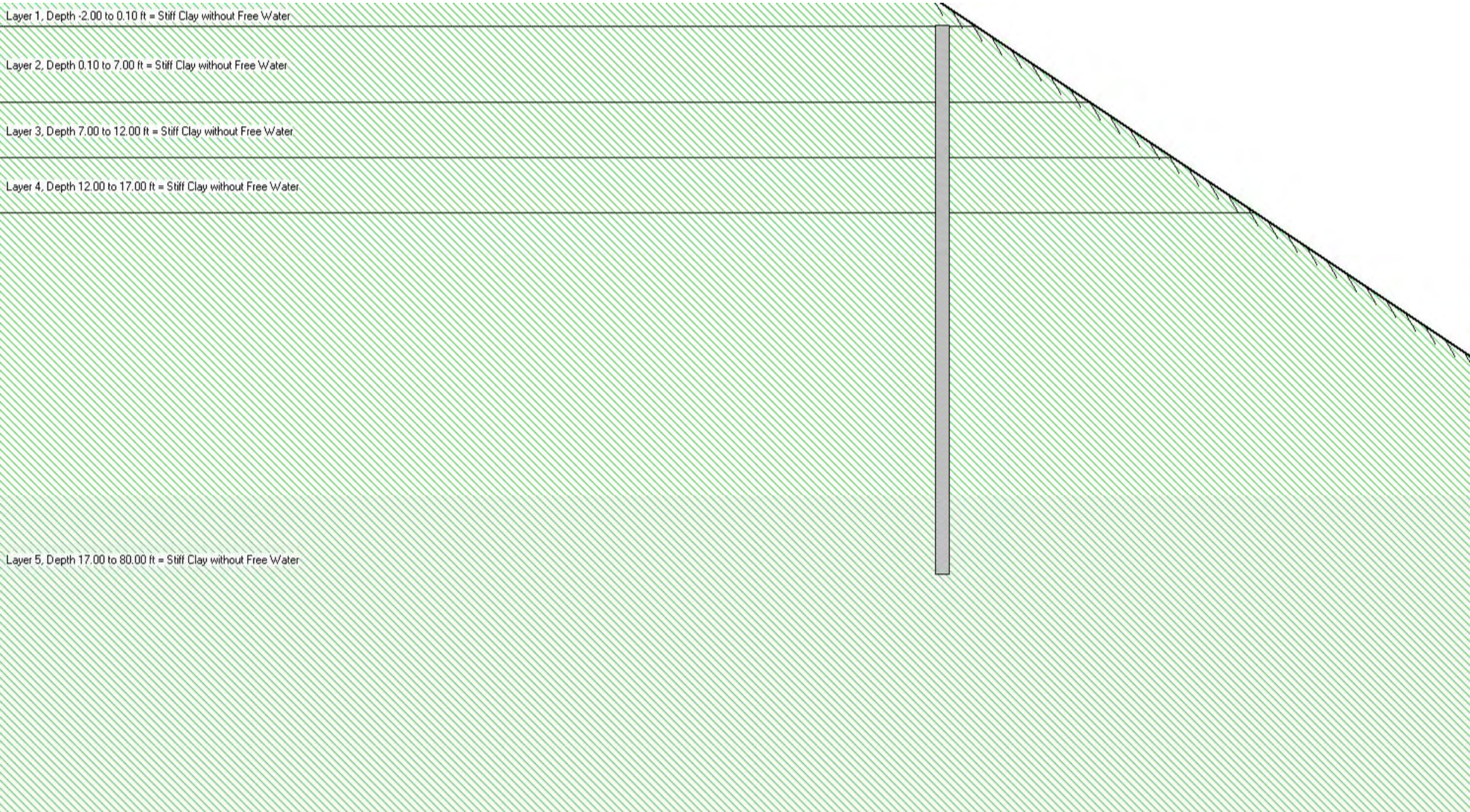
Layer 1, Depth -2.00 to 0.10 ft = Stiff Clay without Free Water

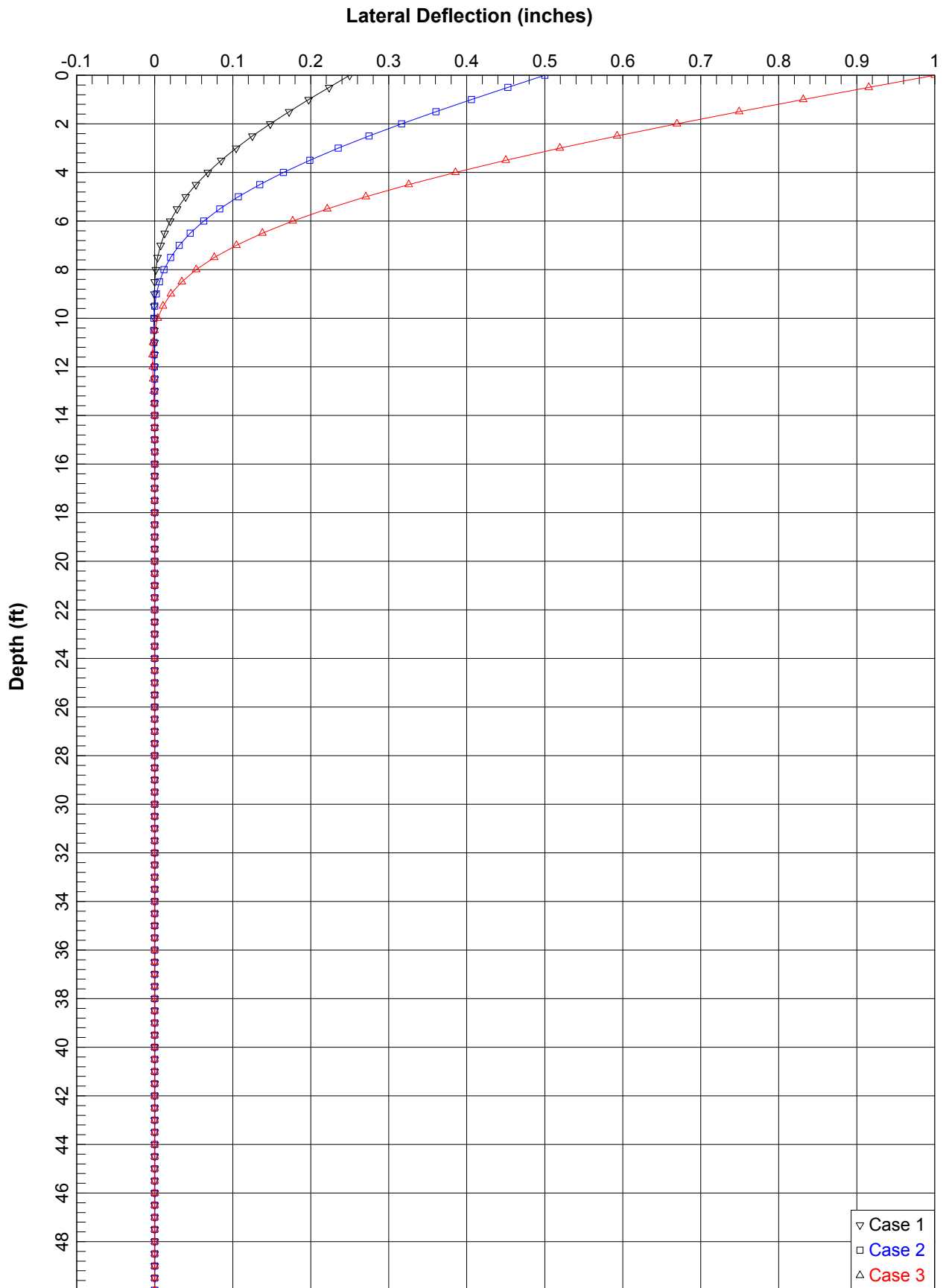
Layer 2, Depth 0.10 to 7.00 ft = Stiff Clay without Free Water

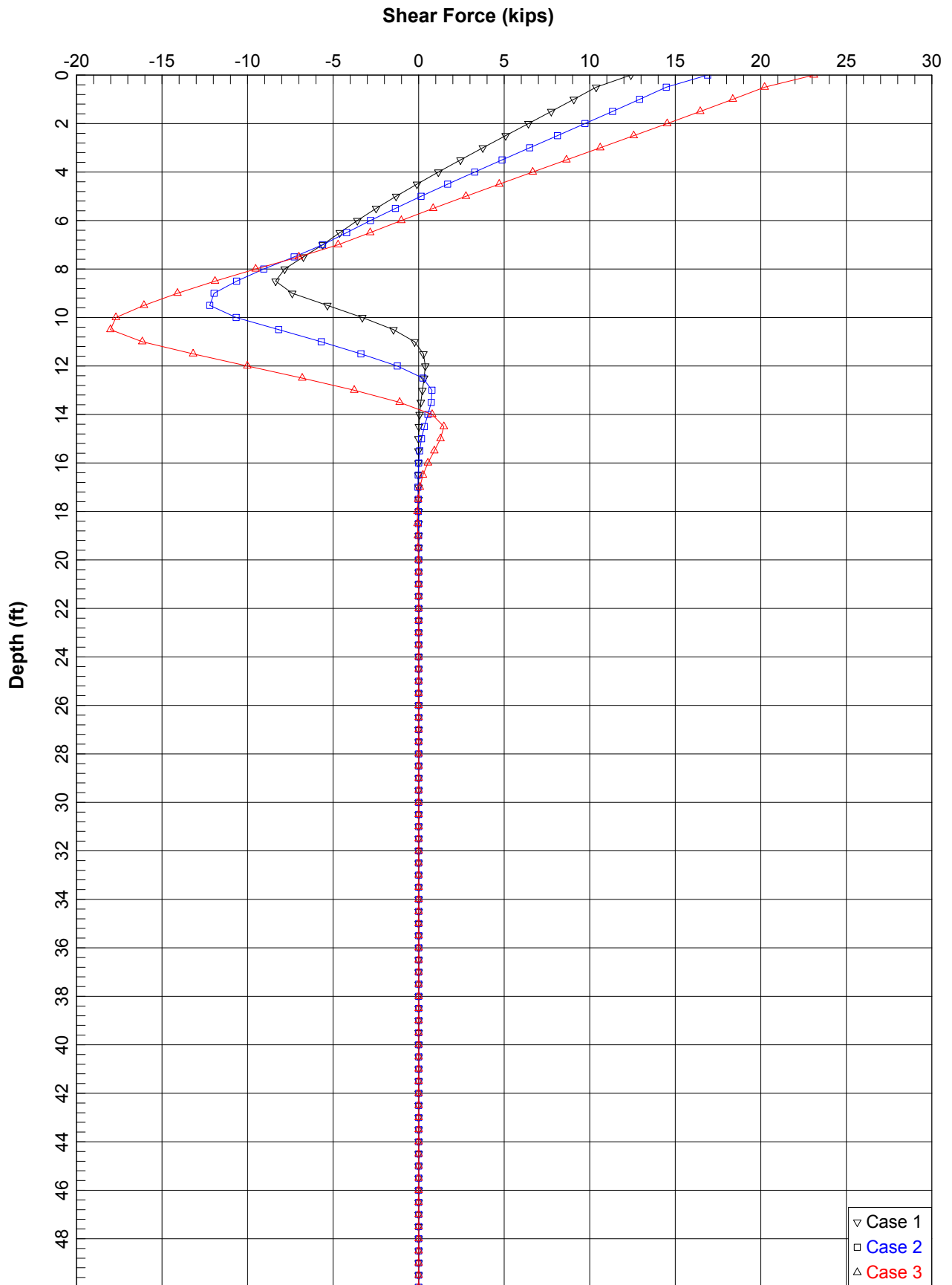
Layer 3, Depth 7.00 to 12.00 ft = Stiff Clay without Free Water

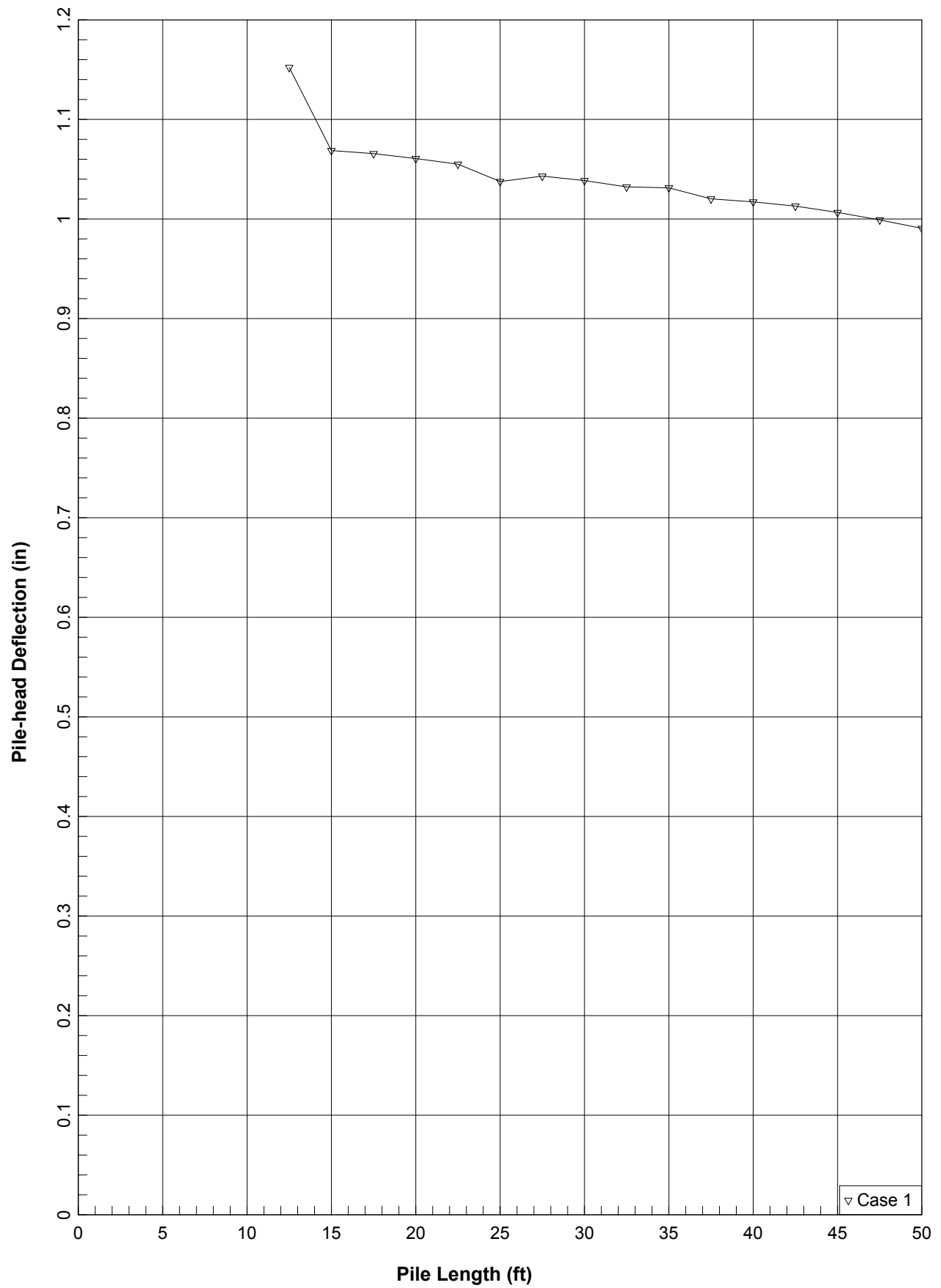
Layer 4, Depth 12.00 to 17.00 ft = Stiff Clay without Free Water

Layer 5, Depth 17.00 to 80.00 ft = Stiff Clay without Free Water









 Abut 5L_long_Critical Length

Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Serial Number of Security Device: 161633771
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 Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 5\
 Name of input data file: Abut 5L_long_Critical Length.lp6d
 Name of output report file: Abut 5L_long_Critical Length.lp6o
 Name of plot output file: Abut 5L_long_Critical Length.lp6p
 Name of runtime message file: Abut 5L_long_Critical Length.lp6r

 Date and Time of Analysis

Date: September 13, 2014 Time: 10:12:45

 Problem Title

Project Name: Palo Comado OC Bridge Widen

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

 Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

 Pile Structural Properties and Geometry

Page 1

 Abut 5L_long_Critical Length

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

 Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 16.0000000 in
 Bottom Width = 16.0000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

 Ground Slope and Pile Batter Angles

Ground Slope Angle = 33.700 degrees
 = 0.588 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

 Soil and Rock Layering Information

The soil profile is modelled using 5 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 7.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 7.00000 ft
 Distance from top of pile to bottom of layer = 12.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi

Page 2

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 12.00000 ft
 Distance from top of pile to bottom of layer = 17.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 17.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 130.00000 pcf
 Effective unit weight at bottom of layer = 130.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Rock Emass	Layer Depth ft	Effective Unit Wt. krm	Undrained Cohesion Test psf	In-situ Friction Test deg.	Angle of Friction Property	Uniaxial Elastic Mod. psi	ROD % or GSI
1	0.00700	Stiff Clay w/o Free Water	--	-2.000	120.000	4000.000	--	--	--	--
	0.00700	--	--	0.10000	120.000	4000.000	--	--	--	--
2	0.00700	Stiff Clay w/o Free Water	--	0.10000	120.000	1500.000	--	--	--	--
	0.00700	--	--	7.000	120.000	1500.000	--	--	--	--
3	0.00700	Stiff Clay w/o Free Water	--	7.000	120.000	3500.000	--	--	--	--
	0.00700	--	--	12.000	120.000	3500.000	--	--	--	--
4	0.00700	Stiff Clay w/o Free Water	--	12.000	125.000	4000.000	--	--	--	--
	0.00700	--	--	17.000	125.000	4000.000	--	--	--	--
5	0.00500	Stiff Clay w/o Free Water	--	17.000	130.000	4000.000	--	--	--	--
	0.00500	--	--	80.000	130.000	4000.000	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.9300	1.0000
2	50.000	0.9300	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Abut 5L_long_Critical Length

Number of loads specified = 1

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	V	23000. lbs	M = 0.0000 in-lbs	131000.	True

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head = 23000.000 lbs
 Applied moment at pile head = 0.000 in-lbs
 Axial thrust load on pile head = 131000.000 lbs

Depth inches	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress x psi*	Bending Stiffness lb-in ²	Soil Res. lb/in	Soil Spr. lb/inch	Distrib. Lat. Load lb/inch
0.00	0.0000	-7.153E-08	23000.	-0.0140	651.5405	5.799E+09	-647.8517	1961.8868	0.000
6.00	0.9066	137345.	20136.	-0.0139	1334.6404	5.799E+09	-306.9753	2031.5239	0.000
12.00	0.8235	263528.	18274.	-0.0137	1962.2210	5.799E+09	-313.5308	2284.4680	0.000
18.00	0.7419	378209.	16377.	-0.0134	2532.5981	5.799E+09	-318.9592	2579.4093	0.000
24.00	0.6628	481100.	14450.	-0.0129	3044.3360	5.799E+09	-323.2051	2926.0290	0.000
30.00	0.5866	571964.	12502.	-0.0124	3496.2581	5.799E+09	-326.2108	3356.8837	0.000
36.00	0.5139	650620.	10539.	-0.0118	3887.4588	5.799E+09	-327.9156	3828.4887	0.000
42.00	0.4453	716941.	8570.8988	-0.0111	4217.3147	5.799E+09	-328.2548	4422.9057	0.000
48.00	0.3811	770863.	6604.6589	-0.0103	4485.4967	5.799E+09	-327.1585	5150.1238	0.000
54.00	0.3218	812379.	4649.5333	-0.009475	4691.9832	5.799E+09	-324.5500	6051.7178	0.000
60.00	0.2675	841551.	2714.8504	-0.008619	4837.0730	5.799E+09	-320.3443	7186.6321	0.000
66.00	0.2183	858506.	810.4842	-0.007739	4921.4014	5.799E+09	-314.4445	8640.6249	0.000
72.00	0.1746	863443.	-1053.0665	-0.006849	4945.9561	5.799E+09	-306.7391	10542.	0.000
78.00	0.1362	856636.	-2864.5733	-0.005959	4912.0966	5.799E+09	-297.0965	13091.	0.000
84.00	0.1031	838436.	-4733.7470	-0.005082	4821.5772	5.799E+09	-325.9614	18975.	0.000
90.00	0.0752	807619.	-7006.5541	-0.004230	4669.3032	5.799E+09	-431.6410	34446.	0.000
96.00	0.0523	761007.	-9527.9358	-0.003418	4436.4765	5.799E+09	-408.8996	46889.	0.000
102.00	0.0342	698858.	-11896.	-0.002663	4127.3726	5.799E+09	-380.6376	66847.	0.000
108.00	0.0204	622437.	-14076.	-0.001979	3747.2890	5.799E+09	-345.9475	101969.	0.000
114.00	0.0104	533056.	-16021.	-0.001382	3302.7459	5.799E+09	-302.3106	174218.	0.000
120.00	0.003776	432359.	-17654.	-0.000882	2801.9182	5.799E+09	-242.1753	384791.	0.000
126.00	-0.000175	322592.	-17891.	-0.000492	2255.9802	5.799E+09	163.4320	5610741.	0.000
132.00	-0.002123	218446.	-19599.	-0.000212	1737.9997	5.799E+09	480.2624	1357325.	0.000
138.00	-0.002715	131411.	-12996.	-0.001382	1305.1263	5.799E+09	510.7302	1128685.	0.000
144.00	-0.002491	62656.	-9847.5517	6.972E-05	963.1672	5.799E+09	535.5737	1289933.	0.000
150.00	-0.001878	13131.	-6643.7754	0.000109	716.8487	5.799E+09	532.3517	1700489.	0.000
156.00	-0.001184	-17240.	-3623.6547	0.000107	737.2867	5.799E+09	474.3552	2403820.	0.000
162.00	-0.000597	-30521.	-1001.5262	8.209E-05	803.3387	5.799E+09	399.6876	4019026.	0.000
168.00	-0.000199	-29388.	835.1320	5.110E-05	797.7028	5.799E+09	212.5318	6412276.	0.000
174.00	1.651E-05	-20580.	1446.1807	2.525E-05	753.8946	5.799E+09	-8.8489	3215874.	0.000
180.00	0.000104	-12073.	1247.6973	3.356E-06	711.5876	5.799E+09	57.3123	3302622.	0.000
186.00	0.000117	-5620.9799	877.8577	7.982E-07	679.4935	5.799E+09	65.9676	3389575.	0.000
192.00	9.454E-05	-1537.6370	515.6340	-4.501E-06	659.1881	5.799E+09	-54.7737	3476132.	0.000
198.00	6.276E-05	574.4048	239.5089	-5.000E-06	654.3974	5.799E+09	-37.2681	3562892.	0.000
204.00	3.454E-05	1344.3297	64.5205	-4.007E-06	658.2267	5.799E+09	-20.9847	3644833.	0.000
210.00	1.467E-05	1357.7104	-26.8878	-2.609E-06	658.2932	5.799E+09	9.5614	3909380.	0.000
216.00	3.234E-06	1025.7776	-62.0459	-1.376E-06	656.6423	5.799E+09	-2.1580	4003958.	0.000
222.00	-1.839E-06	615.3227	-62.1081	-5.270E-07	654.6009	5.799E+09	2.1373	6975000.	0.000
228.00	-3.091E-06	281.3089	-44.9176	-6.315E-08	652.9397	5.799E+09	3.5929	6975000.	0.000
234.00	-2.596E-06	76.4105	-25.0842	1.219E-07	651.9206	5.799E+09	3.0183	6975000.	0.000
240.00	-1.628E-06	-19.8928	-10.3530	1.512E-07	651.6395	5.799E+09	1.8921	6975000.	0.000
246.00	-7.825E-07	-48.0628	-1.9477	1.160E-07	651.7792	5.799E+09	0.9096	6975000.	0.000
252.00	-2.356E-07	-43.4480	1.6029	6.866E-08	651.7566	5.799E+09	0.2739	6975000.	0.000

Abut	5L	long	Critical	Length					
258.000	4.142E-08	-28.9359	2.3281	3.121E-08	651.6845	5.799E+09	-0.0322	4666185	0.000
264.000	1.388E-07	-15.5598	1.9010	8.186E-09	651.6179	5.799E+09	-0.1102	4760810	0.000
270.000	1.397E-07	-6.1368	1.2315	-3.039E-09	651.5711	5.799E+09	-0.1130	4855439	0.000
276.000	1.024E-07	-0.7773	0.6391	-6.616E-09	651.5444	5.799E+09	-0.0845	4950072	0.000
282.000	6.026E-08	1.5423	0.2337	-6.220E-09	651.5482	5.799E+09	-0.0507	5044709	0.000
288.000	2.773E-08	2.0366	0.0104	-4.368E-09	651.5507	5.799E+09	-0.0238	5139350	0.000
294.000	7.845E-09	1.6741	-0.0814	-2.448E-09	651.5489	5.799E+09	-0.006843	5233993	0.000
300.000	-1.649E-09	1.0639	-0.0962	-1.032E-09	651.5458	5.799E+09	0.001917	6975000	0.000
306.000	-4.539E-09	0.5218	-0.0746	-2.116E-10	651.5431	5.799E+09	0.005276	6975000	0.000
312.000	-4.188E-09	0.1693	-0.0441	1.460E-10	651.5414	5.799E+09	0.004869	6975000	0.000
318.000	-2.787E-09	-0.008153	-0.0198	2.294E-10	651.5406	5.799E+09	0.003239	6975000	0.000
324.000	-1.436E-09	-0.0690	-0.005096	1.895E-10	651.5409	5.799E+09	0.001669	6975000	0.000
330.000	-5.131E-10	-0.0699	0.001700	1.178E-10	651.5409	5.799E+09	0.000596	6975000	0.000
336.000	-2.246E-11	-0.0487	0.003568	5.655E-11	651.5408	5.799E+09	2.611E-05	6975000	0.000
342.000	1.656E-10	-0.0269	0.003150	1.744E-11	651.5407	5.799E+09	-0.000165	5991245	0.000
348.000	1.868E-10	-0.0110	0.002086	-2.134E-12	651.5406	5.799E+09	-0.000189	6085912	0.000
354.000	1.400E-10	-0.001843	0.001085	-8.755E-12	651.5406	5.799E+09	-0.000144	6180581	0.000
360.000	8.174E-11	0.002078	0.000396	-8.633E-12	651.5406	5.799E+09	-8.549E-05	6275252	0.000
366.000	3.639E-11	0.002920	2.344E-05	-6.048E-12	651.5406	5.799E+09	-3.863E-05	6369925	0.000
372.000	9.164E-12	0.002369	-0.000122	-3.312E-12	651.5406	5.799E+09	-9.874E-06	6464599	0.000
378.000	-3.352E-12	0.001460	-0.000140	-1.330E-12	651.5406	5.799E+09	3.897E-06	6975000	0.000
384.000	-6.801E-12	0.000691	-0.000105	0.000000	651.5406	5.799E+09	7.907E-06	6975000	0.000
390.000	-5.962E-12	0.000206	-6.008E-05	0.000000	651.5405	5.799E+09	6.930E-06	6975000	0.000
396.000	-3.845E-12	-3.040E-05	2.588E-05	0.000000	651.5405	5.799E+09	4.470E-06	6975000	0.000
402.000	-1.918E-12	-0.000105	-5.775E-06	0.000000	651.5405	5.799E+09	2.230E-06	6975000	0.000
408.000	0.000000	-0.000100	3.164E-06	0.000000	651.5405	5.799E+09	7.501E-07	6975000	0.000
414.000	0.000000	-0.772E-05	5.394E-06	0.000000	651.5405	5.799E+09	-6.994E-09	6975000	0.000
420.000	0.000000	-3.552E-05	4.547E-06	0.000000	651.5405	5.799E+09	-2.753E-07	6975000	0.000
426.000	0.000000	-1.319E-05	2.859E-06	0.000000	651.5405	5.799E+09	-2.873E-07	6975000	0.000
432.000	0.000000	-1.199E-06	1.385E-06	0.000000	651.5405	5.799E+09	-2.040E-07	6975000	0.000
438.000	0.000000	3.451E-06	4.367E-07	0.000000	651.5405	5.799E+09	-1.121E-07	6975000	0.000
444.000	0.000000	4.060E-06	-3.512E-08	0.000000	651.5405	5.799E+09	-4.515E-08	6975000	0.000
450.000	0.000000	3.041E-06	-1.930E-07	0.000000	651.5405	5.799E+09	-7.468E-09	6975000	0.000
456.000	0.000000	1.750E-06	-1.906E-07	0.000000	651.5405	5.799E+09	8.268E-09	6975000	0.000
462.000	0.000000	7.562E-07	-1.317E-07	0.000000	651.5405	5.799E+09	1.137E-08	6975000	0.000
468.000	0.000000	1.707E-07	-7.050E-08	0.000000	651.5405	5.799E+09	9.014E-09	6975000	0.000
474.000	0.000000	-9.047E-08	-2.718E-08	0.000000	651.5405	5.799E+09	5.427E-09	6975000	0.000
480.000	0.000000	-1.562E-07	-3.424E-09	0.000000	651.5405	5.799E+09	2.492E-09	6975000	0.000
486.000	0.000000	-1.321E-07	6.105E-09	0.000000	651.5405	5.799E+09	6.844E-10	6975000	0.000
492.000	0.000000	-8.324E-08	7.649E-09	0.000000	651.5405	5.799E+09	-1.697E-10	6975000	0.000
498.000	0.000000	-4.043E-08	5.870E-09	0.000000	651.5405	5.799E+09	-4.231E-10	6975000	0.000
504.000	0.000000	-1.282E-08	2.446E-09	0.000000	651.5405	5.799E+09	-3.847E-10	6975000	0.000
510.000	0.000000	9.468E-10	1.531E-09	0.000000	651.5405	5.799E+09	-2.538E-10	6975000	0.000
516.000	0.000000	5.576E-09	3.801E-10	0.000000	651.5405	5.799E+09	-1.297E-10	6975000	0.000
522.000	0.000000	5.531E-09	-1.467E-10	0.000000	651.5405	5.799E+09	-4.588E-11	6975000	0.000
528.000	0.000000	-1.004E-10	1.042E-11	0.000000	651.5405	5.799E+09	0.000000	6975000	0.000
534.000	0.000000	2.056E-09	-2.530E-10	0.000000	651.5405	5.799E+09	1.434E-11	6975000	0.000
540.000	0.000000	7.955E-10	-1.627E-10	0.000000	651.5405	5.799E+09	1.579E-11	6975000	0.000
546.000	0.000000	1.031E-10	-8.083E-11	0.000000	651.5405	5.799E+09	1.150E-11	6975000	0.000
552.000	0.000000	-1.755E-10	-2.697E-11	0.000000	651.5405	5.799E+09	6.460E-12	6975000	0.000
558.000	0.000000	-2.215E-10	0.000000	0.000000	651.5405	5.799E+09	2.691E-12	6975000	0.000
564.000	0.000000	-1.704E-10	1.012E-11	0.000000	651.5405	5.799E+09	0.000000	6975000	0.000
570.000	0.000000	-1.004E-10	1.042E-11	0.000000	651.5405	5.799E+09	0.000000	6975000	0.000
576.000	0.000000	-4.551E-11	7.249E-12	0.000000	651.5405	5.799E+09	0.000000	6975000	0.000
582.000	0.000000	-1.346E-11	3.771E-12	0.000000	651.5405	5.799E+09	0.000000	6975000	0.000
588.000	0.000000	0.000000	1.261E-12	0.000000	651.5405	5.799E+09	0.000000	6975000	0.000
594.000	0.000000	1.724E-12	0.000000	0.000000	651.5405	5.799E+09	0.000000	6975000	0.000
600.000	0.000000	0.000000	0.000000	0.000000	651.5405	5.799E+09	0.000000	3487500	0.000

feet	inches	in-lbs	Abut 5L_long_Critical Length lbs
50.000	0.9906561	863443.	23000.
47.500	0.9989905	864583.	23000.
45.000	1.0066277	867806.	23000.
42.500	1.0128473	870832.	23000.
40.000	1.0171452	873997.	23000.
37.500	1.0201248	877542.	23000.
35.000	1.0313167	879328.	23000.
32.500	1.0322958	882758.	23000.
30.000	1.0386211	886080.	23000.
27.500	1.0431617	889208.	23000.
25.000	1.0375694	894718.	23000.
22.500	1.0551199	895149.	23000.
20.000	1.0607051	898353.	23000.
17.500	1.0657033	901454.	23000.
15.000	1.0686449	905182.	23000.
12.500	1.1523432	894572.	23000.

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

- Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
- Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
- Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
- Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
- Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load Type	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	1	V = 23000.	M = 0.000	131000.	0.99065606	863443.	23000.	-0.01400344

The analysis ended normally.

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Pile-head deflection	=	0.9906561	inches
Computed slope at pile head	=	-0.0140034	radians
Maximum bending moment	=	863443.	inch-lbs
Maximum shear force	=	23000.	lbs
Depth of maximum bending moment	=	72.0000000	inches below pile head
Depth of maximum shear force	=	0.0000000	inches below pile head
Number of iterations	=	30	
Number of zero deflection points	=	13	

Pile-head Deflection vs. Pile Length for Load Case 1

Boundary Condition Type 1, Shear and Moment

Shear	=	23000.	lbs
Moment	=	0.	in-lbs
Axial Load	=	131000.	lbs

Pile Length	Pile Head Deflection	Maximum Moment	Maximum Shear
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Abut 5L_long_Ave P

Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 5L
 Name of input data file: Abut 5L_long_Ave P.lpd
 Name of output report file: Abut 5L_long_Ave P.lpo
 Name of plot output file: Abut 5L_long_Ave P.lpp
 Name of runtime message file: Abut 5L_long_Ave P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 10:07:39

Problem Title

Project Name: Palo Comado OC Bridge Widened

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

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Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 16.0000000 in
 Bottom Width = 16.0000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 33.700 degrees
 = 0.588 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 5 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 7.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 7.00000 ft
 Distance from top of pile to bottom of layer = 12.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 12.00000 ft
 Distance from top of pile to bottom of layer = 17.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 17.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Rock Emass	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Uniaxial Elastic Mod.	ROD % or GSI
Num.	Epsilon 50	J	psi	pcf	psf	deg.	psi	
1	0.00700	Stiff Clay w/o Free Water	-2.000	120.000	4000.000	--	--	--
2	0.00700	Stiff Clay w/o Free Water	0.10000	120.000	1500.000	--	--	--
3	0.00700	Stiff Clay w/o Free Water	7.000	120.000	3500.000	--	--	--
4	0.00700	Stiff Clay w/o Free Water	12.000	125.000	4000.000	--	--	--
5	0.00500	Stiff Clay w/o Free Water	17.000	125.000	4500.000	--	--	--
	0.00500		80.000	125.000	4500.000	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X Ft	p-mult	y-mult
1	0.000	0.9300	1.0000
2	50.000	0.9300	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

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Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4	y = 0.25000 in	M = 0.0000 in-lbs	131000.	False
2	4	y = 0.50000 in	M = 0.0000 in-lbs	131000.	False
3	4	y = 1.00000 in	M = 0.0000 in-lbs	131000.	False

V = perpendicular shear force applied to pile head

M = bending moment applied to pile head

y = lateral deflection relative to pile axis

S = pile slope relative to original pile batter angle

R = rotational stiffness applied to pile head

Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.250000 inches
 Moment at pile head = 0.000 in-lbs
 Axial load at pile head = 131000.000 lbs

Depth X inches	Deflect. y inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil Res. p lb/in	Soil Spr. Es ^h lb/inch	Distrib. Lat. Load lb/inch
0.00	0.2500	0.000	12400.	-0.004419	651.5405	5.799E+09	-459.1736	5510.0831	0.000
6.00	0.2235	69606.	10373.	-0.004383	997.7335	5.799E+09	-216.2991	5807.1060	0.000
12.00	0.1974	131369.	9066.1548	-0.004279	1304.9166	5.799E+09	-219.3838	6668.2028	0.000
18.00	0.1721	185127.	7743.9075	-0.004116	1572.2878	5.799E+09	-221.3653	7716.1407	0.000
24.00	0.1480	230766.	6413.2521	-0.003900	1799.2749	5.799E+09	-222.1865	9006.7978	0.000
30.00	0.1253	268218.	5081.3305	-0.003642	1985.5462	5.799E+09	-221.7873	10618.	0.000
36.00	0.1043	297467.	3755.6608	-0.003350	2131.0217	5.799E+09	-220.1026	12661.	0.000
42.00	0.0851	318551.	2444.1709	-0.003031	2235.8847	5.799E+09	-217.0607	15298.	0.000
48.00	0.0679	331562.	1155.2453	-0.002695	2300.5946	5.799E+09	-212.5812	18775.	0.000
54.00	0.0528	336650.	-102.2094	-0.002349	2325.9008	5.799E+09	-206.5704	23476.	0.000
60.00	0.0397	334028.	-1318.6685	-0.002002	2312.8590	5.799E+09	-198.9160	30027.	0.000
66.00	0.0288	323973.	-2483.8446	-0.001661	2262.8503	5.799E+09	-189.4761	39511.	0.000
72.00	0.0198	306534.	-3586.4554	-0.001335	2177.6055	5.799E+09	-178.0609	53930.	0.000
78.00	0.0128	283034.	-4613.8218	-0.001030	2059.2380	5.799E+09	-164.3946	77350.	0.000
84.00	0.007451	253087.	-5614.2733	-0.000753	1910.2908	5.799E+09	-169.0893	136160.	0.000
90.00	0.003721	216846.	-6732.7906	-0.000509	1730.0445	5.799E+09	-203.7498	328508.	0.000
96.00	0.001338	173094.	-7835.4289	-0.000308	1512.4399	5.799E+09	-163.7963	734548.	0.000
102.00	0.0013E-05	123305.	-8359.1587	-0.000154	1264.8075	5.799E+09	-10.7803	2220215.	0.000
108.00	-0.000514	73027.	-7384.3337	-5.277E-05	1014.7461	5.799E+09	335.7220	3917806.	0.000
114.00	-0.000604	34776.	-5327.3676	3.008E-06	824.5001	5.799E+09	349.9334	3475861.	0.000
120.00	-0.000478	9993.6644	-3287.0764	2.570E-05	696.7687	5.799E+09	330.1637	4143826.	0.000
126.00	-0.000296	-4709.7492	-1467.3071	2.797E-05	674.9649	5.799E+09	276.4261	5610741.	0.000
132.00	-0.000142	-8557.9926	-238.5685	2.111E-05	694.1045	5.799E+09	133.1534	5610741.	0.000
138.00	-4.231E-05	-7605.7530	279.5865	1.275E-05	689.3685	5.799E+09	39.5649	5610741.	0.000
144.00	1.085E-05	-5222.9902	383.5555	6.108E-06	677.5176	5.799E+09	-4.9027	2791028.	0.000
150.00	3.099E-05	-3012.6896	321.4874	1.847E-06	666.5244	5.799E+09	-15.7808	3055509.	0.000
156.00	3.272E-05	-1368.0457	222.7376	-4.191E-07	658.3446	5.799E+09	-17.1358	3142256.	0.000
162.00	2.596E-05	-339.1789	129.4197	-1.302E-06	653.2755	5.799E+09	-13.9702	3229007.	0.000
168.00	1.709E-05	187.0377	59.1732	-1.381E-06	652.4708	5.799E+09	-9.4453	3315763.	0.000
174.00	9.386E-06	373.0711	14.8697	-1.091E-06	653.3961	5.799E+09	-5.3225	3402523.	0.000
180.00	3.996E-06	367.1897	-8.0695	-7.083E-07	653.3668	5.799E+09	-2.3239	3489286.	0.000
186.00	8.859E-07	273.8503	-16.6252	-3.749E-07	652.9200	5.799E+09	-0.5280	3576052.	0.000
192.00	-5.023E-07	168.2768	-16.5989	-1.443E-07	652.3775	5.799E+09	0.5368	6412276.	0.000
198.00	-8.457E-07	78.3907	-12.2769	-1.669E-08	651.9304	5.799E+09	0.9039	6412276.	0.000
204.00	-7.025E-07	20.9800	-7.0781	3.472E-08	651.6449	5.799E+09	0.8291	7080727.	0.000
210.00	-4.291E-07	-6.6008	-2.9073	4.214E-08	651.5734	5.799E+09	0.5612	7846875.	0.000
216.00	-1.966E-07	-13.9743	-0.4525	3.152E-08	651.6101	5.799E+09	0.2571	7846875.	0.000
222.00	-5.089E-08	-12.0799	0.5186	1.804E-08	651.6006	5.799E+09	0.0666	7846875.	0.000
228.00	1.983E-08	-7.7798	0.6723	7.762E-09	651.5792	5.799E+09	-0.0153	4635121.	0.000
234.00	4.226E-08	-4.0249	0.5261	1.655E-09	651.6506	5.799E+09	-0.0334	4740399.	0.000

Abut	5L Long Ave P	Bending Stiffness	Soil Res. p	Soil Spr. Es/h	Distrib. Load				
240.000	3.969E-08	-1.4687	0.3298	-1.187E-10	651.5405	5.799E-09	-0.0321	4845679	0.000
246.000	2.801E-08	-0.0652	0.1643	-1.981E-09	651.5409	5.799E-09	-0.0231	4905962	0.000
252.000	1.592E-08	0.5062	0.0547	-1.753E-09	651.5431	5.799E-09	-0.0134	5056247	0.000
258.000	6.977E-09	0.5942	-0.003538	-1.183E-09	651.5435	5.799E-09	-0.006002	5161535	0.000
264.000	1.721E-09	0.4656	-0.0261	-6.352E-10	651.5429	5.799E-09	-0.001510	5266824	0.000
270.000	-6.453E-10	0.2823	-0.0281	-2.483E-10	651.5420	5.799E-09	0.000844	7846875	0.000
276.000	-1.259E-09	0.1291	-0.0206	-3.545E-11	651.5412	5.799E-09	0.001646	7846875	0.000
282.000	-1.071E-09	0.0351	-0.0115	-4.949E-11	651.5407	5.799E-09	0.001400	7846875	0.000
288.000	-6.648E-10	-0.008555	-0.004655	6.322E-11	651.5406	5.799E-09	0.000869	7846875	0.000
294.000	-3.121E-10	-0.0209	-0.000823	4.799E-11	651.5407	5.799E-09	0.000408	7846875	0.000
300.000	-8.897E-11	-0.0185	0.000751	2.761E-11	651.5406	5.799E-09	0.000116	7846875	0.000
306.000	1.925E-11	-0.0119	0.001042	1.187E-11	651.5406	5.799E-09	-1.926E-05	6003897	0.000
312.000	5.348E-11	-0.006017	0.000821	2.892E-12	651.5406	5.799E-09	-5.445E-05	6109199	0.000
318.000	5.036E-11	-0.002071	0.000501	-1.592E-12	651.5406	5.799E-09	-5.216E-05	6214502	0.000
324.000	3.438E-11	-1.481E-06	0.000236	-2.664E-12	651.5405	5.799E-09	-3.621E-05	6319806	0.000
330.000	1.839E-11	0.000764	6.822E-05	-2.269E-12	651.5406	5.799E-09	-1.969E-05	6425112	0.000
336.000	7.148E-12	0.000821	-1.420E-05	651.5406	5.799E-09	-7.780E-06	6530418	0.000	
342.000	1.001E-12	0.000596	-4.086E-05	0.000	651.5406	5.799E-09	-1.107E-06	6635725	0.000
348.000	-1.444E-12	0.000332	-3.851E-05	0.000	651.5405	5.799E-09	1.889E-06	7846875	0.000
354.000	-1.831E-12	0.000135	-2.566E-05	0.000	651.5405	5.799E-09	2.395E-06	7846875	0.000
360.000	-1.382E-12	2.359E-05	-1.306E-05	0.000	651.5405	5.799E-09	1.808E-06	7846875	0.000
366.000	0.000	-2.228E-05	-4.542E-06	0.000	651.5405	5.799E-09	1.030E-06	7846875	0.000
372.000	0.000	-3.106E-05	-1.544E-07	0.000	651.5405	5.799E-09	4.327E-07	7846875	0.000
378.000	0.000	-2.423E-05	1.407E-06	0.000	651.5405	5.799E-09	8.769E-08	7846875	0.000
384.000	0.000	-1.422E-05	1.499E-06	0.000	651.5405	5.799E-09	-5.695E-08	7372899	0.000
390.000	0.000	-6.518E-06	1.061E-06	0.000	651.5405	5.799E-09	-8.903E-08	7478212	0.000
400.000	0.000	6.257E-07	2.235E-07	0.000	651.5405	5.799E-09	-1.543E-09	7846875	0.000
408.000	0.000	1.196E-06	2.914E-08	0.000	651.5405	5.799E-09	-2.037E-08	7794156	0.000
414.000	0.000	1.005E-06	-4.817E-08	0.000	651.5405	5.799E-09	-5.400E-09	7846875	0.000
420.000	0.000	6.198E-07	-5.974E-08	0.000	651.5405	5.799E-09	-4.441E-08	7888841	0.000
426.000	0.000	2.893E-07	-4.475E-08	0.000	651.5405	5.799E-09	3.455E-09	7846875	0.000
432.000	0.000	8.296E-08	-2.533E-08	0.000	651.5405	5.799E-09	3.018E-09	7846875	0.000
438.000	0.000	-1.481E-08	-1.056E-08	0.000	651.5405	5.799E-09	1.907E-09	7846875	0.000
444.000	0.000	-4.392E-08	-2.088E-09	0.000	651.5405	5.799E-09	9.160E-10	7846875	0.000
450.000	0.000	-4.003E-08	1.506E-09	0.000	651.5405	5.799E-09	2.819E-10	7846875	0.000
456.000	0.000	-2.959E-08	2.270E-09	0.000	651.5405	5.799E-09	-2.708E-11	7846875	0.000
462.000	0.000	-1.283E-08	1.813E-09	0.000	651.5405	5.799E-09	-1.254E-10	7846875	0.000
468.000	0.000	-4.209E-09	0.078E-09	0.000	651.5405	5.799E-09	-1.195E-10	7846875	0.000
474.000	0.000	1.119E-10	4.810E-10	0.000	651.5405	5.799E-09	0.000	7846875	0.000
480.000	0.000	1.571E-09	1.215E-10	0.000	651.5405	5.799E-09	-4.036E-11	7846875	0.000
486.000	0.000	-1.576E-09	-4.152E-11	0.000	651.5405	5.799E-09	-1.399E-11	7846875	0.000
492.000	0.000	1.077E-09	-8.472E-11	0.000	651.5405	5.799E-09	0.000	7846875	0.000
498.000	0.000	5.616E-10	-7.272E-11	0.000	651.5405	5.799E-09	4.413E-12	7846875	0.000
504.000	0.000	2.048E-10	-4.545E-11	0.000	651.5405	5.799E-09	4.680E-12	7846875	0.000
510.000	0.000	1.617E-11	-2.156E-11	0.000	651.5405	5.799E-09	3.284E-12	7846875	0.000
516.000	0.000	-5.422E-11	-6.437E-12	0.000	651.5405	5.799E-09	1.757E-12	7846875	0.000
522.000	0.000	-6.133E-11	0.000	0.000	651.5405	5.799E-09	0.000	7846875	0.000
528.000	0.000	-4.429E-11	3.092E-12	0.000	651.5405	5.799E-09	0.000	7846875	0.000
534.000	0.000	-2.431E-11	2.887E-12	0.000	651.5405	5.799E-09	0.000	7846875	0.000
540.000	0.000	-9.665E-12	1.898E-12	0.000	651.5405	5.799E-09	0.000	7846875	0.000
546.000	0.000	-1.526E-12	0.000	0.000	651.5405	5.799E-09	0.000	7846875	0.000
552.000	0.000	-1.774E-12	0.000	0.000	651.5405	5.799E-09	0.000	7846875	0.000
558.000	0.000	2.350E-12	0.000	0.000	651.5405	5.799E-09	0.000	7846875	0.000
564.000	0.000	1.802E-12	0.000	0.000	651.5405	5.799E-09	0.000	7846875	0.000
570.000	0.000	1.041E-12	0.000	0.000	651.5405	5.799E-09	0.000	7846875	0.000
576.000	0.000	0.000	0.000	0.000	651.5405	5.799E-09	0.000	7846875	0.000
582.000	0.000	0.000	0.000	0.000	651.5405	5.799E-09	0.000	7846875	0.000
588.000	0.000	0.000	0.000	0.000	651.5405	5.799E-09	0.000	7846875	0.000
594.000	0.000	0.000	0.000	0.000	651.5405	5.799E-09	0.000	7846875	0.000
600.000	0.000	0.000	0.000	0.000	651.5405	5.799E-09	0.000	3923438	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Pile-head deflection	=	0.2500000	inches
Computed slope at pile head	=	-0.0044193	rad
Maximum bending moment	=	336650	inch-lbs
Maximum shear force	=	12400	lbs
Depth of maximum bending moment	=	54.0000000	inches below pile head
Depth of maximum shear force	=	0.0000000	inches below pile head
Number of iterations	=	15	
Number of zero deflection points	=	14	

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)	=	0.500000	inches
Displacement of pile head	=	0.000000	inches
Moment at pile head	=	0.000	in-lbs
Axial load at pile head	=	1310000	lbs

Depth y	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Abut Stress psi *	5L Long Ave P Stiffness lb-in ²	Soil Res. p/lb/in	Soil Spr. Es/h	Distrib. Load lb/in
0.00	0.5000	0.000	16889	-0.007884	651.5405	5.799E-09	-566.0525	3276.3150	0.000
6.00	0.4527	97700	14476	-0.007834	1137.4582	5.799E-09	-258.0446	3420.1086	0.000
12.00	0.4060	186030	12914	-0.007687	1576.7780	5.799E-09	-262.7233	3882.6359	0.000
18.00	0.3605	264751	11327	-0.007454	1968.3048	5.799E-09	-266.2911	4432.5931	0.000
24.00	0.3166	336571	9722	-0.007144	2311.0815	5.799E-09	-268.6921	5092.8089	0.000
30.00	0.2747	392646	8106	-0.006768	2604.3994	5.799E-09	-269.8676	5893.8754	0.000
36.00	0.2353	441586	6487	-0.006337	2847.8094	5.799E-09	-269.7552	6877.5147	0.000
42.00	0.1987	480456	4873	-0.005860	3041.1337	5.799E-09	-268.2874	8101.7709	0.000
48.00	0.1650	509277	3272	-0.005347	3184.4779	5.799E-09	-265.8900	9649.2527	0.000
54.00	0.1345	528130	1693	-0.004811	3278.2441	5.799E-09	-260.9798	11641	0.000
60.00	0.1073	537158	145	-0.004260	3323.1458	5.799E-09	-254.9611	14258	0.000
66.00	0.0834	536571	-1361	-0.003704	3320.2241	5.799E-09	-247.2204	17785	0.000
72.00	0.0628	526647	-2815	-0.003154	3270.8674	5.799E-09	-237.6192	22687	0.000
78.00	0.0456	507741	-4206	-0.002619	3176.8348	5.799E-09	-225.9807	29764	0.000
84.00	0.0314	480286	-5611	-0.002108	3040.2867	5.799E-09	-212.2433	38264	0.000
90.00	0.0203	443720	-7271	-0.001630	2858.4233	5.799E-09	-191.0805	49212	0.000
96.00	0.0119	395594	-9051	-0.001195	2619.0643	5.799E-09	-162.2183	64270	0.000
102.00	0.005916	336987	-10635	-0.000816	2327.5752	5.799E-09	-125.7187	84292	0.000
108.00	0.002063	269259	-11959	-0.000503	1990.7272	5.799E-09	-81.5618	108746	0.000
114.00	-0.000118	194273	-12215	-0.000263	1617.7748	5.799E-09	-35.1071	142071	0.000
120.00	-0.001093	123095	-10668	-9.878E-05	1263.7645	5.799E-09	405.3649	2226219	0.000
126.00	-0.001303	66410	-8180	-6.650E-05	981.8365	5.799E-09	423.8096	1951252	0.000
132.00	-0.001345	26475	-5744	-4.652E-05	775.5206	5.799E-09	366.1872	142276	0.000
138.00	-0.000745	-1951	-2699	-3.680E-05	614.7454	5.799E-09	368.0186	2563967	0.000
144.00	-0.000401	-15580	-1252	-2.574E-05	4933E-05	5.799E-09	337.1421	5049380	0.000
150.00	-0.000153	-17060	249	-2.299E-05	3.245E-05	5.799E-09	163.4826	6412276	0.000
156.00	-1.124E-05	1240	1240	-1.708E-05	1.708E-05	5.799E-09	12.0124	74276	0.000
162.00	6.620E-05	-7777	0758	729	4.777E-06	5.799E-09	-27.4524	3166681	0.000
168.00	0.000155	-3896	3143	538	1.487E-06	5.799E-09	-36.3239	3253431	0.000
174.00	0.377E-05	-1320	0461	332	6.903E-06	5.799E-09	-32.1622	3340185	0.000
180.00	4.036E-05	688	9678	56	4.790E-06	5.799E-09</			

				Abut	SL_long_Ave P				
522.000	0.000	7.380E-11	-4.632E-11	0.000	651.5405	5.799E+09	6.542E-12	7846875.0	0.000
528.000	0.000	-8.664E-11	-1.566E-11	0.000	651.5405	5.799E+09	3.678E-12	7846875.0	0.000
534.000	0.000	-1.146E-10	0.000	0.000	651.5405	5.799E+09	1.518E-12	7846875.0	0.000
540.000	0.000	-8.782E-11	5.345E-12	0.000	651.5405	5.799E+09	0.000	7846875.0	0.000
546.000	0.000	-5.063E-11	5.519E-12	0.000	651.5405	5.799E+09	0.000	7846875.0	0.000
552.000	0.000	-2.166E-11	3.824E-12	0.000	651.5405	5.799E+09	0.000	7846875.0	0.000
558.000	0.000	-4.751E-12	2.021E-12	0.000	651.5405	5.799E+09	0.000	7846875.0	0.000
564.000	0.000	2.606E-12	0.000	0.000	651.5405	5.799E+09	0.000	7846875.0	0.000
570.000	0.000	4.310E-12	0.000	0.000	651.5405	5.799E+09	0.000	7846875.0	0.000
576.000	0.000	3.507E-12	0.000	0.000	651.5405	5.799E+09	0.000	7846875.0	0.000
582.000	0.000	2.082E-12	0.000	0.000	651.5405	5.799E+09	0.000	7846875.0	0.000
588.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	7846875.0	0.000
594.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	7846875.0	0.000
600.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	3923438.0	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Pile-head deflection = 0.50000000 inches
 Computed slope at pile head = -0.0078841 radians
 Maximum bending moment = 537158.1 inch-lbs
 Maximum shear force = 6884.4 lbs
 Depth of maximum bending moment = 60.000000 inches below pile head
 Depth of maximum shear force = 0.000000 inches below pile head
 Number of iterations = 14
 Number of zero deflection points = 13

 Computed Values of Pile Loading and Deflection
 For Lateral Loading for Load Case Number 3

Pile-head conditions are Diplacement and Moment (Loading Type 4)
 Displacement of pile head = 1.000000 inches
 Moment at pile head = 0.000000 in-lbs
 Axial load at pile head = 131000.000 lbs

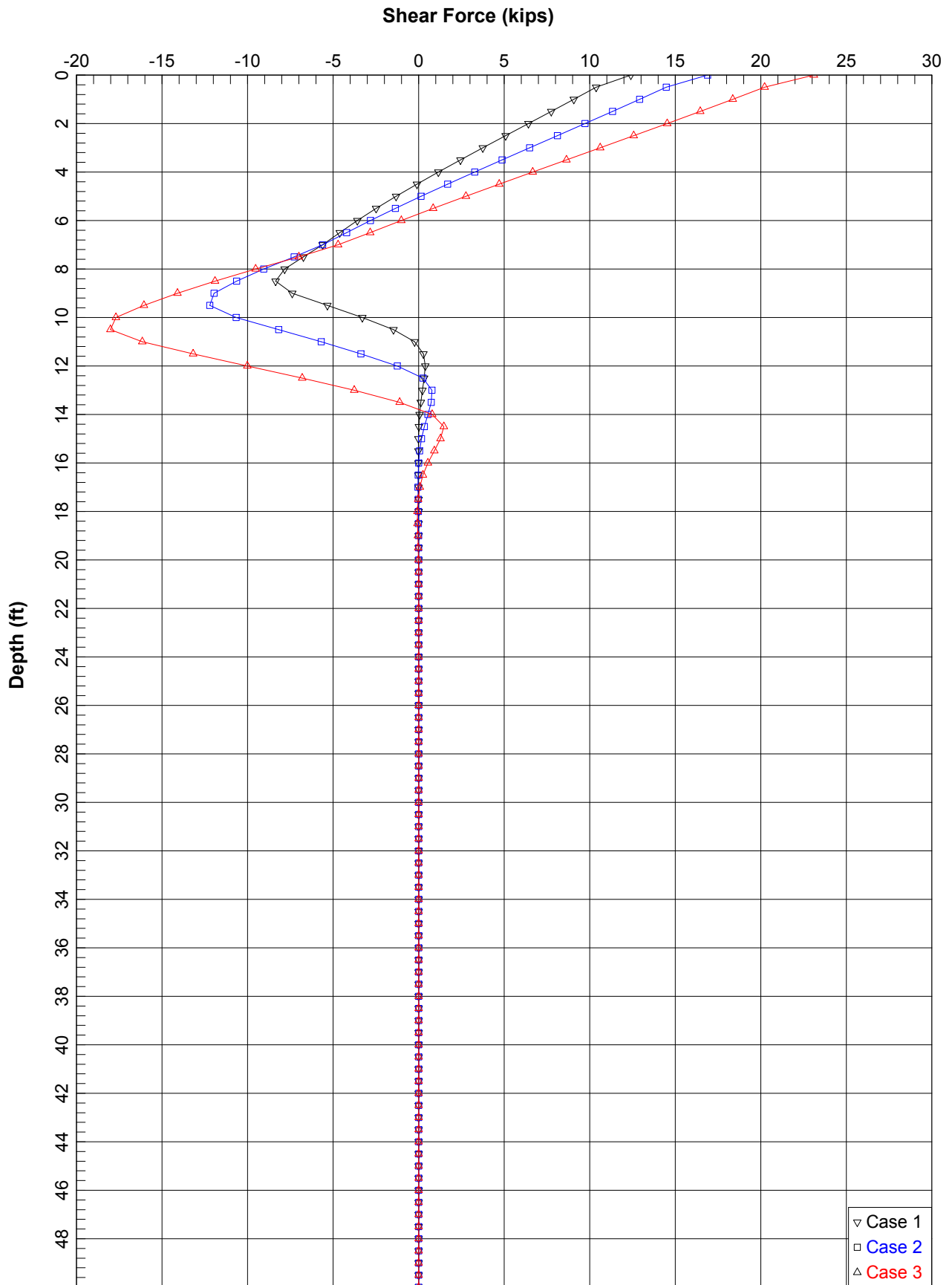
Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil Res.	Soil Spr.	Distrib.
x	y	Moment	Force	radians	Stress	Stiffness	p	E's'h	Lat. Load
inches	inches	in-lbs	lbs		psi	lb/in ²	lb/in	lb/inch	lb/inch
0.00	1.0000	0.000	23099.	-0.0141	651.5405	5.799E+09	-649.3695	1948.1086	0.000
6.00	0.9153	138002.	20228.	-0.0140	1337.9049	5.799E+09	-307.7048	2017.0610	0.000
12.00	0.8315	264814.	18362.	-0.0138	1968.6168	5.799E+09	-314.2882	2267.9478	0.000
18.00	0.7493	380096.	16460.	-0.0135	2541.9844	5.799E+09	-319.7441	2560.4228	0.000
24.00	0.6694	483559.	14529.	-0.0131	3056.5645	5.799E+09	-324.0171	2904.0585	0.000
30.00	0.5926	574963.	12575.	-0.0125	3511.1736	5.799E+09	-327.0496	3311.2646	0.000
36.00	0.5194	654127.	10608.	-0.0119	3904.8990	5.799E+09	-328.7807	3798.3652	0.000
42.00	0.4502	720922.	8634.2012	-0.0112	4237.1105	5.799E+09	-329.1459	4387.1440	0.000
48.00	0.3854	775281.	6662.5384	-0.0104	4507.4725	5.799E+09	-328.0751	5107.2082	0.000
54.00	0.3255	817199.	4701.8381	-0.009562	4715.9569	5.799E+09	-325.4917	5999.5798	0.000
60.00	0.2707	846735.	2761.4312	-0.008702	4862.8566	5.799E+09	-321.3106	7122.3864	0.000
66.00	0.2211	864015.	851.1947	-0.007817	4948.8008	5.799E+09	-315.4349	8560.1439	0.000
72.00	0.1769	869237.	-1018.3698	-0.006920	4974.7117	5.799E+09	-307.7532	10439.	0.000
78.00	0.1381	862673.	-2836.0308	-0.006024	4942.1236	5.799E+09	-298.1338	12957.	0.000
84.00	0.1046	844674.	-4711.9487	-0.005140	4852.6052	5.799E+09	-327.1721	18768.	0.000
90.00	0.0764	814210.	-6993.5524	-0.004282	4701.0902	5.799E+09	-433.3624	34046.	0.000
96.00	0.0532	767483.	-9525.4117	-0.003464	4468.6885	5.799E+09	-410.5907	46301.	0.000
102.00	0.0348	705351.	-11905.	-0.002702	4159.6664	5.799E+09	-382.4576	65929.	0.000
108.00	0.0208	628876.	-14095.	-0.002012	3779.3123	5.799E+09	-347.8193	100406.	0.000
114.00	0.0107	539368.	-16052.	-0.001407	3334.1376	5.799E+09	-304.2539	171132.	0.000
120.00	0.003898	438469.	-17697.	-0.000901	2832.3047	5.799E+09	-244.3319	376044.	0.000
126.00	-0.00148	328417.	-18015.	-0.000505	2284.9507	5.799E+09	-138.6162	5610741.	0.000
132.00	-0.002156	223988.	-16155.	-0.000219	1761.0875	5.799E+09	481.1168	1338918.	0.000
138.00	-0.002779	134897.	-13174.	-3.400E-05	1322.4655	5.799E+09	512.7367	1107125.	0.000
144.00	-0.002564	65056.	-10021.	6.945E-05	975.1029	5.799E+09	538.2701	1259600.	0.000
150.00	-0.001945	14540.	-6799.2696	0.000111	723.8541	5.799E+09	535.5504	1651768.	0.000
156.00	-0.001236	-16709.	-3759.3829	0.000110	734.6446	5.799E+09	477.7452	2318266.	0.000
162.00	-0.000631	-30745.	-1116.4760	8.495E-05	804.4548	5.799E+09	403.2238	3832268.	0.000
168.00	-0.000217	-30240.	788.9981	5.340E-05	801.9436	5.799E+09	231.9343	6412276.	0.000
174.00	9.521E-06	-21361.	1469.4917	2.671E-05	757.7824	5.799E+09	-5.1031	3215874.	0.000
180.00	0.000103	-12648.	1023.3489	9.110E-05	714.6865	5.799E+09	-56.9405	3302627.	0.000
186.00	0.000119	-5975.1885	911.1342	5.248E-07	681.2587	5.799E+09	-67.1351	3389375.	0.000
192.00	9.715E-05	-1713.9719	540.8797	-4.503E-06	660.0651	5.799E+09	-56.2831	3476132.	0.000
198.00	6.481E-05	522.4462	256.5753	-5.119E-06	654.1390	5.799E+09	-38.4850	3562892.	0.000
204.00	3.572E-05	1372.9791	73.8770	-4.139E-06	658.3582	5.799E+09	-73.8770	3765302.	0.000
210.00	1.514E-05	1415.4766	-25.6846	-2.696E-06	658.5806	5.799E+09	-10.7728	4267998.	0.000
216.00	3.362E-06	1069.0022	-65.3538	-1.411E-06	656.8573	5.799E+09	-2.4503	4373264.	0.000
222.00	-1.784E-06	633.4490	-65.7037	-5.300E-07	654.6911	5.799E+09	2.3336	7846875.	0.000
228.00	-2.998E-06	281.3913	-46.9413	-5.665E-08	652.9401	5.799E+09	3.9205	7846875.	0.000
234.00	-2.464E-06	70.2431	-25.5117	1.253E-07	651.8899	5.799E+09	3.2227	7846875.	0.000
240.00	-1.494E-06	-24.9463	-9.9802	1.487E-07	651.6646	5.799E+09	1.9545	7846875.	0.000
246.00	-6.797E-07	-49.7536	-1.4502	1.101E-07	651.7880	5.799E+09	0.8889	7846875.	0.000
252.00	-1.737E-07	-42.5212	1.8981	6.232E-08	651.7520	5.799E+09	0.2272	7846875.	0.000

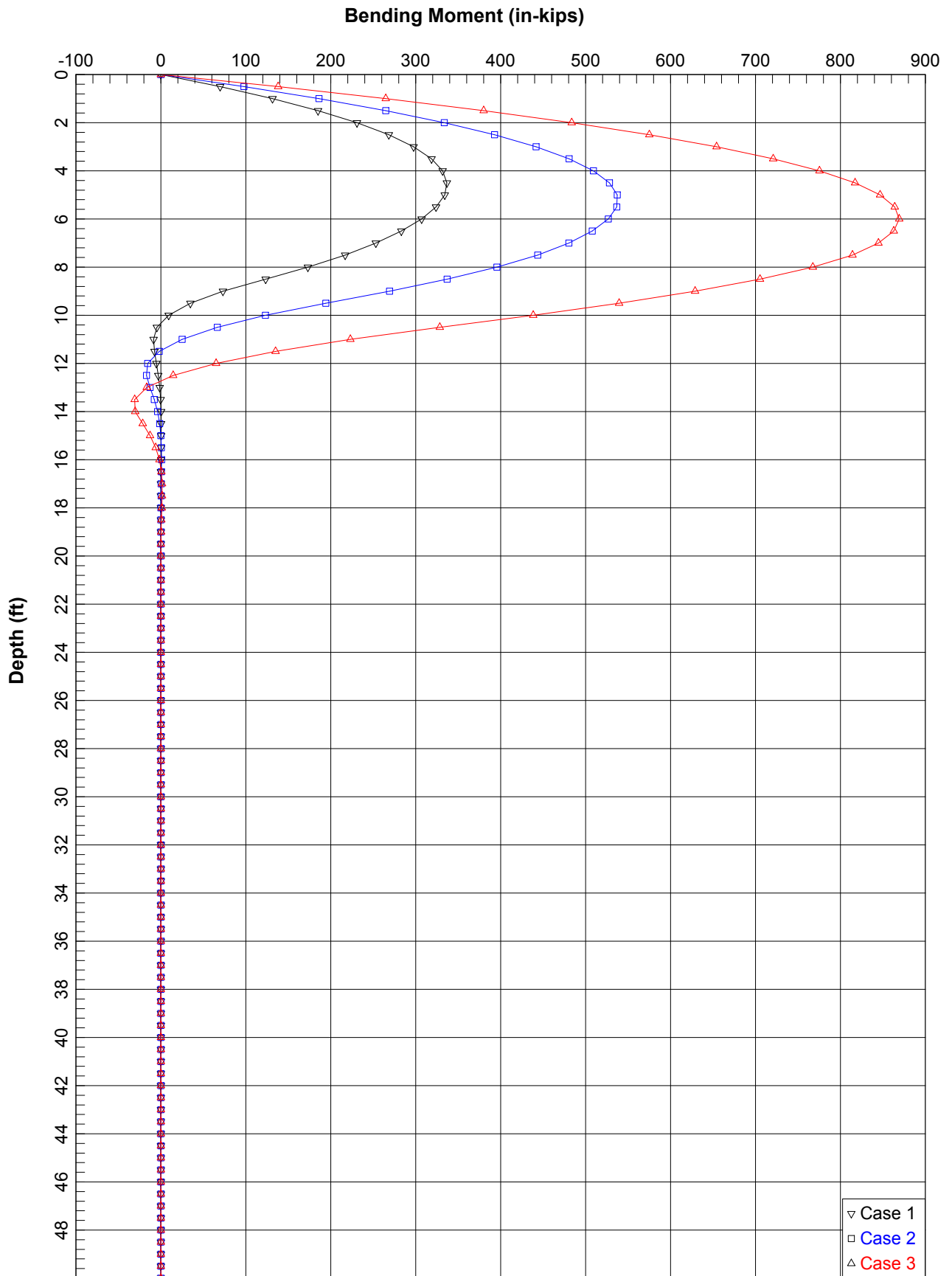
				Abut	SL_long_Ave P				
258.000	6.820E-08	-27.0745	2.4055	2.632E-11	651.6753	7.99E+09	-0.0581	5110210.0	0.000
264.000	1.421E-07	-13.6970	1.8608	5.222E-09	651.6087	5.799E+09	-0.1235	5215498.0	0.000
270.000	1.309E-07	-4.7536	1.1422	-4.324E-09	651.5642	5.799E+09	-0.1161	5320788.0	0.000
276.000	9.017E-08	0.0159	0.5494	-6.775E-09	651.5406	5.799E+09	-0.0815	5426079.0	0.000
282.000	4.957E-08	1.8497	0.1677	-5.810E-09	651.5497	5.799E+09	-0.0467	5531372.0	0.000
288.000	2.045E-08	2.0370	-0.0271	-3.799E-09	651.5507	5.799E+09	-0.0192	5636667.0	0.000
294.000	3.983E-09	1.5309	-0.0961	-1.953E-09	651.5482	5.799E+09	-0.003811	5741964.0	0.000
300.000	-2.982E-09	0.8864	-0.0959	7.022E-10	651.5450	5.799E+09	-0.003900	7846875.0	0.000
306.000	-4.444E-09	0.3816	-0.0667	4.616E-11	651.5424	5.799E+09	0.005812	7846875.0	0.000
312.000	-3.536E-09	0.0857	-0.0354	1.956E-10	651.5410	5.799E+09	0.004625	7846875.0	0.000
318.000	-2.979E-09	-0.0438	-0.0133	2.172E-10	651.5408	5.799E+09	0.002742	7846875.0	0.000
324.000	-9.291E-10	-0.0746	-0.001456	1.560E-10	651.5409	5.799E+09	0.001215	7846875.0	0.000
330.000	-2.248E-10	-0.0615	0.003071	8.556E-11	651.5409	7.99E+09	0.000294	7846875.0	0.000
336.000	9.754E-11	-0.0379	0.003637	3.413E-11	651.5407	5.799E+09	-0.001005	6479075.0	0.000
342.000	1.848E-10	-0.0180	0.002713	5.249E-12	651.5406	5.799E+09	-0.000203	6584381.0	0.000
348.000	1.605E-10	-0.005319	0.001568	-6.790E-12	651.5406	5.799E+09	-0.000179	6689568.0	0.000
354.000	1.033E-10	0.000874	0.000680	-9.090E-12	651.5406	5.799E+09	-0.000117	6794996.0	0.000
360.000	5.144E-11	0.002855	0.000152	-7.161E-12	651.5406	5.799E+09	-5.916E-05	6900305.0	0.000
366.000	1.734E-11	0.002704	-8.662E-05	-4.285E-12	651.5406	5.799E+09	-2.025E-05	7005615.0	0.000
372.000	0.000	0.001822	-0.000147	-1.943E-12	651.5406	5.799E+09	-3.399E-08	7110925.0	0.000
378.000	-5.970E-12	0.000938	-0.000124	0.000	651.5406	5.799E+09	7.808E-06	7846875.0	0.000
384.000	-6.147E-12	0.000334	-7.660E-05	0.000	651.5405	5.799E+09	8.040E-06	7846875.0	0.000
390.000	-4.254E-12	1.839E-05	-3.579E-05	0.000	651.5405	5.799E+09	5.563E-06	7846875.0	0.000
396.000	-2.246E-12	9.648E-05	1.029E-05	0.000	651.5405	5.799E+09	2.937E-06	7846875.0	0.000
402.000	0.000	-0.000106	1.804E-06	0.000	651.5405	5.799E+09	1.095E-06	7846875.0	0.000
408.000	0.000	-7.512E-05	5.415E-06	0.000	651.5405	5.799E+09	1.090E-07	7846875.0	0.000
414.000	0.000	-4.070E-05	4.942E-06	0.000	651.5405	5.799E+09	-2.666E-07	7846875.0	0.000
420.000	0.000	-1.585E-05	3.207E-06	0.000	651.5405	5.799E+09	-3.118E-07	7846875.0	0.000
426.000	0.000	-2.213E-06	1.587E-06	0.000	651.5405	5.799E+09	-2.283E-07	7846875.0	0.000
432.000	0.000	3.209E-06	5.217E-07	0.000	651.5405	5.799E+09	-1.268E-07	7846875.0	0.000
438.000	0.000	4.065E-06	-1.276E-08	0.000	651.5405	5.799E+09	-5.135E-08	7846875.0	0.000
444.000	0.000	3.068E-06	-1.936E-07						

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Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	131000.	0.25000000	336650.	12400.	-0.00441935
2	4	y = 0.5000	M = 0.000	131000.	0.50000000	537158.	16889.	-0.00788410
3	4	y = 1.0000	M = 0.000	131000.	1.00000000	869237.	23099.	-0.01411562

The analysis ended normally.





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Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 5L
 Name of input data file: Abut 5L_long_Ave P.lpd
 Name of output report file: Abut 5L_long_Ave P.lpo
 Name of plot output file: Abut 5L_long_Ave P.lpp
 Name of runtime message file: Abut 5L_long_Ave P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 10:07:39

Problem Title

Project Name: Palo Comado OC Bridge Widened

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

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Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 16.0000000 in
 Bottom Width = 16.0000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 33.700 degrees
 = 0.588 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 5 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 7.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 7.00000 ft
 Distance from top of pile to bottom of layer = 12.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 12.00000 ft
 Distance from top of pile to bottom of layer = 17.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 17.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Rock Emass	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Uniaxial Elastic Mod.	ROD % or GSI
Num.	Epsilon 50	psi	ft	pcf	psf	deg.	psi	
1	0.00700	Stiff Clay w/o Free Water	-2.000	120.000	4000.000	--	--	--
2	0.00700	Stiff Clay w/o Free Water	0.10000	120.000	4000.000	--	--	--
3	0.00700	Stiff Clay w/o Free Water	7.000	120.000	3500.000	--	--	--
4	0.00700	Stiff Clay w/o Free Water	12.000	125.000	4000.000	--	--	--
5	0.00500	Stiff Clay w/o Free Water	17.000	125.000	4500.000	--	--	--
	0.00500		80.000	125.000	4500.000	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X Ft	p-mult	y-mult
1	0.000	0.9300	1.0000
2	50.000	0.9300	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

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Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4	y = 0.25000 in	M = 0.0000 in-lbs	131000.	False
2	4	y = 0.50000 in	M = 0.0000 in-lbs	131000.	False
3	4	y = 1.00000 in	M = 0.0000 in-lbs	131000.	False

V = perpendicular shear force applied to pile head

M = bending moment applied to pile head

y = lateral deflection relative to pile axis

S = pile slope relative to original pile batter angle

R = rotational stiffness applied to pile head

Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection

For Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.250000 inches

Moment at pile head = 0.000 in-lbs

Axial load at pile head = 131000.000 lbs

Depth X inches	Deflect. y inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil Res. p lb/in	Soil Spr. Es ^h lb/inch	Distrib. Lat. Load lb/inch
0.00	0.2500	0.000	12400.	-0.004419	651.5405	5.799E+09	-459.1736	5510.0831	0.000
6.00	0.2235	69606.	10373.	-0.004383	997.7335	5.799E+09	-216.2991	5807.1060	0.000
12.00	0.1974	131369.	9066.1548	-0.004279	1304.9166	5.799E+09	-219.3838	6668.2028	0.000
18.00	0.1721	185127.	7743.9075	-0.004116	1572.2878	5.799E+09	-221.3653	7716.1407	0.000
24.00	0.1480	230766.	6413.2521	-0.003900	1799.2749	5.799E+09	-222.1865	9006.7978	0.000
30.00	0.1253	268218.	5081.3305	-0.003642	1985.5462	5.799E+09	-221.7873	10618.	0.000
36.00	0.1043	297467.	3755.6608	-0.003350	2131.0217	5.799E+09	-220.1026	12661.	0.000
42.00	0.0851	318551.	2444.1709	-0.003031	2235.8847	5.799E+09	-217.0607	15298.	0.000
48.00	0.0679	331562.	1155.2453	-0.002695	2300.5946	5.799E+09	-212.5812	18775.	0.000
54.00	0.0528	336650.	-102.2094	-0.002349	2325.9008	5.799E+09	-206.5704	23476.	0.000
60.00	0.0397	334028.	-1318.6685	-0.002002	2312.8590	5.799E+09	-198.9160	30027.	0.000
66.00	0.0288	323973.	-2483.8446	-0.001661	2262.8503	5.799E+09	-189.4761	39511.	0.000
72.00	0.0198	306534.	-3586.4554	-0.001335	2177.6055	5.799E+09	-178.0609	53930.	0.000
78.00	0.0128	283034.	-4613.8218	-0.001030	2059.2380	5.799E+09	-164.3946	77350.	0.000
84.00	0.007451	253087.	-5614.2733	-0.000753	1910.2908	5.799E+09	-169.0893	136160.	0.000
90.00	0.003721	216846.	-6732.7906	-0.000509	1730.0445	5.799E+09	-203.7498	328508.	0.000
96.00	0.001338	173094.	-7835.4289	-0.000308	1512.4399	5.799E+09	-163.7963	734548.	0.000
102.00	0.0013E-05	123305.	-8359.1587	-0.000154	1264.8075	5.799E+09	-10.7803	2220215.	0.000
108.00	-0.000514	73027.	-7384.3337	-5.277E-05	1014.7461	5.799E+09	335.7220	3917806.	0.000
114.00	-0.000604	34776.	-5327.3676	3.008E-06	824.5001	5.799E+09	349.9334	3475861.	0.000
120.00	-0.000478	9093.6644	-3287.0764	2.570E-05	696.7687	5.799E+09	330.1637	4143826.	0.000
126.00	-0.000296	-4709.7492	-1467.3071	2.797E-05	674.9649	5.799E+09	276.4261	5610741.	0.000
132.00	-0.000142	-8557.9926	-238.5685	2.111E-05	694.1045	5.799E+09	133.1534	5610741.	0.000
138.00	-4.231E-05	-7605.7530	279.5865	1.275E-05	689.3685	5.799E+09	39.5649	5610741.	0.000
144.00	1.085E-05	-5222.9902	383.5555	6.108E-06	677.5176	5.799E+09	-4.9027	2791028.	0.000
150.00	3.099E-05	-3012.6896	321.4874	1.847E-06	666.5244	5.799E+09	-15.7808	3055509.	0.000
156.00	3.272E-05	-1368.0457	222.7376	-4.191E-07	658.3446	5.799E+09	-17.1358	3142256.	0.000
162.00	2.596E-05	-339.1789	129.4197	-1.302E-06	653.2755	5.799E+09	-13.9702	3229007.	0.000
168.00	1.709E-05	187.0377	59.1732	-1.381E-06	652.4708	5.799E+09	-9.4453	3315763.	0.000
174.00	9.386E-06	373.0711	14.8697	-1.091E-06	653.3961	5.799E+09	-5.3225	3402523.	0.000
180.00	3.996E-06	367.1897	-8.0695	-7.083E-07	653.3668	5.799E+09	-2.3239	3489286.	0.000
186.00	8.859E-07	273.8503	-16.6252	-3.749E-07	652.9200	5.799E+09	-0.5280	3576052.	0.000
192.00	-5.023E-07	168.2768	-16.5989	-1.443E-07	652.3775	5.799E+09	0.5368	6412276.	0.000
198.00	-8.457E-07	78.3907	-12.2769	-1.669E-08	651.9304	5.799E+09	0.9039	6412276.	0.000
204.00	-7.025E-07	20.9800	-7.0781	3.472E-08	651.6449	5.799E+09	0.8291	7080727.	0.000
210.00	-4.291E-07	-6.6008	-2.9073	4.214E-08	651.5734	5.799E+09	0.5612	7846875.	0.000
216.00	-1.966E-07	-13.9743	-0.4525	3.152E-08	651.6101	5.799E+09	0.2571	7846875.	0.000
222.00	-5.089E-08	-12.0799	0.5186	1.804E-08	651.6006	5.799E+09	0.0666	7846875.	0.000
228.00	1.983E-08	-7.7798	0.6723	7.762E-09	651.5792	5.799E+09	-0.0153	4635121.	0.000
234.00	4.226E-08	-4.0249	0.5261	1.655E-09	651.6506	5.799E+09	-0.0334	4740399.	0.000

Abut	SL Long Ave P	5.770	5.799E-09	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
240.000	3.969E-08	-1.4687	0.3298	-1.187E-10	651.5405	5.799E-09	-0.0321	4845679	0.000
246.000	2.801E-08	-0.0652	0.1643	-1.981E-09	651.5409	5.799E-09	-0.0231	4905962	0.000
252.000	1.592E-08	0.5062	0.0547	-1.753E-09	651.5431	5.799E-09	-0.0134	5056247	0.000
258.000	6.977E-09	0.5942	-0.003538	-1.183E-09	651.5435	5.799E-09	-0.006002	5161535	0.000
264.000	1.721E-09	0.4656	-0.0261	-6.352E-10	651.5429	5.799E-09	-0.001510	5266824	0.000
270.000	-6.453E-10	0.2823	-0.0281	-2.483E-10	651.5420	5.799E-09	0.000844	7846875	0.000
276.000	-1.259E-09	0.1291	-0.0206	-3.545E-11	651.5412	5.799E-09	0.001646	7846875	0.000
282.000	-1.071E-09	0.0351	-0.0115	-4.949E-11	651.5407	5.799E-09	0.001400	7846875	0.000
288.000	-6.648E-10	-0.008555	-0.004655	6.322E-11	651.5406	5.799E-09	0.000869	7846875	0.000
294.000	-3.121E-10	-0.0209	-0.000823	4.799E-11	651.5407	5.799E-09	0.000408	7846875	0.000
300.000	-8.897E-11	-0.0185	0.000751	2.761E-11	651.5406	5.799E-09	0.000116	7846875	0.000
306.000	1.925E-11	-0.0119	0.001042	1.187E-11	651.5406	5.799E-09	-1.926E-05	6003897	0.000
312.000	5.348E-11	-0.006017	0.000821	2.892E-12	651.5406	5.799E-09	-5.445E-05	6109199	0.000
318.000	5.036E-11	-0.002071	0.000501	-1.592E-12	651.5406	5.799E-09	-5.216E-05	6214502	0.000
324.000	3.438E-11	-1.481E-06	0.000236	-2.664E-12	651.5405	5.799E-09	-3.621E-05	6319806	0.000
330.000	1.839E-11	0.000764	6.822E-05	-2.269E-12	651.5406	5.799E-09	-1.969E-05	6425112	0.000
336.000	7.148E-12	0.000821	-1.420E-05	0.000000	651.5406	5.799E-09	-7.780E-06	6530418	0.000
342.000	1.001E-12	0.000596	-4.086E-05	0.000000	651.5406	5.799E-09	-1.107E-06	6635725	0.000
348.000	-1.444E-12	0.000332	-3.851E-05	0.000000	651.5405	5.799E-09	1.889E-06	7846875	0.000
354.000	-1.831E-12	0.000135	-2.566E-05	0.000000	651.5405	5.799E-09	2.395E-06	7846875	0.000
360.000	-1.382E-12	2.359E-05	-1.306E-05	0.000000	651.5405	5.799E-09	1.808E-06	7846875	0.000
366.000	0.000	-2.228E-05	-4.542E-06	0.000000	651.5405	5.799E-09	1.030E-06	7846875	0.000
372.000	0.000	-3.106E-05	-1.544E-07	0.000000	651.5405	5.799E-09	4.327E-07	7846875	0.000
378.000	0.000	-4.423E-05	1.407E-06	0.000000	651.5405	5.799E-09	8.769E-08	7846875	0.000
384.000	0.000	-1.422E-05	1.499E-06	0.000000	651.5405	5.799E-09	-5.695E-08	7372899	0.000
390.000	0.000	-6.518E-06	1.061E-06	0.000000	651.5405	5.799E-09	-8.903E-08	7478212	0.000
400.000	0.000	6.257E-07	2.235E-07	0.000000	651.5405	5.799E-09	-1.543E-09	7846875	0.000
406.000	0.000	6.581E-07	2.235E-07	0.000000	651.5405	5.799E-09	-4.441E-08	7888841	0.000
412.000	0.000	1.196E-06	2.914E-08	0.000000	651.5405	5.799E-09	-2.037E-08	7794156	0.000
418.000	0.000	1.005E-06	-4.817E-08	0.000000	651.5405	5.799E-09	-5.400E-09	7846875	0.000
424.000	0.000	6.198E-07	-5.974E-08	0.000000	651.5405	5.799E-09	1.543E-09	7846875	0.000
430.000	0.000	2.893E-07	-4.475E-08	0.000000	651.5405	5.799E-09	3.455E-09	7846875	0.000
436.000	0.000	8.296E-08	-2.533E-08	0.000000	651.5405	5.799E-09	3.018E-09	7846875	0.000
442.000	0.000	-1.481E-08	-1.056E-08	0.000000	651.5405	5.799E-09	1.907E-09	7846875	0.000
448.000	0.000	-4.392E-08	-2.088E-09	0.000000	651.5405	5.799E-09	9.160E-10	7846875	0.000
454.000	0.000	-4.003E-08	1.506E-09	0.000000	651.5405	5.799E-09	2.819E-10	7846875	0.000
460.000	0.000	-2.595E-08	2.270E-09	0.000000	651.5405	5.799E-09	-2.708E-11	7846875	0.000
466.000	0.000	-1.283E-08	1.813E-09	0.000000	651.5405	5.799E-09	-1.254E-10	7846875	0.000
472.000	0.000	-4.209E-09	0.078E-09	0.000000	651.5405	5.799E-09	-1.195E-10	7846875	0.000
478.000	0.000	1.119E-10	4.810E-10	0.000000	651.5405	5.799E-09	0.000000	7846875	0.000
484.000	0.000	1.571E-09	1.215E-10	0.000000	651.5405	5.799E-09	-4.036E-11	7846875	0.000
490.000	0.000	-1.576E-09	-4.152E-11	0.000000	651.5405	5.799E-09	-1.399E-11	7846875	0.000
496.000	0.000	0.000	0.000	0.000000	651.5405	5.799E-09	0.000000	7846875	0.000
502.000	0.000	5.616E-10	-7.272E-11	0.000000	651.5405	5.799E-09	4.413E-12	7846875	0.000
508.000	0.000	2.048E-10	-4.545E-11	0.000000	651.5405	5.799E-09	4.680E-12	7846875	0.000
514.000	0.000	1.617E-11	-2.156E-11	0.000000	651.5405	5.799E-09	3.284E-12	7846875	0.000
520.000	0.000	-5.422E-11	-6.437E-12	0.000000	651.5405	5.799E-09	1.757E-12	7846875	0.000
526.000	0.000	-6.133E-11	0.000000	0.000000	651.5405	5.799E-09	0.000000	7846875	0.000
532.000	0.000	-4.429E-11	3.092E-12	0.000000	651.5405	5.799E-09	0.000000	7846875	0.000
538.000	0.000	-2.431E-11	2.887E-12	0.000000	651.5405	5.799E-09	0.000000	7846875	0.000
544.000	0.000	-9.665E-12	1.898E-12	0.000000	651.5405	5.799E-09	0.000000	7846875	0.000
550.000	0.000	-1.526E-12	0.000000	0.000000	651.5405	5.799E-09	0.000000	7846875	0.000
556.000	0.000	1.774E-12	0.000000	0.000000	651.5405	5.799E-09	0.000000	7846875	0.000
562.000	0.000	2.350E-12	0.000000	0.000000	651.5405	5.799E-09	0.000000	7846875	0.000
568.000	0.000	1.802E-12	0.000000	0.000000	651.5405	5.799E-09	0.000000	7846875	0.000
574.000	0.000	1.041E-12	0.000000	0.000000	651.5405	5.799E-09	0.000000	7846875	0.000
580.000	0.000	0.000000	0.000000	0.000000	651.5405	5.799E-09	0.000000	7846875	0.000
586.000	0.000	0.000000	0.000000	0.000000	651.5405	5.799E-09	0.000000	7846875	0.000
592.000	0.000	0.000000	0.000000	0.000000	651.5405	5.799E-09	0.000000	7846875	0.000
598.000	0.000	0.000000	0.000000	0.000000	651.5405	5.799E-09	0.000000	7846875	0.000
604.000	0.000	0.000000	0.000000	0.000000	651.5405	5.799E-09	0.000000	3923438	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Pile-head deflection	=	0.2500000	inches
Computed slope at pile head	=	-0.0044193	rad
Maximum bending moment	=	336650.	inch-lbs
Maximum shear force	=	12400.	lbs
Depth of maximum bending moment	=	54.0000000	inches below pile head
Depth of maximum shear force	=	0.0000000	inches below pile head
Number of iterations	=	15	
Number of zero deflection points	=	14	

 Computed Values of Pile Loading and Deflection
 For Lateral Loading For Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)	=	0.500000	inches
Displacement of pile head	=	0.000000	inches
Moment at pile head	=	0.000000	in-lbs
Axial load at pile head	=	1310000	lbs

Depth	Deflect.	Bending	Shear	Slope	Abut	SL Long Ave P	Bending	Soil Res.	Soil Spr.	Distri b.
inches	inches	moment	Force	radi ans	Stress	psi *	Stiffness	p	Es/h	Lat. Load
		in-lbs	lbs				lb-in ²	lb/in	lb/inch	lb/inch
0.00	0.5000	0.0000	16889.	-0.007884	651.5405	5.799E-09	-56.0525	3276.3150	0.000	0.000
6.00	0.4527	97700.	14476.	-0.007834	1137.4582	5.799E-09	-258.0446	3420.1086	0.000	0.000
12.00	0.4060	186030.	12914.	-0.007687	1576.7780	5.799E-09	-262.7233	3882.6359	0.000	0.000
18.00	0.3605	264751.	11327.	-0.007454	1968.3048	5.799E-09	-266.2911	4432.5931	0.000	0.000
24.00	0.3166	336571.	9722.0096	-0.007144	2311.0815	5.799E-09	-268.6921	5092.8089	0.000	0.000
30.00	0.2747	392646.	8106.3303	-0.006768	2604.3994	5.799E-09	-269.8676	5893.8754	0.000	0.000
36.00	0.2353	441586.	6487.4619	-0.006337	2847.8094	5.799E-09	-269.7552	6877.5147	0.000	0.000
42.00	0.1987	480456.	4873.3342	-0.005860	3041.1337	5.799E-09	-268.2874	8101.7709	0.000	0.000
48.00	0.1650	509277.	3272.3021	-0.005347	3184.4779	5.799E-09	-265.8900	9649.2527	0.000	0.000
54.00	0.1345	528130.	1693.1927	-0.004811	3278.2441	5.799E-09	-260.9798	11641.000	0.000	0.000
60.00	0.1073	537158.	145.3701	-0.004260	3323.1458	5.799E-09	-254.9611	14258.000	0.000	0.000
66.00	0.0834	536571.	-1361.1743	-0.003704	3320.2241	5.799E-09	-247.2204	17785.000	0.000	0.000
72.00	0.0628	526647.	-2815.6929	-0.003154	3270.8674	5.799E-09	-237.6192	22687.000	0.000	0.000
78.00	0.0456	507741.	-4206.4926	-0.002619	3176.8348	5.799E-09	-225.9807	29764.000	0.000	0.000
84.00	0.0314	480286.	-5611.1646	-0.002108	3040.2867	5.799E-09	-214.2433	46264.000	0.000	0.000
90.00	0.0203	443720.	-7271.1360	-0.001630	2858.4233	5.799E-09	-211.0805	92122.000	0.000	0.000
96.00	0.0119	395594.	-9051.0326	-0.001195	2619.0643	5.799E-09	-282.2183	142770.000	0.000	0.000
102.00	0.005916	336987.	-10635.	-0.000816	2327.5752	5.799E-09	-245.7187	249222.000	0.000	0.000
108.00	0.002063	269259.	-11959.	-0.000503	1990.7272	5.799E-09	-195.5618	568746.000	0.000	0.000
114.00	-0.000118	194273.	-12215.	-0.000263	1617.7748	5.799E-09	110.1812	5610741.000	0.000	0.000
120.00	-0.001093	123095.	-10668.	-9.878E-05	1263.7645	5.799E-09	405.3649	2226219.000	0.000	0.000
126.00	-0.001303	66410.	-8180.6650	-7.377E-07	981.8365	5.799E-09	423.8096	1951252.000	0.000	0.000
132.00	-0.001327	0.000000	-5205.7444	4.6						

Abut	SL	long	Ave	P	799E+09	6.542E-12	7846875	0.000
522.000	0.000	7.380E-11	-4.632E-11	0.000	651.5405	5.799E+09	6.542E-12	7846875
528.000	0.000	-8.664E-11	-1.566E-11	0.000	651.5405	5.799E+09	3.678E-12	7846875
534.000	0.000	-1.146E-10	0.000	0.000	651.5405	5.799E+09	1.518E-12	7846875
540.000	0.000	-8.782E-11	5.345E-12	0.000	651.5405	5.799E+09	0.000	7846875
546.000	0.000	-5.063E-11	5.519E-12	0.000	651.5405	5.799E+09	0.000	7846875
552.000	0.000	-2.166E-11	3.824E-12	0.000	651.5405	5.799E+09	0.000	7846875
558.000	0.000	-4.751E-12	2.021E-12	0.000	651.5405	5.799E+09	0.000	7846875
564.000	0.000	2.606E-12	0.000	0.000	651.5405	5.799E+09	0.000	7846875
570.000	0.000	4.310E-12	0.000	0.000	651.5405	5.799E+09	0.000	7846875
576.000	0.000	3.507E-12	0.000	0.000	651.5405	5.799E+09	0.000	7846875
582.000	0.000	2.062E-12	0.000	0.000	651.5405	5.799E+09	0.000	7846875
588.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	7846875
594.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	7846875
600.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	3923438

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Pile-head deflection	=	0.5000000	inches
Computed slope at pile head	=	-0.0078841	radians
Maximum bending moment	=	537158	inch-lbs
Maximum shear force	=	6884	lbs
Depth of maximum bending moment	=	60.0000000	inches below pile head
Depth of maximum shear force	=	0.0000000	inches below pile head
Number of iterations	=	14	
Number of zero deflection points	=	13	

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 3

Pile-head conditions are Diplacement and Moment (Loading Type 4)	=		
Displacement of pile head	=	1.000000	inches
Moment at pile head	=		in-lbs
Axial load at pile head	=	131000.000	lbs

Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil Res.	Soil Spr.	Distrib.
x	y	Moment	Force		Stress	Stiffness	p	E'sh	Lat. Load
inches	inches	in-lbs	lbs	radians	psi	lb/in ²	lb/in	lb/inch	lb/inch
0.00	1.0000	0.000	23099	-0.0141	651.5405	5.799E+09	-649.3695	1948.1086	0.000
6.00	0.9153	138002	20228	-0.0140	1337.9049	5.799E+09	-307.7048	2017.0610	0.000
12.00	0.8315	264814	18362	-0.0138	1968.6168	5.799E+09	-314.2882	2267.9478	0.000
18.00	0.7493	380096	16460	-0.0135	2541.9844	5.799E+09	-319.7441	2560.4228	0.000
24.00	0.6694	483559	14529	-0.0131	3056.5645	5.799E+09	-324.0171	2904.0585	0.000
30.00	0.5926	574963	12575	-0.0125	3511.1736	5.799E+09	-327.0496	3311.2646	0.000
36.00	0.5194	654127	10608	-0.0119	3904.8990	5.799E+09	-328.7807	3798.3652	0.000
42.00	0.4502	720922	8634.2012	-0.0112	4237.1105	5.799E+09	-329.1459	4387.1440	0.000
48.00	0.3854	775281	6662.5384	-0.0104	4507.4725	5.799E+09	-328.0751	5107.2082	0.000
54.00	0.3255	817199	4701.8381	-0.009562	4715.9569	5.799E+09	-325.4917	5999.5798	0.000
60.00	0.2707	846735	2761.4312	-0.008702	4862.8566	5.799E+09	-321.3106	7122.3864	0.000
66.00	0.2211	864015	851.1947	-0.007817	4948.8008	5.799E+09	-315.4349	8560.1439	0.000
72.00	0.1769	869237	-1018.3698	-0.006920	4974.7117	5.799E+09	-307.7532	10439	0.000
78.00	0.1381	862673	-2836.0308	-0.006024	4942.1236	5.799E+09	-298.1338	12957	0.000
84.00	0.1046	844674	-4711.9487	-0.005140	4852.6052	5.799E+09	-327.1721	18768	0.000
90.00	0.0764	814210	-6993.5524	-0.004282	4701.0902	5.799E+09	-433.3624	34046	0.000
96.00	0.0532	767483	-9525.4117	-0.003464	4468.6885	5.799E+09	-410.5907	46301	0.000
102.00	0.0348	705351	-11905	-0.002702	4159.6664	5.799E+09	-382.4576	65929	0.000
108.00	0.0208	628876	-14095	-0.002012	3779.3123	5.799E+09	-347.8193	100406	0.000
114.00	0.0107	539368	-16052	-0.001407	3334.1376	5.799E+09	-304.2539	171132	0.000
120.00	0.003898	438469	-17697	-0.000901	2832.3047	5.799E+09	-244.3319	376044	0.000
126.00	-0.00148	328417	-18015	-0.000505	2284.9507	5.799E+09	-138.6162	5610741	0.000
132.00	-0.002156	223988	-16155	-0.000219	1761.0875	5.799E+09	481.1168	1338918	0.000
138.00	-0.002779	134897	-13174	-3.400E-05	1322.4655	5.799E+09	512.7367	1107125	0.000
144.00	-0.002564	65056	-10021	6.945E-05	975.1029	5.799E+09	538.2701	1259600	0.000
150.00	-0.001945	14540	-6799.2696	0.000111	723.8541	5.799E+09	535.5504	1651768	0.000
156.00	-0.001236	-16709	-3759.3829	0.000110	734.6446	5.799E+09	477.7452	2318266	0.000
162.00	-0.000631	-30745	-1116.4760	8.495E-05	804.4548	5.799E+09	403.2238	3832268	0.000
168.00	-0.000217	-30240	788.9981	5.340E-05	801.9436	5.799E+09	231.9343	6412276	0.000
174.00	9.521E-06	-21361	1469.4917	2.671E-05	757.7824	5.799E+09	-5.1031	3215874	0.000
180.00	0.000103	-12648	1023.3489	9.110E-05	714.6846	5.799E+09	-56.9405	3302622	0.000
186.00	0.000119	-5975.1885	911.1342	-5.248E-07	681.2587	5.799E+09	-67.1351	3389375	0.000
192.00	9.715E-05	-1713.9719	540.8797	-4.503E-06	660.0651	5.799E+09	-56.2831	3476132	0.000
198.00	6.481E-05	522.4462	256.5753	-5.119E-06	654.1390	5.799E+09	-38.4850	3562892	0.000
204.00	3.572E-05	1372.9791	73.8770	-4.139E-06	658.3582	5.799E+09	73.9944	3765302	0.000
210.00	1.514E-05	1415.4766	-25.6846	-2.696E-06	658.5806	5.799E+09	-10.7728	4267998	0.000
216.00	3.362E-06	1069.0022	-65.3538	-1.411E-06	656.8573	5.799E+09	-2.4503	4373264	0.000
222.00	-1.784E-06	633.4490	-65.7037	-5.300E-07	654.6911	5.799E+09	2.3336	7846875	0.000
228.00	-2.998E-06	281.3913	-46.9413	-5.665E-08	652.9401	5.799E+09	3.9205	7846875	0.000
234.00	-2.464E-06	70.2431	-25.5117	1.253E-07	651.8899	5.799E+09	3.2227	7846875	0.000
240.00	-1.494E-06	-24.9463	-9.9802	1.487E-07	651.6646	5.799E+09	1.9545	7846875	0.000
246.00	-6.797E-07	-49.7536	-1.4502	1.101E-07	651.7880	5.799E+09	0.8889	7846875	0.000
252.00	-1.737E-07	-42.5212	1.8981	6.232E-08	651.7520	5.799E+09	0.2272	7846875	0.000

Abut	SL	long	Ave	P	799E+09	-0.0581	5110210	0.000
258.000	6.820E-08	-27.0745	2.4055	2.632E-08	651.6752	5.799E+09	-0.0581	5110210
264.000	1.421E-07	-13.6970	1.8608	5.222E-09	651.6087	5.799E+09	-0.1235	5215498
270.000	1.309E-07	-4.7536	1.1422	-4.324E-09	651.5642	5.799E+09	-0.1161	5350788
276.000	9.017E-08	0.0159	0.5494	-6.775E-09	651.5406	5.799E+09	-0.0815	5426079
282.000	4.957E-08	1.8497	0.1677	-5.810E-09	651.5497	5.799E+09	-0.0467	5531372
288.000	2.045E-08	2.0370	-0.0271	-3.799E-09	651.5507	5.799E+09	-0.0192	5636667
294.000	3.983E-09	1.5309	-0.0961	-1.953E-09	651.5482	5.799E+09	-0.003811	5741964
300.000	-2.982E-09	0.8864	-0.0959	-7.022E-10	651.5450	5.799E+09	-0.003900	7846875
306.000	-4.444E-09	0.3816	-0.0667	-4.616E-11	651.5424	5.799E+09	0.003812	7846875
312.000	-3.536E-09	0.0857	-0.0354	1.956E-10	651.5410	5.799E+09	0.004625	7846875
318.000	-2.977E-09	-0.0438	-0.0133	2.172E-10	651.5408	5.799E+09	0.002742	7846875
324.000	-9.291E-10	-0.0746	-0.001456	1.560E-10	651.5409	5.799E+09	0.001215	7846875
330.000	-2.248E-10	-0.0615	0.003071	8.556E-11	651.5409	5.799E+09	0.000294	7846875
336.000	9.754E-11	-0.0379	0.003637	3.413E-11	651.5407	5.799E+09	-0.000105	6479075
342.000	1.848E-10	-0.0180	0.002713	5.249E-12	651.5406	5.799E+09	-0.000203	6584381
348.000	1.605E-10	-0.005319	0.001568	-6.790E-12	651.5406	5.799E+09	-0.000179	6689688
354.000	1.033E-10	0.000874	0.000680	-9.090E-12	651.5406	5.799E+09	-0.000117	6794996
360.000	5.144E-11	0.002855	0.000152	-7.161E-12	651.5406	5.799E+09	-5.916E-05	6900305
366.000	1.734E-11	0.002704	-8.662E-05	-4.285E-12	651.5406	5.799E+09	-2.025E-05	7005615
372.000	0.000	0.001822	-0.000147	-1.943E-12	651.5406	5.799E+09	-3.399E-08	7110925
378.000	-5.970E-12	0.000938	-0.000124	0.000	651.5406	5.799E+09	-7.808E-06	7846875
384.000	-6.147E-12	0.000334	-7.660E-05	0.000	651.5405	5.799E+09	8.040E-06	7846875
390.000	-4.254E-12	1.839E-05	-3.579E-05	0.000	651.5405	5.799E+09	5.563E-06	7846875
396.000	-2.246E-12	9.648E-05	-1.029E-05	0.000	651.5405	5.799E+09	2.937E-06	7846875
402.000	0.000	-0.000106	1.804E-06	0.000	651.5405	5.799E+09	1.095E-06	7846875
408.000	0.000	-7.512E-05	5.415E-06	0.000	651.5405	5.799E+09	1.090E-07	7846875
414.000	0.000	-4.070E-05	4.942E-06	0.000	651.5405	5.799E+09	-2.666E-07	7846875
420.000	0.000	-1.585E-05	3.207E-06	0.000	651.5405	5.799E+09	-3.118E-07	7846875
426.000	0.000	-2.213E-06	1.587E-06	0.000	651.5405	5.799E+09	-2.283E-07	7846875
432.000	0.000	3.209E-06	5.217E-07	0.000	651.5405	5.799E+09	-1.268E-07	7846875
438.000	0.000	4.065E-06	-1.276E-08	0.000	651.5405	5.799E+09	-5.135E-08	7846875
444.000	0.000	3.068E-06	-1.936E-07	0.000	651.5405	5.799E+09	-8.925E-09	7846875
450.000	0.000	1.748E-06	-1.946E-07	0.000	651.5405	5.799E+09	8.592E-09	7846875
456.000	0.000	7.350E-07	-1.331E-07	0.				

Abut 5L_Long_Ave P

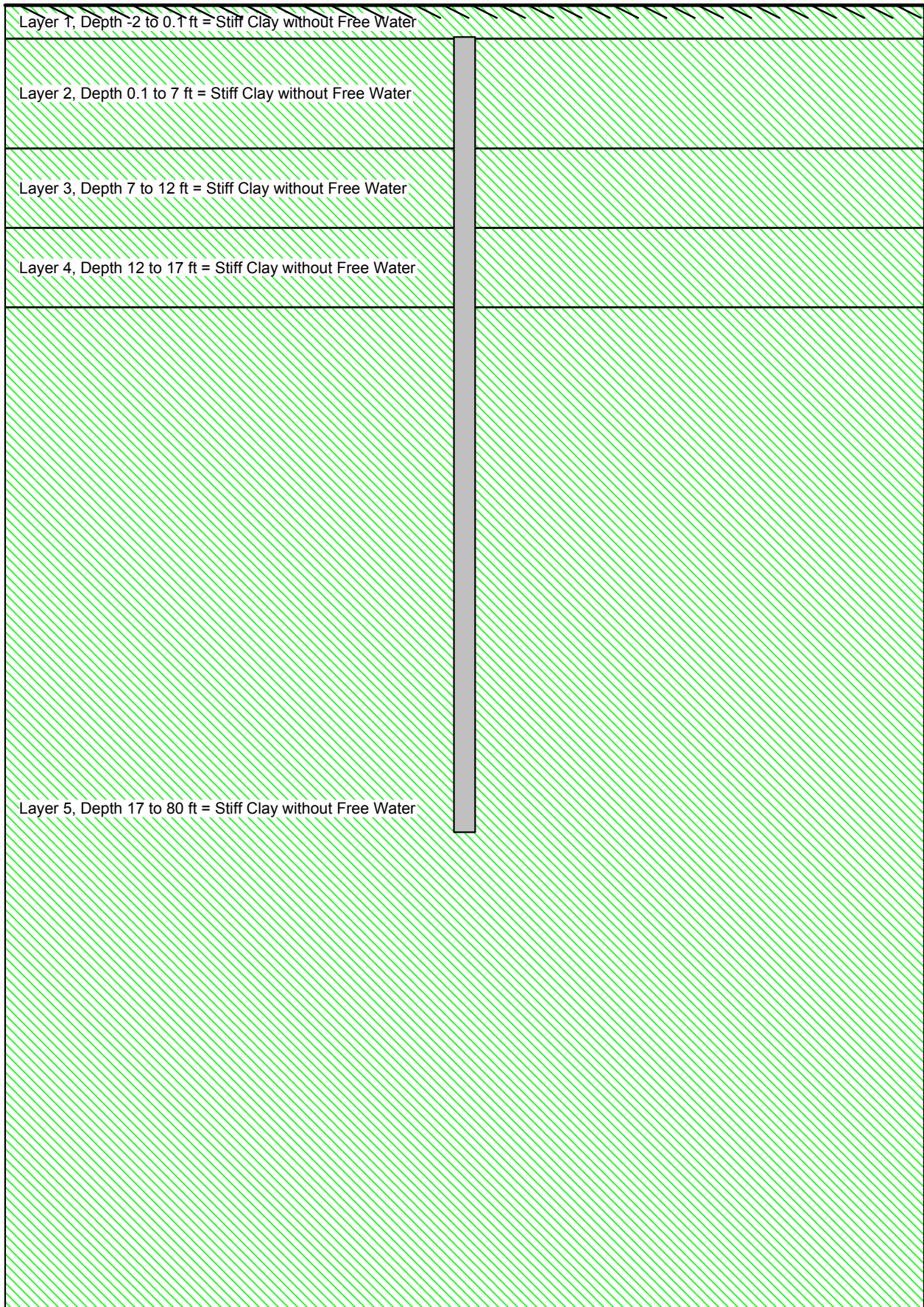
Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	131000.	0.25000000	336650.	12400.	-0.00441935
2	4	y = 0.5000	M = 0.000	131000.	0.50000000	537158.	16889.	-0.00788410
3	4	y = 1.0000	M = 0.000	131000.	1.00000000	869237.	23099.	-0.01411562

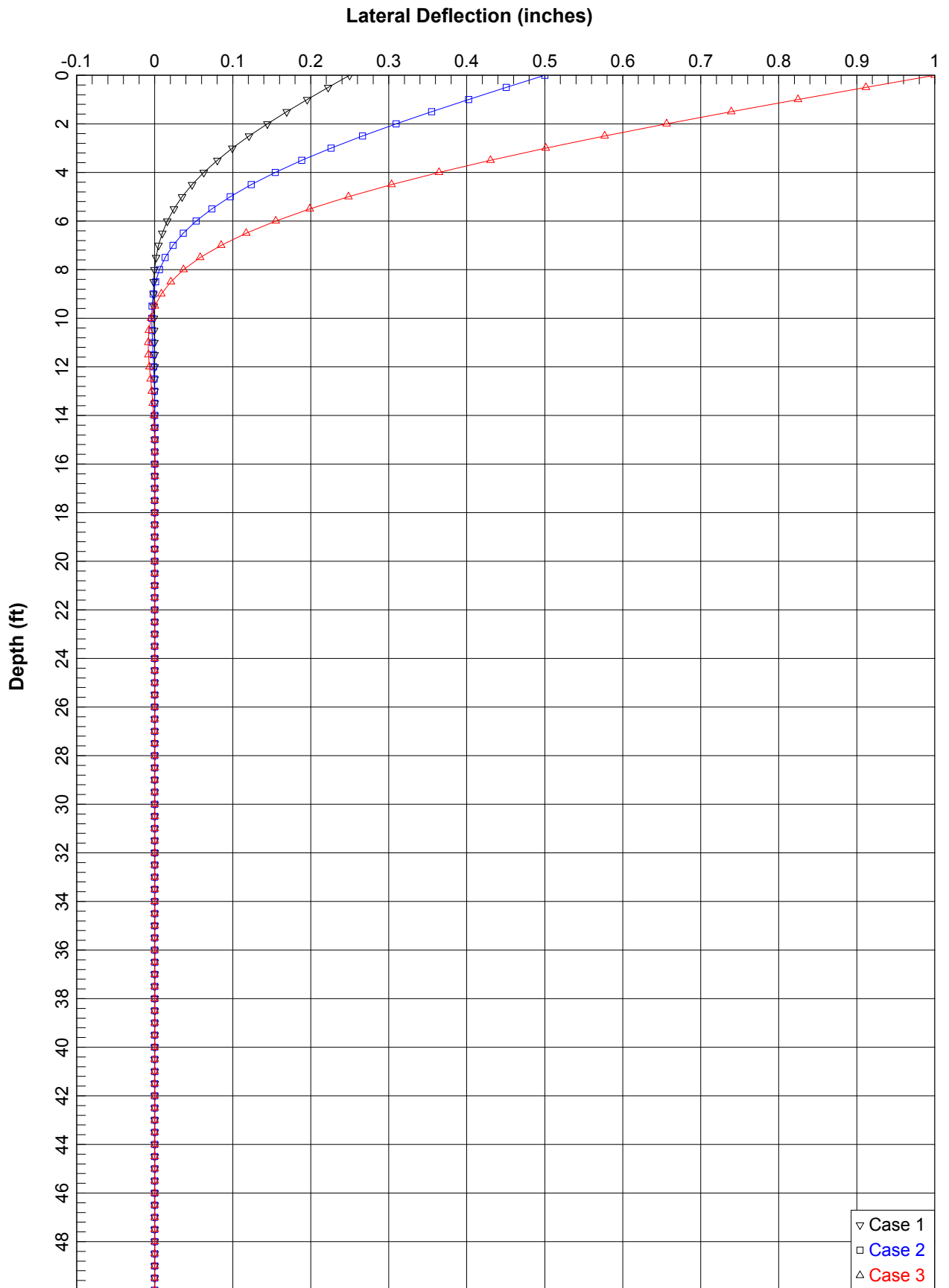
The analysis ended normally.

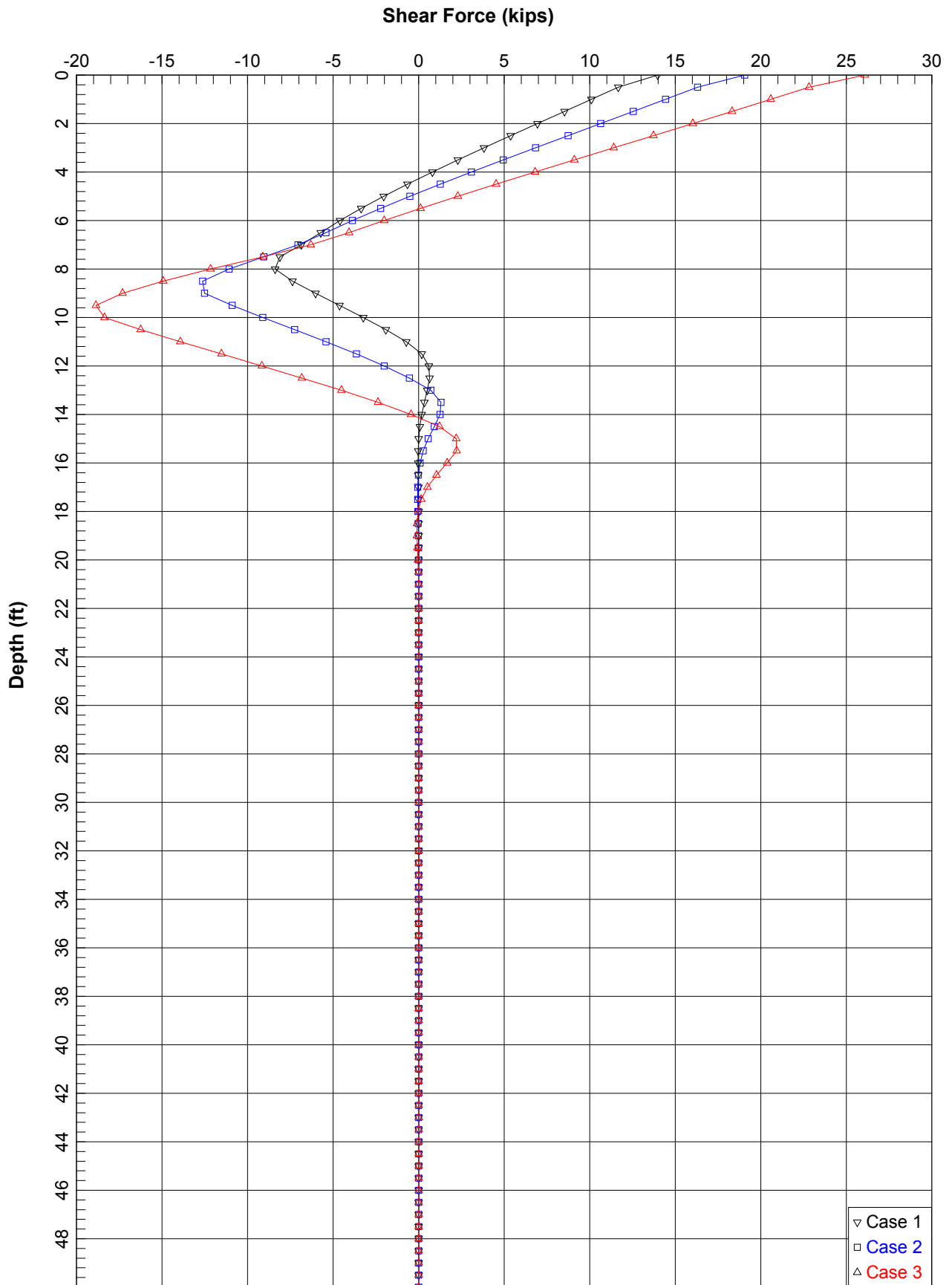
SUPPORT: ABUTMENT 5L

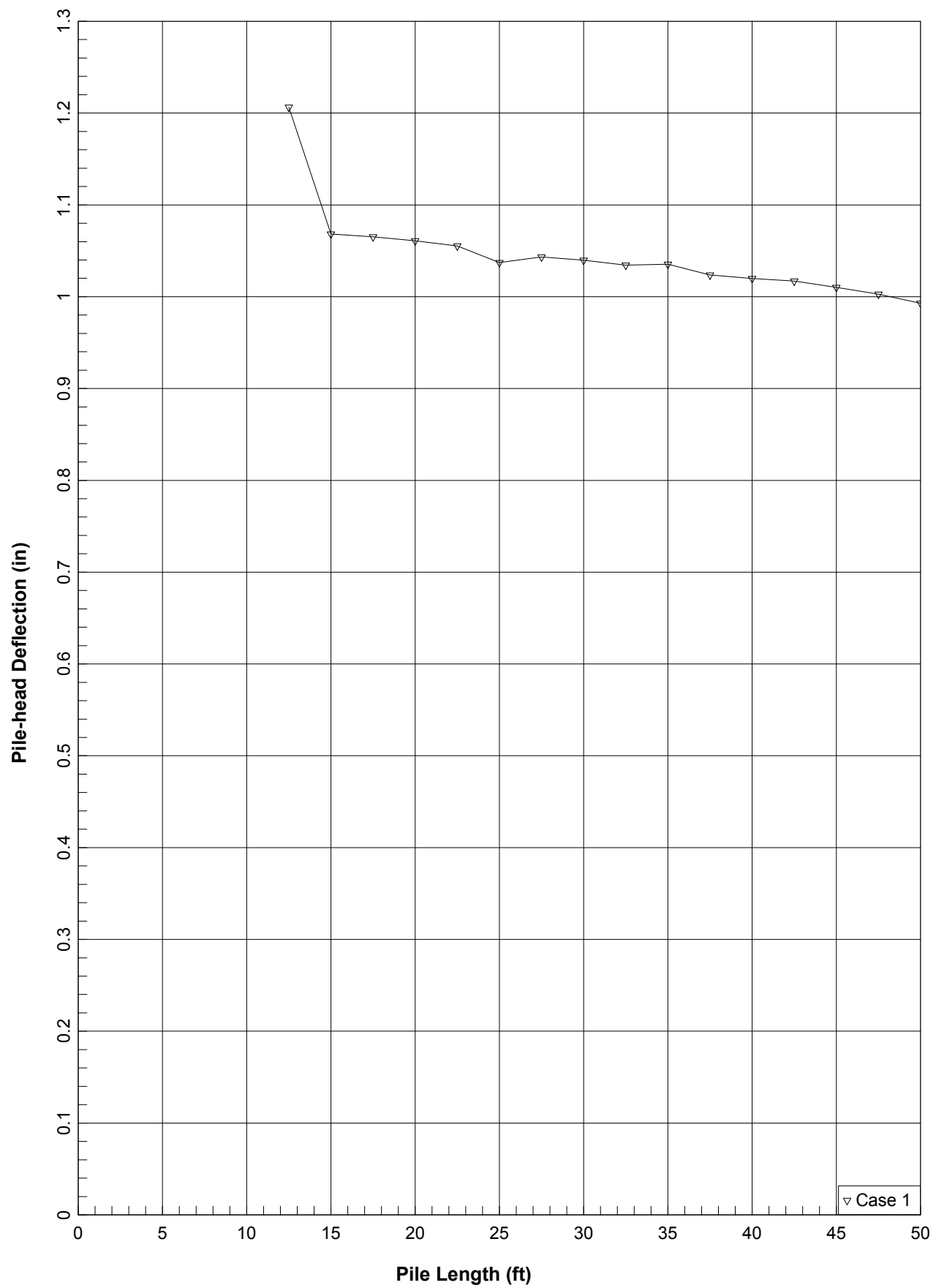
LOAD DIRECTION: TRANSVERSE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE









 Abut 5L_long_Critical Length

Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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gdc
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

 Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 5\
 Name of input data file: Abut 5L_long_Critical Length.lp6d
 Name of output report file: Abut 5L_long_Critical Length.lp6o
 Name of plot output file: Abut 5L_long_Critical Length.lp6p
 Name of runtime message file: Abut 5L_long_Critical Length.lp6r

 Date and Time of Analysis

Date: September 13, 2014 Time: 10:26:15

 Problem Title

Project Name: Palo Comado OC Bridge Widen

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

 Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

 Pile Structural Properties and Geometry

Page 1

 Abut 5L_long_Critical Length

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

 Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 16.0000000 in
 Bottom Width = 16.0000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

 Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

 Soil and Rock Layering Information

The soil profile is modelled using 5 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 7.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 7.00000 ft
 Distance from top of pile to bottom of layer = 12.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi

Page 2

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 12.00000 ft
 Distance from top of pile to bottom of layer = 17.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 17.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 130.00000 pcf
 Effective unit weight at bottom of layer = 130.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Depth	Effective Unit Wt.	Undrained Cohesion	In-situ Friction	Angle of Friction	Uniaxial Elastic Mod.	ROD % or GSI
Num.	Epsilon 50	psi	ft	pcf	psf	Test Type	deg. Property	psi Mod. pci	
1	0.00700	Stiff Clay w/o Free Water	-2.000	120.000	4000.000	--	--	--	--
2	0.00700	Stiff Clay w/o Free Water	0.10000	120.000	4000.000	--	--	--	--
3	0.00700	Stiff Clay w/o Free Water	7.000	120.000	1500.000	--	--	--	--
4	0.00700	Stiff Clay w/o Free Water	7.000	120.000	3500.000	--	--	--	--
5	0.00500	Stiff Clay w/o Free Water	12.000	125.000	4000.000	--	--	--	--
	0.00700		17.000	125.000	4000.000	--	--	--	--
	0.00700		17.000	130.000	4000.000	--	--	--	--
	0.00500		80.000	130.000	4000.000	--	--	--	--

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X Ft	p-mult	y-mult
1	0.000	0.6200	1.0000
2	50.000	0.6200	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Abut 5L_long_Critical Length

Number of loads specified = 1

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	V	26000. lbs	M = 0.0000 in-lbs	131000.	True

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)
 Shear force at pile head = 26000.000 lbs
 Applied moment at pile head = 0.000 in-lbs
 Axial thrust load on pile head = 131000.000 lbs

Depth inches	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil Res. lb/in	Soil Spr. lb/inch	Distrib. Lat. Load lb/inch
0.00	0.9928	1.073E-07	26000.	-0.0146	651.5405	5.799E+09	-720.3306	2176.6923	0.000
6.00	0.9051	184520.	22734.	-0.0145	1420.0586	5.799E+09	-368.2444	2441.1028	0.000
12.00	0.8184	295657.	20506.	-0.0143	2122.0178	5.799E+09	-374.4574	2745.3144	0.000
18.00	0.7335	423073.	18245.	-0.0139	2755.7347	5.799E+09	-379.2998	3102.6129	0.000
24.00	0.6513	536491.	15959.	-0.0134	3319.8269	5.799E+09	-382.7033	3525.8390	0.000
30.00	0.5723	635695.	13657.	-0.0128	3813.2262	5.799E+09	-384.5955	4031.8928	0.000
36.00	0.4974	720536.	11349.	-0.0121	4235.1925	5.799E+09	-384.8987	4643.3765	0.000
42.00	0.4268	790935.	9043.2319	-0.0113	4585.3285	5.799E+09	-383.5273	5391.0732	0.000
48.00	0.3613	846884.	6751.4913	-0.0105	4863.5948	5.799E+09	-380.3862	6317.7866	0.000
54.00	0.3009	888450.	4484.2319	-0.009596	5070.3276	5.799E+09	-375.3669	7484.4829	0.000
60.00	0.2461	915780.	2253.1051	-0.008663	5206.2574	5.799E+09	-368.3421	8980.4745	0.000
66.00	0.1970	929105.	70.6034	-0.007709	5272.5315	5.799E+09	-359.1585	10941.	0.000
72.00	0.1536	928745.	-2049.7457	-0.006747	5270.7403	5.799E+09	-347.6245	13580.	0.000
78.00	0.1160	915115.	-4093.0886	-0.005793	5202.9504	5.799E+09	-333.4898	17251.	0.000
84.00	0.0841	888735.	-6319.0380	-0.004860	5071.7477	5.799E+09	-308.4933	29153.	0.000
90.00	0.0577	846927.	-9128.5388	-0.003962	4863.8096	5.799E+09	-258.1069	54944.	0.000
96.00	0.0365	785418.	-12171.	-0.003118	4557.8885	5.799E+09	-185.9517	79826.	0.000
102.00	0.0203	705776.	-14925.	-0.002346	4161.7811	5.799E+09	-127.997.	127997.	0.000
108.00	0.008372	610002.	-17292.	-0.001665	3685.4405	5.799E+09	-56.7607	255686.	0.000
114.00	0.000273	500888.	-18777.	-0.001091	3142.7547	5.799E+09	-138.3288	3042701.	0.000
120.00	-0.004717	386388.	-18212.	-0.000632	2573.2752	5.799E+09	326.8606	415800.	0.000
126.00	-0.007307	283340.	-16107.	-0.000285	2060.7568	5.799E+09	374.5828	307575.	0.000
132.00	-0.008139	193546.	-13799.	-3.844E-05	1614.1612	5.799E+09	395.0021	291206.	0.000
138.00	-0.007768	117816.	-11412.	0.000123	1237.5075	5.799E+09	400.5052	309331.	0.000
144.00	-0.006667	56407.	-9061.2485	0.000213	932.0874	5.799E+09	383.1418	344815.	0.000
150.00	-0.005215	8746.1722	-6731.1791	0.000246	695.0404	5.799E+09	393.5481	452777.	0.000
156.00	-0.003709	-24754.	-4437.8181	0.000238	774.6585	5.799E+09	370.9056	600001.	0.000
162.00	-0.002357	-44882.	-2306.2052	0.000202	874.7558	5.799E+09	339.6321	864696.	0.000
168.00	-0.001283	-52747.	-390.2293	0.000152	913.8807	5.799E+09	299.0266	1398508.	0.000
174.00	-0.000537	-49803.	1245.9386	9.861E-05	899.2417	5.799E+09	246.3627	2754544.	0.000
180.00	-9.955E-05	37950.	2191.8164	5.321E-05	840.2902	5.799E+09	68.9299	4154447.	0.000
186.00	0.000102	-23585.	2181.9806	2.138E-05	768.8434	5.799E+09	-72.2085	4250889.	0.000
192.00	0.000157	-11800.	1629.8518	3.069E-06	710.2300	5.799E+09	-111.8344	4274851.	0.000
198.00	0.000139	-4031.7361	997.7768	-5.122E-06	671.5928	5.799E+09	-98.8573	4274851.	0.000
204.00	9.551E-05	1811.5583	2305.7055	-7.114E-06	652.4416	5.799E+09	-70.7201	4442809.	0.000
210.00	5.339E-05	1847.9809	152.7585	-6.046E-06	660.7317	5.799E+09	-41.3752	4650000.	0.000
216.00	2.274E-05	2023.7926	-24.2386	-4.061E-06	661.6061	5.799E+09	-17.6238	4650000.	0.000
222.00	4.658E-06	1563.5011	-87.9396	-2.205E-06	659.3168	5.799E+09	-3.6099	4650000.	0.000
228.00	-3.718E-06	971.9833	-90.1251	-8.931E-07	656.3748	5.799E+09	2.8813	4650000.	0.000
234.00	-6.059E-06	483.4036	-67.3935	-1.401E-07	653.9448	5.799E+09	4.6959	4650000.	0.000
240.00	-5.399E-06	163.4819	-40.7524	1.946E-07	652.3536	5.799E+09	4.1845	4650000.	0.000
246.00	-3.725E-06	5.9310	-19.5393	2.761E-07	651.5700	5.799E+09	2.8865	4650000.	0.000
252.00	-2.087E-06	-71.4238	-6.0284	2.360E-07	651.8698	5.799E+09	1.6171	4650000.	0.000

		Abut 5L Long Critical Length							
258.000	-8.920E-07	-78.6426	0.8970	1.584E-07	651.9317	5.799E+09	0.6913	4650000.0	0.000
264.000	-1.857E-07	-60.9092	3.4028	8.620E-08	651.8435	5.799E+09	0.1440	4650000.0	0.000
270.000	1.424E-07	-37.9439	3.5036	3.506E-08	651.7293	5.799E+09	-0.1104	4650000.0	0.000
276.000	2.350E-07	-18.9209	2.6262	5.642E-09	651.6347	5.799E+09	-0.1821	4650000.0	0.000
282.000	2.101E-07	-6.4386	1.5914	-7.478E-09	651.5726	5.799E+09	-0.1628	4650000.0	0.000
288.000	1.452E-07	0.1871	0.7652	-1.071E-08	651.5415	5.799E+09	-0.1126	4650000.0	0.000
294.000	8.155E-08	2.7602	0.2379	-9.188E-09	651.5543	5.799E+09	-0.0632	4650000.0	0.000
300.000	3.499E-08	3.0559	-0.0331	-6.179E-09	651.5557	5.799E+09	-0.0271	4650000.0	0.000
306.000	7.404E-09	2.3728	-0.1317	-3.370E-09	651.5523	5.799E+09	-0.005738	4650000.0	0.000
312.000	-5.453E-09	1.4812	-0.1362	-1.376E-09	651.5479	5.799E+09	0.004226	4650000.0	0.000
318.000	-9.113E-09	0.7406	-0.1023	-2.269E-10	651.5442	5.799E+09	0.007062	4650000.0	0.000
324.000	-8.175E-09	0.2535	-0.0621	-2.874E-10	651.5418	5.799E+09	0.006336	4650000.0	0.000
330.000	-5.664E-09	-0.005572	-0.0300	4.157E-10	651.5406	5.799E+09	0.004390	4650000.0	0.000
336.000	-3.187E-09	-0.1067	-0.009384	3.576E-10	651.5411	5.799E+09	0.002470	4650000.0	0.000
342.000	-1.372E-09	-0.1187	0.001217	2.410E-10	651.5411	5.799E+09	0.001064	4650000.0	0.000
348.000	-2.949E-10	-0.0924	0.005094	1.318E-10	651.5410	5.799E+09	0.000229	4650000.0	0.000
354.000	2.087E-10	-0.0578	0.005294	5.403E-11	651.5408	5.799E+09	-0.000162	4650000.0	0.000
360.000	3.534E-10	-0.0290	0.003988	9.118E-12	651.5407	5.799E+09	-0.000274	4650000.0	0.000
366.000	3.181E-10	-0.009983	0.002426	-1.104E-11	651.5406	5.799E+09	-0.000247	4650000.0	0.000
372.000	2.209E-10	0.000150	0.001173	-1.613E-11	651.5405	5.799E+09	-0.000171	4650000.0	0.000
378.000	1.246E-10	0.004121	0.000370	-1.392E-11	651.5406	5.799E+09	-9.653E-05	4650000.0	0.000
384.000	5.383E-11	0.004614	-4.460E-05	-9.401E-12	651.5406	5.799E+09	-4.172E-05	4650000.0	0.000
390.000	1.174E-11	0.003601	-0.000197	-5.151E-12	651.5406	5.799E+09	-9.102E-06	4650000.0	0.000
396.000	-7.985E-12	0.002257	-0.000206	-2.121E-12	651.5406	5.799E+09	6.189E-06	4650000.0	0.000
402.000	-1.370E-11	0.001134	-0.000155	0.000	651.5406	5.799E+09	1.062E-05	4650000.0	0.000
408.000	-1.238E-11	0.000393	-9.474E-05	0.000	651.5406	5.799E+09	9.593E-06	4650000.0	0.000
414.000	-8.613E-12	-3.233E-06	-4.594E-05	0.000	651.5405	5.799E+09	6.575E-06	4650000.0	0.000
420.000	-8.868E-12	-0.000159	-1.460E-05	0.000	651.5405	5.799E+09	3.772E-06	4650000.0	0.000
426.000	-2.111E-12	-0.000179	1.628E-06	0.000	651.5405	5.799E+09	1.636E-06	4650000.0	0.000
432.000	0.000	-0.000140	7.623E-06	0.000	651.5405	5.799E+09	3.623E-07	4650000.0	0.000
438.000	0.000	-8.810E-05	8.000E-06	0.000	651.5405	5.799E+09	-2.367E-07	4650000.0	0.000
444.000	0.000	-4.439E-05	6.054E-06	0.000	651.5405	5.799E+09	-4.118E-07	4650000.0	0.000
450.000	0.000	-1.547E-05	3.699E-06	0.000	651.5405	5.799E+09	-3.732E-07	4650000.0	0.000
456.000	0.000	2.390E-08	1.799E-06	0.000	651.5405	5.799E+09	-2.603E-07	4650000.0	0.000
462.000	0.000	6.150E-06	5.756E-07	0.000	651.5405	5.799E+09	-1.474E-07	4650000.0	0.000
468.000	0.000	6.965E-06	-5.912E-08	0.000	651.5405	5.799E+09	-6.416E-08	4650000.0	0.000
474.000	0.000	5.463E-06	-2.948E-07	0.000	651.5405	5.799E+09	-1.441E-08	4650000.0	0.000
480.000	0.000	3.439E-06	-3.109E-07	0.000	651.5405	5.799E+09	9.049E-09	4650000.0	0.000
486.000	0.000	1.731E-06	-2.359E-07	0.000	651.5405	5.799E+09	1.597E-08	4650000.0	0.000
492.000	0.000	6.090E-07	-1.444E-07	0.000	651.5405	5.799E+09	1.452E-08	4650000.0	0.000
498.000	0.000	3.052E-07	-7.043E-08	0.000	651.5405	5.799E+09	1.015E-08	4650000.0	0.000
504.000	0.000	-2.376E-07	-2.270E-08	0.000	651.5405	5.799E+09	5.761E-09	4650000.0	0.000
510.000	0.000	-2.706E-07	2.136E-09	0.000	651.5405	5.799E+09	2.516E-09	4650000.0	0.000
516.000	0.000	-2.128E-07	1.140E-08	0.000	651.5405	5.799E+09	5.732E-10	4650000.0	0.000
522.000	0.000	-1.342E-07	1.209E-08	0.000	651.5405	5.799E+09	-3.458E-10	4650000.0	0.000
528.000	0.000	-6.799E-08	9.191E-09	0.000	651.5405	5.799E+09	-6.190E-10	4650000.0	0.000
534.000	0.000	-2.397E-08	5.639E-09	0.000	651.5405	5.799E+09	-5.650E-10	4650000.0	0.000
540.000	0.000	-2.798E-10	2.757E-09	0.000	651.5405	5.799E+09	-3.957E-10	4650000.0	0.000
546.000	0.000	9.166E-09	8.941E-10	0.000	651.5405	5.799E+09	-2.251E-10	4650000.0	0.000
552.000	0.000	1.050E-08	-7.694E-11	0.000	651.5405	5.799E+09	-9.857E-11	4650000.0	0.000
558.000	0.000	8.277E-09	-4.403E-10	0.000	651.5405	5.799E+09	-2.256E-11	4650000.0	0.000
564.000	0.000	5.235E-09	-4.671E-10	0.000	651.5405	5.799E+09	1.364E-11	4650000.0	0.000
570.000	0.000	2.680E-09	-3.523E-10	0.000	651.5405	5.799E+09	2.464E-11	4650000.0	0.000
576.000	0.000	6.09E-09	-2.101E-10	0.000	651.5405	5.799E+09	2.275E-11	4650000.0	0.000
582.000	0.000	1.573E-10	-9.377E-11	0.000	651.5405	5.799E+09	1.601E-11	4650000.0	0.000
588.000	0.000	-1.184E-10	-2.021E-11	0.000	651.5405	5.799E+09	8.510E-12	4650000.0	0.000
594.000	0.000	-8.765E-11	1.005E-11	0.000	651.5405	5.799E+09	1.579E-12	4650000.0	0.000
600.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	-4.930E-12	2325000.0	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Pile-head deflection	=	0.9927870	inches
Computed slope at pile head	=	-0.0146128	radians
Maximum bending moment	=	929105.	inch-lbs
Maximum shear force	=	26000.	lbs
Depth of maximum bending moment	=	66.00000000	inches below pile head
Depth of maximum shear force	=	0.000000	inches below pile head
Number of iterations	=	28	
Number of zero deflection points	=	12	

Pile-head Deflection vs. Pile Length for Load Case 1

Boundary Condition Type 1, Shear and Moment

Shear	=	26000.	lbs
Moment	=	0.	in-lbs
Axial Load	=	131000.	lbs

Pile Length	Pile Head Deflection	Maximum Moment	Maximum Shear
-------------	----------------------	----------------	---------------

feet	inches	in-lbs	Abut 5L Long Critical Length lbs
50.000	0.9927870	929105.	26000.
47.500	1.0027062	932194.	26000.
45.000	1.0102379	933970.	26000.
42.500	1.0170522	935551.	26000.
40.000	1.0197608	939746.	26000.
37.500	1.0236452	942866.	26000.
35.000	1.0353754	944130.	26000.
32.500	1.0343944	948677.	26000.
30.000	1.0398503	951834.	26000.
27.500	1.0453492	955242.	26000.
25.000	1.0372713	960709.	26000.
22.500	1.0551881	960647.	26000.
20.000	1.0609626	963589.	26000.
17.500	1.0652806	966813.	26000.
15.000	1.0682321	970443.	26000.
12.500	1.2063601	950626.	26000.

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

- Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
- Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
- Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
- Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
- Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

Load Case No.	Load No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	1	V = 26000.	M = 0.000	131000.	0.99278701	929105.	26000.	-0.01461283

The analysis ended normally.

Abut 5L_transv_Ave P

Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 5L
 Name of input data file: Abut 5L_transv_Ave P.lpd
 Name of output report file: Abut 5L_transv_Ave P.lpp
 Name of plot output file: Abut 5L_transv_Ave P.lpp
 Name of runtime message file: Abut 5L_transv_Ave P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 10:22:47

Problem Title

Project Name: Palo Comado OC Bridge Widened

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Page 1

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Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 16.0000000 in
 Bottom Width = 16.0000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 5 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 7.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 7.00000 ft
 Distance from top of pile to bottom of layer = 12.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi

Page 2

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 12.00000 ft
 Distance from top of pile to bottom of layer = 17.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 17.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Rock Emass	Effective Unit Wt. krm	Undrained Cohesion Test psf	Angle of Friction Test deg.	Uniaxial Elastic Mod. psi	ROD % or GSI
1	0.00700	Stiff Clay w/o Free Water	---	120.000	4000.000	---	---	---
2	0.00700	Stiff Clay w/o Free Water	---	120.000	1500.000	---	---	---
3	0.00700	Stiff Clay w/o Free Water	---	120.000	3500.000	---	---	---
4	0.00700	Stiff Clay w/o Free Water	---	125.000	4000.000	---	---	---
5	0.00500	Stiff Clay w/o Free Water	---	125.000	4500.000	---	---	---

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X Ft	p-mult	y-mult
1	0.000	0.6200	1.0000
2	50.000	0.6200	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Abut SL_transv_Ave P

Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4	y = 0.25000 in	M = 0.0000 in-lbs	131000.	False
2	4	y = 0.50000 in	M = 0.0000 in-lbs	131000.	False
3	4	y = 1.00000 in	M = 0.0000 in-lbs	131000.	False

V = perpendicular shear force applied to pile head

M = bending moment applied to pile head

y = lateral deflection relative to pile axis

S = pile slope relative to original pile batter angle

R = rotational stiffness applied to pile head

Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection

For Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.250000 inches

Moment at pile head = 0.000 in-lbs

Axial load at pile head = 131000.000 lbs

Depth X inches	Deflect. y inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi	Bending Stiffness lb-in ²	Soil Res. p	Soil Spr. Es ^h lb/inch	Distrib. Lat. Load lb/inch
0.00	0.2500	0.000	13972.	-0.004592	651.5405	5.799E+09	-510.2695	6123.2345	0.000
6.000	0.2224	78257.	11663.	-0.004552	1040.7569	5.799E+09	-259.2775	6993.4449	0.000
12.000	0.1954	147116.	10100.	-0.004435	1383.2333	5.799E+09	-261.7459	8038.1327	0.000
18.000	0.1692	206432.	8526.4134	-0.004252	1678.2492	5.799E+09	-262.8732	9320.4554	0.000
24.000	0.1444	256117.	6950.0188	-0.004013	1925.3628	5.799E+09	-262.5917	10915.	0.000
30.000	0.1211	296141.	5379.7605	-0.003727	2124.4235	5.799E+09	-260.8277	12926.	0.000
36.000	0.0996	326534.	3824.7764	-0.003405	2275.5853	5.799E+09	-257.5003	15509.	0.000
42.000	0.0802	347391.	2294.7237	-0.003056	2379.3211	5.799E+09	-252.5173	18890.	0.000
48.000	0.0629	358875.	799.8601	-0.002691	2436.4386	5.799E+09	-245.7706	23427.	0.000
54.000	0.0479	361220.	-648.8348	-0.002319	2448.0994	5.799E+09	-237.1278	29695.	0.000
60.000	0.0351	354734.	-2039.4698	-0.001948	2415.8415	5.799E+09	-226.4172	38679.	0.000
66.000	0.0245	339808.	-3358.9203	-0.001589	2341.6088	5.799E+09	-213.3996	52186.	0.000
72.000	0.0161	316924.	-4592.2366	-0.001249	2227.7926	5.799E+09	-197.7059	73875.	0.000
78.000	0.009547	286665.	-5721.4001	-0.000937	2077.2953	5.799E+09	-178.6820	112995.	0.000
84.000	0.004816	249740.	-6857.3593	-0.000659	1893.6456	5.799E+09	-199.9711	249108.	0.000
90.000	0.001636	205413.	-8108.6207	-0.000424	1673.1810	5.799E+09	-217.1161	796083.	0.000
96.000	-0.000268	153103.	-8385.8027	-0.000238	1413.0110	5.799E+09	124.7221	2787546.	0.000
102.000	-0.001223	105158.	-7370.4246	-0.000105	1174.5531	5.799E+09	213.7373	1048781.	0.000
108.000	-0.001524	64822.	-6031.3220	-1.671E-05	973.9394	5.799E+09	232.6302	915725.	0.000
114.000	-0.001423	32808.	-4627.7030	3.380E-05	814.7157	5.799E+09	235.2428	991708.	0.000
120.000	-0.001119	9236.5526	-3239.0891	5.556E-05	697.4794	5.799E+09	227.6285	1220971.	0.000
126.000	-0.000757	-6148.0919	-1920.3475	5.715E-05	682.1186	5.799E+09	211.9520	1468056.	0.000
132.000	-0.000433	-13897.	-717.2517	4.678E-05	720.6609	5.799E+09	189.0799	2621576.	0.000
138.000	-0.000195	-14829.	180.1415	3.192E-05	725.2922	5.799E+09	110.0511	3382908.	0.000
144.000	4.969E-05	-11786.	593.8363	1.815E-05	710.1590	5.799E+09	27.8472	3362323.	0.000
150.000	2.263E-05	-7731.1539	635.8219	8.054E-06	689.9922	5.799E+09	-13.8520	3677280.	0.000
156.000	4.696E-05	-4168.7449	505.7781	1.898E-06	672.2742	5.799E+09	-29.4960	3768707.	0.000
162.000	4.541E-05	-1664.8002	329.5414	-1.120E-06	659.8366	5.799E+09	-39.2496	3851137.	0.000
168.000	3.352E-05	-212.4870	175.4055	-2.092E-06	652.5974	5.799E+09	-22.1290	3961571.	0.000
174.000	2.031E-05	443.3537	67.8162	-1.972E-06	653.7456	5.799E+09	-13.7341	4058008.	0.000
180.000	9.850E-06	604.4070	6.1528	-1.430E-06	654.5466	5.799E+09	-6.8204	4154447.	0.000
186.000	3.146E-06	519.4355	20.9953	-8.486E-07	654.1240	5.799E+09	-2.2290	4250889.	0.000
192.000	-3.330E-07	353.7969	-26.9706	-3.968E-07	653.3002	5.799E+09	0.2373	4274851.	0.000
198.000	-1.616E-06	196.4117	-22.8055	-1.122E-07	652.5174	5.799E+09	1.1511	4274851.	0.000
204.000	-1.679E-06	80.3076	-15.3893	3.100E-08	651.9400	5.799E+09	1.3209	4270485.	0.000
210.000	-1.244E-06	11.6914	-8.1735	7.860E-08	651.5987	5.799E+09	1.0843	5231250.	0.000
216.000	-7.358E-07	-17.8983	-2.9959	7.539E-08	651.6296	5.799E+09	0.6415	5231250.	0.000
222.000	-3.390E-07	-24.3784	-0.1845	5.351E-08	651.6618	5.799E+09	0.2956	5231250.	0.000
228.000	-9.364E-08	-20.1968	0.9472	3.045E-08	651.6461	5.799E+09	0.0816	5231250.	0.000
234.000	2.637E-08	-13.0596	1.1232	1.325E-08	651.6055	5.799E+09	-0.0230	5231250.	0.000

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240.000	6.531E-08	-6.7395	0.8834	3.000E-09	651.5475	5.799E+09	-0.0569	5231250.0	0.000													
246.000	6.241E-08	-2.4639	0.5493	-1.759E-09	651.5528	5.799E+09	-0.0544	5231250.0	0.000													
252.000	4.420E-08	-0.1450	0.2705	-3.109E-09	651.5413	5.799E+09	-0.0385	5231250.0	0.000													
258.000	2.510E-08	0.7865	0.0892	-2.777E-09	651.5445	5.799E+09	-0.0219	5231250.0	0.000													
264.000	1.089E-08	0.9294	-0.004958	-1.889E-09	651.5452	5.799E+09	-0.009490	5231250.0	0.000													
270.000	2.437E-09	0.7300	-0.0398	-1.030E-09	651.5442	5.799E+09	-0.002125	5231250.0	0.000													
276.000	-1.479E-09	0.4534	-0.0423	-4.181E-10	651.5428	5.799E+09	0.001290	5231250.0	0.000													
282.000	-2.580E-09	0.2229	-0.0317	-6.819E-11	651.5417	5.799E+09	0.002250	5231250.0	0.000													
288.000	-2.298E-09	0.0733	-0.0189	8.506E-11	651.5409	5.799E+09	0.002003	5231250.0	0.000													
294.000	-1.560E-09	-0.004356	-0.008841	1.207E-10	651.5406	5.799E+09	0.001360	5231250.0	0.000													
300.000	-8.490E-10	-0.0330	-0.002540	1.014E-10	651.5407	5.799E+09	0.007400	5231250.0	0.000													
306.000	-3.433E-10	-0.0350	0.000578	6.619E-11	651.5407	5.799E+09	0.000299	5231250.0	0.000													
312.000	-5.477E-11	-0.0262	0.001619	3.454E-11	651.5407	5.799E+09	4.775E-05	5231250.0	0.000													
318.000	7.117E-11	-0.0156	0.001576	1.291E-11	651.5406	5.799E+09	-6.205E-05	5231250.0	0.000													
324.000	1.001E-10	-0.007285	0.001128	1.056E-12	651.5406	5.799E+09	-8.729E-05	5231250.0	0.000													
330.000	8.385E-11	-0.002084	0.000647	-3.791E-12	651.5406	5.799E+09	-7.310E-05	5231250.0	0.000													
336.000	5.463E-11	0.000487	0.000285	-4.617E-12	651.5406	5.799E+09	-4.763E-05	5231250.0	0.000													
342.000	2.844E-11	0.001342	6.760E-05	-3.671E-12	651.5406	5.799E+09	-2.480E-05	5231250.0	0.000													
348.000	1.058E-11	0.001304	-3.447E-05	-2.302E-12	651.5406	5.799E+09	-9.227E-06	5231250.0	0.000													
354.000	0.000	0.000932	-6.430E-05	-1.145E-12	651.5406	5.799E+09	-7.128E-07	5231250.0	0.000													
360.000	-3.162E-12	0.000534	-5.816E-05	0.000	651.5406	5.799E+09	2.757E-06	5231250.0	0.000													
366.000	-3.827E-12	0.000235	-3.988E-05	0.000	651.5405	5.799E+09	3.337E-06	5231250.0	0.000													
372.000	-3.035E-12	5.533E-05	-2.193E-05	0.000	651.5405	5.799E+09	2.646E-06	5231250.0	0.000													
378.000	-1.900E-12	-2.879E-05	-9.026E-06	0.000	651.5405	5.799E+09	1.656E-06	5231250.0	0.000													
384.000	0.000	-5.326E-05	-1.591E-06	0.000	651.5405	5.799E+09	8.221E-07	5231250.0	0.000													
390.000	0.000	-4.809E-05	1.704E-06	0.000	651.5405	5.799E+09	2.762E-07	5231250.0	0.000													
396.000	0.000	-3.294E-05	2.505E-06	0.000	651.5405	5.799E+09	-9.319E-09	5231250.0	0.000													
402.000	0.000	-1.809E-05	-2.127E-06	0.000	651.5405	5.799E+09	-1.166E-07	5231250.0	0.000													
408.000	0.000	-7.430E-06	1.399E-06	0.000	651.5405	5.799E+09	-1.259E-07	5231250.0	0.000													
414.000	0.000	-1.296E-06	7.365E-07	0.000	651.5405	5.799E+09	-9.504E-08	5231250.0	0.000													
420.000	0.000	1.418E-06	2.792E-07	0.000	651.5405	5.799E+09	-5.715E-08	5231250.0	0.000													
426.000	0.000	2.074E-06	2.771E-08	0.000	651.5405	5.799E+09	-2.693E-08	5231250.0	0.000													
432.000	0.000	1.758E-06	-7.688E-08	0.000	651.5405	5.799E+09	-7.935E-08	5231250.0	0.000													
438.000	0.000	1.155E-06	-9.606E-08	0.000	651.5405	5.799E+09	1.542E-09	5231250.0	0.000													
444.000	0.000	6.074E-07	-7.714E-08	0.000	651.5405	5.799E+09	4.765E-09	5231250.0	0.000													
450.000	0.000	2.303E-07	-4.874E-08	0.000	651.5405	5.799E+09	4.700E-09	5231250.0	0.000													
456.000	0.000	2.224E-08	-2.448E-08	0.000	651.5405	5.799E+09	3.388E-09	5231250.0	0.000													
462.000	0.000	-6.387E-08	-8.447E-09	0.000	651.5405	5.799E+09	1.956E-09	5231250.0	0.000													
468.000	0.000	-7.950E-08	3.196E-11	0.000	651.5405	5.799E+09	8.700E-10	5231250.0	0.000													
474.000	0.000	-6.375E-08	3.284E-09	0.000	651.5405	5.799E+09	2.140E-10	5231250.0	0.000													
480.000	0.000	-4.024E-08	3.636E-09	0.000	651.5405	5.799E+09	-9.681E-11	5231250.0	0.000													
486.000	0.000	-2.018E-08	-2.776E-09	0.000	651.5405	5.799E+09	-1.899E-10	5231250.0	0.000													
492.000	0.000	-6.943E-09	1.685E-09	0.000	651.5405	5.799E+09	-1.737E-10	5231250.0	0.000													
498.000	0.000	4.938E-11	8.043E-10	0.000	651.5405	5.799E+09	-1.199E-10	5231250.0	0.000													
504.000	0.000	2.725E-09	2.454E-10	0.000	651.5405	5.799E+09	-6.640E-11	5231250.0	0.000													
510.000	0.000	3.008E-09	-3.673E-11	0.000	651.5405	5.799E+09	-2.764E-11	5231250.0	0.000													
516.000	0.000	2.293E-09	-1.352E-10	0.000	651.5405	5.799E+09	-5.125E-12	5231250.0	0.000													
522.000	0.000	1.391E-09	-1.360E-10	0.000	651.5405	5.799E+09	4.887E-12	5231250.0	0.000													
528.000	0.000	6.628E-10	-9.712E-11	0.000	651.5405	5.799E+09	7.417E-12	5231250.0	0.000													
534.000	0.000	2.015E-10	-5.799E-11	0.000	651.5405	5.799E+09	6.360E-12	5231250.0	0.000													
540.000	0.000	-3.110E-11	-2.607E-11	0.000	651.5405	5.799E+09	4.212E-12	5231250.0	0.000													
546.000	0.000	-1.120E-10	-6.733E-12	0.000	651.5405	5.799E+09	2.233E-12	5231250.0	0.000													
552.000	0.000	-1.124E-10	2.545E-12	0.000	651.5405	5.799E+09	0.000	5231250.0	0.000													
558.000	0.000	-8.177E-11	5.410E-12	0.000	651.5405	5.799E+09	0.000	5231250.0	0.000													
564.000	0.000	-4.764E-11	5.014E-12	0.000	651.5405	5.799E+09	0.000	5231250.0	0.000													
570.000	0.000	-2.165E-11	3.458E-12	0.000	651.5405	5.799E+09	0.000	5231250.0	0.000													
576.000	0.000	-6.143E-12	1.868E-12	0.000	651.5405	5.799E+09	0.000	5231250.0	0.000													
582.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	5231250.0	0.000													
588.000	0.000	2.226E-12	0.000	0.000	651.5405	5.799E+09	0.000	5231250.0	0.000													
594.000	0.000	1.126E-12	0.000	0.000	651.5405	5.799E+09	0.000	5231250.0	0.000													
600.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	2615625.0	0.000													

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Pile-head deflection	=	0.2500000	inches
Computed slope at pile head	=	-0.0049293	radians
Maximum bending moment	=	361220.	inch-lbs
Maximum shear force	=	13972.	lbs
Depth of maximum bending moment	=	54.0000000	inches below pile head
Depth of maximum shear force	=	19.	inches below pile head
Number of iterations	=	16	
Number of zero deflection points	=	13	

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)			
Displacement of pile head	=	0.500000	inches
Moment at pile head	=	0.000	in-lbs
Axial load at pile head	=	131000.000	lbs

Depth y inches	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	SI gage radi ans	Abut 5L	transv	Ave P	Bending Stiffness lb-in ²	Soil Res. lb/p in	Soil Spr. Es/h lb/inch	Distri b. Lat. Load lb/inch
0.00	0.5000	0.000	19052.	-0.008206	651.5405	5.799E+09	-60.8110</				

Abut SL_transv Ave P									
522.000	0.000	5.721E-09	1.981E-10	0.000	651.5405	5.799E+09	-9.234E-11	5231250.0	0.000
528.000	0.000	5.257E-09	-1.747E-10	0.000	651.5405	5.799E+09	-3.191E-11	5231250.0	0.000
534.000	0.000	3.639E-09	-2.702E-10	0.000	651.5405	5.799E+09	0.000	5231250.0	0.000
540.000	0.000	2.020E-09	-2.330E-10	0.000	651.5405	5.799E+09	1.235E-11	5231250.0	0.000
546.000	0.000	8.450E-10	-1.549E-10	0.000	651.5405	5.799E+09	1.369E-11	5231250.0	0.000
552.000	0.000	1.616E-10	-8.243E-11	0.000	651.5405	5.799E+09	1.046E-11	5231250.0	0.000
558.000	0.000	-1.453E-10	-3.198E-11	0.000	651.5405	5.799E+09	6.355E-12	5231250.0	0.000
564.000	0.000	-2.233E-10	-3.810E-12	0.000	651.5405	5.799E+09	3.037E-12	5231250.0	0.000
570.000	0.000	-1.918E-10	8.080E-12	0.000	651.5405	5.799E+09	0.000	5231250.0	0.000
576.000	0.000	-1.268E-10	1.042E-11	0.000	651.5405	5.799E+09	0.000	5231250.0	0.000
582.000	0.000	-6.694E-11	8.395E-12	0.000	651.5405	5.799E+09	0.000	5231250.0	0.000
588.000	0.000	-2.612E-11	5.142E-12	0.000	651.5405	5.799E+09	0.000	5231250.0	0.000
594.000	0.000	-5.224E-12	2.174E-12	0.000	651.5405	5.799E+09	0.000	5231250.0	0.000
600.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	2615625.0	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Pile-head deflection	=	0.5000000	inches
Computed slope at pile head	=	-0.0082062	radians
Maximum bending moment	=	578428	inch-lbs
Maximum shear force	=	60.0000000	inches below pile head
Depth of maximum bending moment	=	60.0000000	inches below pile head
Depth of maximum shear force	=	0.0000000	inches below pile head
Number of iterations	=	18	
Number of zero deflection points	=	12	

Computed Values of Pile Loading and Deflection
For Lateral Loading for Load Case Number 3

Pile-head conditions are Displacement and Moment (Loading Type 4)	=	1.0000000	inches
Displacement of pile head	=	1.0000000	inches
Moment at pile head	=	0.0000000	in-lbs
Axial load at pile head	=	131000.000	lbs

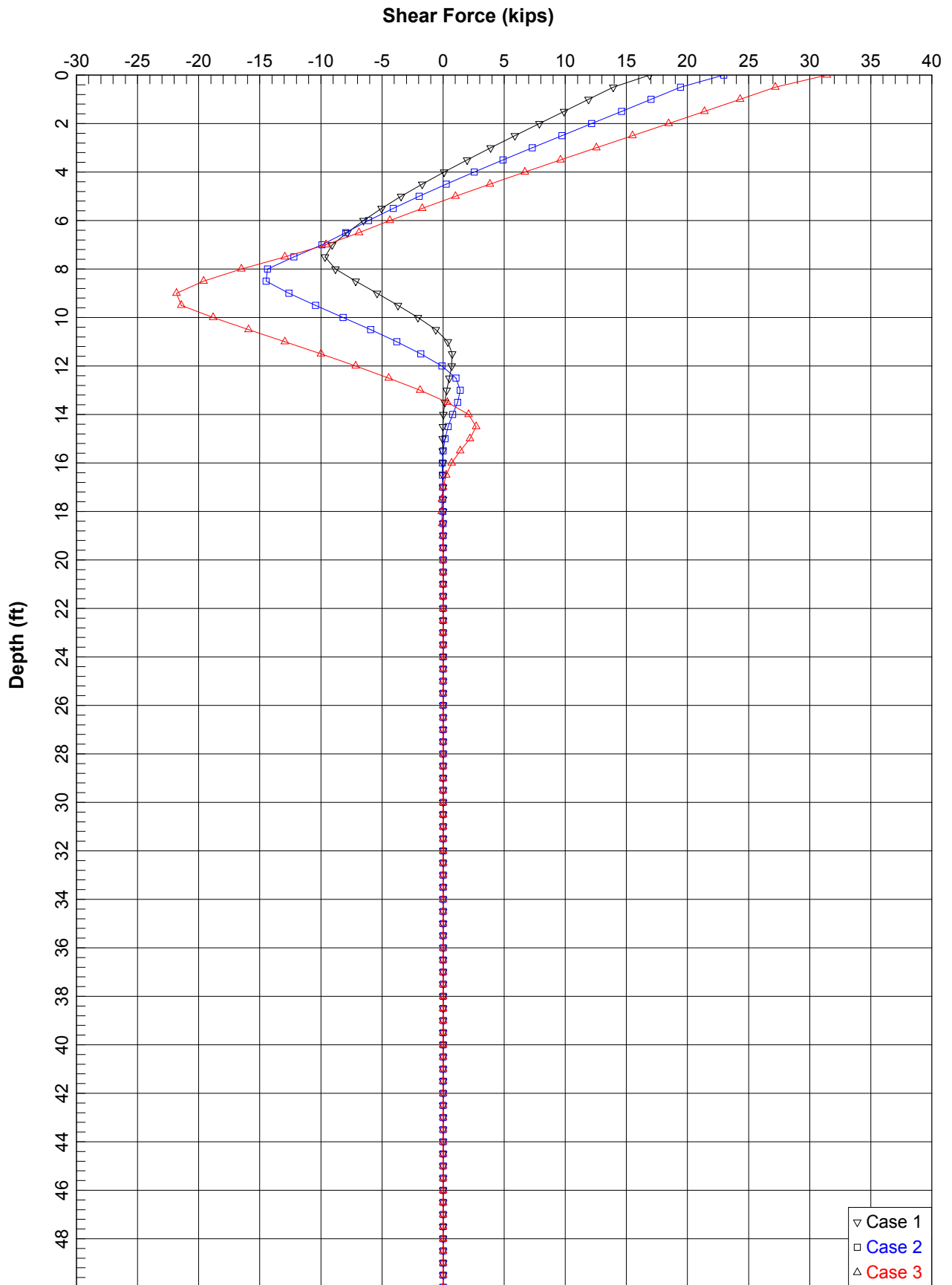
Depth inches	Deflect. inches	Bending Force in-lbs	Shear Force lbs	Slope radians	Total Stress psi	Bending Stiffness lb/in ²	Soil Res. lb/in	Soil Spr. lb/inch	Distrib. Load lb/inch
0.00	1.0000	0.000	26088.	-0.0147	651.5405	5.799E+09	-721.6301	2164.8903	0.000
6.00	0.9118	155097.	22817.	-0.0146	1422.9309	5.799E+09	-368.9180	2427.6896	0.000
12.00	0.8245	296787.	20584.	-0.0144	2127.6394	5.799E+09	-375.1533	2729.9961	0.000
18.00	0.7391	424730.	18319.	-0.0140	2763.9765	5.799E+09	-380.0175	3084.9963	0.000
24.00	0.6563	538648.	16028.	-0.0135	3330.5536	5.799E+09	-383.4422	3505.4231	0.000
30.00	0.5769	638323.	13722.	-0.0129	3826.2969	5.799E+09	-385.3552	4008.0309	0.000
36.00	0.5014	723606.	11409.	-0.0122	4250.4606	5.799E+09	-385.6783	4615.2215	0.000
42.00	0.4304	794416.	9098.9396	-0.0114	4602.6418	5.799E+09	-384.3261	5357.4964	0.000
48.00	0.3644	850744.	6802.3518	-0.0106	4882.7963	5.799E+09	-381.2032	6277.2560	0.000
54.00	0.3036	892658.	4530.1392	-0.009666	5091.2554	5.799E+09	-376.2010	7434.8716	0.000
60.00	0.2484	920302.	2293.9601	-0.008728	5228.7451	5.799E+09	-369.1921	8918.7535	0.000
66.00	0.1989	933906.	106.3155	-0.007769	5296.4087	5.799E+09	-360.0228	10863.	0.000
72.00	0.1551	933790.	-2019.2569	-0.006803	5295.8327	5.799E+09	-348.5013	13478.	0.000
78.00	0.1172	920369.	-4067.8911	-0.005844	5229.0807	5.799E+09	-334.3768	17115.	0.000
84.00	0.0850	894162.	-6299.9649	-0.004905	5098.7358	5.799E+09	-409.6478	20910.	0.000
90.00	0.0584	852480.	-9118.0361	-0.004001	4891.4269	5.799E+09	-529.7093	54454.	0.000
96.00	0.0370	791035.	-12170.	-0.003151	4585.8256	5.799E+09	-687.5590	79051.	0.000
102.00	0.0206	711395.	-14934.	-0.002373	4189.7274	5.799E+09	-433.7662	126605.	0.000
108.00	0.008524	615560.	-17310.	-0.001687	3713.0862	5.799E+09	-358.3875	252262.	0.000
114.00	0.000313	506323.	-18862.	-0.001107	3169.7859	5.799E+09	-158.7936	3042701.	0.000
120.00	0.004754	390958.	-18355.	-0.000642	2596.0057	5.799E+09	327.5882	113407.	0.000
126.00	-0.007395	287068.	-16245.	-0.000292	2079.2986	5.799E+09	375.7948	304911.	0.000
132.00	-0.008253	196473.	-13928.	-4.138E-05	1628.7160	5.799E+09	396.5046	288262.	0.000
138.00	-0.007891	119992.	-11532.	0.000122	1248.3326	5.799E+09	402.2389	305831.	0.000
144.00	-0.006785	57895.	-9170.3690	0.000214	939.4844	5.799E+09	385.0243	340486.	0.000
150.00	-0.005319	9610.7240	-6828.0036	0.000249	699.3404	5.799E+09	395.7642	446448.	0.000
156.00	-0.003793	-24433.	-4520.6763	0.000242	773.0623	5.799E+09	373.3449	590522.	0.000
162.00	-0.002419	-45017.	-2373.6755	0.000206	875.4380	5.799E+09	342.3227	849013.	0.000
168.00	-0.001325	-53241.	-440.5851	0.000155	916.3388	5.799E+09	302.0401	1368023.	0.000
174.00	-0.000561	-60548.	1215.3506	0.000101	902.9443	5.799E+09	249.9385	2674259.	0.000
180.00	-0.000111	-38814.	515.2719	5.494E-05	844.5940	5.799E+09	76.6036	415447.	0.000
186.00	9.852E-05	-24294.	2215.3981	2.229E-05	872.3708	5.799E+09	-69.7946	4250889.	0.000
192.00	0.000157	-12266.	1670.7816	3.374E-06	712.5464	5.799E+09	-111.7423	4274851.	0.000
198.00	0.000139	-4250.2892	1038.4392	-5.171E-06	672.6798	5.799E+09	-99.0385	4274851.	0.000
204.00	0.179E-06	353.4457	203.6732	-7.264E-06	552.5524	5.799E+09	-74.5745	4720485.	0.000
210.00	5.183E-05	1972.3323	158.2993	-6.139E-06	661.3501	5.799E+09	-45.1924	5231250.0	0.000
216.00	2.112E-05	2112.6878	-32.5298	-4.025E-06	662.0482	5.799E+09	-18.4173	5231250.0	0.000
222.00	3.530E-06	1588.3028	-97.0155	-2.111E-06	659.4401	5.799E+09	-3.0780	5231250.0	0.000
228.00	-4.202E-06	95.81896	95.2513	-7.964E-07	656.2745	5.799E+09	3.6640	5231250.0	0.000
234.00	-6.026E-06	446.4666	-68.5038	-7.293E-08	653.7611	5.799E+09	5.2539	5231250.0	0.000
240.00	-5.078E-06	129.8892	-39.4612	2.253E-07	652.1866	5.799E+09	4.4270	5231250.0	0.000
246.00	-3.323E-06	-27.4215	-17.4889	2.783E-07	651.6769	5.799E+09	2.8971	5231250.0	0.000
252.00	-1.738E-06	-80.4148	-4.2508	2.225E-07	651.9405	5.799E+09	1.5156	5231250.0	0.000

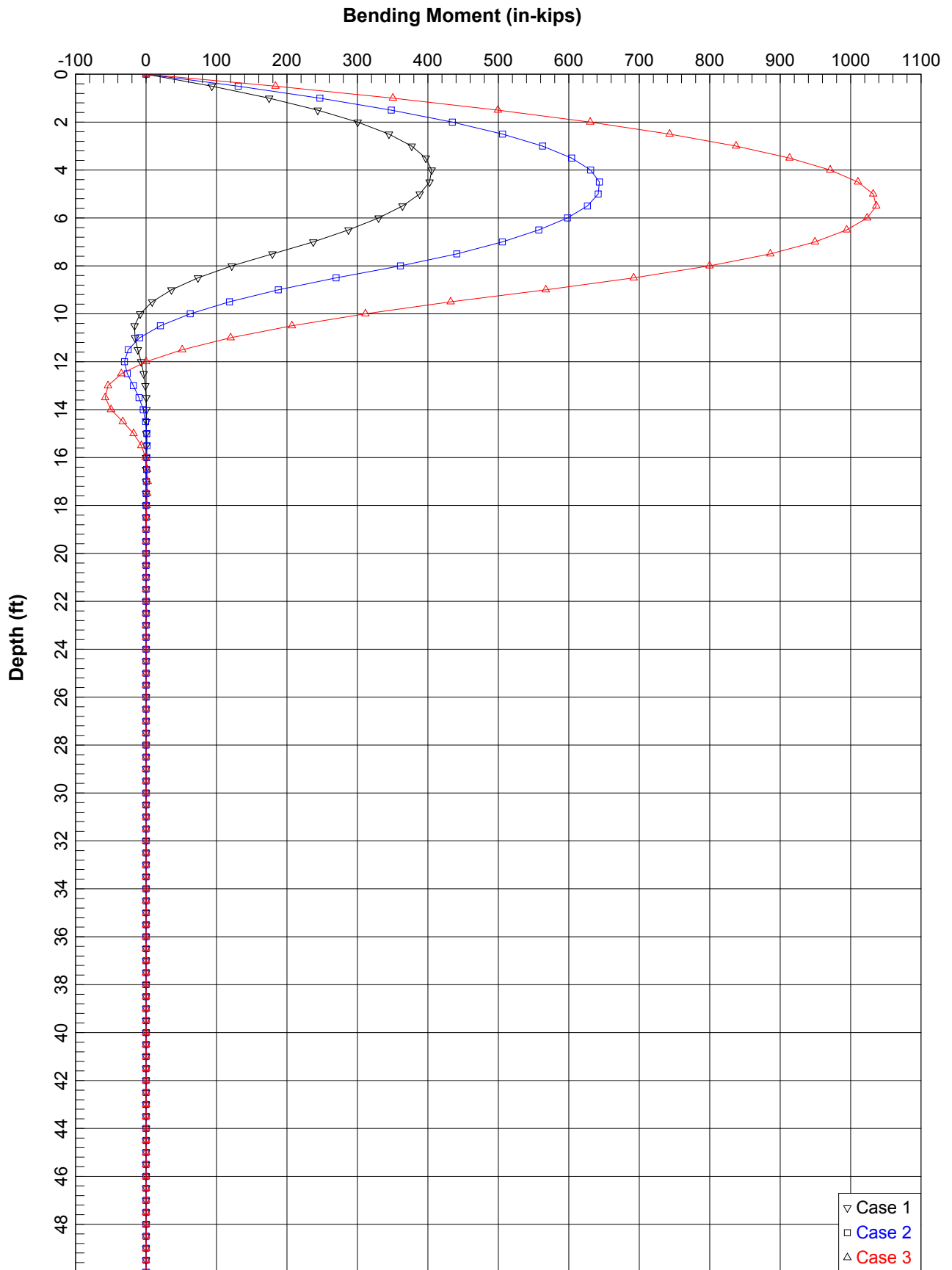
Abut SL_transv Ave P									
258.000	-6.531E-07	-78.7814	2.0041	1.401E-09	651.9324	5.799E+09	0.5694	5231250.0	0.000
264.000	-5.489E-08	-56.5862	3.8610	7.008E-08	651.8220	5.799E+09	0.0496	5231250.0	0.000
270.000	1.680E-07	-32.5592	3.5182	2.396E-08	651.7025	5.799E+09	-0.1639	5231250.0	0.000
276.000	2.307E-07	-14.4053	2.4232	-3.341E-10	651.6122	5.799E+09	-0.2011	5231250.0	0.000
282.000	1.840E-07	-3.4800	1.3387	-9.587E-09	651.5579	5.799E+09	-0.1604	5231250.0	0.000
288.000	1.156E-07	1.6745	0.5552	-1.052E-08	651.5489	5.799E+09	-0.1008	5231250.0	0.000
294.000	5.769E-08	3.1984	0.1018	-8.000E-09	651.5565	5.799E+09	-0.0503	5231250.0	0.000
300.000	1.962E-08	2.9089	-0.1004	-4.841E-09	651.5550	5.799E+09	-0.0171	5231250.0	0.000
306.000	-3.939E-10	2.0013	-0.1507	-2.300E-09	651.5505	5.799E+09	0.000343	5231250.0	0.000
312.000	-7.983E-09	1.1043	-0.1288	-6.935E-10	651.5460	5.799E+09	0.006960	5231250.0	0.000
318.000	-8.716E-09	0.4570	-0.0851	1.142E-10	651.5428	5.799E+09	0.007600	5231250.0	0.000
324.000	-6.612E-09	0.0830	-0.0450	3.936E-10	651.5410	5.799E+09	0.005765	5231250.0	0.000
330.000	-3.943E-09	-0.0836	-0.0173	3.933E-10	651.5410	5.799E+09	0.003481	5231250.0	0.000
336.000	-1.892E-09	-0.1248	-0.001868	2.855E-10	651.5412	5.799E+09	0.001650	5231250.0	0.000
342.000	-5.665E-10	-0.1064	0.004564	1.659E-10	651.5411	5.799E+09	0.000494	5231250.0	0.000
348.000	9.850E-11	-0.0703	0.005788	7.448E-11	651.5409	5.799E+09	-8.588E-05	5231250.0	0.000
354.000	3.273E-10	-0.0371	0.004674	1.893E-11	651.5407	5.799E+09	-0.000285	5231250.0	0.000
360.000	3.257E-10	-0.0142	0.002966	-7.615E-12	651.5406	5.799E+09	-0.000284	5231250.0	0.000
366.000	2.359E-10	-0.001503	0.001497	-1.574E-11	651.5406	5.799E+09	-0.000206	5231250.0	0.000
372.000	1.368E-10	0.003792	0.000523	-1.456E-11	651.5406	5.799E+09	-0.000119	5231250.0	0.000
378.000	6.123E-11	0.004790	4.587E-06	-1.012E-11	651.5406	5.799E+09	-5.339E-05	5231250.0	0.000
384.000	1.541E-11	0.003863	-0.000196	-5.639E-12	651.5406	5.799E+09	-1.343E-05	5231250.0	0.000
390.000	-6.434E-12	0.002449	-0.000219	-2.373E-12	651.5406	5.799E+09	5.609E-06	5231250.0	0.000
396.000	-1.307E-11	0.001235	-0.000168	0.000	651.5406	5.799E+09	1.140E-05	5231250.0	0.000
402.000	-1.205E-11	0.000430	-0.000103	0.000	651.5406	5.799E+09	1.050E-05	5231250.0	0.000
408.000	-8.355E-12	2.392E-06	-4.926E-05	0.000	651.5405	5.799E+09	7.284E-06	5231250.0	0.000
414.000	-4.616E-12	-0.000163	-1.535E-05	0.000	651.5405	5.799E+09	4.052E-06	5231250.0	0.000
420.000	-1.949E-12	0.000181	2.002E-06	0.000	651.5405	5.799E+09	1.700E-06	5231250.0	0.000
426.000	0.000	-0.000139	8.090E-06	0.000	651.5405	5.799E+09	3.297E-07	5231250.0	0.000
432.000	0.000	-8.470E-05	8.217E-06	0.000	651.5405	5.799E+09	-2.875E-07	5231250.0	0.000
438.000</									

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Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	131000.	0.25000000	361220.	13972.	-0.00459231
2	4	y = 0.5000	M = 0.000	131000.	0.50000000	578428.	19052.	-0.00820524
3	4	y = 1.0000	M = 0.000	131000.	1.00000000	933906.	26088.	-0.01470409

The analysis ended normally.





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Pile Plus For Windows, Version 2012-06.031
 Analysis of Individual Piles and Drilled Shafts
 Subjected to Lateral Loading Using the p-y Method
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 Serial Number of Security Device: 161633771
 Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: C:\Users\ethant\Desktop\Updated_ET 9-14-14\Abut 5\
 Name of input data file: Abut 5L_transv_Max P.lpd
 Name of output report file: Abut 5L_transv_Max P.lpp
 Name of plot output file: Abut 5L_transv_Max P.lpp
 Name of runtime message file: Abut 5L_transv_Max P.lpr

Date and Time of Analysis

Date: September 13, 2014 Time: 10:28:46

Problem Title

Project Name: Palo Comado OC Bridge Widened

Job Number: LA-1143

Client: Parson Transportation

Engineer: Mario Di Nicola

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 1 -

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes pile response to lateral loading and will compute nonlinear moment-curvature and nominal moment capacity for section types with nonlinear properties.

Computation Options:

- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix values
- Report pile response for full length of pile
- Analysis assumes no loading by soil movements acting on pile
- No p-y curves to be computed and reported for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05
- Maximum allowable deflection = 100.0000 in

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Abut 5L_transv_Max P

Total Number of Sections = 1
 Total Pile Length = 50.00 ft
 Depth of ground surface below top of pile = -2.00 ft

Pile dimensions used for p-y curve computations defined using 2 points.
 p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:
 Section Type = Elastic Pile
 Cross-sectional Shape = Circular
 Section Length = 50.0000000 ft
 Top Width = 16.0000000 in
 Bottom Width = 16.0000000 in
 Top Area = 201.06192983 in
 Bottom Area = 201.06192983 in
 Moment of Inertia at Top = 1608.49543864 in
 Moment of Inertia at Bottom = 1608.49543864 in
 Elastic Modulus = 3605000. lbs/in²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
 = 0.000 radians
 Pile Batter Angle = 0.000 degrees
 = 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 5 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -2.00000 ft
 Distance from top of pile to bottom of layer = 0.10000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.10000 ft
 Distance from top of pile to bottom of layer = 7.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 7.00000 ft
 Distance from top of pile to bottom of layer = 12.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 12.00000 ft
 Distance from top of pile to bottom of layer = 17.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 17.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Rock Emass	Effective Unit Wt.	Undrained Cohesion Test	Angle of Friction Test	Uniaxial Elastic Mod.	ROD % or GSI
Num.	Epsilon 50	psi	pcf	psi	deg.	psi		
1	0.00700	Stiff Clay w/o Free Water	120.000	120.000	4000.000			
2	0.00700	Stiff Clay w/o Free Water	120.000	120.000	1500.000			
3	0.00700	Stiff Clay w/o Free Water	120.000	120.000	3500.000			
4	0.00700	Stiff Clay w/o Free Water	120.000	125.000	4000.000			
5	0.00500	Stiff Clay w/o Free Water	120.000	125.000	4500.000			
	0.00500		80.000	125.000	4500.000			

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X Ft	p-mult	y-mult
1	0.000	0.8000	1.0000
2	50.000	0.8000	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

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Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4 y =	0.25000 in	M = 0.0000 in-lbs	131000.	False
2	4 y =	0.50000 in	M = 0.0000 in-lbs	131000.	False
3	4 y =	1.00000 in	M = 0.0000 in-lbs	131000.	False

V = perpendicular shear force applied to pile head

M = bending moment applied to pile head

y = lateral deflection relative to pile axis

S = pile slope relative to original pile batter angle

R = rotational stiffness applied to pile head

Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection

For Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.250000 inches

Moment at pile head = 0.000 in-lbs

Axial load at pile head = 131000.000 lbs

Depth X inches	Deflect. Y inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi	Bending Stiffness lb-in ²	Soil Res. p lb/in	Soil Spr. Es ^h lb/inch	Distrib. Lat. Load lb/inch
0.00	0.2500	0.000	16898.	-0.004866	651.5405	5.799E+09	-658.4123	7900.9477	0.000
6.00	0.2208	93362.	13921.	-0.004818	1115.8862	5.799E+09	-333.9334	9074.1124	0.000
12.00	0.1922	174627.	11910.	-0.004679	1520.0637	5.799E+09	-336.3515	10501.	0.000
18.00	0.1647	243641.	9890.5694	-0.004463	1863.3113	5.799E+09	-336.8825	12276.	0.000
24.00	0.1386	300329.	7873.6337	-0.004181	2145.2547	5.799E+09	-335.4294	14517.	0.000
30.00	0.1145	344697.	5871.6863	-0.003848	2365.9250	5.799E+09	-331.8864	17394.	0.000
36.00	0.0925	376838.	3897.6232	-0.003474	2525.7769	5.799E+09	-326.1347	21163.	0.000
42.00	0.0728	396930.	1965.1073	-0.003074	2625.7103	5.799E+09	-318.0373	26215.	0.000
48.00	0.0556	405251.	88.7069	-0.002659	2667.0938	5.799E+09	-307.4295	33188.	0.000
54.00	0.0409	402175.	-1715.8886	-0.002241	2651.7930	5.799E+09	-294.1023	43162.	0.000
60.00	0.0287	388183.	-3431.5096	-0.001832	2582.2066	5.799E+09	-277.7713	58101.	0.000
66.00	0.0189	363877.	-5038.8533	-0.001443	2461.3152	5.799E+09	-258.0099	81922.	0.000
72.00	0.0114	329986.	-6515.1376	-0.001084	2292.7555	5.799E+09	-234.0849	123556.	0.000
78.00	0.005887	287399.	-7830.7491	-0.000765	2080.9482	5.799E+09	-204.4523	208388.	0.000
84.00	0.002190	237219.	-9081.0994	-0.000493	1831.3713	5.799E+09	-212.3311	581660.	0.000
90.00	-3.341E-05	179202.	-9659.8495	-0.000278	1542.8171	5.799E+09	19.4144	3487090.	0.000
96.00	-0.001145	121738.	-8814.4433	-0.000122	1257.0143	5.799E+09	262.3877	1375533.	0.000
102.00	-0.001500	73621.	-7158.4468	-2.113E-05	1017.6993	5.799E+09	289.6111	1158565.	0.000
108.00	-0.001398	35870.	-5410.8852	3.551E-05	829.9411	5.799E+09	292.9094	1257028.	0.000
114.00	-0.001074	8634.1260	-3686.6743	5.854E-05	694.4832	5.799E+09	281.8276	1574935.	0.000
120.00	-0.000696	-8462.5460	-2062.6451	5.863E-05	693.6298	5.799E+09	259.5155	2238367.	0.000
126.00	-0.000370	-16210.	-602.7898	4.586E-05	732.1614	5.799E+09	227.1029	3681346.	0.000
132.00	-0.000145	-15768.	387.6253	2.932E-05	729.9647	5.799E+09	103.0354	4255299.	0.000
138.00	-1.831E-05	-11604.	736.7035	1.516E-05	709.2559	5.799E+09	13.3239	4365043.	0.000
144.00	3.661E-05	-6951.5062	697.2649	5.557E-06	686.1145	5.799E+09	-26.4701	4338482.	0.000
150.00	4.837E-05	-3245.9208	503.2509	2.814E-07	667.6844	5.799E+09	-38.2012	4378425.	0.000
156.00	3.998E-05	-912.9378	291.4278	-1.870E-06	656.0811	5.799E+09	-32.4065	4862847.	0.000
162.00	2.593E-05	254.1530	129.5497	-2.211E-06	652.8046	5.799E+09	-21.5528	4987244.	0.000
168.00	1.345E-05	645.1349	30.5097	-1.746E-06	654.7492	5.799E+09	-11.4605	5111705.	0.000
174.00	4.980E-06	623.0143	-16.9096	-1.090E-06	654.6392	5.799E+09	-4.3460	5236139.	0.000
180.00	3.757E-07	443.9326	30.9546	-5.377E-07	653.7485	5.799E+09	-0.3357	5360577.	0.000
186.00	-1.472E-07	252.4046	-27.9237	-1.714E-07	652.7959	5.799E+09	1.3460	5485018.	0.000
192.00	-1.753E-06	109.1271	-19.0498	9.610E-09	652.0833	5.799E+09	1.6120	5515936.	0.000
198.00	-1.357E-06	23.7924	-10.4711	7.838E-08	651.6589	5.799E+09	1.2476	5515936.	0.000
204.00	-8.129E-07	-16.6493	-4.2527	8.207E-08	651.6234	5.799E+09	0.8252	6090948.	0.000
210.00	-3.722E-07	-27.3687	-0.5209	5.930E-08	651.6767	5.799E+09	0.4187	6750000.	0.000
216.00	-1.013E-07	-22.9933	1.0771	3.324E-08	651.6549	5.799E+09	0.1140	6750000.	0.000
222.00	2.677E-08	-14.4956	1.3287	1.385E-08	651.6126	5.799E+09	-0.0301	6750000.	0.000
228.00	6.487E-08	-7.0704	0.0194	2.692E-09	651.5758	5.799E+09	-0.0730	6750000.	0.000
234.00	5.907E-08	-2.2666	0.6011	-2.139E-09	651.5318	5.799E+09	-0.0665	6750000.	0.000

Abut SL_transv_Max P									
				651.5413	5.799E+09	-0.0441	6750000.	0.000	
240.000	3.920E-08	0.1466	0.2695	-3.237E-09	651.5413	5.799E+09	-0.0441	6750000.	0.000
246.000	2.024E-08	0.9720	0.0688	-2.657E-09	651.5454	5.799E+09	-0.0228	6750000.	0.000
252.000	7.317E-09	0.9769	-0.0242	-1.649E-09	651.5454	5.799E+09	-0.00823	6750000.	0.000
258.000	4.576E-10	0.6846	-0.0504	-7.891E-10	651.5440	5.799E+09	-0.00015	6750000.	0.000
264.000	-2.152E-09	0.3732	-0.0447	-2.418E-10	651.5424	5.799E+09	0.002421	6750000.	0.000
270.000	-2.445E-09	0.1487	-0.0292	2.815E-11	651.5413	5.799E+09	0.002750	6750000.	0.000
276.000	-1.814E-09	0.0230	-0.0148	1.170E-10	651.5407	5.799E+09	0.002041	6750000.	0.000
282.000	-1.041E-09	-0.0292	-0.005171	1.138E-10	651.5407	5.799E+09	0.001171	6750000.	0.000
288.000	-4.490E-10	-0.0392	-0.000142	7.837E-11	651.5407	5.799E+09	0.000305	6750000.	0.000
294.000	-1.006E-10	-0.0310	0.001713	4.202E-11	651.5407	5.799E+09	0.000113	6750000.	0.000
300.000	5.527E-11	-0.0187	0.001865	1.628E-11	651.5406	5.799E+09	-6.218E-05	6750000.	0.000
306.000	9.478E-11	-0.008666	0.001359	2.102E-12	651.5406	5.799E+09	-0.000107	6750000.	0.000
312.000	8.049E-11	-0.002430	0.000767	-3.639E-12	651.5406	5.799E+09	-9.859E-05	6750000.	0.000
318.000	5.111E-11	0.000549	0.000323	-4.612E-12	651.5406	5.799E+09	-5.750E-05	6750000.	0.000
324.000	2.514E-11	0.001457	6.593E-05	-3.575E-12	651.5406	5.799E+09	-2.828E-05	6750000.	0.000
330.000	8.216E-12	0.001346	-4.665E-05	-2.125E-12	651.5406	5.799E+09	-9.243E-06	6750000.	0.000
336.000	0.000	0.0000900	-7.317E-05	0.000	651.5406	5.799E+09	4.008E-07	6750000.	0.000
342.000	-3.338E-12	0.000469	-6.071E-05	0.000	651.5406	5.799E+09	3.755E-06	6750000.	0.000
348.000	-3.407E-12	0.000172	-3.794E-05	0.000	651.5406	5.799E+09	3.833E-06	6750000.	0.000
354.000	-2.407E-12	1.361E-05	-1.832E-05	0.000	651.5405	5.799E+09	2.708E-06	6750000.	0.000
360.000	-1.322E-12	-4.770E-05	-5.733E-06	0.000	651.5405	5.799E+09	1.487E-06	6750000.	0.000
366.000	0.000	-5.544E-05	5.274E-07	0.000	651.5405	5.799E+09	5.997E-07	6750000.	0.000
372.000	0.000	-4.154E-05	2.624E-06	0.000	651.5405	5.799E+09	9.937E-08	6750000.	0.000
378.000	0.000	-2.403E-05	2.590E-06	0.000	651.5405	5.799E+09	-1.108E-07	6750000.	0.000
384.000	0.000	-1.048E-05	1.798E-06	0.000	651.5405	5.799E+09	-1.532E-07	6750000.	0.000
390.000	0.000	-2.449E-06	9.715E-07	0.000	651.5405	5.799E+09	-1.224E-07	6750000.	0.000
396.000	0.000	1.184E-06	3.812E-08	0.000	651.5405	5.799E+09	-7.441E-08	6750000.	0.000
402.000	0.000	1.136E-06	5.377E-08	0.000	651.5405	5.799E+09	-3.474E-08	6750000.	0.000
408.000	0.000	1.837E-06	-8.041E-08	0.000	651.5405	5.799E+09	-9.987E-09	6750000.	0.000
414.000	0.000	1.176E-06	-1.046E-07	0.000	651.5405	5.799E+09	1.938E-09	6750000.	0.000
420.000	0.000	5.837E-07	-8.178E-08	0.000	651.5405	5.799E+09	5.652E-09	6750000.	0.000
426.000	0.000	1.947E-07	-4.896E-08	0.000	651.5405	5.799E+09	5.289E-09	6750000.	0.000
432.000	0.000	-4.097E-09	-2.240E-08	0.000	651.5405	5.799E+09	3.566E-09	6750000.	0.000
438.000	0.000	-7.449E-08	-6.083E-09	0.000	651.5405	5.799E+09	1.872E-09	6750000.	0.000
444.000	0.000	-7.743E-08	1.626E-09	0.000	651.5405	5.799E+09	6.980E-10	6750000.	0.000
450.000	0.000	-5.519E-08	3.915E-09	0.000	651.5405	5.799E+09	6.488E-11	6750000.	0.000
456.000	0.000	-3.056E-08	3.561E-09	0.000	651.5405	5.799E+09	-1.828E-10	6750000.	0.000
462.000	0.000	-1.249E-08	2.362E-09	0.000	651.5405	5.799E+09	-2.170E-10	6750000.	0.000
468.000	0.000	-2.216E-09	1.219E-09	0.000	651.5405	5.799E+09	-1.640E-10	6750000.	0.000
474.000	0.000	2.152E-09	4.400E-10	0.000	651.5405	5.799E+09	-9.555E-11	6750000.	0.000
480.000	0.000	3.078E-09	2.695E-11	0.000	651.5405	5.799E+09	-4.212E-11	6750000.	0.000
486.000	0.000	2.485E-09	-1.093E-10	0.000	651.5405	5.799E+09	1.019E-11	6750000.	0.000
492.000	0.000	1.524E-09	-1.474E-10	0.000	651.5405	5.799E+09	4.383E-12	6750000.	0.000
498.000	0.000	7.185E-10	-1.093E-10	0.000	651.5405	5.799E+09	8.315E-12	6750000.	0.000
504.000	0.000	2.121E-10	-6.269E-11	0.000	651.5405	5.799E+09	7.229E-12	6750000.	0.000
510.000	0.000	3.422E-11	-2.702E-11	0.000	651.5405	5.799E+09	4.662E-12	6750000.	0.000
516.000	0.000	-1.127E-10	-6.030E-12	0.000	651.5405	5.799E+09	2.333E-12	6750000.	0.000
522.000	0.000	-1.070E-10	3.347E-12	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
528.000	0.000	-7.278E-11	5.718E-12	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
534.000	0.000	-3.853E-11	4.852E-12	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
540.000	0.000	-1.459E-11	3.079E-12	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
546.000	0.000	-1.576E-12	1.513E-12	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
552.000	0.000	3.587E-12	0.000	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
558.000	0.000	4.365E-12	0.000	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
564.000	0.000	3.331E-12	0.000	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
570.000	0.000	1.960E-12	0.000	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
576.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
582.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
588.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
594.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
600.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	3375000.	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Pile-head deflection	=	0.2500000	inches
Computed slope at pile head	=	-0.0048660	rad
Maximum bending moment	=	405251.	inch-lbs
Maximum shear force	=	16898.	lbs
Depth of maximum bending moment	=	48.0000000	inches below pile head
Depth of maximum shear force	=	0.0000000	inches below pile head
Number of iterations	=	12	
Number of zero deflection points	=	14	

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)	=		
Displacement of pile head	=	0.500000	inches
Moment at pile head	=	0.000	in-lbs
Axial load at pile head	=	1310000	lbs

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				651.5413	5.799E+09	-0.0441	6750000.	0.000	
0.00	0.5000	0.000	22973.	-0.008667	651.5405	5.799E+09	-78.9886	4697.9316	0.000
6.00	0.4480	130558.	19429.	-0.008599	1300.8837	5.799E+09	-398.5438	5337.6418	0.000
12.00	0.3968	246663.	17024.	-0.008404	1878.3397	5.799E+09	-403.1848	6096.3883	0.000
18.00	0.3472	348052.	14596.	-0.008096	2382.6080	5.799E+09	-405.9367	7016.0664	0.000
24.00	0.2997	434544.	12158.	-0.007691	2812.7857	5.799E+09	-406.7038	8143.4552	0.000
30.00	0.2549	506042.	9721.9939	-0.007205	3168.3857	5.799E+09	-405.3835	9543.8672	0.000
36.00	0.2132	562534.	7300.2542	-0.006652	3449.3551	5.799E+09	-401.8630	11130.0000	0.000
42.00	0.1750	604102.	4906.6180	-0.006048	3656.0957	5.799E+09	-396.0157	13575.0000	0.000
48.00	0.1406	630921.	2855.4860	-0.005409	3789.4864	5.799E+09	-387.6950	16843.0000	0.000
54.00	0.1101	643271.	262.2268	-0.004750	3850.9085	5.799E+09	-376.7248	20527.0000	0.000
60.00	0.0836	641535.	-1956.5999	-0.004085	3842.2763	5.799E+09	-362.8841	26040.0000	0.000
66.00	0.0611	626214.	-4082.8877	-0.003430	3766.0749	5.799E+09	-345.8785	33969.0000	0.000
72.00	0.0425	597932.	-6096.3780	-0.002796	3625.4112	5.799E+09	-325.2849	45967.0000	0.000
78.00	0.0275	557453.	-7973.5247	-0.002199	3424.0867	5.799E+09	-300.4306	65640.0000	0.000
84.00	0.0161	505706.	-9920.8530	-0.001648	3166.7155	5.799E+09	-348.6788	130131.0000	0.000
90.00	0.007756	440995.	-12206.	-0.001159	2844.8680	5.799E+09	-412.9604	319481.0000	0.000
96.00	0.002172	361058.	-14376.	-0.000744	2447.2964	5.799E+09	-310.4493	857433.0000	0.000
102.00	-0.001169	269652.	-14491.	-0.000417	1992.6786	5.799E+09	-272.0986	1396334.0000	0.000
108.00	-0.002837	187822.	-12623.	-0.000181	1585.6891	5.799E+09	-350.6229	741612.0000	0.000
114.00	-0.003338	118461.	-10443.	-0.000114	1240.7187	5.799E+09	-375.8467	675548.0000	0.000
120.00	-0.003104	62535.	-8177.6167	-0.000114	962.5641	5.799E+09	-379.4408	733421.0000	0.000
126.00	-0.002482	20218.	-5993.6218	0.000114	752.0952	5.799E+09	-368.5575	809091.0000	0.000
132.00	-0.001734	-8847.3961	-3790.9923	0.000120	695.5420	5.799E+09	-365.8520	916663.0000	0.000
138.00	-0.001041	-25456.	-1816.1015	0.000102	778.1469	5.799E+09	-310.2552	1799180.0000	0.000
144.00	-0.000506	-30802.	-102.0861	7.320E-05	804.7370	5.799E+09	-259.0933	3069253.0000	0.000
150.00	-0.000163	-26796.	1061.2022	4.340E-05	784.8120	5.799E+09	-128.6695	4738425.0000	0.000
156.00	1.428E-05	-18137.	1412.4843	2.018E-05	745.7405	5.799E+09	-11.5788	658477.0000	0.000
162.0									

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522.000	0.000	6.901E-11	-6.794E-11	0.000	651.5405	5.799E+09	9.815E-12	6750000.	0.000
528.000	0.000	-1.625E-10	2.209E-11	0.000	651.5405	5.799E+09	5.468E-12	6750000.	0.000
534.000	0.000	-1.970E-10	1.078E-12	0.000	651.5405	5.799E+09	2.256E-12	6750000.	0.000
540.000	0.000	-1.501E-10	9.103E-12	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
546.000	0.000	-8.804E-11	9.255E-12	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
552.000	0.000	-3.917E-11	6.523E-12	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
558.000	0.000	-9.770E-12	3.574E-12	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
564.000	0.000	3.752E-12	1.433E-12	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
570.000	0.000	7.460E-12	0.000	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
576.000	0.000	6.484E-12	0.000	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
582.000	0.000	4.079E-12	0.000	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
588.000	0.000	1.874E-12	0.000	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
594.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	6750000.	0.000
600.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	3375000.	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Pile-head deflection	=	0.5000000	inches
Computed slope at pile head	=	-0.0086667	radians
Maximum bending moment	=	643271.	inch-lbs
Maximum shear force	=	54.0000000	lbs
Depth of maximum bending moment	=	54.0000000	inches below pile head
Depth of maximum shear force	=	0.0000000	inches below pile head
Number of iterations	=	20	
Number of zero deflection points	=	13	

Computed Values of Pile Loading and Deflection
For Lateral Loading for Load Case Number 3

Pile-head conditions are Displacement and Moment (Loading Type 4)	=	1.0000000	inches
Displacement of pile head	=	1.0000000	inches
Moment at pile head	=	131000.000	in-lbs
Axial load at pile head	=	131000.000	lbs

Depth inches	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope radians	Total Stress psi	Bending Stiffness lb/in ²	Soil Res. lb/in	Soil Spr. lb/inch	Distrib. lb/inch
0.00	1.0000	0.000	31398.	-0.0155	651.5405	5.799E+09	-931.1356	2793.4069	0.000
6.00	0.9069	183819.	27178.	-0.0154	1565.7809	5.799E+09	-475.3879	3145.0792	0.000
12.00	0.8150	350374.	24304.	-0.0151	2394.1598	5.799E+09	-482.6627	3553.4496	0.000
18.00	0.7252	499269.	21392.	-0.0147	3134.7010	5.799E+09	-488.0258	4037.6647	0.000
24.00	0.6385	630189.	18454.	-0.0141	3785.8419	5.799E+09	-491.3809	4617.2034	0.000
30.00	0.5558	742906.	15502.	-0.0134	4346.4524	5.799E+09	-492.6255	5318.1159	0.000
36.00	0.4776	837285.	12549.	-0.0126	4815.8535	5.799E+09	-491.6485	6175.8715	0.000
42.00	0.4047	913283.	9608.8151	-0.0117	5193.8385	5.799E+09	-488.3271	7239.7636	0.000
48.00	0.3374	970599.	6695.2669	-0.0107	5480.6946	5.799E+09	-482.5223	8579.9404	0.000
54.00	0.2762	1010474.	3826.4801	-0.009685	5677.2279	5.799E+09	-474.0732	10299.	0.000
60.00	0.2212	1032101.	1015.8997	-0.008628	5784.7914	5.799E+09	-462.7869	12552.	0.000
66.00	0.1726	1036228.	-1717.7312	-0.007558	5805.3183	5.799E+09	-448.4234	15584.	0.000
72.00	0.1305	1023370.	-4355.0124	-0.006492	5741.3637	5.799E+09	-430.6703	19798.	0.000
78.00	0.0947	994174.	-6874.3130	-0.005449	5596.1584	5.799E+09	-409.0565	25099.	0.000
84.00	0.0651	949443.	-9585.2261	-0.004443	5373.6832	5.799E+09	-494.5412	45556.	0.000
90.00	0.0414	886136.	-12951.	-0.003493	5058.8203	5.799E+09	-627.3987	90877.	0.000
96.00	0.0232	799522.	-16513.	-0.002621	4628.0376	5.799E+09	-559.9760	144738.	0.000
102.00	0.009967	692099.	-19595.	-0.001850	4093.7576	5.799E+09	-467.2647	281274.	0.000
108.00	0.001018	567291.	-21816.	-0.001198	3473.0145	5.799E+09	-273.2096	1609608.	0.000
114.00	0.000409	432186.	-21427.	-0.000681	2801.0588	5.799E+09	402.9830	584840.	0.000
120.00	0.0007153	311237.	-18815.	-0.000296	2199.5087	5.799E+09	467.7378	923264.	0.000
126.00	0.0007964	206874.	-15931.	-2.825E-05	1680.4478	5.799E+09	493.6039	371864.	0.000
132.00	0.0007492	120112.	-12953.	0.000141	1248.9296	5.799E+09	499.0017	399651.	0.000
138.00	0.0006273	51217.	-9987.0106	0.000230	936.2713	5.799E+09	489.6582	468336.	0.000
144.00	0.0004737	-92.8130	-7157.0391	0.000256	652.0022	5.799E+09	453.6656	574648.	0.000
150.00	0.0003201	-35070.	-4448.3571	0.000238	428.9657	5.799E+09	449.2284	842039.	0.000
156.00	0.0001883	-53847.	-1889.5006	0.000192	919.3533	5.799E+09	403.7238	1286468.	0.000
162.00	0.0000899	-58046.	354.1524	0.000134	940.2367	5.799E+09	344.1605	229501.	0.000
168.00	0.0000276	-49808.	2091.4997	7.813E-05	899.2635	5.799E+09	234.9503	5111705.	0.000
174.00	3.838E-05	-33071.	2695.8741	3.525E-05	816.0203	5.799E+09	-33.4971	5236139.	0.000
180.00	0.000147	-1738.	2203.7423	9.082E-06	638.6410	5.799E+09	331.5468	5360577.	0.000
186.00	0.0000147	-6675.9957	1401.9448	-3.432E-06	484.7442	5.799E+09	-134.7190	5485018.	0.000
192.00	0.0000106	-683.8569	705.3044	-7.240E-06	654.9418	5.799E+09	-97.4944	5515936.	0.000
198.00	6.049E-05	1799.0390	245.9993	-6.663E-06	660.4882	5.799E+09	-55.6073	5515936.	0.000
204.00	2.609E-05	2278.094	141.2430	-4.553E-06	652.2430	5.799E+09	-26.4888	6090244.	0.000
210.00	5.846E-06	1802.7289	-99.4851	-2.442E-06	660.5066	5.799E+09	-6.5765	6750000.	0.000
216.00	-3.210E-06	1088.6270	-108.3820	-9.460E-07	656.9549	5.799E+09	3.6109	6750000.	0.000
222.00	-5.507E-06	503.6317	-78.9647	-1.223E-07	654.0454	5.799E+09	6.1949	6750000.	0.000
228.00	-4.677E-06	141.2430	-44.5960	-2.114E-07	652.2430	5.799E+09	5.2613	6750000.	0.000
234.00	-2.970E-06	-31.8529	-18.7883	2.680E-07	651.6990	5.799E+09	3.3413	6750000.	0.000
240.00	-1.461E-06	-84.6377	-3.8335	2.077E-07	651.9615	5.799E+09	1.6437	6750000.	0.000
246.00	-4.775E-07	-78.1818	2.7091	1.235E-07	651.9294	5.799E+09	0.5372	6750000.	0.000
252.00	2.061E-08	-52.3226	4.2512	5.595E-08	651.8008	5.799E+09	-0.0232	6750000.	0.000

Abut SL_transv_Max P									
258.000	1.939E-07	-27.2554	3.5272	1.470E-08	651.6745	5.799E+09	-0.2181	6750000.	0.000
264.000	1.980E-07	-10.0189	2.2047	-4.503E-09	651.5904	5.799E+09	-0.2227	6750000.	0.000
270.000	1.399E-07	-0.7922	1.0645	-1.010E-08	651.5445	5.799E+09	-0.1573	6750000.	0.000
276.000	7.682E-08	2.7709	0.3332	-9.073E-09	651.5543	5.799E+09	-0.0864	6750000.	0.000
282.000	3.098E-08	3.2208	-0.0306	-5.973E-09	651.5566	5.799E+09	-0.0349	6750000.	0.000
288.000	5.137E-09	2.4134	-0.1525	-3.058E-09	651.5526	5.799E+09	-0.00779	6750000.	0.000
294.000	-5.721E-09	1.3961	-0.1505	-1.087E-09	651.5475	5.799E+09	0.006436	6750000.	0.000
300.000	-7.911E-09	0.6093	-0.1045	-4.987E-11	651.5436	5.799E+09	0.008900	6750000.	0.000
306.000	-6.319E-09	0.1423	-0.0565	-3.390E-10	651.5413	5.799E+09	0.007109	6750000.	0.000
312.000	-3.843E-09	-0.0687	-0.0222	3.771E-10	651.5409	5.799E+09	0.004324	6750000.	0.000
318.000	-1.794E-09	-0.1241	-0.003128	2.773E-10	651.5412	5.799E+09	0.002019	6750000.	0.000
324.000	-5.160E-10	-0.1067	0.004670	1.579E-10	651.5411	5.799E+09	0.000581	6750000.	0.000
330.000	9.999E-11	-0.0683	0.004074	6.732E-11	651.5409	5.799E+09	-0.000112	6750000.	0.000
336.000	2.919E-10	-0.0339	0.004752	1.443E-11	651.5407	5.799E+09	-0.000328	6750000.	0.000
342.000	2.731E-10	-0.0113	0.002845	-8.973E-12	651.5406	5.799E+09	-0.000307	6750000.	0.000
348.000	3.357E-12	0.003207	-0.000227	-3.791E-12	651.5406	5.799E+09	-3.776E-06	6750000.	0.000
372.000	-9.437E-12	0.001776	-0.000207	-1.214E-12	651.5406	5.799E+09	1.062E-05	6750000.	0.000
378.000	-1.121E-11	0.000726	-0.000137	0.000	651.5406	5.799E+09	1.261E-05	6750000.	0.000
384.000	-8.471E-12	0.000129	-7.082E-05	0.000	651.5405	5.799E+09	9.530E-06	6750000.	0.000
390.000	-4.935E-12	-0.000125	-2.557E-05	0.000	651.5405	5.799E+09	5.552E-06	6750000.	0.000
396.000	-2.176E-12	-0.000179	-1.570E-06	0.000	651.5405	5.799E+09	2.448E-06	6750000.	0.000
402.000	0.000	-0.000144	7.551E-06	0.000	651.5405	5.799E+09	5.924E-07	6750000.	0.000
408.000	0.000	-8.853E-05	8.565E-06	0.000	651.5405	5.799E+09	-2.545E-07	6750000.	0.000
414.000	0.000	-4.175E-05	6.352E-06	0.000	651.5405	5.799E+09	-4.831E-07	6750000.	0.000
420.000	0.000	-1.235E-05	3.643E-06	0.000	651.5405	5.799E+09	-4.200E-07	6750000.	0.000
426.000	0.000	1.985E-06	1.570E-06	0.000	651.5405	5.799E+09	-2.709E-07	6750000.	0.000
432.000	0.000	6.545E-06	3.506E-07	0.000	651.5405	5.799E+09	-1.356E-07	6750000.	0.000
438.000	0.000	6.218E-06	-1.944E-07	0.000	651.5405	5.799E+09	-4.604E-08	6750000.	0.000
444.000	0.000	4.229E-06	-3.322E-07	0.000	651.5405	5.799E+09	9.013E-11	6750000.	0.000
450.000	0.000	2.239E-06	-2.819E-07	0.000	651.5405	5.799E+09	1.669E-08	6750000.	0.000
456.000	0.000	8.480E-07	-1.789E-07	0.000	651.5405	5.799E+09	1.764E-08	6750000.	0.000
462.000	0.000	9.158E-08	-8.7						

Abut SL_transv_Max P

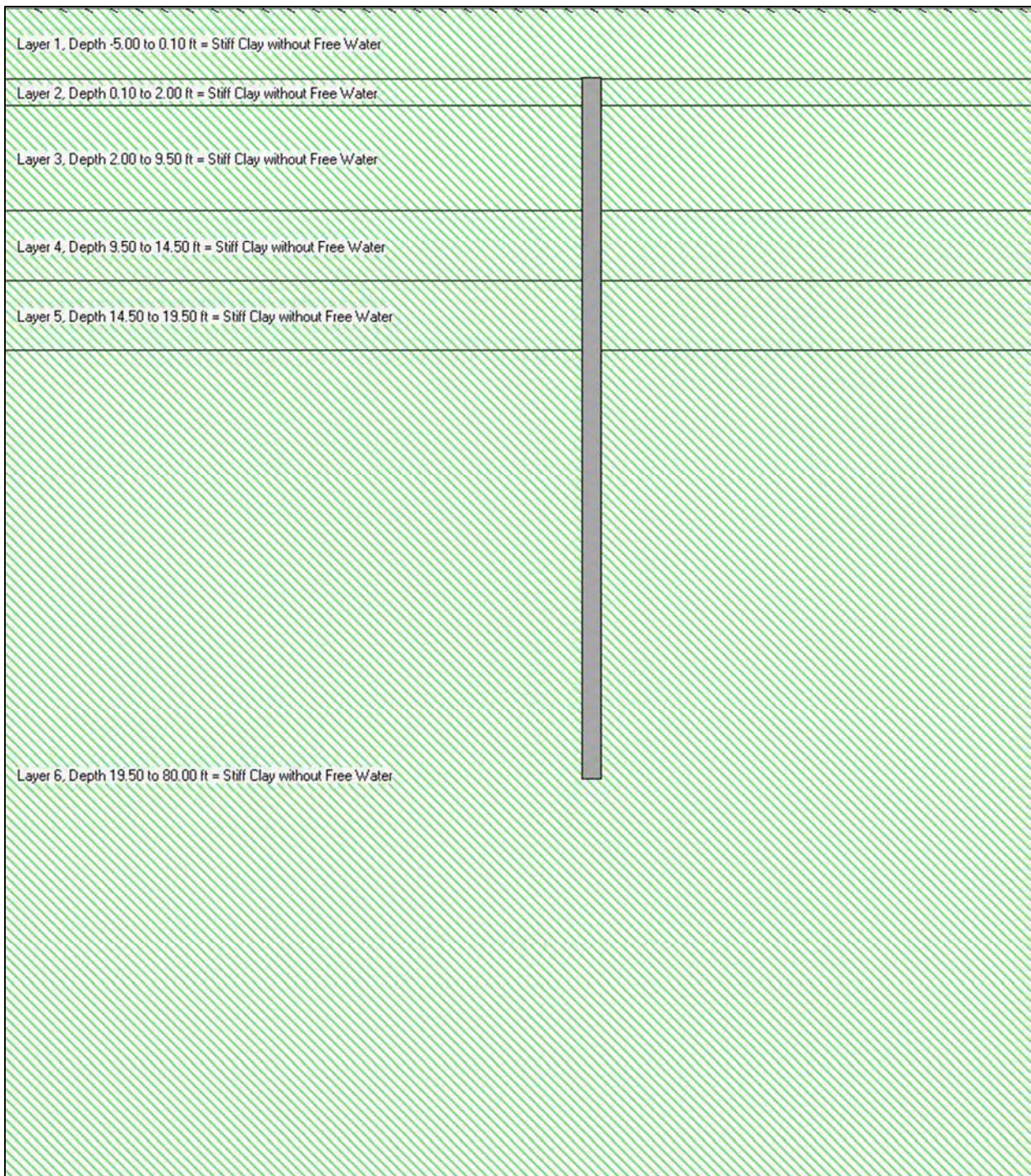
Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 M = in-lb, rad, or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	131000.	0.25000000	405251.	16898.	-0.00486600
2	4	y = 0.5000	M = 0.000	131000.	0.50000000	643271.	22973.	-0.00866670
3	4	y = 1.0000	M = 0.000	131000.	1.00000000	1036228.	31398.	-0.01551376

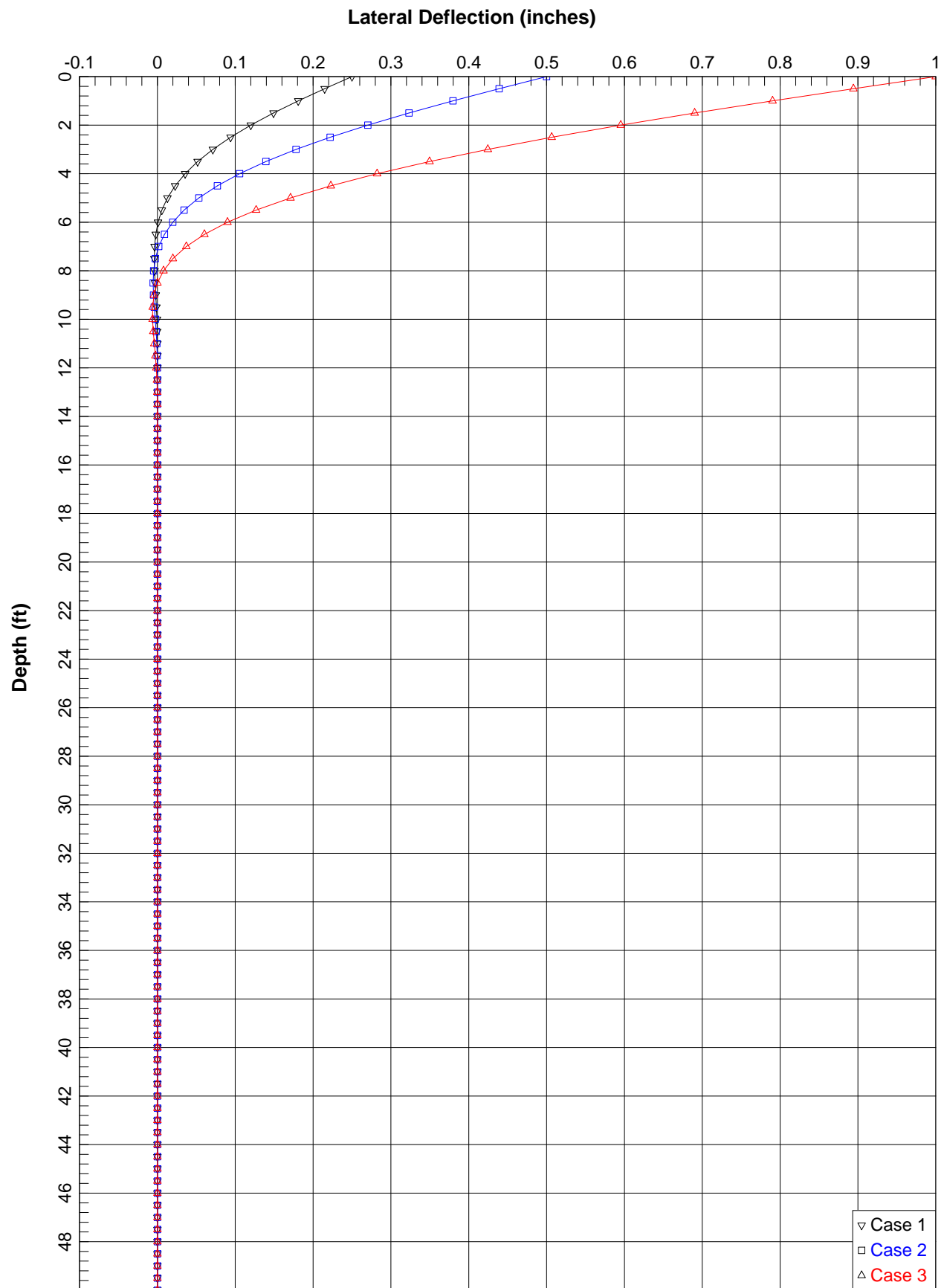
The analysis ended normally.

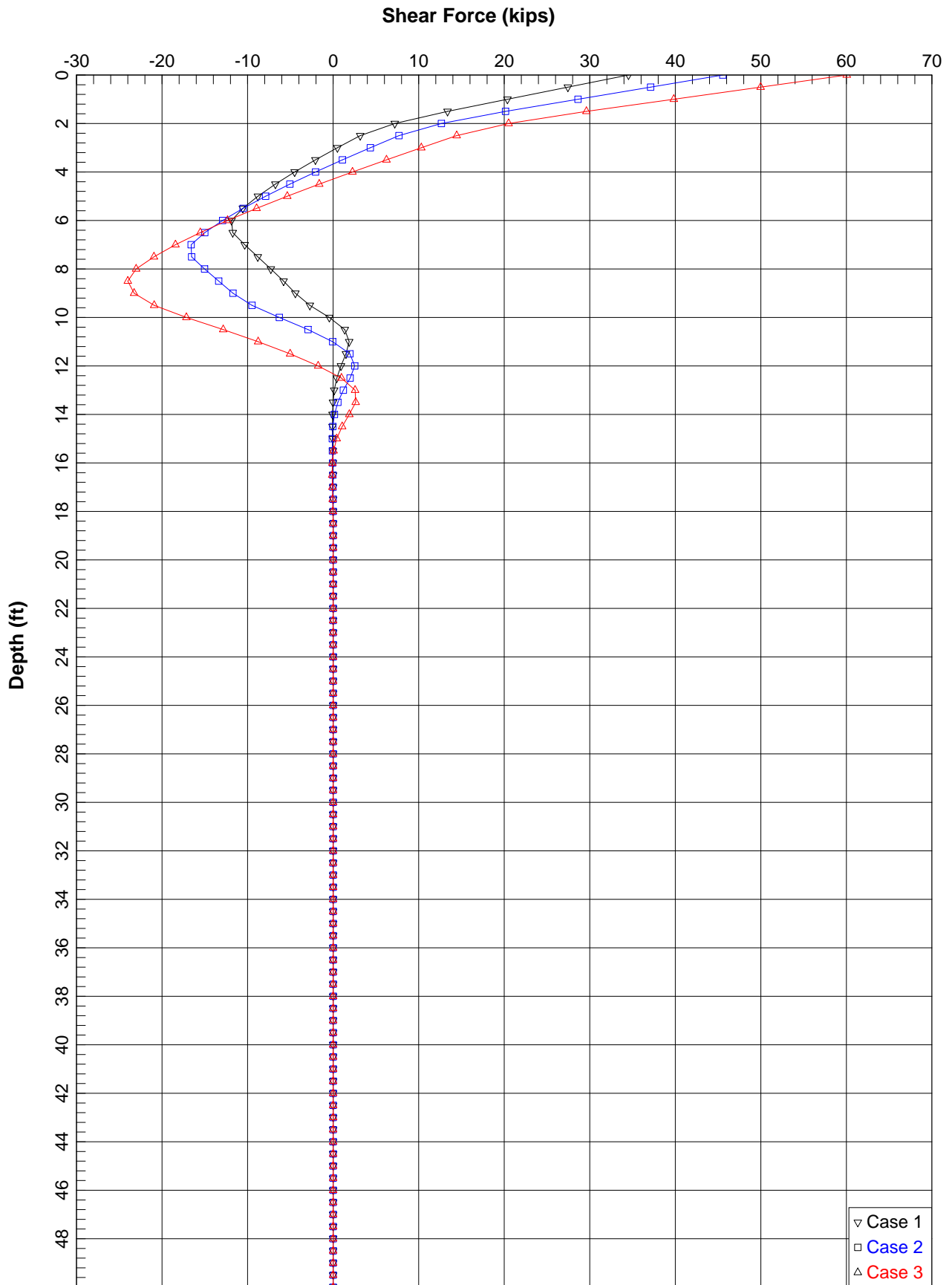
SUPPORT: ABUTMENT 5 PILASTER

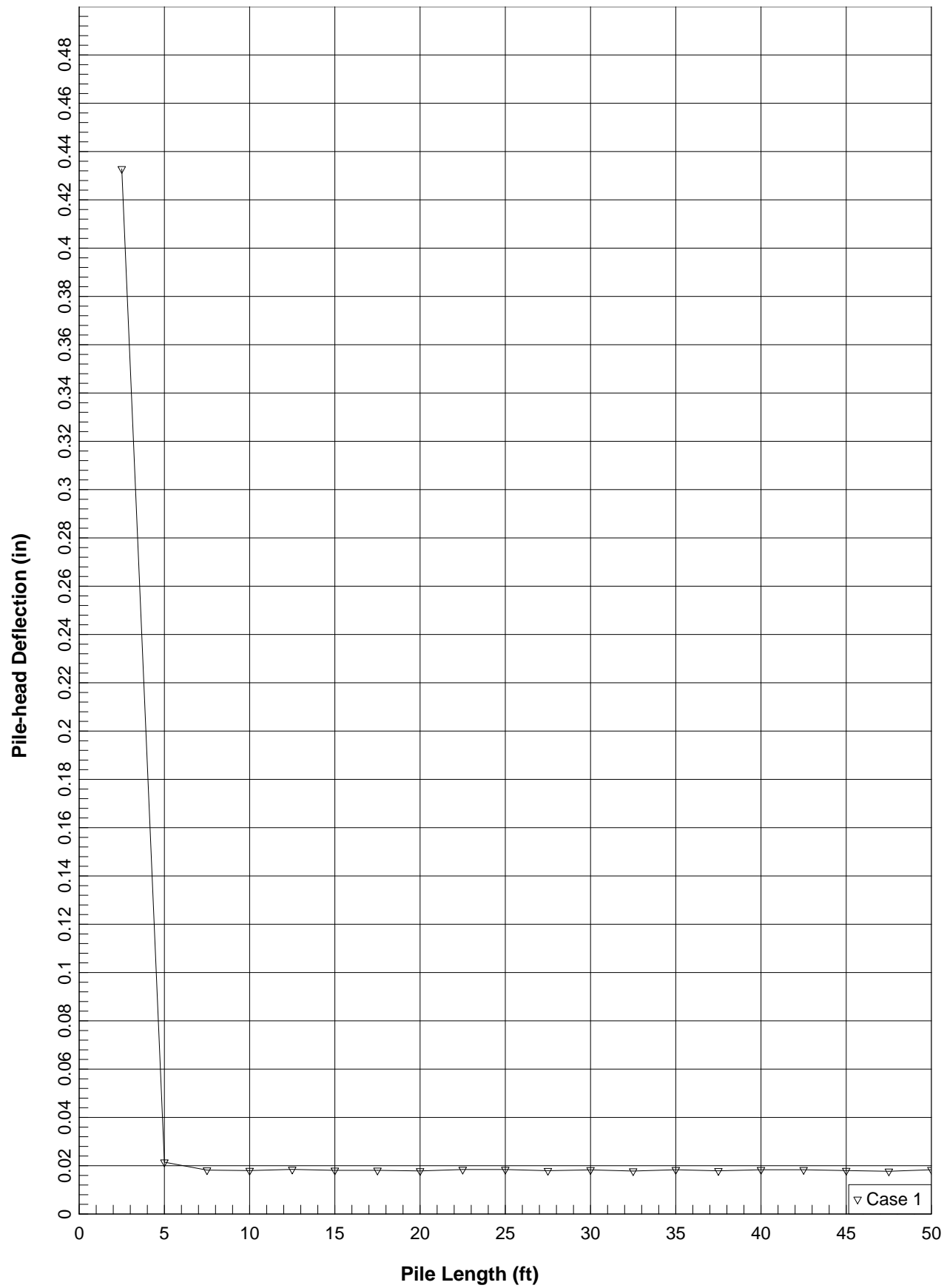
LOAD DIRECTION: LONGITUDINAL

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. MOMENT VS. DEPTH PLOT (LEADING ROW)
5. CRITICAL LENGTH PLOT (P-AVG CASE)
6. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
7. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)









Abut 5_Pil_long_Critical Length.lp6o

LPILE Plus for Windows, Version 6 (6.0.25)

Analysis of Individual Piles and Drilled Shafts
Subjected to Lateral Loading Using the p-y Method

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Group Delta Consultants Inc.
Irvine, Ca

Serial Number of Security Device: 156242237
Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: N:\Projects\LA\1100\LA1143 PTG - 101 & Palo Comado Cyn\Irvine Foundation
Report\Calculations\Lateral Pile Capacity\Updated_LG_6-05-17\Abut 5\
Name of input data file: Abut 5_Pil_long_Critical Length.lp6d
Name of output report file: Abut 5_Pil_long_Critical Length.lp6o
Name of plot output file: Abut 5_Pil_long_Critical Length.lp6p
Name of runtime message file: Abut 5_Pil_long_Critical Length.lp6r

Date and Time of Analysis

Date: June 6, 2017 Time: 17:13:40

Problem Title

Project Name: Palo Comado OC Bridge widen

Job Number: LA-1143

Client: Parson Transportation

Engineer: LG

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 5 Pilaster

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes nonlinear bending stiffness and nominal moment capacity with pile response computed using nonlinear EI

Computation Options:

- Only internally-generated p-y curves used in analysis
- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix elements
- Output pile response for full length of pile
- Analysis assumes no soil movements acting on pile
- No p-y curves to be computed and output for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

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Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
Total Pile Length = 50.00 ft
Depth of ground surface below top of pile = -5.00 ft
Slope angle of ground surface = 0.00 deg.

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:

Section Type	=	Elastic Pile
Cross-sectional Shape	=	Circular
Section Length	=	50.000 ft
Top Width	=	16.000 in
Bottom Width	=	16.000 in
Top Area	=	201.061930 sq. in
Bottom Area	=	201.061930 sq. in
Moment of Inertia at Top	=	1608.495 in ⁴
Moment of Inertia at Bottom	=	1608.495 in ⁴
Elastic Modulus	=	3605000. lbs/in ²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
= 0.000 radians
Pile Batter Angle = 0.000 degrees
= 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 6 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.000 ft
Distance from top of pile to bottom of layer = 0.100 ft

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.100 ft
Distance from top of pile to bottom of layer = 2.000 ft

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 2.000 ft
Distance from top of pile to bottom of layer = 9.500 ft

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Abut 5_Pil_long_Critical Length.1p60

Layer 4 is stiff clay without free water
 Distance from top of pile to top of layer = 9.500 ft
 Distance from top of pile to bottom of layer = 14.500 ft
 Layer 5 is stiff clay without free water
 Distance from top of pile to top of layer = 14.500 ft
 Distance from top of pile to bottom of layer = 19.500 ft
 Layer 6 is stiff clay without free water
 Distance from top of pile to top of layer = 19.500 ft
 Distance from top of pile to bottom of layer = 80.000 ft

(Depth of lowest layer extends 30.00 ft below pile tip)

Effective Unit weight of Soil vs. Depth

Effective unit weight of soil with depth defined using 12 points

Point No.	Depth X ft	Eff. Unit weight pcf
1	-5.00	120.00000
2	0.10	120.00000
3	0.10	120.00000
4	2.00	120.00000
5	2.00	120.00000
6	9.50	120.00000
7	9.50	120.00000
8	14.50	120.00000
9	14.50	125.00000
10	19.50	125.00000
11	19.50	125.00000
12	80.00	125.00000

Summary of Soil Properties

Layer Rqd Subgr. Num. percent	Soil Type (p-y Curve Criteria)	kpy pci	Depth Rock ft	Eff. Unit Emass krm psi	Cohesion Test Type psf	Friction Test Prop. Ang., deg.	qu Elas. psi
1	Stiff Clay w/o Free Water	--	-5.000	120.000	4000.000	--	--
--	0.00	--	0.10000	120.000	4000.000	--	--
2	Stiff Clay w/o Free Water	--	0.10000	120.000	4000.000	--	--
--	0.00	--	2.000	120.000	4000.000	--	--
3	Stiff Clay w/o Free Water	--	2.000	120.000	1500.000	--	--
--	0.00	--	9.500	120.000	1500.000	--	--
4	Stiff Clay w/o Free Water	--	9.500	120.000	3500.000	--	--
--	0.00	--	14.500	120.000	3500.000	--	--
5	Stiff Clay w/o Free Water	--	14.500	125.000	4000.000	--	--
--	0.00	--	19.500	125.000	4000.000	--	--
6	Stiff Clay w/o Free Water	--	19.500	125.000	4500.000	--	--
--	0.00	--	80.000	125.000	4500.000	--	--
--	0.00	--	--	--	--	--	--

Abut 5_Pil_long_Critical Length.1p60
 p-y Modification Factors For Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	1.0000	1.0000
2	50.000	1.0000	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs
1	V =	12000. lbs	M = 0.0000 in-lbs	60000.

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-Curvature properties derived from elastic section properties

Computed values of Pile Loading and Deflection
 For Lateral Loading for Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Horizontal shear force at pile head = 12000.000 lbs
 Applied moment at pile head = 0.000 in-lbs
 Axial thrust load on pile head = 60000.000 lbs

Depth X inches	Deflect. y inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness lb-in^2	Soil Res. p lb/in	Soil Spr. Es*H lb/inch	Distrib. Lat. Load lb/inch
0.00	0.0183	1.677E-09	12000.	-0.000737	298.4155	5.799E+09	-614.1449	100540.	0.000
6.000	0.0139	61211.	8371.6245	-0.000705	602.8523	5.799E+09	-595.3136	256891.	0.000
12.000	0.009863	100967.	4883.1889	-0.000621	800.5853	5.799E+09	-567.4983	345220.	0.000
18.000	0.006449	120256.	1592.7571	-0.000507	896.5210	5.799E+09	-529.3123	492458.	0.000
24.000	0.003781	120445.	-1121.0391	-0.000382	897.4609	5.799E+09	-375.2864	595472.	0.000
30.000	0.001862	107079.	-2758.3449	-0.000265	830.9829	5.799E+09	-170.4822	549485.	0.000
36.000	0.000606	87536.	-3668.0448	-0.000164	733.7817	5.799E+09	-132.7511	1313324.	0.000
42.000	-0.000105	63180.	-3951.1160	-8.591E-05	612.6495	5.799E+09	38.3941	2191204.	0.000
48.000	-0.000424	40184.	-3448.2400	-3.244E-05	498.2745	5.799E+09	129.2313	1826605.	0.000
54.000	-0.000494	21825.	-2646.3840	-3.565E-07	406.9640	5.799E+09	138.0541	1675466.	0.000
60.000	-0.000429	8427.6898	-1821.4165	1.530E-05	340.3314	5.799E+09	136.9351	1916181.	0.000
66.000	-0.000311	-43.0534	-1029.4181	1.963E-05	298.6296	5.799E+09	127.0644	2452637.	0.000
72.000	-0.000193	-3939.4635	-405.0130	1.757E-05	318.0088	5.799E+09	81.0707	2517995.	0.000
78.000	-9.997E-05	-4915.8615	-32.6689	1.299E-05	322.8650	5.799E+09	43.0440	2583353.	0.000

84.000	-3.729E-05	-4340.8436	144.6654	8.202E-06	320.0051	5.799E+09	16.0674	2585595.	0.000
90.000	-1.348E-05	-3185.7818	194.8683	4.308E-06	314.2663	5.799E+09	0.6669	2585595.	0.000
96.000	1.441E-05	-2005.5255	178.2377	1.622E-06	308.3902	5.799E+09	-6.2104	2585595.	0.000
102.000	1.792E-05	-1048.0980	136.4397	4.244E-08	303.6283	5.799E+09	-7.7222	2585595.	0.000
108.000	1.492E-05	-368.2796	93.9833	-6.903E-07	300.2472	5.799E+09	-6.4299	2585595.	0.000
114.000	9.636E-06	-80.1932	52.1922	-8.594E-07	298.8144	5.799E+09	-7.5005	4670451.	0.000
120.000	4.848E-06	258.6307	13.8203	-6.641E-07	299.7018	5.799E+09	-5.2901	6546780.	0.000
126.000	1.667E-06	246.5207	-7.5188	-4.027E-07	299.6416	5.799E+09	-1.8229	6562500.	0.000
132.000	1.545E-08	168.6952	-13.0381	-1.879E-07	299.2545	5.799E+09	-0.0169	6562500.	0.000
138.000	-5.884E-07	90.1984	-11.1581	-5.398E-08	298.8641	5.799E+09	0.6436	6562500.	0.000
144.000	-6.323E-07	34.8370	-7.1526	1.071E-08	298.5888	5.799E+09	0.6916	6562500.	0.000
150.000	-4.599E-07	4.3593	-3.5689	3.099E-08	298.4372	5.799E+09	0.5030	6562500.	0.000
156.000	-2.604E-07	-8.0118	-1.2053	2.910E-08	298.4554	5.799E+09	0.2848	6562500.	0.000
162.000	-1.107E-07	-10.1253	0.0125	1.972E-08	298.4659	5.799E+09	0.1211	6562500.	0.000
168.000	-2.384E-08	-7.8761	0.4540	1.040E-08	298.4547	5.799E+09	0.0261	6562500.	0.000
174.000	1.412E-08	-4.6851	0.4826	3.904E-09	298.4388	5.799E+09	-0.0165	7031250.	0.000
180.000	2.300E-08	-2.0881	0.3467	3.994E-10	298.4259	5.799E+09	-0.0288	7500000.	0.000
186.000	1.892E-08	-0.5255	0.1895	-9.528E-10	298.4181	5.799E+09	-0.0236	7500000.	0.000
192.000	1.157E-08	0.1862	0.0752	-1.128E-09	298.4164	5.799E+09	-0.0145	7500000.	0.000
198.000	5.376E-09	0.3772	0.0116	-8.368E-10	298.4174	5.799E+09	-0.005720	7500000.	0.000
204.000	1.526E-09	0.3262	-0.0143	-4.729E-10	298.4171	5.799E+09	-0.001907	7500000.	0.000
210.000	-2.992E-10	0.2063	-0.0189	-1.975E-10	298.4165	5.799E+09	0.000374	7500000.	0.000
216.000	-8.434E-10	0.0999	-0.0146	-3.902E-11	298.4160	5.799E+09	0.001054	7500000.	0.000
222.000	-7.675E-10	0.0314	-0.008542	2.888E-11	298.4157	5.799E+09	0.000959	7500000.	0.000
228.000	-4.969E-10	-0.002637	-4.374E-11	298.4155	5.799E+09	0.000621	7500000.	0.000	
234.000	-2.429E-10	-0.01043	-0.000915	3.499E-11	298.4156	5.799E+09	0.000341	8425927.	0.000
240.000	-7.697E-11	-0.0136	0.000450	2.054E-11	298.4156	5.799E+09	0.000114	8921570.	0.000
246.000	3.927E-12	-0.008893	0.000776	8.882E-12	298.4156	5.799E+09	-5.839E-06	8921570.	0.000
252.000	2.961E-11	-0.004345	0.000626	2.033E-12	298.4155	5.799E+09	-4.403E-05	8921570.	0.000
258.000	2.832E-11	-0.001381	0.000368	0.000	298.4155	5.799E+09	-4.211E-05	8921570.	0.000
264.000	1.846E-11	6.829E-05	0.000159	-1.608E-12	298.4155	5.799E+09	-2.745E-05	8921570.	0.000
270.000	9.022E-12	0.000529	3.645E-05	-1.299E-12	298.4155	5.799E+09	-1.342E-05	8921570.	0.000
276.000	2.869E-12	0.000507	-1.660E-05	0.000	298.4155	5.799E+09	-4.265E-06	8921570.	0.000
282.000	0.000	0.000330	-2.877E-05	0.000	298.4155	5.799E+09	2.080E-07	8921570.	0.000
288.000	-1.097E-12	0.000162	-2.325E-05	0.000	298.4155	5.799E+09	1.631E-06	8921570.	0.000
294.000	-1.051E-12	5.145E-05	-1.367E-05	0.000	298.4155	5.799E+09	1.563E-06	8921570.	0.000
300.000	0.000	-2.430E-06	-5.918E-06	0.000	298.4155	5.799E+09	1.020E-06	8921570.	0.000
306.000	0.000	-1.960E-05	-1.362E-06	0.000	298.4155	5.799E+09	4.989E-07	8921570.	0.000
312.000	0.000	-1.880E-05	6.121E-07	0.000	298.4155	5.799E+09	1.590E-07	8921570.	0.000
318.000	0.000	-1.238E-05	1.067E-06	0.000	298.4155	5.799E+09	-7.398E-09	8921570.	0.000
324.000	0.000	-6.010E-06	8.633E-07	0.000	298.4155	5.799E+09	-6.045E-08	8921570.	0.000
330.000	0.000	-1.918E-06	5.079E-07	0.000	298.4155	5.799E+09	-5.802E-08	8921570.	0.000
336.000	0.000	8.629E-08	2.202E-07	0.000	298.4155	5.799E+09	-3.789E-08	8921570.	0.000
342.000	0.000	7.262E-07	5.086E-08	0.000	298.4155	5.799E+09	-1.851E-08	8921570.	0.000
348.000	0.000	6.979E-07	-2.258E-08	0.000	298.4155	5.799E+09	-5.925E-09	8921570.	0.000
354.000	0.000	4.561E-07	-3.956E-08	0.000	298.4155	5.799E+09	-2.625E-10	8921570.	0.000
360.000	0.000	2.235E-07	-3.206E-08	0.000	298.4155	5.799E+09	2.240E-09	8921570.	0.000
366.000	0.000	7.147E-08	-1.888E-08	0.000	298.4155	5.799E+09	2.154E-09	8921570.	0.000
372.000	0.000	-3.058E-08	-8.193E-09	0.000	298.4155	5.799E+09	1.408E-09	8921570.	0.000
378.000	0.000	-2.691E-08	-1.900E-09	0.000	298.4155	5.799E+09	6.900E-10	8921570.	0.000
384.000	0.000	-2.590E-08	8.326E-10	0.000	298.4155	5.799E+09	2.208E-10	8921570.	0.000
390.000	0.000	-1.694E-08	1.467E-09	0.000	298.4155	5.799E+09	-9.297E-12	8921570.	0.000
396.000	0.000	-8.312E-09	1.190E-09	0.000	298.4155	5.799E+09	-8.298E-11	8921570.	0.000
402.000	0.000	-2.664E-09	7.015E-10	0.000	298.4155	5.799E+09	-7.995E-11	8921570.	0.000
408.000	0.000	1.081E-10	3.049E-10	0.000	298.4155	5.799E+09	-5.230E-11	8921570.	0.000
414.000	0.000	9.969E-10	7.097E-11	0.000	298.4155	5.799E+09	-2.566E-11	8921570.	0.000
420.000	0.000	9.613E-10	-3.070E-11	0.000	298.4155	5.799E+09	-8.229E-12	8921570.	0.000
426.000	0.000	6.295E-10	-5.441E-11	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
432.000	0.000	3.091E-10	-4.420E-11	0.000	298.4155	5.799E+09	3.074E-12	8921570.	0.000
438.000	0.000	9.926E-11	-2.607E-11	0.000	298.4155	5.799E+09	-2.967E-12	8921570.	0.000
444.000	0.000	-3.812E-12	-1.134E-11	0.000	298.4155	5.799E+09	1.943E-12	8921570.	0.000
450.000	0.000	-3.694E-11	-2.651E-12	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
456.000	0.000	-3.569E-11	1.132E-12	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
462.000	0.000	-2.339E-11	2.018E-12	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
468.000	0.000	-1.150E-11	1.641E-12	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
474.000	0.000	-3.699E-12	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
480.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
486.000	0.000	1.368E-12	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
492.000	0.000	1.325E-12	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
498.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
504.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
510.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
516.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
522.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
528.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
534.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
540.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
546.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
552.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
558.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
564.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
570.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
576.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
582.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000

588.000	0.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
594.000	0.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
600.000	0.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	4460785.	0.000

* This analysis makes computations of pile response using nonlinear moment-curvature relationships. The above values of total stress are computed for combined axial stress and do not equal the actual stresses in concrete and steel in the range of nonlinear bending.

Output verification: Computed forces and moments are within specified convergence limits.

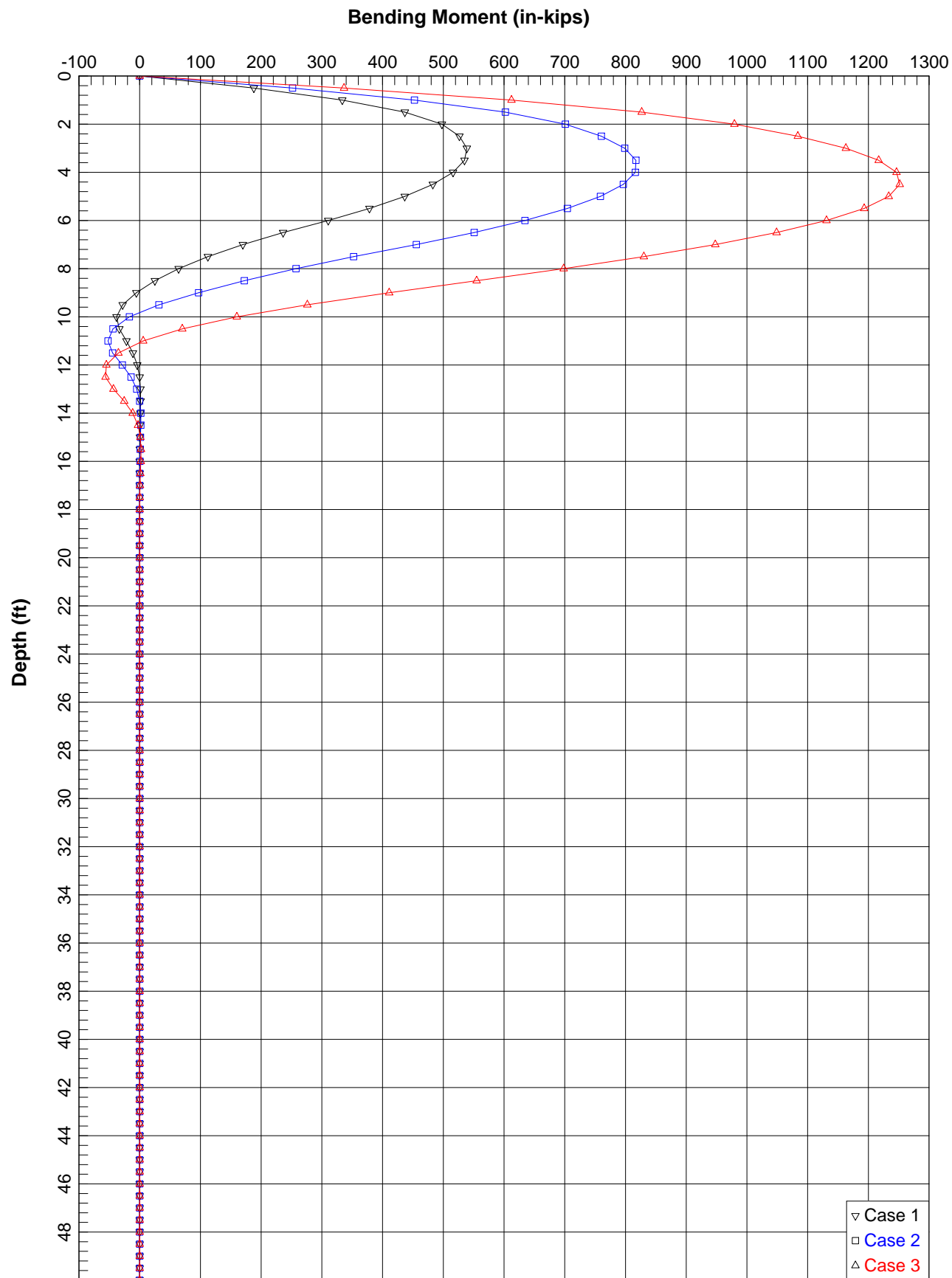
Output Summary for Load Case No. 1:

Pile-head deflection	=</
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Abut 5_Pil_long_Critical Length.1p60

1 1 V = 12000. M = 0.000 60000. 0.01832536 120445. 12000.
-0.00073685

The analysis ended normally.



Abut 5_Pil_long_Ave P.1p60

LPILE Plus for Windows, Version 6 (6.0.25)

Analysis of Individual Piles and Drilled Shafts
Subjected to Lateral Loading Using the p-y Method

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Files Used for Analysis

Path to file locations: N:\Projects\LA\11100\LA1143 PTG - 101 & Palo Comado Cyn\Irvine Foundation
Report\Calculations\Lateral Pile Capacity\Updated_LG_6-05-17\Abut 5\
Name of input data file: Abut 5_Pil_long_Ave P.1p6d
Name of output report file: Abut 5_Pil_long_Ave P.1p6o
Name of plot output file: Abut 5_Pil_long_Ave P.1p6p
Name of runtime message file: Abut 5_Pil_long_Ave P.1p6r

Date and Time of Analysis

Date: June 6, 2017 Time: 10:56:05

Problem Title

Project Name: Palo Comado OC Bridge widen

Job Number: LA-1143

Client: Parson Transportation

Engineer: LG

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 5 Pilaster

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes nonlinear bending stiffness and nominal moment capacity with pile response computed using nonlinear EI

Computation Options:

- Only internally-generated p-y curves used in analysis
- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix elements
- Output pile response for full length of pile
- Analysis assumes no soil movements acting on pile
- No p-y curves to be computed and output for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Abut 5_Pil_long_Ave P.1p60

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
Total Pile Length = 50.00 ft
Depth of ground surface below top of pile = -5.00 ft
Slope angle of ground surface = 0.00 deg.

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.0000000
2	50.00000	16.0000000

Input Structural Properties:

Pile Section No. 1:

Section Type	=	Elastic Pile
Cross-sectional Shape	=	Circular
Section Length	=	50.000 ft
Top Width	=	16.000 in
Bottom Width	=	16.000 in
Top Area	=	201.061930 sq. in
Bottom Area	=	201.061930 sq. in
Moment of Inertia at Top	=	1608.000 in ⁴
Moment of Inertia at Bottom	=	1608.000 in ⁴
Elastic Modulus	=	3605000. lbs/in ²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
= 0.000 radians
Pile Batter Angle = 0.000 degrees
= 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 6 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.000 ft
Distance from top of pile to bottom of layer = 0.100 ft

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.100 ft
Distance from top of pile to bottom of layer = 2.000 ft

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 2.000 ft
Distance from top of pile to bottom of layer = 9.500 ft

Abut 5_Pil_long_Ave P.1p60

Layer 4 is stiff clay without free water
 Distance from top of pile to top of layer = 9.500 ft
 Distance from top of pile to bottom of layer = 14.500 ft
 Layer 5 is stiff clay without free water
 Distance from top of pile to top of layer = 14.500 ft
 Distance from top of pile to bottom of layer = 19.500 ft
 Layer 6 is stiff clay without free water
 Distance from top of pile to top of layer = 19.500 ft
 Distance from top of pile to bottom of layer = 80.000 ft

(Depth of lowest layer extends 30.00 ft below pile tip)

Effective Unit weight of Soil vs. Depth

Effective unit weight of soil with depth defined using 12 points

Point No.	Depth X ft	Eff. Unit weight pcf
1	5.00	120.00000
2	0.10	120.00000
3	0.10	120.00000
4	2.00	120.00000
5	2.00	120.00000
6	9.50	120.00000
7	9.50	120.00000
8	14.50	120.00000
9	14.50	125.00000
10	19.50	125.00000
11	19.50	125.00000
12	80.00	125.00000

Summary of Soil Properties

Layer Rqd Subgr. Num. percent	Soil Type (p-y Curve Criteria)	Epsilon 50 kpy	Depth Rock ft	Eff. Unit Emass krm	Cohesion Test psf	Friction Test Prop. Ang., deg.	qu Elas. psi
1	Stiff Clay w/o Free Water	0.00	5.000	120.000	4000.000	--	--
2	Stiff Clay w/o Free Water	0.00	0.10000	120.000	4000.000	--	--
3	Stiff Clay w/o Free Water	0.00	2.000	120.000	4000.000	--	--
4	Stiff Clay w/o Free Water	0.00	9.500	120.000	1500.000	--	--
5	Stiff Clay w/o Free Water	0.00	14.500	120.000	3500.000	--	--
6	Stiff Clay w/o Free Water	0.00	19.500	125.000	4500.000	--	--
7	Stiff Clay w/o Free Water	0.00	80.000	125.000	4500.000	--	--

Abut 5_Pil_long_Ave P.1p60
 p-y Modification Factors For Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	1.0000	1.0000
2	50.000	1.0000	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs
1	4	y = 0.25000 in	M = 0.0000 in-lbs	60000.
2	4	y = 0.50000 in	M = 0.0000 in-lbs	60000.
3	4	y = 1.00000 in	M = 0.0000 in-lbs	60000.

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-Curvature properties derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 0.250000 inches
 Moment at pile head = 0.000 in-lbs
 Axial load at pile head = 60000.000 lbs

Depth X inches	Deflect. y inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil Res. p lb/in	Soil Spr. Es ^h lb/inch	Distrib. Lat. Load lb/inch
0.00	0.2500	0.000	34535.	-0.005847	298.4155	5.797E+09	-1180.7313	14169.	0.000
6.000	0.2149	188059.	27450.	-0.005750	1234.0349	5.797E+09	-1180.8825	32968.	0.000
12.000	0.1810	333537.	20382.	-0.005480	1957.8042	5.797E+09	-1175.1519	38955.	0.000
18.000	0.1492	436585.	13372.	-0.005081	2470.4803	5.797E+09	-1161.4861	46722.	0.000
24.000	0.1200	497657.	7212.8503	-0.004598	2774.3196	5.797E+09	-891.4806	44565.	0.000
30.000	0.0940	526450.	3173.5497	-0.004068	2917.5683	5.797E+09	-454.9529	29045.	0.000
36.000	0.0712	538668.	494.8738	-0.003517	2978.3569	5.797E+09	-437.9390	36900.	0.000
42.000	0.0518	534920.	-2069.5343	-0.002961	2959.7100	5.797E+09	-416.8637	48302.	0.000
48.000	0.0357	515966.	-4493.5689	-0.002417	2865.4094	5.797E+09	-391.1478	65781.	0.000
54.000	0.0228	482738.	-6746.4284	-0.001900	2700.0959	5.797E+09	-359.8054	94785.	0.000
60.000	0.0129	436377.	-8788.3593	-0.001425	2469.4448	5.797E+09	-320.8382	149541.	0.000
66.000	0.005680	378303.	-10557.	-0.001003	2180.5211	5.797E+09	-268.8430	284001.	0.000
72.000	0.000836	310410.	-11881.	-0.000647	1842.7452	5.797E+09	-172.2299	1236110.	0.000

Node	U	V	W	UX	UY	UZ	MX	MY	MZ	QX	QY	QZ
78.000	-0.002080	236201.	-11739.	-0.00064	1473.5466	5.797E+09	219.2749	632509.	0.000			
80.000	-0.003529	169798.	-10329.	-0.00134	1443.1833	5.797E+09	250.8562	4246749.	0.000			
94.000	-0.003924	112363.	-8803.4603	-7.628E-06	857.4348	5.797E+09	257.6881	394030.	0.000			
96.000	-0.003621	64162.	-7272.6247	8.373E-05	617.6309	5.797E+09	252.5905	418571.	0.000			
102.000	-0.002919	25031.	-5796.8009	0.000130	422.9483	5.797E+09	239.3508	491960.	0.000			
108.000	-0.002062	-5492.8289	-4420.5056	0.000140	325.7430	5.797E+09	219.4143	638420.	0.000			
114.000	-0.001239	-28116.	-2715.5882	0.000123	438.2950	5.797E+09	348.8915	1689324.	0.000			
120.000	-0.000591	-38168.	-450.1672	8.830E-05	488.3069	5.797E+09	406.2488	4125524.	0.000			
126.000	-0.000180	-33581.	1357.6823	5.117E-05	465.4870	5.797E+09	196.3677	6562500.	0.000			
132.000	2.321E-05	-21913.	1870.6262	2.245E-05	407.4345	5.797E+09	-25.3864	6562500.	0.000			
138.000	8.987E-05	-11150.	1499.5739	5.340E-06	353.8882	5.797E+09	-98.2977	6562500.	0.000			
144.000	8.729E-05	-3921.7759	918.2628	-2.460E-06	317.9268	5.797E+09	-95.4727	6562500.	0.000			
150.000	6.035E-05	-129.0906	433.8180	-4.557E-06	299.0578	5.797E+09	-66.0090	6562500.	0.000			
156.000	3.261E-05	1287.3205	128.7859	-3.957E-06	304.8201	5.797E+09	-35.6684	6562500.	0.000			
162.000	1.287E-05	1419.1894	-20.4352	-2.556E-06	305.4762	5.797E+09	-14.0720	6562500.	0.000			
168.000	1.934E-06	1043.9383	-68.9973	-1.282E-06	303.6092	5.797E+09	-2.1154	6562500.	0.000			
174.000	-2.515E-06	592.1446	-66.5033	-4.350E-07	301.3615	5.797E+09	2.9467	7031250.	0.000			
180.000	-3.286E-06	246.2123	-45.3416	-1.115E-09	299.6405	5.797E+09	4.1072	7500000.	0.000			
186.000	-2.528E-06	48.0468	-23.5403	1.512E-07	298.6546	5.797E+09	3.1599	7500000.	0.000			
192.000	-1.472E-06	-36.3805	-8.5418	1.572E-07	298.5965	5.797E+09	1.8396	7500000.	0.000			
198.000	-6.414E-07	-54.5681	0.6177	1.101E-07	298.6870	5.797E+09	0.8018	7500000.	0.000			
204.000	-1.500E-07	-43.8720	2.3501	5.920E-08	298.6338	5.797E+09	0.1875	7500000.	0.000			
210.000	6.894E-08	-26.4095	2.6541	2.282E-08	298.5469	5.797E+09	-0.0862	7500000.	0.000			
216.000	1.239E-07	-12.0396	1.9310	2.925E-09	298.4754	5.797E+09	-0.1548	7500000.	0.000			
222.000	1.040E-07	-3.0298	-0.0833	-1.837E-10	298.4182	5.797E+09	-0.05521	7500000.	0.000			
228.000	6.409E-08	0.8792	0.4458	-6.204E-09	298.4399	5.797E+09	-0.0801	7500000.	0.000			
234.000	2.960E-08	2.1137	0.0807	-4.655E-09	298.4260	5.797E+09	-0.0416	8425927.	0.000			
240.000	8.233E-09	1.8510	-0.0807	-2.603E-09	298.4247	5.797E+09	-0.0122	8921570.	0.000			
246.000	-1.637E-09	1.1469	-0.1101	-1.052E-09	298.4212	5.797E+09	0.002455	8921570.	0.000			
252.000	-4.385E-09	0.5300	-0.0833	-1.837E-10	298.4182	5.797E+09	0.005712	8921570.	0.000			
258.000	-3.842E-09	0.1477	-0.0466	-1.670E-10	298.4163	5.797E+09	0.005712	8921570.	0.000			
264.000	-2.381E-09	-0.0291	-0.0188	2.284E-10	298.4157	5.797E+09	0.003540	8921570.	0.000			
270.000	-1.101E-09	-0.0784	-0.003293	1.728E-10	298.4159	5.797E+09	0.001636	8921570.	0.000			
276.000	-3.069E-10	-0.0687	0.002985	9.673E-11	298.4159	5.797E+09	0.000456	8921570.	0.000			
282.000	6.015E-11	-0.0426	0.004086	3.912E-11	298.4157	5.797E+09	-8.943E-05	8921570.	0.000			
288.000	1.626E-10	-0.0197	0.003092	6.871E-12	298.4156	5.797E+09	-0.000242	8921570.	0.000			
294.000	1.426E-10	-0.005504	0.001731	-6.177E-12	298.4155	5.797E+09	-0.000212	8921570.	0.000			
300.000	8.845E-11	0.001068	0.001068	-8.473E-12	298.4155	5.797E+09	-0.000132	8921570.	0.000			
306.000	4.092E-11	0.002905	0.00123	-0.00129	298.4155	5.797E+09	6.085E-05	8921570.	0.000			
312.000	1.144E-11	0.002500	-0.000110	-3.594E-12	298.4155	5.797E+09	-1.701E-05	8921570.	0.000			
318.000	-2.209E-12	0.001583	-0.000152	-1.455E-12	298.4155	5.797E+09	3.285E-06	8921570.	0.000			
324.000	-6.026E-12	0.000733	-0.000115	0.000	298.4155	5.797E+09	8.961E-06	8921570.	0.000			
330.000	-5.293E-12	0.000205	-6.432E-05	0.000	298.4155	5.797E+09	7.870E-06	8921570.	0.000			
336.000	-3.286E-12	-3.921E-05	-2.605E-05	0.000	298.4155	5.797E+09	4.885E-06	8921570.	0.000			
342.000	-1.522E-12	-0.000108	-4.607E-06	0.000	298.4155	5.797E+09	2.626E-06	8921570.	0.000			
348.000	0.000	-9.466E-05	4.082E-06	0.000	298.4155	5.797E+09	6.338E-07	8921570.	0.000			
354.000	0.000	-5.879E-05	5.621E-06	0.000	298.4155	5.797E+09	-1.206E-07	8921570.	0.000			
360.000	0.000	-2.725E-05	4.263E-06	0.000	298.4155	5.797E+09	-3.322E-07	8921570.	0.000			
366.000	0.000	-7.646E-06	2.390E-06	0.000	298.4155	5.797E+09	-2.921E-07	8921570.	0.000			
372.000	0.000	1.440E-06	9.691E-07	0.000	298.4155	5.797E+09	-1.815E-07	8921570.	0.000			
378.000	0.000	3.992E-06	1.723E-07	0.000	298.4155	5.797E+09	-8.412E-08	8921570.	0.000			
384.000	0.000	3.514E-06	-1.509E-07	0.000	298.4155	5.797E+09	-2.362E-08	8921570.	0.000			
390.000	0.000	2.184E-06	-2.085E-07	0.000	298.4155	5.797E+09	4.429E-09	8921570.	0.000			
396.000	0.000	1.013E-06	-1.583E-07	0.000	298.4155	5.797E+09	1.231E-08	8921570.	0.000			
402.000	0.000	2.850E-07	-8.881E-08	0.000	298.4155	5.797E+09	1.084E-08	8921570.	0.000			
408.000	0.000	-5.286E-08	-3.605E-08	0.000	298.4155	5.797E+09	6.742E-09	8921570.	0.000			
414.000	0.000	-1.480E-07	-6.444E-09	0.000	298.4155	5.797E+09	3.128E-09	8921570.	0.000			
420.000	0.000	-1.304E-07	5.581E-09	0.000	298.4155	5.797E+09	8.804E-10	8921570.	0.000			
426.000	0.000	-8.113E-08	7.734E-09	0.000	298.4155	5.797E+09	-1.626E-10	8921570.	0.000			
432.000	0.000	-3.767E-08	5.877E-09	0.000	298.4155	5.797E+09	-4.565E-10	8921570.	0.000			
438.000	0.000	-1.062E-08	3.300E-09	0.000	298.4155	5.797E+09	-4.025E-10	8921570.	0.000			
444.000	0.000	1.940E-09	1.341E-09	0.000	298.4155	5.797E+09	-2.504E-10	8921570.	0.000			
450.000	0.000	5.485E-09	2.410E-10	0.000	298.4155	5.797E+09	-1.163E-10	8921570.	0.000			
456.000	0.000	4.841E-09	-2.063E-10	0.000	298.4155	5.797E+09	-3.281E-11	8921570.	0.000			
462.000	0.000	3.014E-09	-2.869E-10	0.000	298.4155	5.797E+09	5.970E-12	8921570.	0.000			
468.000	0.000	1.401E-09	-2.182E-10	0.000	298.4155	5.797E+09	1.692E-11	8921570.	0.000			
474.000	0.000	3.958E-10	-1.226E-10	0.000	298.4155	5.797E+09	1.494E-11	8921570.	0.000			
480.000	0.000	-7.122E-11	-4.089E-11	0.000	298.4155	5.797E+09	9.309E-12	8921570.	0.000			
486.000	0.000	-2.033E-10	-9.011E-12	0.000	298.4155	5.797E+09	4.324E-12	8921570.	0.000			
492.000	0.000	-1.797E-10	7.630E-12	0.000	298.4155	5.797E+09	1.223E-12	8921570.	0.000			
498.000	0.000	-1.120E-10	1.064E-11	0.000	298.4155	5.797E+09	0.000	8921570.	0.000			
504.000	0.000	-5.907E-11	8.102E-12	0.000	298.4155	5.797E+09	0.000	8921570.	0.000			
510.000	0.000	-1.474E-11	4.556E-12	0.000	298.4155	5.797E+09	0.000	8921570.	0.000			
516.000	0.000	2.614E-12	1.856E-12	0.000	298.4155	5.797E+09	0.000	8921570.	0.000			
522.000	0.000	7.537E-12	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000			
528.000	0.000	6.670E-12	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000			
534.000	0.000	4.159E-12	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000			
540.000	0.000	1.936E-12	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000			
546.000	0.000	0.000	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000			
552.000	0.000	0.000	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000			
558.000	0.000	0.000	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000			
564.000	0.000	0.000	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000			
570.000	0.000	0.000	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000			
576.000	0.000	0.000	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000			

Node	U	V	W	UX	UY	UZ	MX	MY	MZ	QX	QY	QZ
582.000	0.000	0.000	0.000	0.000	0.000	5.797E+09	0.000	8921570.	0.000			
588.000	0.000	0.000	0.000	0.000	0.000	5.797E+09	0.000	8921570.	0.000			
594.000	0.000	0.000	0.000	0.000	0.000	5.						

Depth	Deflect.	Bending Moment	Shear Force	Slope	Total Stress	Bending Stiffness	Soil Res. p	Soil Spr. Es ^h	Distrib. Lat. Load
x	inches	in-lbs	lbs	radians	psi*	lb-in ²	lb/in	lb/inch	lb/inch
0.00	1.0000	0.000	60045.	-0.0177	298.4355	5.797E+09	-1669.8061	5009.4184	0.000
6.000	0.8941	336567.	49976.	-0.0175	1972.8760	5.797E+09	-1686.4812	11318.	0.000
12.000	0.7903	612294.	39820.	-0.0170	3344.6562	5.797E+09	-1698.6761	12897.	0.000
18.000	0.6902	826624.	29614.	-0.0162	4411.0609	5.797E+09	-1703.5021	14808.	0.000
24.000	0.5953	979355.	20512.	-0.0153	5170.8283	5.797E+09	-1730.3666	13408.	0.000
30.000	0.5065	1083810.	14442.	-0.0142	5690.5055	5.797E+09	-693.1611	8210.5671	0.000
36.000	0.4245	1162908.	10309.	0.0131	6084.0252	5.797E+09	-684.2303	9671.9759	0.000
42.000	0.3496	1216939.	6241.1378	-0.0118	6352.8405	5.797E+09	-671.8753	11531.	0.000
48.000	0.2832	1246330.	2257.8032	-0.0106	6499.0639	5.797E+09	-655.9209	13940.	0.000
54.000	0.2228	1251644.	-1618.1543	-0.009278	6525.5017	5.797E+09	-636.0829	17133.	0.000
60.000	0.1710	1233593.	-5362.7901	-0.00792	6435.6938	5.797E+09	-612.1290	21482.	0.000
66.000	0.1268	1193045.	-8950.1699	-0.006736	6233.9641	5.797E+09	-583.6642	27608.	0.000
72.000	0.0901	1131041.	-12352.	-0.005534	5925.4858	5.797E+09	-550.1563	36624.	0.000
78.000	0.0604	1048810.	-15534.	-0.004406	5516.3753	5.797E+09	-510.7781	50705.	0.000
84.000	0.0373	947800.	-18426.	-0.003372	5013.8378	5.797E+09	-453.0090	72938.	0.000
90.000	0.0210	830138.	-20948.	-0.002452	4428.4076	5.797E+09	-387.6320	116436.	0.000
96.000	0.007840	698193.	-23003.	-0.001661	3772.0114	5.797E+09	-306.8658	234851.	0.000
102.000	4.080E-05	554950.	-24005.	-0.001013	3059.3601	5.797E+09	-17.5805	2585955.	0.000
108.000	-0.004312	410867.	-23265.	-0.000513	2342.5313	5.797E+09	263.9947	367352.	0.000
114.000	-0.006113	276135.	-20912.	-0.000157	1672.2234	5.797E+09	520.3894	510777.	0.000
120.000	-0.006199	166035.	-17155.	6.846E-05	1094.6077	5.797E+09	731.9378	708431.	0.000
126.000	-0.005291	70224.	-12844.	0.000188	647.7887	5.797E+09	705.0815	799502.	0.000
132.000	-0.003948	5770.1584	-8763.6427	0.000227	327.1228	5.797E+09	655.0762	995654.	0.000
138.000	-0.002568	-35103.	-5034.3696	0.000212	473.0578	5.797E+09	588.0149	1373874.	0.000
144.000	-0.001406	-54795.	-1754.0862	0.000165	571.0262	5.797E+09	505.4129	2156264.	0.000
150.000	-0.000585	-56271.	97.7394	0.000108	578.3713	5.797E+09	405.1956	4155713.	0.000
156.000	-0.000113	-43139.	2564.5722	5.632E-05	513.0398	5.797E+09	123.7487	6562500.	0.000
162.000	9.083E-05	-25537.	2637.7881	2.078E-05	425.4643	5.797E+09	-99.3434	6562500.	0.000
168.000	0.000136	11501.	1892.8276	1.611E-06	355.6343	5.797E+09	-148.9768	6562500.	0.000
174.000	0.000110	-2824.0297	1058.6081	-6.846E-06	312.4645	5.797E+09	-139.0964	7031256.	0.000
180.000	6.658E-05	1206.4988	421.6473	-6.839E-06	304.4380	5.797E+09	-83.2239	7500000.	0.000
186.000	3.049E-05	2240.5183	57.6432	-4.856E-06	309.5624	5.797E+09	-38.1100	7500000.	0.000
192.000	8.312E-06	1901.7135	-87.8609	-2.712E-06	307.8768	5.797E+09	-10.3906	7500000.	0.000
198.000	-2.054E-06	1188.1397	-111.3317	-1.113E-06	304.3267	5.797E+09	2.5670	7500000.	0.000
204.000	-5.041E-06	565.5340	-84.7274	-2.047E-07	301.2341	5.797E+09	6.3011	7500000.	0.000
210.000	-4.510E-06	171.5584	-48.9117	-1.773E-07	299.2690	5.797E+09	5.6374	7500000.	0.000
216.000	-2.439E-06	-51.6724	-21.0738	2.554E-07	298.5177	5.797E+09	3.6419	7500000.	0.000
222.000	-1.445E-06	-81.5114	-4.7308	2.026E-07	298.8210	5.797E+09	1.8058	7500000.	0.000
228.000	-4.819E-07	-77.4500	2.4938	1.204E-07	298.8008	5.797E+09	1.6024	7500000.	0.000
234.000	2.439E-06	-51.6724	4.3021	5.354E-08	298.6726	5.797E+09	0.000343	8425927.	0.000
240.000	1.606E-07	-25.8632	3.5869	1.341E-08	298.5442	5.797E+09	-0.2387	8921570.	0.000
246.000	1.607E-07	-8.6387	2.1538	-4.441E-09	298.4585	5.797E+09	-0.2390	8921570.	0.000
252.000	1.073E-07	-0.0148	0.9583	-8.919E-09	298.4156	5.797E+09	-0.1595	8921570.	0.000
258.000	5.370E-08	2.8674	0.2403	-7.443E-09	298.4298	5.797E+09	-0.0798	8921570.	0.000
264.000	-7.994E-08	8.8741	-0.0793	-4.472E-09	298.298	5.797E+09	-0.0267	8921570.	0.000
270.000	3.912E-11	1.9191	-0.1595	-1.991E-09	298.4251	5.797E+09	-5.817E-05	8921570.	0.000
276.000	-5.948E-09	0.9614	-0.1332	-5.003E-10	298.4203	5.797E+09	0.008844	8921570.	0.000
282.000	-5.965E-09	0.3217	-0.0800	1.637E-10	298.4171	5.797E+09	0.008869	8921570.	0.000
288.000	-3.984E-09	0.001088	0.0356	3.307E-10	298.4155	5.797E+09	0.005294	8921570.	0.000
294.000	-1.996E-09	-0.1062	-0.008962	2.763E-10	298.4160	5.797E+09	0.002968	8921570.	0.000
300.000	-6.682E-10	-0.1067	0.002923	1.661E-10	298.4160	5.797E+09	0.000993	8921570.	0.000
306.000	-2.570E-12	-0.0713	0.005914	7.404E-11	298.4159	5.797E+09	3.821E-06	8921570.	0.000
312.000	2.204E-10	-0.0357	0.004943	1.866E-11	298.4157	5.797E+09	-0.000328	8921570.	0.000
318.000	2.213E-10	-0.0120	0.002973	6.033E-12	298.4156	5.797E+09	-0.000329	8921570.	0.000
324.000	1.480E-10	-6.040E-05	0.001325	-1.226E-11	298.4155	5.797E+09	-0.000220	8921570.	0.000
330.000	7.420E-11	0.003935	0.000334	-1.026E-11	298.4155	5.797E+09	-0.000110	8921570.	0.000
336.000	2.488E-11	0.003958	-0.000108	-6.172E-12	298.4155	5.797E+09	-3.699E-05	8921570.	0.000
342.000	0.000	0.002647	-0.000217	-2.753E-12	298.4155	5.797E+09	-2.036E-07	8921570.	0.000
348.000	-8.163E-12	0.001328	-0.00183	0.000	298.4155	5.797E+09	1.214E-05	8921570.	0.000
354.000	-8.214E-12	0.000446	-0.000110	0.000	298.4155	5.797E+09	1.221E-05	8921570.	0.000
360.000	-5.495E-12	2.985E-06	-4.928E-05	0.000	298.4155	5.797E+09	8.171E-06	8921570.	0.000
366.000	-2.758E-12	-0.000146	-1.247E-05	0.000	298.4155	5.797E+09	4.101E-06	8921570.	0.000
372.000	0.000	-0.000147	3.970E-06	0.000	298.4155	5.797E+09	1.377E-06	8921570.	0.000
378.000	0.000	-9.832E-05	8.131E-06	0.000	298.4155	5.797E+09	9.851E-09	8921570.	0.000
384.000	0.000	-4.938E-05	6.812E-06	0.000	298.4155	5.797E+09	-4.497E-07	8921570.	0.000
390.000	0.000	-1.660E-05	4.103E-06	0.000	298.4155	5.797E+09	-4.532E-07	8921570.	0.000
396.000	0.000	-1.384E-07	1.833E-06	0.000	298.4155	5.797E+09	-3.035E-07	8921570.	0.000
402.000	0.000	5.401E-06	4.649E-07	0.000	298.4155	5.797E+09	-1.524E-07	8921570.	0.000
408.000	0.000	5.450E-06	-1.463E-07	0.000	298.4155	5.797E+09	-5.128E-08	8921570.	0.000
414.000	0.000	3.652E-06	-3.015E-07	0.000	298.4155	5.797E+09	-4.509E-10	8921570.	0.000
420.000	0.000	1.835E-06	-2.529E-07	0.000	298.4155	5.797E+09	1.666E-08	8921570.	0.000
426.000	0.000	6.182E-07	-1.524E-07	0.000	298.4155	5.797E+09	1.682E-08	8921570.	0.000
432.000	0.000	6.165E-09	-6.815E-08	0.000	298.4155	5.797E+09	1.137E-08	8921570.	0.000
438.000	0.000	-2.001E-07	-1.734E-08	0.000	298.4155	5.797E+09	5.667E-09	8921570.	0.000
444.000	0.000	-2.023E-07	5.390E-09	0.000	298.4155	5.797E+09	1.909E-09	8921570.	0.000

Abut 5_P11_long_Ave P.1p60

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 1.000000 inches

Moment at pile head = 0.000 in-lbs

Axial load at pile head = 60000.000 lbs

Depth	Deflect.	Bending Moment	Shear Force	Slope	Total Stress	Bending Stiffness	Soil Res. p	Soil Spr. Es ^h	Distrib. Lat. Load
x	inches	in-lbs	lbs	radians	psi*	lb-in ²	lb/in	lb/inch	lb/inch
0.00	1.0000	0.000	60045.	-0.0177	298.4355	5.797E+09	-1669.8061	5009.4184	0.000
6.000	0.8941	336567.	49976.	-0.0175	1972.8760	5.797E+09	-1686.4812	11318.	0.000
12.000	0.7903	612294.	39820.	-0.0170	3344.6562	5.797E+09	-1698.6761	12897.	0.000
18.000	0.6902	826624.	29614.	-0.0162	4411.0609	5.797E+09	-1703.5021	14808.	0.000
24.000	0.5953	979355.	20512.	-0.0153	5170.8283	5.797E+09	-1730.3666	13408.	0.000
30.000	0.5065	1083810.	14442.	-0.0142	5690.5055	5.797E+09	-693.1611	8210.5671	0.000
36.000	0.4245	1162908.	10309.	0.0131	6084.0252	5.797E+09	-684.2303	9671.9759	0.000
42.000	0.3496	1216939.	6241.1378	-0.0118	6352.8405	5.797E+09	-671.8753	11531.	0.000
48.000	0.2832	1246330.	2257.8032	-0.0106	6499.0639	5.797E+09	-655.9209	13940.	0.000
54.000	0.2228	1251644.	-1618.1543	-0.009278	6525.5017	5.797E+09	-636.0829	17133.	0.000
60.000	0.1710	1233593.	-5362.7901	-0.00792	6435.6938	5.797E+09	-612.1290	21482.	0.000
66.000	0.1268	1193045.	-8950.1699	-0.006736	6233.9641	5.797E+09	-583.6642	27608.	0.000
72.000	0.0901	1131041.	-12352.	-0.005534	5925.4858	5.797E+09	-550.1563	36624.	0.000
78.000	0.0604	1048810.	-15534.	-0.004406	5516.3753	5.797E+09	-510.7781	50705.	0.000
84.000	0.0373	947800.	-18426.	-0.003372	5013.8378	5.797E+09	-453.0090	72938.	0.000
90.000	0.0210	830138.	-20948.	-0.002452	4428.4076	5.797E+09	-387.6320	116436.	0.000
96.000	0.007840	698193.	-23003.	-0.001661	3772.0114	5.797E+09	-306.8658	234851.	0.000
102.000	4.080E-05	554950.	-24005.	-0.001013	3059.3601	5.797E+09			

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450.000	0.000	-1.356E-07	1.118E-08	0.000	298.4155	5.797E+09	1.991E-11	8921570.	0.000
456.000	0.000	-6.823E-08	9.386E-09	0.000	298.4155	5.797E+09	-6.171E-10	8921570.	0.000
462.000	0.000	-2.302E-08	5.663E-09	0.000	298.4155	5.797E+09	-6.241E-10	8921570.	0.000
468.000	0.000	-2.670E-10	2.534E-09	0.000	298.4155	5.797E+09	-4.186E-10	8921570.	0.000
474.000	0.000	7.412E-09	6.466E-10	0.000	298.4155	5.797E+09	-2.106E-10	8921570.	0.000
480.000	0.000	7.506E-09	-1.986E-10	0.000	298.4155	5.797E+09	-7.109E-11	8921570.	0.000
486.000	0.000	5.037E-09	-4.145E-10	0.000	298.4155	5.797E+09	0.000	8921570.	0.000
492.000	0.000	2.536E-09	-3.484E-10	0.000	298.4155	5.797E+09	2.286E-11	8921570.	0.000
498.000	0.000	8.569E-10	-2.104E-10	0.000	298.4155	5.797E+09	2.316E-11	8921570.	0.000
504.000	0.000	1.133E-11	-9.424E-11	0.000	298.4155	5.797E+09	1.555E-11	8921570.	0.000
510.000	0.000	-2.746E-10	-2.411E-11	0.000	298.4155	5.797E+09	7.829E-12	8921570.	0.000
516.000	0.000	-2.785E-10	7.318E-12	0.000	298.4155	5.797E+09	2.647E-12	8921570.	0.000
522.000	0.000	-1.871E-10	1.537E-11	0.000	298.4155	5.797E+09	0.000	8921570.	0.000
528.000	0.000	-9.427E-11	1.293E-11	0.000	298.4155	5.797E+09	0.000	8921570.	0.000
534.000	0.000	-3.191E-11	7.815E-12	0.000	298.4155	5.797E+09	0.000	8921570.	0.000
540.000	0.000	0.000	3.504E-12	0.000	298.4155	5.797E+09	0.000	8921570.	0.000
546.000	0.000	1.017E-11	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000
552.000	0.000	1.033E-11	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000
558.000	0.000	6.943E-12	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000
564.000	0.000	3.499E-12	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000
570.000	0.000	1.190E-12	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000
576.000	0.000	0.000	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000
582.000	0.000	0.000	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000
588.000	0.000	0.000	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000
594.000	0.000	0.000	0.000	0.000	298.4155	5.797E+09	0.000	8921570.	0.000
600.000	0.000	0.000	0.000	0.000	298.4155	5.797E+09	0.000	4460765.	0.000

* This analysis makes computations of pile response using nonlinear moment-curvature relationships. The above values of total stress are computed for combined axial stress and do not equal the actual stresses in concrete and steel in the range of nonlinear bending.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

Pile-head deflection = 1.0000000 inches
 Computed slope at pile head = -0.0176526 radians
 Maximum bending moment = 1251644. inch-lbs
 Maximum shear force = 60045. lbs
 Depth of maximum bending moment = 54.0000000 inches below pile head
 Depth of maximum shear force = 0.0000000 inches below pile head
 Number of iterations = 15
 Number of zero deflection points = 14

 Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
 Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
 Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
 Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
 Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

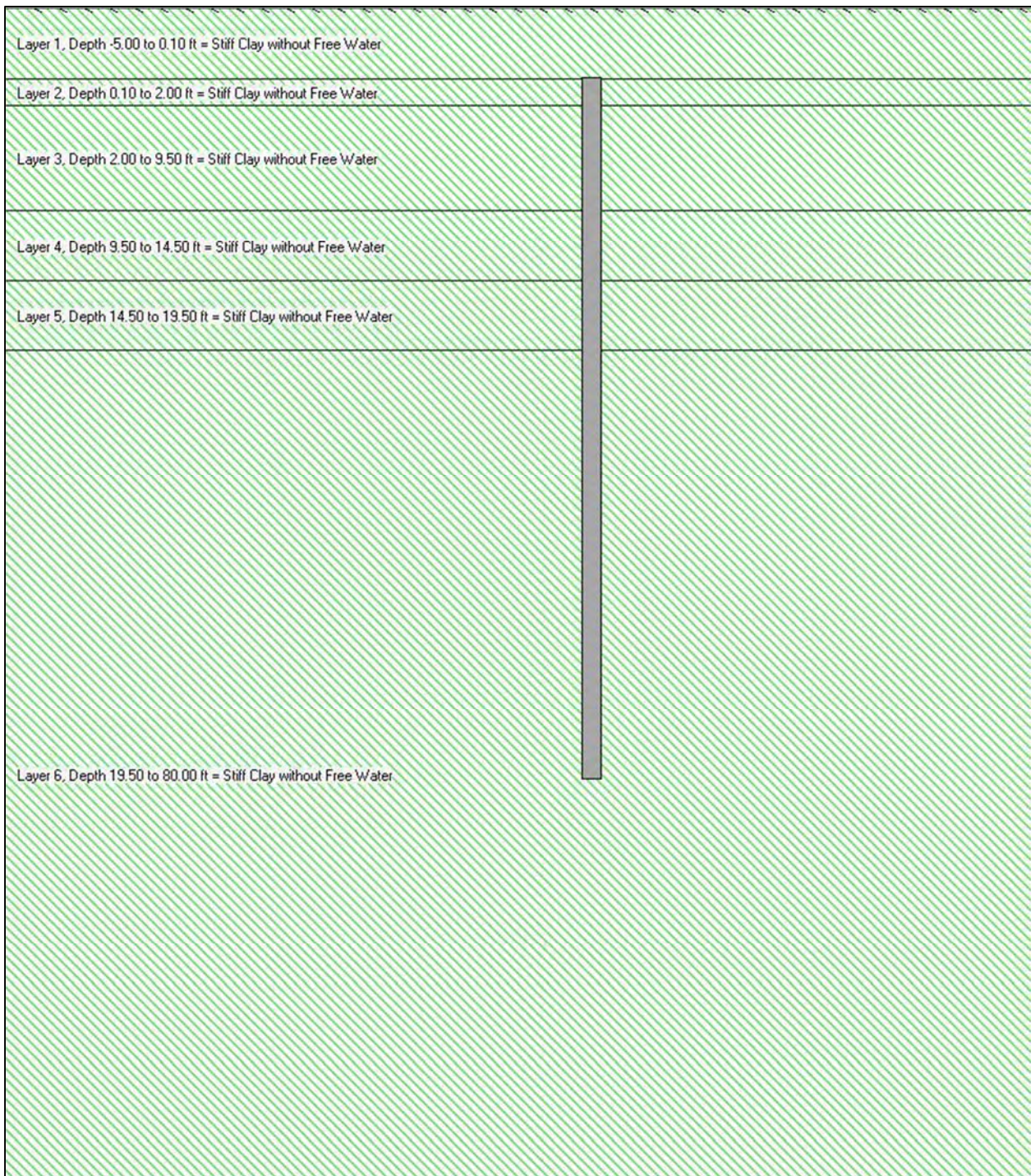
Load Case No.	Load Type	Pile-head Condition 1	Pile-head Condition 2	Axial Loading	Pile-head Deflection	Maximum Moment	Maximum Shear
		v(lbs) or y(inches)	in-lb, rad., or in-lb/rad.	lbs	inches	in-lbs	lbs
1	4	y = 0.2500	M = 0.000	60000.	0.25000000	538668.	34535.
-0.00584721							
2	4	y = 0.5000	M = 0.000	60000.	0.50000000	817242.	45555.
-0.01015495							
3	4	y = 1.0000	M = 0.000	60000.	1.00000000	1251644.	60045.
-0.01765265							

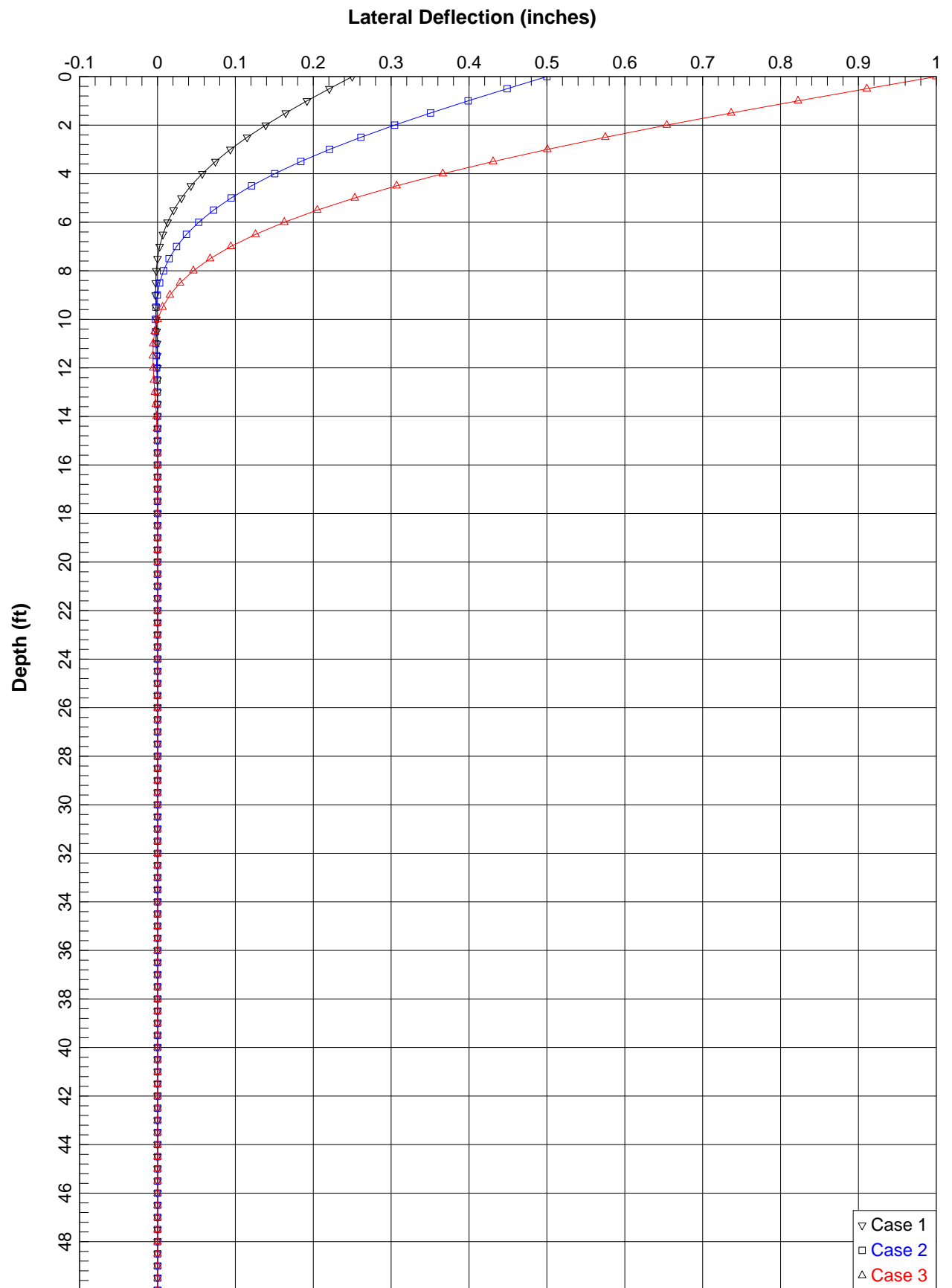
The analysis ended normally.

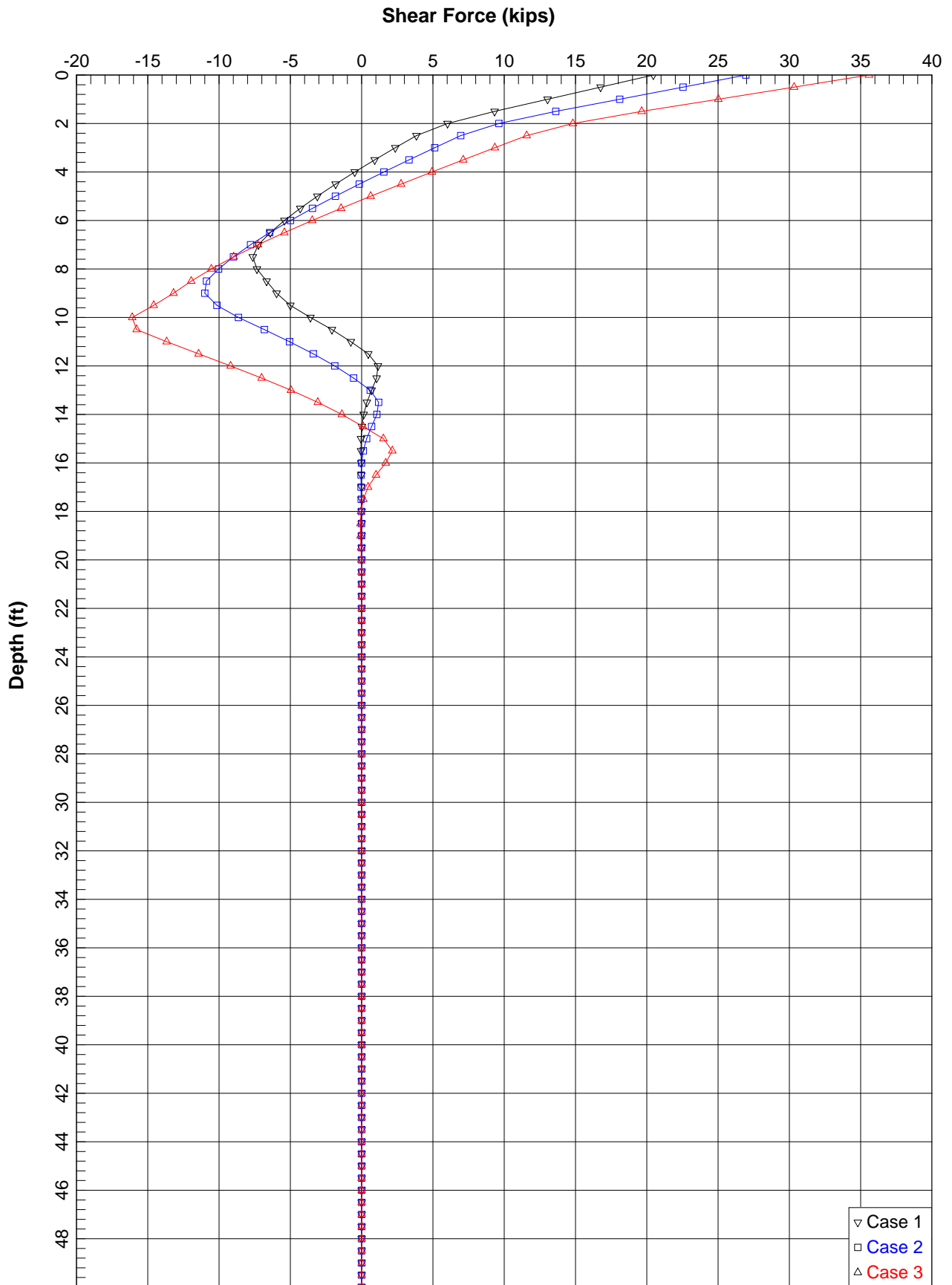
SUPPORT: ABUTMENT 5 PILASTER

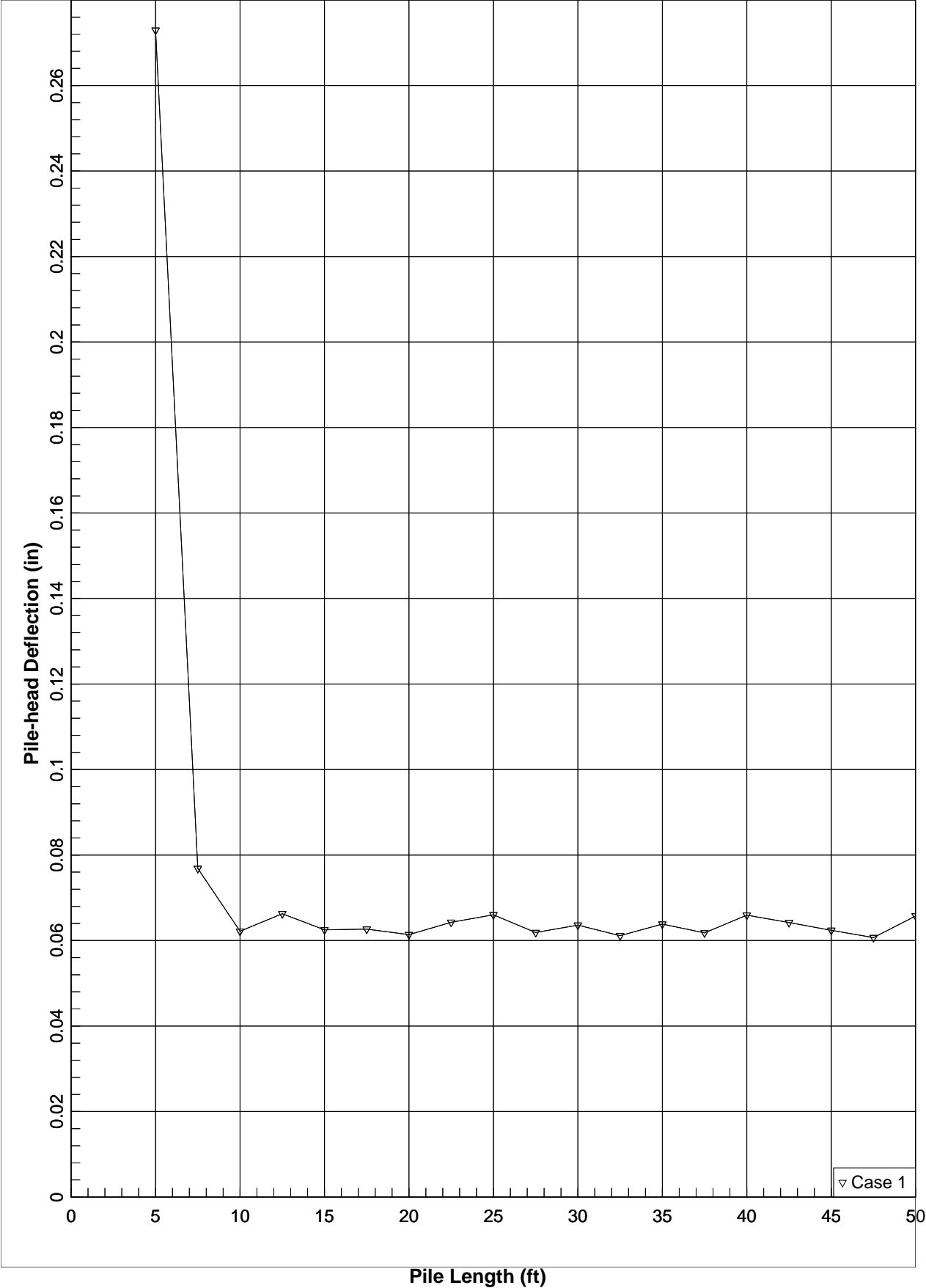
LOAD DIRECTION: TRANSVERSE

1. SOIL-PILE PROFILE PLOT
2. DEFLECTION VS DEPTH PLOT (P-AVG CASE)
3. SHEAR VS. DEPTH PLOT (P-AVG CASE)
4. CRITICAL LENGTH PLOT (P-AVG CASE)
5. OUTPUT FILE FOR CRITICAL LENGTH ANALYSIS (P-AVG CASE)
6. OUTPUT FILE FOR DEFLECTION (P-AVG CASE)
7. SHEAR VS DEPTH PLOT (LEADING ROW CASE)
8. MOMENT VS DEPTH PLOT (LEADING ROW CASE)
9. OUTPUT FILE FOR LEADING ROW CASE









Abut 5_Pil_transv_Critical Length.lp6o

LPILE Plus for Windows, Version 6 (6.0.25)

Analysis of Individual Piles and Drilled Shafts
Subjected to Lateral Loading Using the p-y Method

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Serial Number of Security Device: 156242237
Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: N:\Projects\LA\11100\LA1143 PTG - 101 & Palo Comado Cyn\Irvine Foundation
Report\Calculations\Lateral Pile Capacity\Updated_LG_6-05-17\Abut 5\
Name of input data file: Abut 5_Pil_transv_Critical Length.lp6d
Name of output report file: Abut 5_Pil_transv_Critical Length.lp6o
Name of plot output file: Abut 5_Pil_transv_Critical Length.lp6p
Name of runtime message file: Abut 5_Pil_transv_Critical Length.lp6r

Date and Time of Analysis

Date: June 6, 2017 Time: 17:29:11

Problem Title

Project Name: Palo Comado OC Bridge widen

Job Number: LA-1143

Client: Parson Transportation

Engineer: LG

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 5 Pilaster

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes nonlinear bending stiffness and nominal moment capacity with pile response computed using nonlinear EI

Computation Options:

- Only internally-generated p-y curves used in analysis
- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix elements
- Output pile response for full length of pile
- Analysis assumes no soil movements acting on pile
- No p-y curves to be computed and output for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Abut 5_Pil_transv_Critical Length.lp6o

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
Total Pile Length = 50.00 ft
Depth of ground surface below top of pile = -5.00 ft
Slope angle of ground surface = 0.00 deg.

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:

Section Type	=	Elastic Pile
Cross-sectional Shape	=	Circular
Section Length	=	50.000 ft
Top Width	=	16.000 in
Bottom Width	=	16.000 in
Top Area	=	201.061930 sq. in
Bottom Area	=	201.061930 sq. in
Moment of Inertia at Top	=	1608.495 in ⁴
Moment of Inertia at Bottom	=	1608.495 in ⁴
Elastic Modulus	=	3605000. lbs/in ²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
= 0.000 radians
Pile Batter Angle = 0.000 degrees
= 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 6 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.000 ft
Distance from top of pile to bottom of layer = 0.100 ft

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.100 ft
Distance from top of pile to bottom of layer = 2.000 ft

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 2.000 ft
Distance from top of pile to bottom of layer = 9.500 ft

Abut 5_Pil_transv_critical Length.lp60

Layer 4 is stiff clay without free water
 Distance from top of pile to top of layer = 9.500 ft
 Distance from top of pile to bottom of layer = 14.500 ft
 Layer 5 is stiff clay without free water
 Distance from top of pile to top of layer = 14.500 ft
 Distance from top of pile to bottom of layer = 19.500 ft
 Layer 6 is stiff clay without free water
 Distance from top of pile to top of layer = 19.500 ft
 Distance from top of pile to bottom of layer = 80.000 ft

(Depth of lowest layer extends 30.00 ft below pile tip)

Effective Unit weight of Soil vs. Depth

Effective unit weight of soil with depth defined using 12 points

Point No.	Depth X ft	Eff. Unit weight pcf
1	-5.00	120.00000
2	0.10	120.00000
3	0.10	120.00000
4	2.00	120.00000
5	2.00	120.00000
6	9.50	120.00000
7	9.50	125.00000
8	14.50	125.00000
9	14.50	125.00000
10	19.50	125.00000
11	19.50	125.00000
12	80.00	125.00000

Summary of Soil Properties

Layer Rqd Subgr. Num. percent	Soil Type (p-y Curve Criteria)	Epsilon 50 kpy	Depth Rock ft	Eff. Unit Emass krm	Cohesion Test Type psf	Friction Test Prop. Ang., deg.	qu Elas. psi
1	Stiff Clay w/o Free Water	0.00	-5.000	120.000	4000.000	--	--
2	Stiff Clay w/o Free Water	0.00	0.10000	120.000	4000.000	--	--
3	Stiff Clay w/o Free Water	0.00	2.000	120.000	4000.000	--	--
4	Stiff Clay w/o Free Water	0.00	9.500	120.000	1500.000	--	--
5	Stiff Clay w/o Free Water	0.00	14.500	125.000	3500.000	--	--
6	Stiff Clay w/o Free Water	0.00	19.500	125.000	4500.000	--	--
7	Stiff Clay w/o Free Water	0.00	80.000	125.000	4500.000	--	--

Abut 5_Pil_transv_critical Length.lp60
 p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.5200	1.0000
2	50.000	0.5200	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs
1	V =	12000. lbs	M = 0.0000 in-lbs	60000.

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-Curvature properties derived from elastic section properties

Computed values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Horizontal shear force at pile head = 12000.000 lbs
 Applied moment at pile head = 0.000 in-lbs
 Axial thrust load on pile head = 60000.000 lbs

Depth X inches	Deflect. y inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness lb-in^2	Soil Res. p lb/in	Soil Spr. Es*H lb/inch	Distrib. Lat. Load lb/inch
0.00	0.0658	-2.235E-09	12000.	-0.001691	298.4155	5.799E+09	-439.7289	20063.	0.000
6.000	0.0556	64694.	9366.8509	-0.001658	620.1753	5.799E+09	-437.9875	47259.	0.000
12.000	0.0459	113596.	6752.1203	-0.001565	863.3938	5.799E+09	-433.8894	56724.	0.000
18.000	0.0368	146846.	4174.0442	-0.001431	1028.7681	5.799E+09	-425.7693	69374.	0.000
24.000	0.0287	164714.	1924.1896	-0.001269	1117.6365	5.799E+09	-324.1823	67781.	0.000
30.000	0.0216	170850.	460.2456	-0.001096	1148.1552	5.799E+09	-163.7991	45517.	0.000
36.000	0.0155	171026.	-498.1824	-0.000919	1149.0292	5.799E+09	-155.6769	60078.	0.000
42.000	0.0106	165534.	-1402.2926	-0.000745	1121.7126	5.799E+09	-145.6931	82739.	0.000
48.000	0.006611	154735.	-2239.7120	-0.000579	1068.0030	5.799E+09	-133.4467	121120.	0.000
54.000	0.003617	139074.	-2994.3486	-0.000427	990.1132	5.799E+09	-118.0989	195924.	0.000
60.000	0.001486	119110.	-3640.3280	-0.000293	890.8202	5.799E+09	-97.2276	392545.	0.000
66.000	9.503E-05	95601.	-4048.5455	-0.000182	773.8980	5.799E+09	-38.8450	2452637.	0.000
72.000	-0.000703	70659.	-3910.0965	-9.637E-05	649.8436	5.799E+09	84.9947	725908.	0.000
78.000	-0.001061	48750.	-3365.0354	-3.459E-05	540.8764	5.799E+09	96.6924	546593.	0.000

Node	U	V	W	UX	UY	UZ	MX	MY	MZ	FX	FY	FZ
84.000	-0.001118	30303.	-2780.8411	6.308E-06	449.1317	5.799E+09	98.0390	526327.	0.000			
90.000	-0.000986	15375.	-2201.6869	2.994E-05	374.8845	5.799E+09	95.0124	578340.	0.000			
96.000	-0.000758	3861.4851	-1649.6903	3.989E-05	317.6210	5.799E+09	88.9865	704063.	0.000			
102.000	-0.000507	-4449.9800	-1141.3262	3.959E-05	320.5479	5.799E+09	80.4682	952287.	0.000			
108.000	-0.000283	-9862.9320	-533.6900	3.218E-05	347.4697	5.799E+09	122.0772	2585595.	0.000			
114.000	-0.000121	-10877.	114.6489	2.145E-05	352.5154	5.799E+09	94.0358	4670451.	0.000			
120.000	-2.586E-05	-8502.5907	481.3978	1.143E-05	340.7039	5.799E+09	28.2138	6547288.	0.000			
126.000	1.631E-05	-5108.8851	512.5314	4.384E-06	323.8250	5.799E+09	-17.8359	6562500.	0.000			
132.000	2.675E-05	-2355.3701	371.2440	5.222E-07	310.1302	5.799E+09	-29.2599	6562500.	0.000			
138.000	2.257E-05	-654.3330	209.3947	-1.035E-06	301.6699	5.799E+09	-24.6899	6562500.	0.000			
144.000	1.433E-05	158.1120	88.2949	-1.292E-06	299.2019	5.799E+09	-15.6767	6562500.	0.000			
150.000	7.074E-06	406.1362	18.0532	-9.997E-07	300.4355	5.799E+09	-7.7372	6562500.	0.000			
156.000	2.336E-06	375.4699	-12.8249	-5.953E-07	300.2830	5.799E+09	-2.5555	6562500.	0.000			
162.000	-7.003E-08	252.6656	-20.2617	-2.704E-07	299.6722	5.799E+09	0.0766	6562500.	0.000			
168.000	-9.079E-07	132.5245	-17.0529	-7.108E-08	299.0746	5.799E+09	0.9930	6562500.	0.000			
174.000	-9.230E-07	48.0820	-10.8291	2.236E-08	298.6547	5.799E+09	1.0816	7031250.	0.000			
180.000	-6.396E-07	2.5596	-5.1859	4.856E-08	298.4282	5.799E+09	0.7994	7500000.	0.000			
186.000	-3.402E-07	-14.1839	-1.5117	4.255E-08	298.4861	5.799E+09	0.4253	7500000.	0.000			
192.000	-1.290E-07	-15.6112	0.2480	2.713E-08	298.4932	5.799E+09	0.1612	7500000.	0.000			
198.000	-1.466E-08	-11.2279	0.7867	1.325E-08	298.4714	5.799E+09	0.0183	7500000.	0.000			
204.000	2.996E-08	-6.1808	0.7293	4.240E-09	298.4463	5.799E+09	-0.0375	7500000.	0.000			
210.000	3.622E-08	-2.4798	0.4811	-2.410E-10	298.4279	5.799E+09	-0.0453	7500000.	0.000			
216.000	2.707E-08	-0.4074	0.2438	-1.735E-09	298.4175	5.799E+09	-0.0338	7500000.	0.000			
222.000	1.540E-08	0.4468	0.0845	-1.714E-09	298.4177	5.799E+09	-0.0192	7500000.	0.000			
228.000	6.499E-09	0.5079	0.00297	-1.169E-09	298.4155	5.799E+09	-0.0085	7500000.	0.000			
234.000	1.374E-09	0.4764	-0.0278	-6.077E-10	298.4179	5.799E+09	-0.001929	8425927.	0.000			
240.000	-7.939E-10	0.2752	-0.0300	-2.189E-10	298.4169	5.799E+09	0.001180	8921570.	0.000			
246.000	-1.253E-09	0.1164	-0.0209	-1.624E-11	298.4161	5.799E+09	0.001863	8921570.	0.000			
252.000	-9.887E-10	0.0247	-0.0109	5.678E-11	298.4156	5.799E+09	0.001470	8921570.	0.000			
258.000	-5.714E-10	-0.0141	-0.003920	6.274E-11	298.4156	5.799E+09	0.000895	8921570.	0.000			
264.000	-2.418E-10	-0.0224	-0.000293	4.333E-11	298.4156	5.799E+09	0.000360	8921570.	0.000			
270.000	-5.136E-11	-0.0177	0.000105	2.260E-11	298.4156	5.799E+09	7.636E-05	8921570.	0.000			
276.000	2.931E-11	-0.0102	0.001114	8.152E-12	298.4156	5.799E+09	-4.358E-05	8921570.	0.000			
282.000	4.646E-11	-0.004333	0.000776	0.000000	298.4155	5.799E+09	-6.909E-05	8921570.	0.000			
288.000	3.672E-11	-0.000923	0.000405	-2.102E-12	298.4155	5.799E+09	-5.459E-05	8921570.	0.000			
294.000	2.124E-11	0.000522	0.000146	-2.310E-12	298.4155	5.799E+09	-3.158E-05	8921570.	0.000			
300.000	9.000E-12	0.000831	1.113E-05	-1.610E-12	298.4155	5.799E+09	-1.338E-05	8921570.	0.000			
306.000	1.920E-12	0.000657	-3.758E-05	0.000000	298.4155	5.799E+09	-2.855E-06	8921570.	0.000			
312.000	-1.082E-12	0.000380	-4.132E-05	0.000000	298.4155	5.799E+09	1.609E-06	8921570.	0.000			
318.000	-1.733E-12	0.000161	-2.881E-05	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
324.000	-1.363E-12	3.451E-05	-1.504E-05	0.000000	298.4155	5.799E+09	2.027E-06	8921570.	0.000			
330.000	0.000000	-1.928E-05	-5.438E-06	0.000000	298.4155	5.799E+09	1.174E-06	8921570.	0.000			
336.000	0.000000	-3.080E-05	-4.227E-07	0.000000	298.4155	5.799E+09	4.980E-07	8921570.	0.000			
342.000	0.000000	-2.439E-05	1.391E-06	0.000000	298.4155	5.799E+09	1.067E-07	8921570.	0.000			
348.000	0.000000	-1.413E-05	1.533E-06	0.000000	298.4155	5.799E+09	-5.938E-08	8921570.	0.000			
354.000	0.000000	-6.001E-06	1.070E-06	0.000000	298.4155	5.799E+09	-9.503E-08	8921570.	0.000			
360.000	0.000000	-1.290E-06	5.592E-07	0.000000	298.4155	5.799E+09	-7.528E-08	8921570.	0.000			
366.000	0.000000	7.116E-07	2.025E-07	0.000000	298.4155	5.799E+09	-4.362E-08	8921570.	0.000			
372.000	0.000000	1.142E-06	1.605E-08	0.000000	298.4155	5.799E+09	-1.853E-08	8921570.	0.000			
378.000	0.000000	9.058E-07	-5.151E-08	0.000000	298.4155	5.799E+09	-3.989E-09	8921570.	0.000			
384.000	0.000000	5.252E-07	-5.690E-08	0.000000	298.4155	5.799E+09	2.192E-09	8921570.	0.000			
390.000	0.000000	2.233E-07	-3.975E-08	0.000000	298.4155	5.799E+09	3.524E-09	8921570.	0.000			
396.000	0.000000	4.821E-08	-2.079E-08	0.000000	298.4155	5.799E+09	2.795E-09	8921570.	0.000			
402.000	0.000000	-2.627E-08	-7.542E-09	0.000000	298.4155	5.799E+09	1.621E-09	8921570.	0.000			
408.000	0.000000	-4.237E-08	-6.092E-10	0.000000	298.4155	5.799E+09	6.896E-10	8921570.	0.000			
414.000	0.000000	-3.364E-08	1.907E-09	0.000000	298.4155	5.799E+09	1.491E-10	8921570.	0.000			
420.000	0.000000	-1.952E-08	2.111E-09	0.000000	298.4155	5.799E+09	-8.091E-11	8921570.	0.000			
426.000	0.000000	-8.310E-09	1.477E-09	0.000000	298.4155	5.799E+09	-1.307E-10	8921570.	0.000			
432.000	0.000000	-1.802E-09	7.730E-10	0.000000	298.4155	5.799E+09	-1.038E-10	8921570.	0.000			
438.000	0.000000	9.695E-10	2.809E-10	0.000000	298.4155	5.799E+09	-6.026E-11	8921570.	0.000			
444.000	0.000000	1.571E-09	2.311E-11	0.000000	298.4155	5.799E+09	-2.566E-11	8921570.	0.000			
450.000	0.000000	1.249E-09	-7.059E-11	0.000000	298.4155	5.799E+09	-5.572E-12	8921570.	0.000			
456.000	0.000000	7.255E-10	-7.835E-11	0.000000	298.4155	5.799E+09	2.986E-12	8921570.	0.000			
462.000	0.000000	3.092E-10	-5.485E-11	0.000000	298.4155	5.799E+09	4.848E-12	8921570.	0.000			
468.000	0.000000	6.735E-11	-2.874E-11	0.000000	298.4155	5.799E+09	3.854E-12	8921570.	0.000			
474.000	0.000000	-3.578E-11	-1.046E-11	0.000000	298.4155	5.799E+09	2.240E-12	8921570.	0.000			
480.000	0.000000	-5.828E-11	0.000000	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
486.000	0.000000	-4.638E-12	2.613E-12	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
492.000	0.000000	-2.696E-12	2.907E-12	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
498.000	0.000000	-1.151E-11	2.037E-12	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
504.000	0.000000	-2.517E-12	1.069E-12	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
510.000	0.000000	3.271E-12	0.000000	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
516.000	0.000000	2.161E-12	0.000000	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
522.000	0.000000	1.722E-12	0.000000	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
528.000	0.000000	1.002E-12	0.000000	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
534.000	0.000000	0.000000	0.000000	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
540.000	0.000000	0.000000	0.000000	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
546.000	0.000000	0.000000	0.000000	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
552.000	0.000000	0.000000	0.000000	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
558.000	0.000000	0.000000	0.000000	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
564.000	0.000000	0.000000	0.000000	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
570.000	0.000000	0.000000	0.000000	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
576.000	0.000000	0.000000	0.000000	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			
582.000	0.000000	0.000000	0.000000	0.000000	298.4155	5.799E+09	0.000000	8921570.	0.000			

Node	U	V	W	UX	UY	UZ	MX	MY	MZ
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Case No.	Type No.	V(lbs) or y(inches)	Abut in-lb, rad., or in-lb/rad.	5_Pil_transv_critical Loading lbs	Length.lp60 Deflection inches	Moment in-lbs	Shear lbs
1	1	V = 12000.	M = 0.000	60000.	0.06575341	171026.	12000.
Rotation		-0.00169100					

The analysis ended normally.

Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water

Distance from top of pile to top of layer = 12.00000 ft
 Distance from top of pile to bottom of layer = 17.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4000.00000 psi
 Undrained cohesion at bottom of layer = 4000.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water

Distance from top of pile to top of layer = 17.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type (p-y Curve Criteria)	Rock Mass Depth	Layer Mass Depth	Effective Unit wt.	Undrained Cohesion	In-situ Friction	Angle of Friction	Elastic Mod.	Uniaxial Subgrade Mod.	RQD %	or GSI
Num.	Epsilon 50	J	Rock	Emass	krm	Test	Test	deg.	psi	psi		
		Factor	psi	ft	pcf	psf	Property		Mod. pcf			
1	0.00700	Stiff Clay w/o Free water		-2.000	120.000	4000.000						
	0.00700			0.10000	120.000	4000.000						
2	0.00700	Stiff Clay w/o Free water		0.10000	120.000	1500.000						
	0.00700			7.000	120.000	1500.000						
3	0.00700	Stiff Clay w/o Free water		7.000	120.000	3500.000						
	0.00700			12.000	120.000	3500.000						
4	0.00700	Stiff Clay w/o Free water		12.000	125.000	4000.000						
	0.00700			17.000	125.000	4000.000						
5	0.00500	Stiff Clay w/o Free water		17.000	125.000	4500.000						
	0.00500			80.000	125.000	4500.000						

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X Ft	p-mult	y-mult
1	0.000	0.6200	1.0000
2	50.000	0.6200	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

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Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	4	y = 0.25000 in	M = 0.0000 in-lbs	131000.	False
2	4	y = 0.50000 in	M = 0.0000 in-lbs	131000.	False
3	4	y = 1.00000 in	M = 0.0000 in-lbs	131000.	False

V = perpendicular shear force applied to pile head

M = bending moment applied to pile head

y = lateral deflection relative to pile axis

S = pile slope relative to original pile batter angle

R = rotational stiffness applied to pile head

Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed values of Pile Loading and Deflection

For Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head = 0.250000 inches

Moment at pile head = 0.000 in-lbs

Axial load at pile head = 131000.000 lbs

Depth X inches	Deflect. inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness lb-in ²	Soil Res. p lb/in	Soil Spr. E _s ^H lb/inch	Distrib. Lat. Load lb/inch
0.00	0.2500	0.000	13972.	-0.004592	651.5405	5.799E+09	-510.2695	6123.2345	0.000
6.00	0.1224	78237.	11663.	-0.004552	1040.7569	5.799E+09	-259.2775	6993.4449	0.000
12.00	0.1954	147116.	10100.	-0.004435	1383.2333	5.799E+09	-261.7459	8038.1327	0.000
18.00	0.1692	206432.	8526.4134	-0.004252	1678.2492	5.799E+09	-262.8732	9320.4554	0.000
24.00	0.1444	256117.	6950.0188	-0.004013	1925.3628	5.799E+09	-262.5917	10915.	0.000
30.00	0.1211	296141.	5379.7605	-0.003727	2124.4235	5.799E+09	-260.8277	12926.	0.000
36.00	0.0996	326534.	3824.7764	-0.003405	2275.5853	5.799E+09	-257.5003	15509.	0.000
42.00	0.0802	347391.	2294.7237	-0.003056	2379.3211	5.799E+09	-252.5173	18890.	0.000
48.00	0.0629	358875.	799.8601	-0.002691	2436.4386	5.799E+09	-245.7706	23427.	0.000
54.00	0.0479	361220.	-648.8348	-0.002319	2448.0994	5.799E+09	-237.1278	29695.	0.000
60.00	0.0351	354734.	-2039.4698	-0.001948	2415.8415	5.799E+09	-226.4172	38679.	0.000
66.00	0.0245	339808.	-3358.9203	-0.001589	2341.6088	5.799E+09	-213.3996	52186.	0.000
72.00	0.0161	316924.	-4592.2366	-0.001249	2227.7926	5.799E+09	-197.7059	73875.	0.000
78.00	0.0095	286665.	-5721.4001	-0.000937	2077.2953	5.799E+09	-178.6820	112295.	0.000
84.00	0.004816	249740.	-6857.3593	-0.000659	1893.6456	5.799E+09	-199.9711	249108.	0.000
90.00	0.001636	205413.	-8108.6207	-0.000424	1673.1810	5.799E+09	-217.1161	796083.	0.000
96.00	-0.000268	153103.	-8385.8027	-0.000238	1413.0110	5.799E+09	-124.7221	2787546.	0.000
102.00	-0.001223	105158.	-7370.4246	-0.000105	1174.5531	5.799E+09	-213.7373	1048781.	0.000
108.00	-0.001524	64822.	-6031.3220	-1.671E-05	973.9394	5.799E+09	232.6302	915725.	0.000
114.00	-0.001423	32808.	-4627.7030	3.380E-05	814.7157	5.799E+09	235.2428	991708.	0.000
120.00	-0.001119	9236.5526	-3239.0891	5.556E-05	697.4794	5.799E+09	227.6285	1220971.	0.000
126.00	-0.000757	-6148.0919	-1920.3475	5.715E-05	682.1186	5.799E+09	211.9520	1680856.	0.000
132.00	-0.000433	-13897.	-717.2517	4.678E-05	720.6609	5.799E+09	189.0799	2621576.	0.000
138.00	-0.000195	-14829.	180.1415	3.192E-05	725.2922	5.799E+09	110.0511	3382908.	0.000
144.00	-4.869E-05	-11786.	593.8363	1.815E-05	710.1590	5.799E+09	27.8472	336233.	0.000
150.00	2.263E-05	-7731.1539	635.8219	8.054E-06	689.9922	5.799E+09	-13.8520	3672280.	0.000
156.00	4.696E-05	-4168.7449	505.7781	1.898E-06	672.2742	5.799E+09	-29.4960	3768707.	0.000
162.00	4.541E-05	-1664.8002	319.4335	-1.120E-06	659.8206	5.799E+09	-29.2496	3865197.	0.000
168.00	3.352E-05	-212.4870	173.4055	-2.092E-06	652.5974	5.799E+09	-22.1290	3961571.	0.000
174.00	2.031E-05	443.3537	67.8162	-1.972E-06	653.7456	5.799E+09	-13.7341	4058008.	0.000
180.00	9.850E-06	604.4070	6.1528	-1.430E-06	654.5466	5.799E+09	-6.8204	4154447.	0.000
186.00	3.146E-06	519.4335	319.9393	-8.486E-07	654.1240	5.799E+09	-2.2290	4250889.	0.000
192.00	-3.330E-07	353.7969	-26.9706	-3.968E-07	653.3002	5.799E+09	0.2373	4274851.	0.000
198.00	-1.616E-06	196.4117	-22.8055	-1.122E-07	652.5174	5.799E+09	1.1511	4274851.	0.000
204.00	-1.679E-06	80.3076	-15.3893	3.100E-08	651.9400	5.799E+09	1.3209	4270485.	0.000
210.00	-1.244E-06	11.6914	-8.1735	7.860E-08	651.9887	5.799E+09	1.0843	5231250.	0.000
216.00	-7.358E-07	-17.8983	-2.9959	7.539E-08	651.6296	5.799E+09	0.6415	5231250.	0.000
222.00	-3.390E-07	-24.3784	-0.1845	5.351E-08	651.6618	5.799E+09	0.2956	5231250.	0.000
228.00	-3.864E-08	-20.3968	0.9472	3.045E-08	651.6410	5.799E+09	0.0816	5231250.	0.000
234.00	2.637E-08	-13.0596	1.1232	1.325E-08	651.6055	5.799E+09	-0.0230	5231250.	0.000

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Y	X	Moment	Shear	Slope	Total stress	Bending	Soil Res.	Soil Spr.	Distrib.
inches	inches	in-lbs	lbs	radians	psi*	lb-inA2	lb/in	lb/inch	lb/inch
522.000	0.000	5.721E-09	1.981E-10	0.000	651.5405	5.799E+09	-9.234E-11	5231250.	0.000
528.000	0.000	5.257E-09	-1.747E-10	0.000	651.5405	5.799E+09	-3.191E-11	5231250.	0.000
534.000	0.000	3.639E-09	-2.702E-10	0.000	651.5405	5.799E+09	0.000	5231250.	0.000
540.000	0.000	2.020E-09	-2.330E-10	0.000	651.5405	5.799E+09	1.235E-11	5231250.	0.000
546.000	0.000	8.450E-10	-1.549E-10	0.000	651.5405	5.799E+09	1.369E-11	5231250.	0.000
552.000	0.000	1.616E-10	-8.243E-11	0.000	651.5405	5.799E+09	0.000	5231250.	0.000
558.000	0.000	-1.453E-10	-3.198E-11	0.000	651.5405	5.799E+09	6.355E-12	5231250.	0.000
564.000	0.000	-2.233E-10	-3.810E-12	0.000	651.5405	5.799E+09	3.037E-12	5231250.	0.000
570.000	0.000	-1.918E-10	8.080E-12	0.000	651.5405	5.799E+09	0.000	5231250.	0.000
576.000	0.000	-1.268E-10	1.042E-11	0.000	651.5405	5.799E+09	0.000	5231250.	0.000
582.000	0.000	-6.694E-11	8.395E-12	0.000	651.5405	5.799E+09	0.000	5231250.	0.000
588.000	0.000	-2.612E-11	5.142E-12	0.000	651.5405	5.799E+09	0.000	5231250.	0.000
594.000	0.000	-5.244E-12	2.174E-12	0.000	651.5405	5.799E+09	0.000	5231250.	0.000
600.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	0.000	2615625.	0.000

* The above values of total stress are combined axial and bending stress.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

File-head deflection	=	0.5000000	inches
Computed slope at pile head	=	-0.0082062	radians
Maximum bending moment	=	578428.	inch-lbs
Maximum shear force	=	60.0000000	lbs
Depth of maximum bending moment	=	60.0000000	inches below pile head
Depth of maximum shear force	=	0.0000000	inches below pile head
Number of iterations	=	18	
Number of zero deflection points	=	12	

Computed values of Pile Loading and Deflection
for Lateral Loading for Load Case Number 3

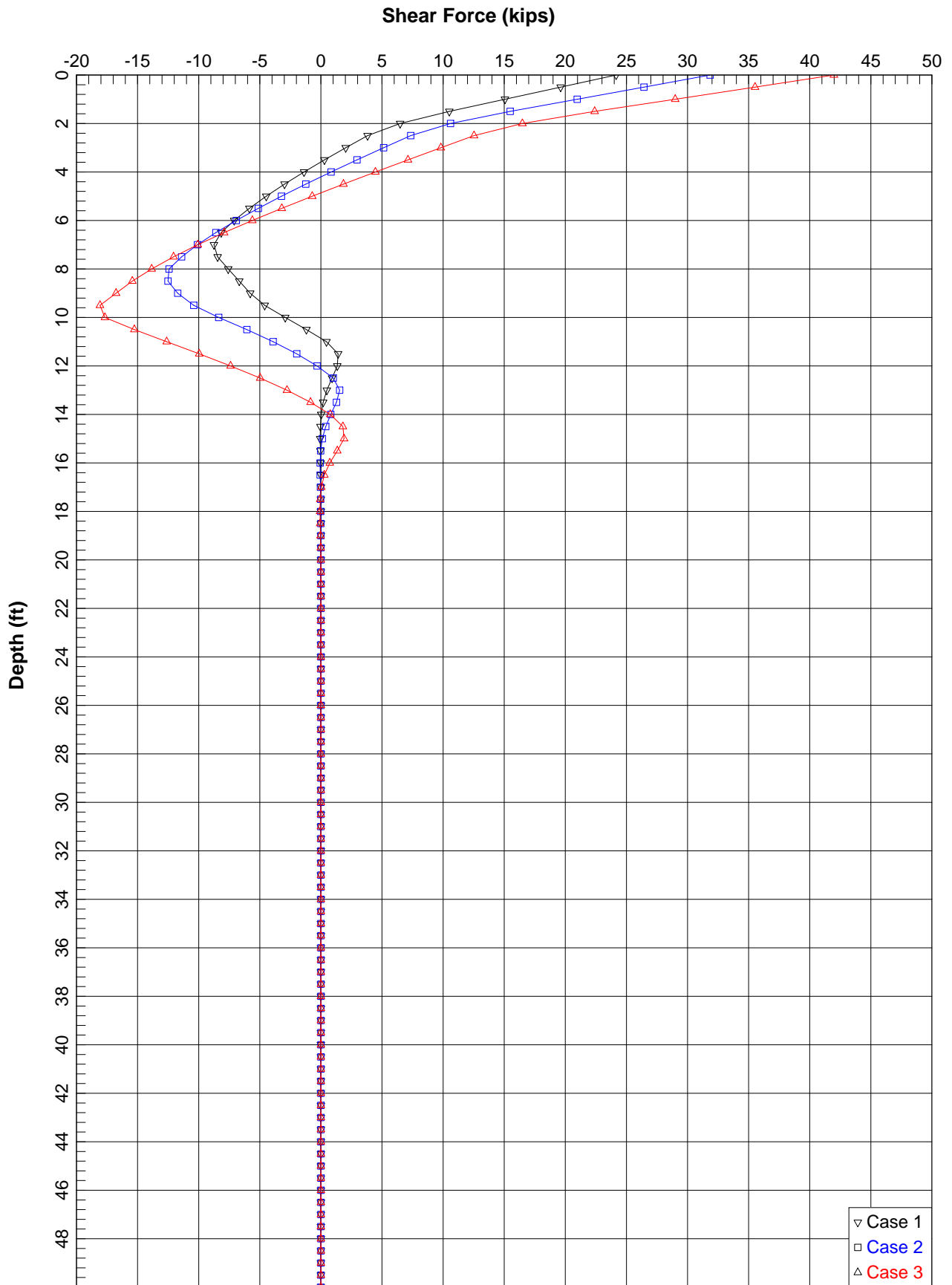
Pile-head conditions are Displacement and Moment (Loading Type 4)									
Displacement of pile head = 1.000000 inches									
Moment at pile head = 578428. inch-lbs									
Axial load at pile head = 131000.000 lbs									
Depth	Deflect.	Bending	Shear	Slope	Total	Bending	Soil Res.	Soil Spr.	Distrib.
inches	inches	in-lbs	lbs	radians	stress	lb-inA2	lb/in	lb/inch	lb/inch
0.00	1.0000	0.000	26088.	-0.0147	651.5405	5.799E+09	-721.6301	2164.8903	0.000
6.00	0.9118	155097.	22817.	-0.0146	1422.9309	5.799E+09	-368.9180	2427.6896	0.000
12.00	0.8245	296787.	20584.	-0.0144	2127.6394	5.799E+09	-375.1533	2729.9961	0.000
18.00	0.7391	424730.	18319.	-0.0140	2763.9765	5.799E+09	-380.0175	3084.9963	0.000
24.00	0.6563	538648.	16028.	-0.0135	3330.5536	5.799E+09	-383.4422	3505.4231	0.000
30.00	0.5769	638323.	13722.	-0.0129	3826.2969	5.799E+09	-385.3552	4008.0309	0.000
36.00	0.5014	723606.	11409.	-0.0122	4250.4606	5.799E+09	-385.6783	4615.2215	0.000
42.00	0.4304	794416.	9098.9396	-0.0114	4602.6418	5.799E+09	-384.3261	5357.4964	0.000
48.00	0.3644	850744.	6802.3518	-0.0106	4882.7963	5.799E+09	-381.2032	6277.2560	0.000
54.00	0.3036	892568.	4530.1392	-0.009666	5091.2554	5.799E+09	-376.2010	7434.8716	0.000
60.00	0.2484	920302.	2293.9601	-0.008728	5228.7451	5.799E+09	-369.1921	8918.7535	0.000
66.00	0.1989	933906.	106.3155	-0.007769	5296.4087	5.799E+09	-360.0228	10863.	0.000
72.00	0.1551	933790.	-2019.2569	-0.006803	5295.8327	5.799E+09	-348.5013	13478.	0.000
78.00	0.1172	920369.	-4067.8911	-0.005844	5229.0807	5.799E+09	-334.3768	17115.	0.000
84.00	0.0850	894162.	-6299.9649	-0.004905	5098.7358	5.799E+09	-409.6478	28910.	0.000
90.00	0.0584	852480.	-9118.0361	-0.004001	4891.4269	5.799E+09	-529.7093	54454.	0.000
96.00	0.0370	791035.	-12170.	-0.003151	4585.8296	5.799E+09	-687.5390	79055.	0.000
102.00	0.0206	711395.	-14934.	-0.002373	4189.7274	5.799E+09	-933.7662	126605.	0.000
108.00	0.008524	615560.	-17310.	-0.001687	3713.0862	5.799E+09	-1358.3875	252267.	0.000
114.00	0.000313	506323.	-18862.	-0.001107	3169.7859	5.799E+09	-158.7936	3042701.	0.000
120.00	0.004754	390958.	-18355.	-0.000642	2596.0057	5.799E+09	-327.5882	413407.	0.000
126.00	-0.007395	287068.	-16245.	-0.000292	2079.2986	5.799E+09	375.7948	304911.	0.000
132.00	-0.008253	196473.	-13928.	-4.138E-05	1628.7160	5.799E+09	396.5046	208822.	0.000
138.00	-0.007891	119092.	-11532.	0.000122	1248.3326	5.799E+09	402.2389	305831.	0.000
144.00	-0.006785	57895.	-9170.3690	0.000214	939.4844	5.799E+09	385.0243	304486.	0.000
150.00	-0.005319	9610.7240	-6828.0036	0.000249	699.3404	5.799E+09	395.7642	446448.	0.000
156.00	-0.003793	-24433.	-4520.8763	0.000242	773.0623	5.799E+09	373.3449	590552.	0.000
162.00	-0.002419	-45017.	-2373.6735	0.000206	875.4380	5.799E+09	342.3227	849013.	0.000
168.00	-0.001325	-53241.	-440.5851	0.000155	916.3388	5.799E+09	302.0401	1368023.	0.000
174.00	-0.000561	-50548.	1215.3506	0.000101	902.9443	5.799E+09	249.9385	2674259.	0.000
180.00	0.000139	-38516.	2949.5445	0.000076	844.5945	5.799E+09	174.5447	4154477.	0.000
186.00	9.852E-05	-24524.	2215.3981	2.229E-05	772.3708	5.799E+09	-69.7966	4250889.	0.000
192.00	0.000157	-12266.	1670.7816	3.374E-06	712.5464	5.799E+09	-111.7423	4274851.	0.000
198.00	0.000139	-4250.2892	1038.4392	-5.171E-06	672.6798	5.799E+09	-99.0385	4274851.	0.000
204.00	9.479E-05	303.4457	517.6002	7.264E-06	552.5524	5.799E+09	52.5524	4720485.	0.000
210.00	5.183E-05	1972.3323	158.2993	-6.139E-06	661.3501	5.799E+09	-45.1924	5231250.	0.000
216.00	2.112E-05	2112.6878	-32.5298	-4.025E-06	662.0482	5.799E+09	-18.4173	5231250.	0.000
222.00	3.530E-06	1588.3028	-57.0155	-2.111E-06	659.4401	5.799E+09	-3.0780	5231250.	0.000
228.00	-4.202E-06	951.8196	-95.2573	-7.964E-07	636.2745	5.799E+09	3.6640	5231250.	0.000
234.00	-6.026E-06	446.4666	-68.5038	-7.293E-08	653.7611	5.799E+09	5.2539	5231250.	0.000
240.00	-5.078E-06	129.8892	-39.4612	2.253E-07	652.1866	5.799E+09	4.4270	5231250.	0.000
246.00	-3.323E-06	-27.4215	-17.4889	2.783E-07	651.6639	5.799E+09	2.8971	5231250.	0.000
252.00	-1.738E-06	-80.4148	-4.2508	2.253E-07	651.9405	5.799E+09	1.5136	5231250.	0.000

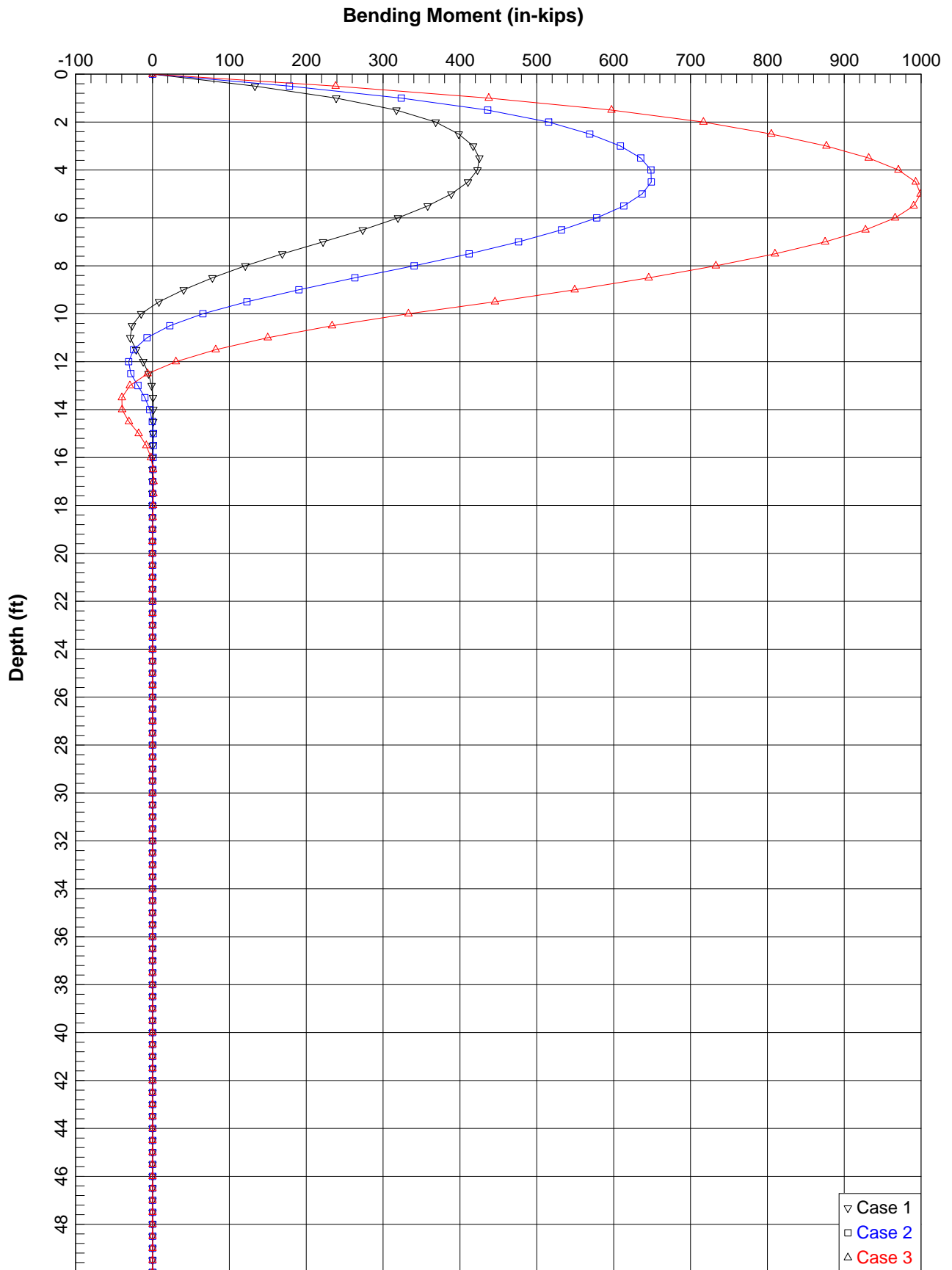
Abut SL_transv_Ave P									
Y	X	Moment	Shear	Slope	Total stress	Bending	Soil Res.	Soil Spr.	Distrib.
inches	inches	in-lbs	lbs	radians	psi*	lb-inA2	lb/in	lb/inch	lb/inch
258.000	-6.531E-07	-78.7814	2.0041	1.401E-07	651.9423	5.799E+09	0.5694	5231250.	0.000
264.000	-5.689E-08	-56.5862	3.8610	7.008E-08	651.8220	5.799E+09	0.0496	5231250.	0.000
270.000	1.880E-07	-32.5592	3.5182	2.396E-08	651.7025	5.799E+09	-0.1639	5231250.	0.000
276.000	2.307E-07	-14.4053	2.4232	-3.341E-10	651.6122	5.799E+09	-0.2011	5231250.	0.000
282.000	1.840E-07	-3.4800	1.3387	-9.587E-09	651.5379	5.799E+09	-0.1604	5231250.	0.000
288.000	1.156E-07	1.6745	0.5552	-1.052E-08	651.5489	5.799E+09	-0.1008	5231250.	0.000
294.000	5.769E-08	3.1984	0.1018	-8.000E-09	651.5565	5.799E+09	-0.5053	5231250.	0.000
300.000	1.962E-08	2.9089	-0.1004	-4.841E-09	651.5550	5.799E+09	-0.1071	5231250.	0.000
306.000	-3.939E-10	2.0013	-0.1507	-2.300E-09	651.5505	5.799E+09	0.000343	5231250.	0.000
312.000	-7.983E-09	1.1043	-0.1288	-6.935E-10	651.5460	5.799E+09	0.006960	5231250.	0.000
318.000	-8.716E-09	0.4570	-0.0851	1.142E-10	651.5428	5.799E+09	0.007600	5231250.	0.000
324.000	-6.612E-09	0.0830	-0.0450	3.936E-10	651.5410	5.799E+09	0.005765	5231250.	0.000
330.000	-3.993E-09	-0.0836	-0.0173	3.933E-10	651.5410	5.799E+09	0.003481	5231250.	0.000
336.000	-1.892E-09	-0.1248	-0.001868	2.855E-10	651.5412	5.799E+09	0.001650	5231250.	0.000
342.000	-5.665E-10	-0.1064	0.004564	1.659E-10	651.5411	5.799E+09	0.000494	5231250.	0.000
348.000	9.850E-11	-0.0703	0.005788	7.448E-11	651.5409	5.799E+09	-8.588E-05	5231250.	0.000
354.000	3.273E-10	-0.0371	0.004674	1.893E-11	651.5407	5.799E+09	-0.000285	5231250.	0.000
360.000	3.257E-10	-0.0142	0.002966	-7.615E-12	651.5406	5.799E+09	-0.000284	5231250.	0.000
366.000	2.359E-10	-0.001503	0.001497	-1.574E-11	651.5406	5.799E+09	-0.000206	5231250.	0.000
372.000	1.368E-10	0.003792	0.000523	-1.456E-11	651.5406	5.799E+09	-0.000119	5231250.	0.000
378.000	6.123E-11	0.004790	4.587E-06	-1.012E-11	651.5406	5.799E+09	-5.339E-05	5231250.	0.000
384.000	1.541E-11	0.003863	-0.000196	-5.639E-12	651.5406	5.799E+09	-1.343E-05	5231250.	0.000
390.000	-6.434E-12	0.002449	-0.000219	-2.373E-12	651.5406	5.799E+09	5.609E-06	5231250.	0.000
396.000	-1.307E-11	0.001235	-0.000168	0.000	651.5406	5.799E+09	1.140E-05	5231250.	0.000
402.000	-1.205E-11	0.000430	-0.000103	0.000	651.5406	5.799E+09	1.050E-05	5231250.	0.000
408.000	-8.355E-12	2.392E-06	-4.926E-05	0.000	651.5405	5.799E+09	7.284E-06	5231250.	0.000
414.000	0.000	0.000	0.000	0.000	651.5405	5.799E+09	4.052E-06	5231250.	0.000
420.000	-1.949E-12	-0.000181	-2.002E-06	0.000	651.5405	5.799E+09	-1.700E-06	5231250.	0.000
426.000	0.000	-0.000139	8.090E-06	0.000	651.5405	5.799E+09	3.297E-07	5231250.	0.0

Abut SL_transv_Ave P

Load Case No.	Load Type No.	Pile-head Condition 1 V(lbs) or y(inches)	Pile-head Condition 2 in-lb, rad. or in-lb/rad.	Axial Loading lbs	Pile-head Deflection inches	Maximum Moment in-lbs	Maximum Shear lbs	Pile-head Rotation radians
1	4	y = 0.2500	M = 0.000	131000.	0.25000000	361220.	13972.	-0.00459231
2	4	y = 0.5000	M = 0.000	131000.	0.50000000	578428.	19052.	-0.00820624
3	4	y = 1.0000	M = 0.000	131000.	1.00000000	933906.	26088.	-0.01470409

The analysis ended normally.





Abut 5_Pil_transv_ Max P.lp6o

LPILE Plus for Windows, Version 6 (6.0.25)

Analysis of Individual Piles and Drilled Shafts
Subjected to Lateral Loading Using the p-y Method

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Serial Number of Security Device: 156242237
Company Name Stored in Security Device: Group Delta Consultants

Files Used for Analysis

Path to file locations: N:\Projects\LA\1100\LA1143 PTG - 101 & Palo Comado Cyn\Irvine Foundation
Report\Calculations\Lateral Pile Capacity\Updated_LG_6-05-17\Abut 5\
Name of input data file: Abut 5_Pil_transv_ Max P.lp6d
Name of output report file: Abut 5_Pil_transv_ Max P.lp6o
Name of plot output file: Abut 5_Pil_transv_ Max P.lp6p
Name of runtime message file: Abut 5_Pil_transv_ Max P.lp6r

Date and Time of Analysis

Date: June 6, 2017 Time: 10:58:14

Problem Title

Project Name: Palo Comado OC Bridge widen

Job Number: LA-1143

Client: Parson Transportation

Engineer: LG

Description: 16 Inch CIDH Lateral Capacity Analysis - Abutment 5 Pilaster

Program Options

Engineering units are US Customary Units: pounds, inches, feet

Basic Program Options:

This analysis computes nonlinear bending stiffness and nominal moment capacity with pile response computed using nonlinear EI

Computation Options:

- Only internally-generated p-y curves used in analysis
- Analysis uses p-y multipliers for group action
- Analysis assumes no shear resistance at pile tip
- Analysis for fixed-length pile or shaft only
- No computation of foundation stiffness matrix elements
- Output pile response for full length of pile
- Analysis assumes no soil movements acting on pile
- No p-y curves to be computed and output for user-specified depths

Solution Control Parameters:

- Number of pile increments = 100
- Maximum number of iterations allowed = 100
- Deflection tolerance for convergence = 1.0000E-05 in
- Maximum allowable deflection = 100.0000 in

Page 1

Abut 5_Pil_transv_ Max P.lp6o

Pile Response Output Options:

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1

Pile Structural Properties and Geometry

Total Number of Sections = 1
Total Pile Length = 50.00 ft
Depth of ground surface below top of pile = -5.00 ft
Slope angle of ground surface = 0.00 deg.

Pile dimensions used for p-y curve computations defined using 2 points. p-y curves are computed using values of pile diameter interpolated over the length of the pile.

Point	Depth X ft	Pile Diameter in
1	0.00000	16.000000
2	50.00000	16.000000

Input Structural Properties:

Pile Section No. 1:

Section Type	=	Elastic Pile
Cross-sectional Shape	=	Circular
Section Length	=	50.000 ft
Top Width	=	16.000 in
Bottom Width	=	16.000 in
Top Area	=	201.061930 sq. in
Bottom Area	=	201.061930 sq. in
Moment of Inertia at Top	=	1608.495 in ⁴
Moment of Inertia at Bottom	=	1608.495 in ⁴
Elastic Modulus	=	3605000. lbs/in ²

Ground Slope and Pile Batter Angles

Ground Slope Angle = 0.000 degrees
= 0.000 radians
Pile Batter Angle = 0.000 degrees
= 0.000 radians

Soil and Rock Layering Information

The soil profile is modelled using 6 layers

Layer 1 is stiff clay without free water

Distance from top of pile to top of layer = -5.000 ft
Distance from top of pile to bottom of layer = 0.100 ft

Layer 2 is stiff clay without free water

Distance from top of pile to top of layer = 0.100 ft
Distance from top of pile to bottom of layer = 2.000 ft

Layer 3 is stiff clay without free water

Distance from top of pile to top of layer = 2.000 ft
Distance from top of pile to bottom of layer = 9.500 ft

Page 2

Abut 5_Pil_transv_ Max P.1p6o

Layer 4 is stiff clay without free water
 Distance from top of pile to top of layer = 9.500 ft
 Distance from top of pile to bottom of layer = 14.500 ft
 Layer 5 is stiff clay without free water
 Distance from top of pile to top of layer = 14.500 ft
 Distance from top of pile to bottom of layer = 19.500 ft
 Layer 6 is stiff clay without free water
 Distance from top of pile to top of layer = 19.500 ft
 Distance from top of pile to bottom of layer = 80.000 ft

(Depth of lowest layer extends 30.00 ft below pile tip)

Effective Unit weight of Soil vs. Depth

Effective unit weight of soil with depth defined using 12 points

Point No.	Depth X ft	Eff. Unit weight pcf
1	5.00	120.00000
2	0.10	120.00000
3	0.10	120.00000
4	2.00	120.00000
5	2.00	120.00000
6	9.50	120.00000
7	9.50	120.00000
8	14.50	120.00000
9	14.50	125.00000
10	19.50	125.00000
11	19.50	125.00000
12	80.00	125.00000

Summary of Soil Properties

Layer Rqd Subgr. Num. percent	Soil Type (p-y Curve Criteria)	Epsilon 50 kpy	Depth Rock ft	Eff. Unit Emass krm	Cohesion Test Type psf	Friction Test Prop. Ang., deg.	qu Elas. psi
1	Stiff Clay w/o Free Water	0.00	5.000	120.000	4000.000	--	--
2	Stiff Clay w/o Free Water	0.00	0.10000	120.000	4000.000	--	--
3	Stiff Clay w/o Free Water	0.00	2.000	120.000	4000.000	--	--
4	Stiff Clay w/o Free Water	0.00	9.500	120.000	1500.000	--	--
5	Stiff Clay w/o Free Water	0.00	14.500	120.000	3500.000	--	--
6	Stiff Clay w/o Free Water	0.00	19.500	125.000	4500.000	--	--
7	Stiff Clay w/o Free Water	0.00	80.000	125.000	4500.000	--	--

Abut 5_Pil_transv_ Max P.1p6o
 p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	0.6400	1.0000
2	50.000	0.6400	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 3

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs
1	4	y = 0.25000 in	M = 0.0000 in-lbs	60000.
2	4	y = 0.50000 in	M = 0.0000 in-lbs	60000.
3	4	y = 1.00000 in	M = 0.0000 in-lbs	60000.

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-Curvature properties derived from elastic section properties

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 0.250000 inches
 Moment at pile head = 0.000 in-lbs
 Axial load at pile head = 60000.000 lbs

Depth X inches	Deflect. y inches	Bending Moment in-lbs	Shear Force lbs	Slope S radians	Total Stress psi*	Bending Stiffness lb-in^2	Soil Res. p lb/in	Soil Spr. Es^h lb/inch	Distrib. Lat. Load lb/inch
0.00	0.2500	0.000	24160.	-0.005178	298.4155	5.799E+09	-755.6680	9068.0160	0.000
6.000	0.2189	133221.	19615.	-0.005109	961.0017	5.799E+09	-759.2649	20808.	0.000
12.000	0.1887	239059.	15057.	-0.004917	1487.3952	5.799E+09	-759.9484	24165.	0.000
18.000	0.1599	317449.	10508.	-0.004629	1877.2776	5.799E+09	-756.4066	28377.	0.000
24.000	0.1331	368491.	6482.5232	-0.004274	2131.1377	5.799E+09	-585.5144	26386.	0.000
30.000	0.1086	398316.	3820.2849	-0.003877	2279.4793	5.799E+09	-301.8984	16673.	0.000
36.000	0.0866	417126.	2031.6250	-0.003455	2373.0281	5.799E+09	-294.3216	20387.	0.000
42.000	0.0672	425184.	294.5694	-0.003019	2413.1061	5.799E+09	-284.6969	25426.	0.000
48.000	0.0504	422834.	-1378.0437	-0.002581	2401.4216	5.799E+09	-272.8407	32491.	0.000
54.000	0.0362	410505.	-2972.0501	-0.002150	2340.1018	5.799E+09	-258.4947	42829.	0.000
60.000	0.0246	388718.	-4471.3132	-0.001736	2231.7381	5.799E+09	-241.2396	58868.	0.000
66.000	0.0154	358100.	-5856.3942	-0.001350	2079.4569	5.799E+09	-220.4340	85995.	0.000
72.000	0.008393	319413.	-7101.2889	-0.000999	1887.0437	5.799E+09	-194.5309	139062.	0.000

Abut 5_Pil_transv Max P_Lp60									
Node	X	Y	Z	U	V	W	MX	MY	MZ
78.000	0.003390	273604	-8162.3877	-0.000692	1659.2081	5.799E+09	-159.1687	281753.	0.000
84.000	8.444E-05	221963.	-8749.0521	-0.000436	1402.3635	5.799E+09	-36.3861	2585593.	0.000
90.000	-0.001843	168929.	-8448.9624	-0.000234	1138.5989	5.799E+09	136.4160	444198.	0.000
96.000	-0.002721	120743.	-7588.4423	-8.392E-05	898.9434	5.799E+09	150.4240	331703.	0.000
102.000	-0.002850	77928.	-6680.7468	1.887E-05	685.9976	5.799E+09	152.1411	320339.	0.000
108.000	-0.002495	40561.	-5783.0338	8.017E-05	500.1481	5.799E+09	147.0966	353809.	0.000
114.000	-0.001888	8473.8688	-4598.8180	0.000106	340.5611	5.799E+09	247.6200	787178.	0.000
120.000	-0.001228	-14701.	-2921.5935	0.000102	371.5326	5.799E+09	311.4328	1521631.	0.000
126.000	-0.000660	-26659.	-1186.7220	8.092E-05	431.0061	5.799E+09	266.8577	2426913.	0.000
132.000	-0.000257	-29000.	457.0585	5.212E-05	442.6496	5.799E+09	281.0692	6562500.	0.000
138.000	-3.425E-05	-21212.	1412.6548	2.615E-05	403.9141	5.799E+09	37.4629	6562500.	0.000
144.000	5.678E-05	-12067.	1338.7223	8.930E-06	358.4316	5.799E+09	-62.1071	6562500.	0.000
150.000	7.290E-05	-5153.5113	913.1882	2.032E-08	324.0470	5.799E+09	-79.7376	6562500.	0.000
156.000	5.703E-05	-1108.7063	486.8542	-3.220E-06	303.9298	5.799E+09	-62.3737	6562500.	0.000
162.000	3.427E-05	691.0572	187.2891	-3.438E-06	301.8526	5.799E+09	-37.4813	6562500.	0.000
168.000	1.580E-05	1141.2366	23.0010	-2.488E-06	304.0916	5.799E+09	-17.2814	6562500.	0.000
174.000	4.417E-06	968.8598	-44.3715	-1.396E-06	303.2342	5.799E+09	-5.1761	7031250.	0.000
180.000	-9.513E-07	609.7838	-56.3323	-5.792E-07	301.4483	5.799E+09	-5.1891	7500000.	0.000
186.000	-2.534E-06	293.2893	-43.2634	-1.120E-07	299.8742	5.799E+09	3.1672	7500000.	0.000
192.000	-2.295E-06	90.7042	-25.1542	8.666E-08	298.8666	5.799E+09	2.8692	7500000.	0.000
198.000	-1.494E-06	-8.6240	-10.9449	1.291E-07	298.4584	5.799E+09	1.8673	7500000.	0.000
204.000	-7.458E-07	-40.7271	-2.5462	1.036E-07	298.6181	5.799E+09	0.9323	7500000.	0.000
210.000	-2.507E-07	-39.2524	-1.1909	6.222E-08	298.6107	5.799E+09	0.3134	7500000.	0.000
216.000	7.452E-10	-26.4816	-2.1282	2.821E-08	298.5472	5.799E+09	-0.000931	7500000.	0.000
222.000	3.347E-10	-13.7346	-1.7962	7.400E-09	298.4635	5.799E+09	-0.000498	7500000.	0.000
228.000	8.955E-08	-4.9325	-1.1312	-2.257E-09	298.4401	5.799E+09	-0.1119	7500000.	0.000
234.000	6.069E-08	-0.1583	0.5397	-4.891E-09	298.4163	5.799E+09	-0.0852	8425927.	0.000
240.000	3.085E-08	1.5477	0.1464	-4.172E-09	298.4232	5.799E+09	-0.0459	8921570.	0.000
246.000	1.062E-08	1.6015	-0.0386	-2.543E-09	298.4235	5.799E+09	-0.0158	8921570.	0.000
252.000	3.347E-10	1.0862	0.0875	-1.153E-09	298.4209	5.799E+09	-0.009498	8921570.	0.000
258.000	-3.209E-09	0.5525	-0.0747	-3.048E-10	298.4183	5.799E+09	0.004772	8921570.	0.000
264.000	-3.323E-09	0.1905	-0.0455	7.957E-11	298.4165	5.799E+09	0.004942	8921570.	0.000
270.000	-2.255E-09	0.006234	-0.0206	1.813E-10	298.4155	5.799E+09	0.003352	8921570.	0.000
276.000	-1.147E-09	-0.0573	-0.005463	1.549E-10	298.4158	5.799E+09	0.001706	8921570.	0.000
282.000	-3.577E-10	-0.00594	0.001420	9.451E-11	298.4158	5.799E+09	0.000588	8921570.	0.000
288.000	-1.316E-11	-0.0404	0.003243	4.288E-11	298.4157	5.799E+09	1.957E-05	8921570.	0.000
294.000	1.189E-10	-0.0205	0.002772	1.137E-11	298.4156	5.799E+09	-0.000177	8921570.	0.000
300.000	1.233E-10	-0.007095	0.001692	-2.925E-12	298.4156	5.799E+09	-0.000183	8921570.	0.000
306.000	8.376E-11	-0.000764	-6.723E-09	-0.007612	298.4155	5.799E+09	-0.000125	8921570.	0.000
312.000	4.286E-11	0.002123	0.000204	-5.751E-12	298.4155	5.799E+09	-6.343E-05	8921570.	0.000
318.000	1.474E-11	0.002206	-5.219E-05	-3.512E-12	298.4155	5.799E+09	-2.192E-05	8921570.	0.000
324.000	0.000	0.001499	-0.000120	-1.595E-12	298.4155	5.799E+09	-7.676E-07	8921570.	0.000
330.000	-4.402E-12	0.000784	-0.000103	0.000	298.4155	5.799E+09	6.545E-06	8921570.	0.000
336.000	-4.577E-12	0.000654	-6.286E-05	0.000	298.4155	5.799E+09	6.806E-06	8921570.	0.000
342.000	-3.111E-12	9.576E-06	-2.856E-05	0.000	298.4155	5.799E+09	4.626E-06	8921570.	0.000
348.000	-1.586E-12	-7.861E-05	-7.607E-06	0.000	298.4155	5.799E+09	2.359E-06	8921570.	0.000
354.000	0.000	-8.186E-05	1.918E-06	0.000	298.4155	5.799E+09	8.165E-07	8921570.	0.000
360.000	0.000	-5.568E-05	4.458E-06	0.000	298.4155	5.799E+09	3.002E-08	8921570.	0.000
366.000	0.000	-2.841E-05	3.821E-06	0.000	298.4155	5.799E+09	-2.424E-07	8921570.	0.000
372.000	0.000	-9.846E-06	2.336E-06	0.000	298.4155	5.799E+09	-2.526E-07	8921570.	0.000
378.000	0.000	-3.738E-07	1.063E-06	0.000	298.4155	5.799E+09	-1.719E-07	8921570.	0.000
384.000	0.000	2.911E-06	2.838E-07	0.000	298.4155	5.799E+09	-8.770E-08	8921570.	0.000
390.000	0.000	3.038E-06	-7.051E-08	0.000	298.4155	5.799E+09	-3.041E-08	8921570.	0.000
396.000	0.000	2.069E-06	-1.653E-07	0.000	298.4155	5.799E+09	-1.171E-09	8921570.	0.000
402.000	0.000	1.056E-06	-1.419E-07	0.000	298.4155	5.799E+09	8.977E-09	8921570.	0.000
408.000	0.000	3.668E-07	-6.880E-08	0.000	298.4155	5.799E+09	9.374E-09	8921570.	0.000
414.000	0.000	1.456E-08	-3.953E-08	0.000	298.4155	5.799E+09	6.385E-09	8921570.	0.000
420.000	0.000	-1.078E-07	-1.059E-08	0.000	298.4155	5.799E+09	3.261E-09	8921570.	0.000
426.000	0.000	-1.127E-07	2.592E-09	0.000	298.4155	5.799E+09	1.133E-09	8921570.	0.000
432.000	0.000	-7.684E-08	6.127E-09	0.000	298.4155	5.799E+09	4.557E-11	8921570.	0.000
438.000	0.000	-3.928E-08	5.267E-09	0.000	298.4155	5.799E+09	-3.324E-10	8921570.	0.000
444.000	0.000	-1.366E-08	3.226E-09	0.000	298.4155	5.799E+09	-3.479E-10	8921570.	0.000
450.000	0.000	-5.658E-10	1.470E-09	0.000	298.4155	5.799E+09	-2.372E-10	8921570.	0.000
456.000	0.000	3.993E-09	3.952E-10	0.000	298.4155	5.799E+09	-1.213E-10	8921570.	0.000
462.000	0.000	4.184E-09	-9.523E-11	0.000	298.4155	5.799E+09	-4.220E-11	8921570.	0.000
468.000	0.000	2.855E-09	-2.271E-10	0.000	298.4155	5.799E+09	-1.770E-12	8921570.	0.000
474.000	0.000	1.460E-09	-1.955E-10	0.000	298.4155	5.799E+09	1.231E-11	8921570.	0.000
480.000	0.000	5.089E-10	-1.138E-05	0.000	298.4155	5.799E+09	1.291E-06	8921570.	0.000
486.000	0.000	2.195E-11	-5.470E-11	0.000	298.4155	5.799E+09	8.811E-12	8921570.	0.000
492.000	0.000	-1.479E-10	-1.474E-11	0.000	298.4155	5.799E+09	4.509E-12	8921570.	0.000
498.000	0.000	-1.553E-10	3.499E-12	0.000	298.4155	5.799E+09	1.572E-12	8921570.	0.000
504.000	0.000	-1.061E-10	8.421E-12	0.000	298.4155	5.799E+09	1.100E-12	8921570.	0.000
510.000	0.000	-5.430E-11	-7.255E-12	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
516.000	0.000	-1.896E-11	4.454E-12	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
522.000	0.000	0.000	2.035E-12	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
528.000	0.000	5.475E-12	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
534.000	0.000	5.762E-12	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
540.000	0.000	3.939E-12	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
546.000	0.000	2.019E-12	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
552.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
558.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
564.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
570.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
576.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000

Abut 5_Pil_transv Max P_Lp60										
Node	X	Y	Z	U	V	W	MX	MY	MZ	
582.000	0.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
588.000	0.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
594.000	0.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
600.000	0.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	4460785.	0.000

* This analysis makes computations of pile response using nonlinear moment-curvature relationships. The above values of total stress are computed for combined axial stress and do not equal the actual stresses in concrete and steel in the range of nonlinear bending.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 1:

Pile-head deflection	=	0.2500000 inches
Computed slope at pile head	=	-0.0051782 radians
Maximum bending moment	=	425184. inch-lbs
Maximum shear force	=	24160. lbs
Depth of maximum bending moment	=	42.000000 inches below pile head
Depth of maximum shear force	=	0.000000 inches below pile head
Number of iterations	=	13
Number of zero deflection points	=	14

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 2

Pile-head conditions are Displacement and Moment (Loading Type 4)

Displacement of pile head	=	0.500000 inches
Moment at pile head	=	0.000 in-lbs
Axial load at pile head	=	60000.00 lbs

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Abut 5_Pil_transv_Max P_Lp60									
Depth	Deflect.	Bending Moment	Shear Force	Slope	Total Stress	Bending Stiffness	Soil Res. p	Soil Spr. Es^h	Distrib. Lat. Load
x	y	in-lbs	lbs	radians	psi*	lb-in^2	lb/in	lb/inch	lb/inch
264.000	4.151E-09	1.3710	-0.0772	-1.765E-09	298.4223	5.799E+09	-0.006172	8921570.	0.000
270.000	-2.186E-09	0.7974	-0.0859	-6.436E-10	298.4193	5.799E+09	-0.003250	8921570.	0.000
276.000	-3.572E-09	0.3404	-0.0602	-5.497E-11	298.4172	5.799E+09	0.005312	8921570.	0.000
282.000	-2.845E-09	0.0746	-0.0316	1.598E-10	298.4159	5.799E+09	0.004231	8921570.	0.000
288.000	-1.655E-09	-0.0389	-0.0115	1.782E-10	298.4157	5.799E+09	0.002461	8921570.	0.000
294.000	-7.070E-10	-0.0639	-0.000990	1.250E-10	298.4158	5.799E+09	0.001051	8921570.	0.000
300.000	-1.551E-10	-0.0509	0.002856	6.564E-11	298.4158	5.799E+09	0.000231	8921570.	0.000
306.000	8.067E-11	-0.0296	0.003188	2.397E-11	298.4157	5.799E+09	-0.000120	8921570.	0.000
312.000	1.325E-10	-0.0127	0.002237	2.083E-12	298.4156	5.799E+09	-0.000197	8921570.	0.000
318.000	1.057E-10	-0.002788	0.001175	-5.914E-12	298.4155	5.799E+09	-0.000157	8921570.	0.000
324.000	6.152E-11	0.001437	0.000429	-6.613E-12	298.4155	5.799E+09	-9.148E-05	8921570.	0.000
330.000	2.631E-11	0.002368	3.750E-05	-4.644E-12	298.4155	5.799E+09	-3.912E-05	8921570.	0.000
336.000	5.798E-12	0.001890	-0.000106	-2.440E-12	298.4155	5.799E+09	-8.621E-06	8921570.	0.000
342.000	-2.977E-12	0.001101	-0.000118	0.000	298.4155	5.799E+09	4.426E-06	8921570.	0.000
348.000	-4.913E-12	0.000471	-8.311E-05	0.000	298.4155	5.799E+09	7.306E-06	8921570.	0.000
354.000	-3.923E-12	0.000104	-4.369E-05	0.000	298.4155	5.799E+09	5.834E-06	8921570.	0.000
360.000	-2.287E-12	-5.303E-05	-1.599E-05	0.000	298.4155	5.799E+09	3.400E-06	8921570.	0.000
366.000	0.000	-8.783E-05	-1.420E-06	0.000	298.4155	5.799E+09	1.456E-06	8921570.	0.000
372.000	0.000	-7.020E-05	3.913E-06	0.000	298.4155	5.799E+09	3.222E-07	8921570.	0.000
378.000	0.000	-4.094E-05	4.390E-06	0.000	298.4155	5.799E+09	-1.633E-07	8921570.	0.000
384.000	0.000	-1.734E-05	3.087E-06	0.000	298.4155	5.799E+09	-2.709E-07	8921570.	0.000
390.000	0.000	-3.893E-06	1.624E-06	0.000	298.4155	5.799E+09	-2.166E-07	8921570.	0.000
396.000	0.000	1.957E-06	5.953E-07	0.000	298.4155	5.799E+09	-1.264E-07	8921570.	0.000
402.000	0.000	3.257E-06	5.376E-08	0.000	298.4155	5.799E+09	-5.417E-08	8921570.	0.000
408.000	0.000	2.607E-06	-1.449E-07	0.000	298.4155	5.799E+09	-1.204E-08	8921570.	0.000
414.000	0.000	1.521E-06	-1.629E-07	0.000	298.4155	5.799E+09	6.027E-09	8921570.	0.000
420.000	0.000	6.527E-07	-1.147E-07	0.000	298.4155	5.799E+09	1.005E-08	8921570.	0.000
426.000	0.000	1.455E-07	-6.039E-08	0.000	298.4155	5.799E+09	8.044E-09	8921570.	0.000
432.000	0.000	-7.221E-08	-2.217E-08	0.000	298.4155	5.799E+09	4.696E-09	8921570.	0.000
438.000	0.000	-1.208E-07	-2.034E-09	0.000	298.4155	5.799E+09	2.016E-09	8921570.	0.000
444.000	0.000	-9.679E-08	5.362E-09	0.000	298.4155	5.799E+09	4.498E-10	8921570.	0.000
450.000	0.000	-5.654E-08	6.044E-09	0.000	298.4155	5.799E+09	-2.224E-10	8921570.	0.000
456.000	0.000	-2.429E-08	4.259E-09	0.000	298.4155	5.799E+09	-3.726E-10	8921570.	0.000
462.000	0.000	-5.436E-09	2.245E-09	0.000	298.4155	5.799E+09	-2.987E-10	8921570.	0.000
468.000	0.000	2.664E-09	8.256E-10	0.000	298.4155	5.799E+09	-1.745E-10	8921570.	0.000
474.000	0.000	4.480E-09	7.695E-11	0.000	298.4155	5.799E+09	-7.500E-11	8921570.	0.000
480.000	0.000	3.594E-09	-1.985E-10	0.000	298.4155	5.799E+09	-1.681E-11	8921570.	0.000
486.000	0.000	2.102E-09	-2.243E-10	0.000	298.4155	5.799E+09	8.205E-12	8921570.	0.000
492.000	0.000	9.038E-10	-1.582E-10	0.000	298.4155	5.799E+09	1.382E-11	8921570.	0.000
498.000	0.000	2.031E-10	-8.348E-11	0.000	298.4155	5.799E+09	-1.109E-11	8921570.	0.000
504.000	0.000	-9.829E-11	-3.074E-11	0.000	298.4155	5.799E+09	6.487E-12	8921570.	0.000
510.000	0.000	-1.661E-10	-2.910E-12	0.000	298.4155	5.799E+09	2.791E-12	8921570.	0.000
516.000	0.000	-1.335E-10	7.346E-12	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
522.000	0.000	-7.811E-11	8.322E-12	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
528.000	0.000	-3.363E-11	5.877E-12	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
534.000	0.000	-7.590E-12	3.104E-12	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
540.000	0.000	3.626E-12	1.145E-12	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
546.000	0.000	6.160E-12	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
552.000	0.000	4.954E-12	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
558.000	0.000	2.901E-12	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
564.000	0.000	1.250E-12	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
570.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
576.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
582.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
588.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
594.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	8921570.	0.000
600.000	0.000	0.000	0.000	0.000	298.4155	5.799E+09	0.000	4460785.	0.000

* This analysis makes computations of pile response using nonlinear moment-curvature relationships. The above values of total stress are computed for combined axial stress and do not equal the actual stresses in concrete and steel in the range of nonlinear bending.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 2:

Pile-head deflection	=	0.5000000	inches
Computed slope at pile head	=	-0.0089994	radians
Maximum bending moment	=	648972.	inch-lbs
Maximum shear force	=	31849	lbs
Depth of maximum bending moment	=	54.0000000	inches below pile head
Depth of maximum shear force	=	0.0000000	inches below pile head
Number of iterations	=	19	
Number of zero deflection points	=	14	

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 3

Abut 5_Pil_transv_Max P_Lp60
 Pile-head conditions are Displacement and Moment (Loading Type 4)
 Displacement of pile head = 1.000000 inches
 Moment at pile head = 0.000 in-lbs
 Axial load at pile head = 60000.000 lbs

Depth	Deflect.	Bending Moment	Shear Force	Slope	Total Stress	Bending Stiffness	Soil Res. p	Soil Spr. Es^h	Distrib. Lat. Load
x	y	in-lbs	lbs	radians	psi*	lb-in^2	lb/in	lb/inch	lb/inch
0.000	1.0000	0.000	41978.	-0.0157	298.4155	5.799E+09	-1068.6759	3206.0278	0.000
6.000	0.9058	238282.	35523.	-0.0156	1483.5333	5.799E+09	-1082.8765	7172.7082	0.000
12.000	0.8131	437492.	28990.	-0.0152	2474.3214	5.799E+09	-1094.9401	8079.3407	0.000
18.000	0.7232	597121.	22996.	-0.0147	3268.2506	5.799E+09	-1103.0219	9151.5972	0.000
24.000	0.6369	716819.	16489.	-0.0140	3863.5783	5.799E+09	-865.9216	8157.5261	0.000
30.000	0.5551	805076.	12530.	-0.0132	4302.5353	5.799E+09	-453.8926	4906.2074	0.000
36.000	0.4783	876694.	9814.5497	-0.0123	4658.7315	5.799E+09	-451.1752	5660.1184	0.000
42.000	0.4069	931742.	7121.1420	-0.0114	4932.5213	5.799E+09	-446.6294	6585.9666	0.000
48.000	0.3413	970365.	4460.7219	-0.0104	5124.6162	5.799E+09	-440.1773	7738.2645	0.000
54.000	0.2817	992780.	1845.0221	-0.009414	5236.0999	5.799E+09	-431.7227	9194.2999	0.000
60.000	0.2283	999284.	-713.6173	-0.008383	5268.4447	5.799E+09	-421.1571	11067.	0.000
66.000	0.1811	990253.	-3202.1452	-0.007354	5223.5302	5.799E+09	-408.3521	13527.	0.000
72.000	0.1401	966153.	-5606.6465	-0.006342	5103.6659	5.799E+09	-393.1483	16840.	0.000
78.000	0.1050	927540.	-7912.1059	-0.005362	4911.6187	5.799E+09	-375.3382	21442.	0.000
84.000	0.0757	875068.	-10077.	-0.004430	4650.6491	5.799E+09	-346.1818	27427.	0.000
90.000	-0.002488	809096.	-17681.	-0.003518	4326.0746	5.799E+09	-314.9412	36430.	0.000
96.000	0.0330	732910.	-15849.	-0.002760	3943.6098	5.799E+09	-281.3676	51100.	0.000
102.000	0.0188	645608.	-15426.	-0.002047	3509.4085	5.799E+09	-244.2556	78149.	0.000
108.000	0.008477	549273.	-16760.	-0.001428	3007.2773	5.799E+09	-200.3467	141797.	0.000
114.000	0.001612	445521.	-18079.	-0.000914	2514.2565	5.799E+09	-153.5485	891690.	0.000
120.000	-0.002488	332979.	-17681.	-0.000511	1954.5193	5.799E+09	-107.4689	898325.	0.000
126.000	-0.004250	233722.	-15262.	-0.000218	1460.8556	5.799E+09	-43.8173	575920.	0.000
132.000	-0.005101	149998.	-12618.	-0.000117	1044.4432	5.799E+09	447.2850	526607.	0.000
138.000	-0.004752	82319.	-9957.9027	0.000101	707.8390	5.799E+09	439.4376	554897.	0.000
144.000	-0.003891	30430.	-7385.5385	0.000139	449.7633	5.799E+09	418.0171	644661.	0.000
150.000	-0.002841	-6421.6293	-4927.3033	0.000172	300.3541	5.799E+09	386.3946	816131.	0.000
156.000	-0.001831	-29361.	-2774.5996	0.000153	444.4449	5.799E+09	346.1733	1134591.	0.000
162.000	-0.001003	-39827.	-842.7359	0.000117	496.4992	5.799E+09	297.7812	1781514.	0.000
168.000	-0.000422	-39558.	770.0901	7.628E-05	495.1622	5.799E+09	239.8274	3406492.	0.000
174.000	-8.753E-05	-30641.	1797.2779	3.996E-05	450.8117	5.799E+09	102.5685	702150.	0.000
180.000	0.000	-18020.	1890.7161	1.479E-05	388.0382	5.799E+09	-71.4224	750000.	0.000
186.000									

```

Abut 5_Pil_transv_ Max P.1p60
450.000 0.000 -4.043E-08 -3.995E-08 0.000 298.4155 5.799E+09 7.218E-09 8921570. 0.000
456.000 0.000 -1.504E-07 -8.024E-09 0.000 298.4155 5.799E+09 3.424E-09 8921570. 0.000
462.000 0.000 -1.370E-07 5.301E-09 0.000 298.4155 5.799E+09 1.018E-09 8921570. 0.000
468.000 0.000 -8.689E-08 7.982E-09 0.000 298.4155 5.799E+09 -1.241E-10 8921570. 0.000
474.000 0.000 -4.124E-08 6.218E-09 0.000 298.4155 5.799E+09 -4.637E-10 8921570. 0.000
480.000 0.000 -1.228E-08 3.559E-09 0.000 298.4155 5.799E+09 -4.226E-10 8921570. 0.000
486.000 0.000 1.474E-09 1.487E-09 0.000 298.4155 5.799E+09 -2.682E-10 8921570. 0.000
492.000 0.000 5.572E-09 3.001E-10 0.000 298.4155 5.799E+09 -1.273E-10 8921570. 0.000
498.000 0.000 5.084E-09 -1.958E-10 0.000 298.4155 5.799E+09 -3.794E-11 8921570. 0.000
504.000 0.000 3.228E-09 -2.960E-10 0.000 298.4155 5.799E+09 4.522E-12 8921570. 0.000
510.000 0.000 1.534E-09 -2.309E-10 0.000 298.4155 5.799E+09 1.719E-11 8921570. 0.000
516.000 0.000 4.579E-10 -1.323E-10 0.000 298.4155 5.799E+09 1.569E-11 8921570. 0.000
522.000 0.000 -5.371E-11 -5.533E-11 0.000 298.4155 5.799E+09 9.965E-12 8921570. 0.000
528.000 0.000 -2.065E-10 -1.122E-11 0.000 298.4155 5.799E+09 4.737E-12 8921570. 0.000
534.000 0.000 -1.887E-10 7.230E-12 0.000 298.4155 5.799E+09 1.415E-12 8921570. 0.000
540.000 0.000 -1.200E-10 1.098E-11 0.000 298.4155 5.799E+09 0.000 8921570. 0.000
546.000 0.000 -5.706E-11 8.575E-12 0.000 298.4155 5.799E+09 0.000 8921570. 0.000
552.000 0.000 -1.707E-11 4.916E-12 0.000 298.4155 5.799E+09 0.000 8921570. 0.000
558.000 0.000 1.950E-12 2.058E-12 0.000 298.4155 5.799E+09 0.000 8921570. 0.000
564.000 0.000 7.643E-12 0.000 0.000 298.4155 5.799E+09 0.000 8921570. 0.000
570.000 0.000 6.993E-12 0.000 0.000 298.4155 5.799E+09 0.000 8921570. 0.000
576.000 0.000 4.449E-12 0.000 0.000 298.4155 5.799E+09 0.000 8921570. 0.000
582.000 0.000 2.138E-12 0.000 0.000 298.4155 5.799E+09 0.000 8921570. 0.000
588.000 0.000 0.000 0.000 0.000 298.4155 5.799E+09 0.000 8921570. 0.000
594.000 0.000 0.000 0.000 0.000 298.4155 5.799E+09 0.000 8921570. 0.000
600.000 0.000 0.000 0.000 0.000 298.4155 5.799E+09 0.000 4460785. 0.000

```

* This analysis makes computations of pile response using nonlinear moment-curvature relationships. The above values of total stress are computed for combined axial stress and do not equal the actual stresses in concrete and steel in the range of nonlinear bending.

Output Verification: Computed forces and moments are within specified convergence limits.

Output Summary for Load Case No. 3:

```

Pile-head deflection = 1.0000000 inches
Computed slope at pile head = -0.0156949 radians
Maximum bending moment = 999284. inch-lbs
Maximum shear force = 41978. lbs
Depth of maximum bending moment = 60.0000000 inches below pile head
Depth of maximum shear force = 0.0000000 inches below pile head
Number of iterations = 19
Number of zero deflection points = 14

```

Summary of Pile Response(s)

Definitions of Pile-head Loading Conditions:

```

Load Type 1: Load 1 = Shear, lbs, and Load 2 = Moment, in-lbs
Load Type 2: Load 1 = Shear, lbs, and Load 2 = Slope, radians
Load Type 3: Load 1 = Shear, lbs, and Load 2 = Rotational Stiffness, in-lbs/radian
Load Type 4: Load 1 = Top Deflection, inches, and Load 2 = Moment, in-lbs
Load Type 5: Load 1 = Top Deflection, inches, and Load 2 = Slope, radians

```

Load Case No.	Load Type	Pile-head Condition 1	Pile-head Condition 2	Axial Loading	Pile-head Deflection	Maximum Moment	Maximum Shear
		v(lbs) or y(inches)	in-lb, rad., or in-lb/rad.	lbs	inches	in-lbs	lbs
1	4	y = 0.2500	M = 0.000	60000.	0.25000000	425184.	24160.
-0.00517817							
2	4	y = 0.5000	M = 0.000	60000.	0.50000000	648972.	31849.
-0.00899944							
3	4	y = 1.0000	M = 0.000	60000.	1.00000000	999284.	41978.
-0.01569489							

The analysis ended normally.

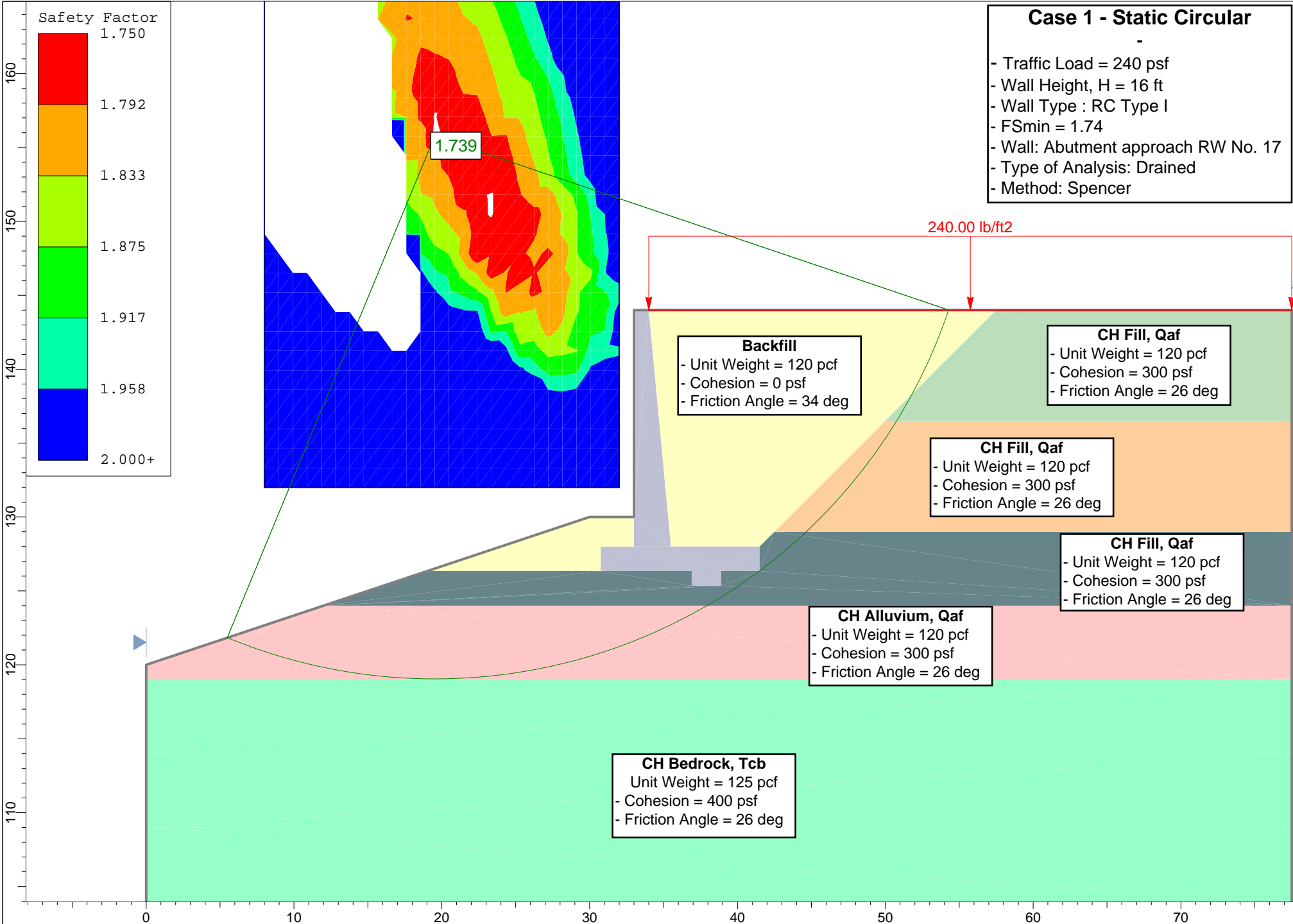
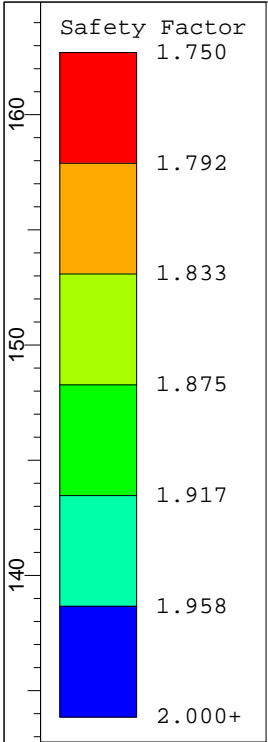
APPENDIX D-4
RETAINING WALL CALCULATIONS

Palo Comado Canyon Rd OC (Widen) - Retaining Wall Type I - No. 17

Global Stability Analysis

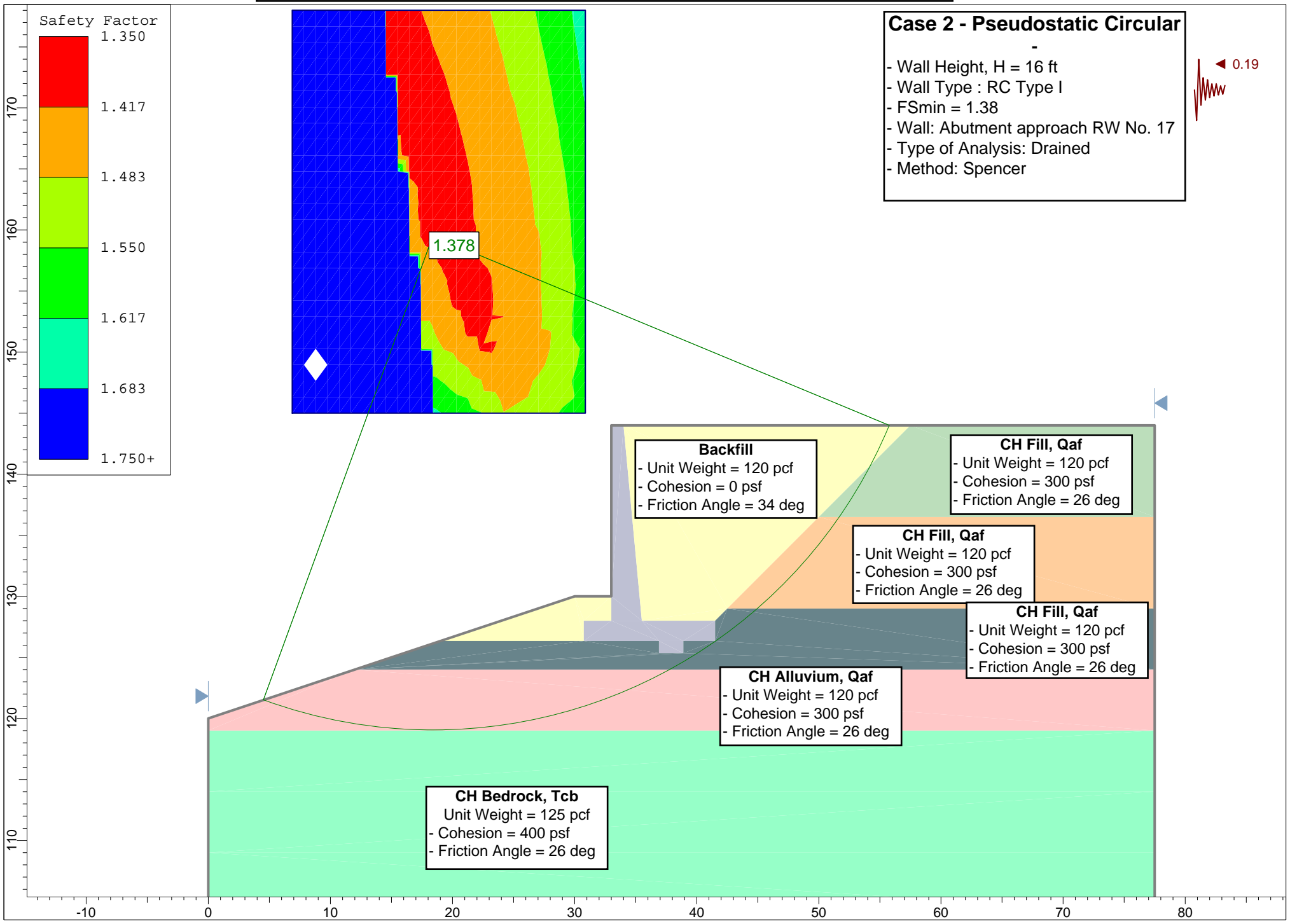
Case 1 - Static Circular

- Traffic Load = 240 psf
- Wall Height, H = 16 ft
- Wall Type : RC Type I
- FSmin = 1.74
- Wall: Abutment approach RW No. 17
- Type of Analysis: Drained
- Method: Spencer



Palo Comado Canyon Rd OC (Widen) - Retaining Wall Type I - No. 17

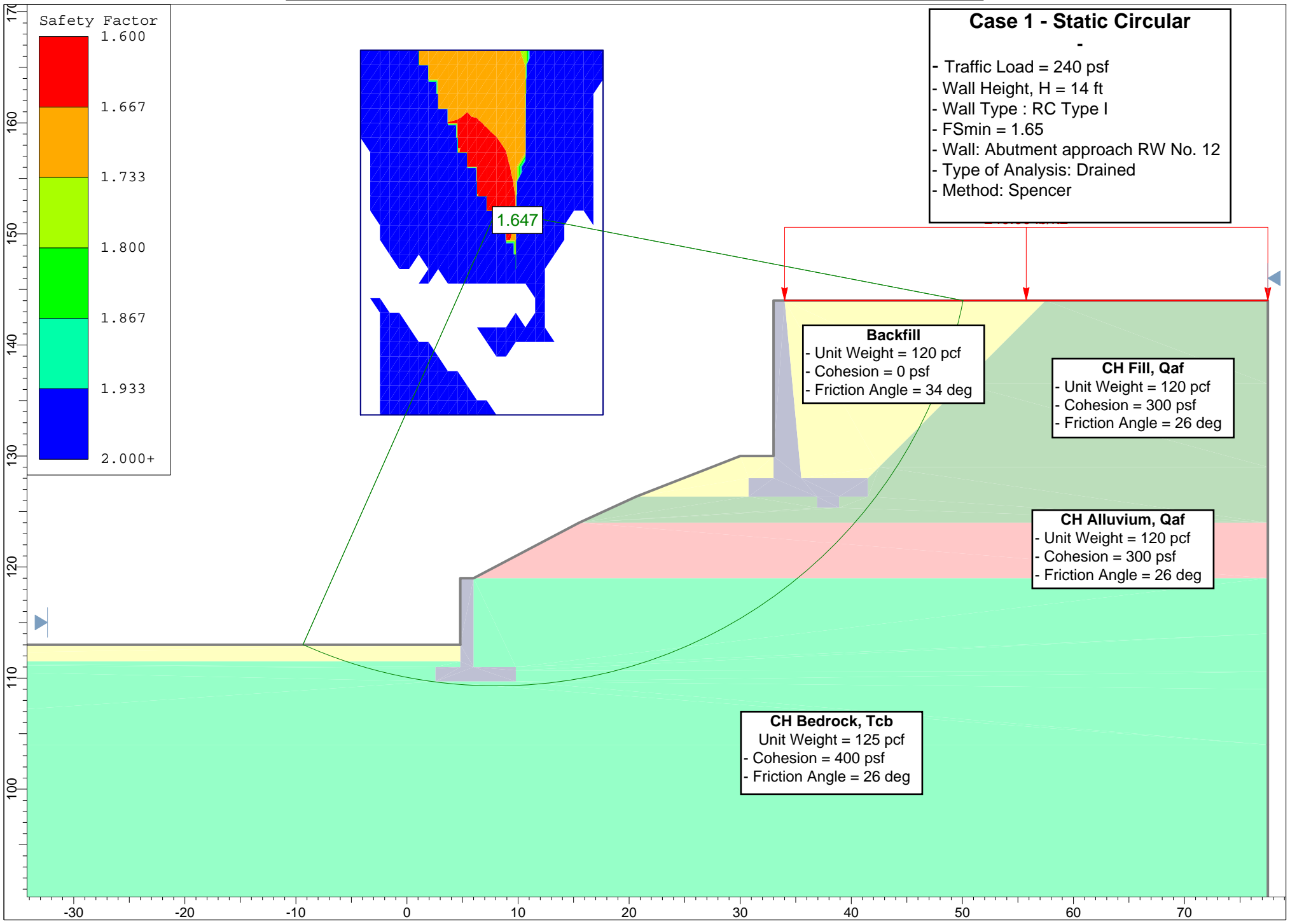
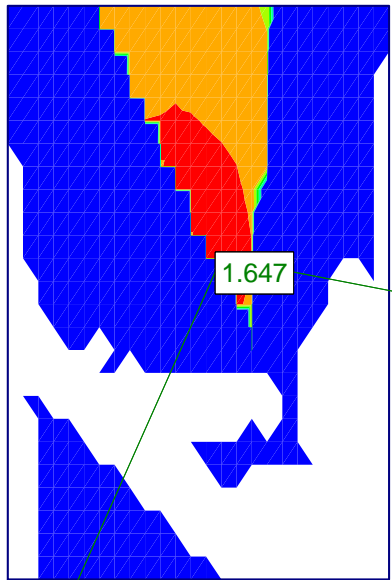
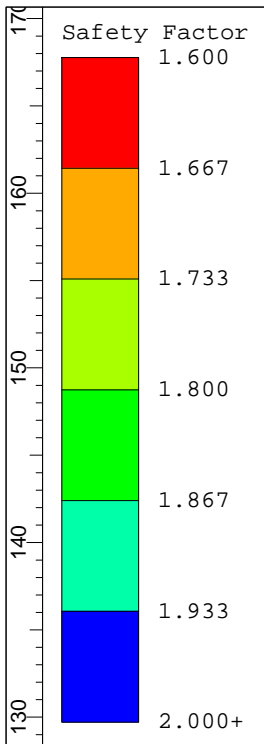
Global Stability Analysis



Palo Comado Canyon Rd OC (Widen) - Retaining Wall Type I - No. 12
Global Stability Analysis

Case 1 - Static Circular

- Traffic Load = 240 psf
- Wall Height, H = 14 ft
- Wall Type : RC Type I
- FSmin = 1.65
- Wall: Abutment approach RW No. 12
- Type of Analysis: Drained
- Method: Spencer



Backfill

- Unit Weight = 120 pcf
- Cohesion = 0 psf
- Friction Angle = 34 deg

CH Fill, Qaf

- Unit Weight = 120 pcf
- Cohesion = 300 psf
- Friction Angle = 26 deg

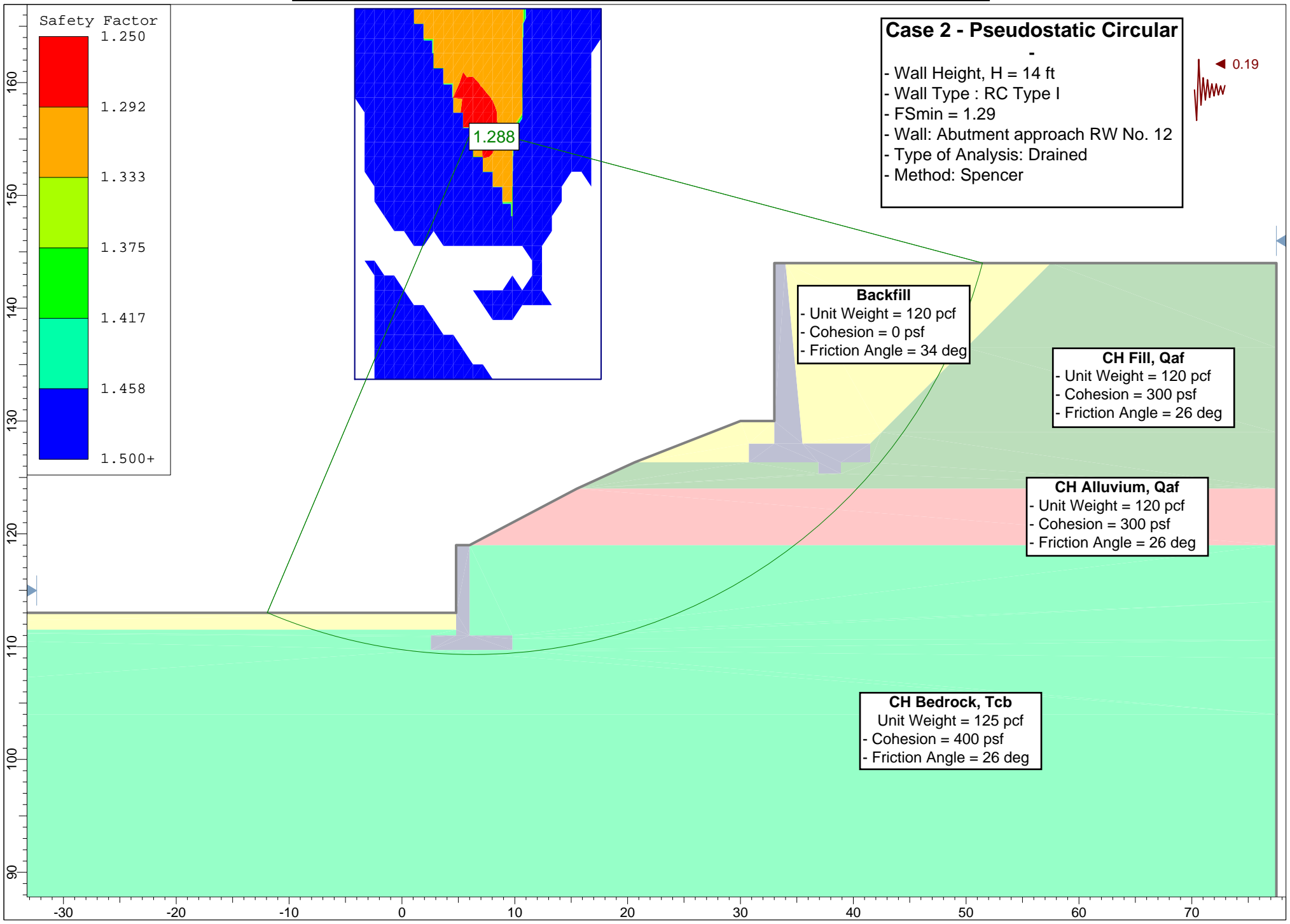
CH Alluvium, Qaf

- Unit Weight = 120 pcf
- Cohesion = 300 psf
- Friction Angle = 26 deg

CH Bedrock, Tcb

- Unit Weight = 125 pcf
- Cohesion = 400 psf
- Friction Angle = 26 deg

Palo Comado Canyon Rd OC (Widen) - Retaining Wall Type I - No. 12 Global Stability Analysis



SETTLEMENT CALCULATION

INSTRUCTIONS:

- 1 Program calculates settlement under center, short edge, long edge, or corner of shaded rectangular loaded areas, using Boussinesq stress distribution and consolidation theory or elastic modulus compressibility.
- 2 Input data in shaded fields. Unshaded fields are automatically calculated. Up to 26 soil layers may be used.
- 3 Explanation of the calculation procedure and guidance for input of data in rows (A) through (E) and columns (1) through (16) is provided below.

ROW AND COLUMN NOTES

- (A) Input length (long side) of rectangular loaded area.
- (B) Input width (short side) of rectangular loaded area.
- (C) Input applied load at the base of the loaded area (pounds per square foot)
- (D) Input depth of applied load below the ground surface (the depth must coincide with a bottom-of-layer boundary specified in Column (2))
- (E) Input 1, 2, 3, or 4 to calculate the settlement under the center, midpoint of short edge, midpoint of long edge, or corner, respectively, of the rectangular loaded area.
- (1) Input Soil Layer number and/or description (optional).
- (2) Starting with the ground surface (depth = 0) input the depth to top and bottom of each soil layer below the ground surface. The depth to center of the layer is automatically calculated.
- (3) The layer height or thickness is automatically computed ($H = \text{depth to top of layer} - \text{depth to bottom of layer}$).
- (4) Input unit weight of soil in the layer (total unit weight above the water table, buoyant unit weight below the water table).
- (5) Vertical effective stress (pounds per square foot) at the center of each layer prior to the new loading is automatically computed.
- (6) Input Overconsolidation Ratio (OCR) defined as the ratio of maximum past preconsolidation pressure (column (7)) to current effective vertical stress (Column (5)). OCR=1 is Normally Consolidated.
- (7) Maximum past preconsolidation pressure is calculated as the product of Column (5) and Column (6), or $\sigma'_p = \text{OCR} * \sigma'_v$.
- (8) The stress increase coefficient (I_σ) at the center of each layer is computed using Newmark integration of Boussinesq theory based on vertical depth below bottom of loaded area and position on loaded area input in Row E.
- (9) The increase in stress ($\Delta\sigma$) at the center of each layer due to the loaded area is computed as the product of I_σ (Column (8)) and load Q (Row C).
- (10) Input compressibility type for each layer. "E" means elastic modulus (slope of stress versus strain curve) is used, "C" means consolidation theory is used (slope of log stress versus strain curve) is used.
- (11) Input elastic modulus (E in ksf) value for each layer where "E" is selected in Column 10.
- (12) Input Recompression Ratio, or slope of log stress versus strain curve, in the overconsolidated range (if soil is normally consolidated this value need not be input).
- (13) Input Virgin Compression Ratio, or slope of log stress versus strain curve, in the normally consolidated range.
- (14) Virgin and/or Recom. Case determined ("C" Comp. Type Only). Case 1 = entire loading is within recompression range, Case 2 - Loading partially recompression partially virgin, Case 3 - entirely virgin (norm cons.)
- (15) Strain ϵ is calculated as $\Delta\sigma / E$ if "E" is specified in Column (10), or by consolidation theory using the appropriate recompression and/or virgin slopes if "C" is specified in Column (10).
- (16) Layer settlement (inches) is computed as Strain (Column (15)) times Height (Column (3)) converted to inches. Total settlement (inches) of all layers is summed up at the bottom of Column (16).

COULOMB AND MONONABE-OKABE EARTH PRESSURE CALCULATIONS

<INPUT>				<<OUTPUT>>								
Unit Weight = γ =	120	pcf =	18.9	kN/m ³	COULOMB STATIC			SEISMIC INCREMENT				
Friction Angle = ϕ =	34	degrees =	0.593412	radians	EFP			EFP				
Wall Friction Angle = ϕ_w =	0.0	degrees =	0	radians	K_A	pcf	kN/m3	i_A	$K_{AE}-K_A$	pcf	kN/m3	i_{AE}
Wall Inclination = α =	0	degrees =	0	radians		deg				deg		
Slope Inclination = β =	0.000	degrees =	0	radians	0.2827	33.93	5.33	62.0	0.120	14.4	2.3	53.18
Horiz. EQ Coeff. = K_h =	0.190		0.003316		RANKINE STATIC			max K_h = 0.674508516842427				
Vert. EQ Coeff. = K_v =	0				0.2827	33.93	5.33	62.0	max β = 23.24203291161000 deg			

<< COULOMB CALCULATION >>										
STATIC ACTIVE EARTH PRESSURE						STATIC CRITICAL INCLINATION				
	A	B	C	D	E	K_A	C1	C2	i_A	
degrees	34.0	0.0	34.0	34.0	0.0				62.00	
radians	0.593	0.000	0.593	0.593	0.000	0.283	1.206	1.000	1.082104	
SEISMIC ACTIVE EARTH PRESSURE						SEISMIC CRITICAL INCLINATION				
	θ	A'	B'	C'	D'	E'	K_{AE}	C1E	C2E	i_{AE}
degrees	10.8	23.2	10.8	34.0	23.2	0				53.18
radians	0.188	0.406	0.188	0.593	0.406	0.000	0.4027	1.307	1.524	0.928127

Appendix E ***Caltrans' Review Comments and Responses***

Memorandum

*Flex your power!
Be energy efficient!*

To: MR. RICHARD HARTZELL
Liaison Engineer Dist 7
Office of Special Funded Projects

Date: July 12, 2017
File: 7-LA-101-PM33.5/33.9
07-257201
Palo Comado Bridge
No. 53-1678

From: DEPARTMENT OF TRANSPORTATION
DIVISION OF ENGINEERING SERVICES
Geotechnical Services
Office of Geotechnical Design – South

Subject: Review of Foundation Report for US 101 Palo Comado Canyon Road OC (Widen)
Improvement Project

Per your request, the Office of Geotechnical Design – South of the Division of Engineering Services has performed a review of Foundation Report for the subject project. The information provided and reviewed for this project is listed as follows:

- Foundation Report for US 101 Palo Comado Canyon Road OC (Widen) in the city of Agoura Hills, California, prepared by Group Delta Consultants, Inc. for Parson Transportation on June 26, 2017.
- Structure Special Provisions for US 101 Palo Comado Canyon Road OC (Widen)

Based on the review of the report, our comments are as follows:

1. Section 3.3 Subsurface Soil Condition: verify the range of undrained shear strength of 1.5 to 4.5 ksf. Shear strength from the pocket penetrometer tests may not represent actual undrained shear strength of clay soils if the tests were done on significantly disturbed soil sample. [Agree. Pocket penetrometer readings were taken on relatively undisturbed samples and Group Delta judge that the pocket penetrometer readings are representative.](#)
2. Appendix D Analysis and Calculations: Verify undrained shear strength of clay soils used in Lpile analysis (for example, undrained shear strength may be 4500 psf, instead of 4500 psi in Lpile analysis)

[Group Delta verified calculations. The input undrained shear strength values are in "psf". The output summary table shows "psf", but the output print from LPILE shows "psi" by mistake \(See attached for sample\). GDC will add a note to the LPILE output \(Appendix D\)](#)
If you have any questions or comments, please contact me at 916-227-4533.

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NOTE: LPILE output print shows the undrained shear strength value of individual layers in "psi" - This is an error from LPILE output format. It should be in "psf" as shown in Summary of Soil Properties (LPILE output)

Abut 1R_long_Critical Length
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 4 is stiff clay without free water
 Distance from top of pile to top of layer = 8.00000 ft
 Distance from top of pile to bottom of layer = 13.00000 ft
 Effective unit weight at top of layer = 120.00000 pcf
 Effective unit weight at bottom of layer = 120.00000 pcf
 Undrained cohesion at top of layer = 1500.00000 psi
 Undrained cohesion at bottom of layer = 1500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 5 is stiff clay without free water
 Distance from top of pile to top of layer = 13.00000 ft
 Distance from top of pile to bottom of layer = 18.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 6 is stiff clay without free water
 Distance from top of pile to top of layer = 18.00000 ft
 Distance from top of pile to bottom of layer = 23.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 2500.00000 psi
 Undrained cohesion at bottom of layer = 2500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 7 is stiff clay without free water
 Distance from top of pile to top of layer = 23.00000 ft
 Distance from top of pile to bottom of layer = 28.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 3500.00000 psi
 Undrained cohesion at bottom of layer = 3500.00000 psi
 Epsilon-50 at top of layer = 0.00700
 Epsilon-50 at bottom of layer = 0.00700

Layer 8 is stiff clay without free water
 Distance from top of pile to top of layer = 28.00000 ft
 Distance from top of pile to bottom of layer = 80.00000 ft
 Effective unit weight at top of layer = 125.00000 pcf
 Effective unit weight at bottom of layer = 125.00000 pcf
 Undrained cohesion at top of layer = 4500.00000 psi
 Undrained cohesion at bottom of layer = 4500.00000 psi
 Epsilon-50 at top of layer = 0.00500
 Epsilon-50 at bottom of layer = 0.00500

(Depth of lowest soil layer extends 30.00 ft below pile tip)

Summary of Soil Properties

Layer	Strain Factor	Layer Soil Type	Layer Rock Mass Depth	Effective Unit Wt.	Undrained Cohesion	Angle of Friction	Uniaxial Elastic Mod.	ROD %
Num.	Epsilon on 50	(p-y Curve Criteria) Factor	Rock Mass Depth ft	pcf	psi	deg.	psi	GSI
1	0.00700	Stiff Clay w/o Free Water	-2.000	120.000	3500.000	--	--	--
	0.00700	--	0.10000	120.000	3500.000	--	--	--
2	0.00700	Stiff Clay w/o Free Water	0.10000	120.000	1500.000	--	--	--
	0.00700	--	3.000	120.000	1500.000	--	--	--
3	0.00700	Stiff Clay w/o Free Water	3.000	120.000	2500.000	--	--	--
	0.00700	--	8.000	120.000	2500.000	--	--	--

		Abut 1R_long_Critical Length			
4	0.00700	Stiff Clay w/o Free Water	8.000	120.000	1500.000
	0.00700	--	13.000	120.000	1500.000
5	0.00700	Stiff Clay w/o Free Water	13.000	125.000	4500.000
	0.00700	--	18.000	125.000	4500.000
6	0.00700	Stiff Clay w/o Free Water	18.000	125.000	2500.000
	0.00700	--	23.000	125.000	2500.000
7	0.00700	Stiff Clay w/o Free Water	23.000	125.000	3500.000
	0.00700	--	28.000	125.000	3500.000
8	0.00500	Stiff Clay w/o Free Water	28.000	125.000	4500.000
	0.00500	--	80.000	125.000	4500.000

p-y Modification Factors for Group Action

Distribution of p-y modifiers with depth defined using 2 points

Point No.	Depth X ft	p-mult	y-mult
1	0.000	1.0000	1.0000
2	50.000	1.0000	1.0000

Loading Type

Static loading criteria were used when computing p-y curves for all analyses.

Pile-head Loading and Pile-head Fixity Conditions

Number of loads specified = 1

Load No.	Load Type	Condition 1	Condition 2	Axial Thrust Force, lbs	Compute Top y vs. Pile Length
1	1	V = 24000. lbs	M = 0.0000 in-lbs	154000.	True

V = perpendicular shear force applied to pile head
 M = bending moment applied to pile head
 y = lateral deflection relative to pile axis
 S = pile slope relative to original pile batter angle
 R = rotational stiffness applied to pile head
 Axial thrust is assumed to be acting axially for all pile batter angles.

Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Moment-curvature properties were derived from elastic section properties

Computed Values of Pile Loading and Deflection For Lateral Loading For Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

Shear force at pile head = 24000.000 lbs
 Applied moment at pile head = 0.000 in-lbs
 Axial thrust load on pile head = 154000.000 lbs